



639 Alpha Drive
Pittsburgh, Pennsylvania 15238
Telephone (412) 967-1900
FAX (412) 967-1911

ADVANCED TECHNOLOGY SYSTEMS, INC.

ATS Project No. 00-117-P

November 14, 2000

Mr. William C. Graeser
Manager – Environmental and Quality Assurance
U.S. Steel Clairton Works
400 State Street
Clairton, PA 15025

**RE: LETTER REPORT – HYDROCHLORIC ACID, CHLORINE GAS AND AMMONIA
GAS EMISIONS TESTING CONDUCTED AT NO. 20 BATTERY COMBUSTION
STACK ON OCTOBER 11, 2000**

Dear Mr. Graeser:

This letter, with attachments, constitutes the report that summarizes the results of the hydrochloric acid (HCl), chlorine gas (Cl₂) and ammonia gas (NH₃) emissions testing conducted at No. 20 Battery Combustion Stack by Advanced Technology Systems, Inc. (ATS). Three two-hour test runs were conducted on October 11, 2000 simultaneous with the compliance test program at this stack (particulate matter and visible emissions were measured as part of the compliance test program).

The test results have been summarized in the attached Table 1. Hydrochloric acid, chlorine gas and ammonia gas concentrations are listed in units of milligrams per dry standard cubic meter (mg/dscm). Hydrochloric acid, chlorine gas and ammonia gas mass emission rates are listed in units of pounds per hour (lb/hr). Table 1 also presents pertinent exhaust gas and sampling parameters including exhaust gas flow rates in units of actual cubic feet per minute (acfm), standard cubic feet per minute (scfm), and dry standard cubic feet per minute (dscfm), exhaust gas temperature (°F), and moisture content of the exhaust gas (percent by volume), gas volume sampled for each test run in units of dry standard cubic feet (dscf) and the isokinetic variation value for each test run. The isokinetic variation value is equal to the ratio of the average linear gas velocity sampled through the probe nozzle to the average exhaust gas velocity. All isokinetic variation values are between 90 percent and 110 percent, which is the acceptable range of values. Actual test sampling times have also been included in Table 1.

Hydrochloric acid, chlorine gas and ammonia gas emission testing were performed in accordance with U.S. EPA Reference Methods 1 through 4 and 26A, U.S. EPA Conditional Test Method 027 and the requirements of the Pennsylvania Department of Environmental Protection (PA DEP) Source Testing Manual (Draft Revision 3.1, May 3, 1999). Detailed information regarding the procedures used to measure the exhaust gas stream velocity and volumetric flow rate (i.e., U.S. EPA Reference

Methods 1 through 4) can be found in the summary report for the compliance test program. Hydrochloric acid and chlorine gas sampling was performed in accordance with U.S. EPA Reference Method 26A. Ammonia gas sampling was performed, where possible, in accordance with U.S. EPA Conditional Test Method 027. (The test procedures specified in Method 027 were modified slightly for this test program based on the expected exhaust gas temperatures of 450°F. The modifications were made after ATS consulted with Ms. Rima Howell of the U.S. EPA, who is the pertinent contact for Method 027. It should also be noted that the U.S. EPA had not promulgated Method 027 at the time of this test program, however, this method was apparently the only test method available from the U.S. EPA designed for measuring ammonia gas emissions from stationary sources.) Process gas samples were withdrawn isokinetically from the stack, with particulate matter collected in a glass nozzle, a heated glass-lined probe, a heated Teflon-lined flexible probe, and on a heated quartz filter. Vapor phase hydrochloric acid, chlorine gas and ammonia gas were collected in a series of chilled impingers. The impinger type and sequence are listed below:

<u>No.</u>	<u>Impinger Type</u>	<u>Contents</u>
1.	Modified Greenburg-Smith	50 mL 0.1 N sulfuric acid (for HCl and NH ₃ collection)
2.	Greenburg-Smith	100 mL 0.1 N sulfuric acid (for HCl & NH ₃ collection)
3.	Greenburg-Smith	100 mL 0.1 N sulfuric acid (for HCl & NH ₃ collection)
4.	Modified Greenburg-Smith	100 mL 0.1 N sodium hydroxide (for Cl ₂ collection)
5.	Modified Greenburg-Smith	100 mL 0.1 N sodium hydroxide (for Cl ₂ collection)
6.	Modified Greenburg-Smith	200 g Silica Gel

A gas volume greater than 50 dry standard cubic feet (dscf) – the minimum gas volume required by the PA DEP for the compliance test program - was sampled for each test run. The flow rate through each sample train was less than 1 dry standard cubic foot per minute as required by U.S. EPA Reference Method 26A.

Following each test run, the sample trains were processed in accordance with PA DEP requirements. Detailed information regarding the procedures used to recover the particulate matter catch (essentially U.S. EPA Reference Method 5 procedures) can be found in the summary report for the compliance test program. Following the gravimetric analysis of the impingers for moisture gain, the following four samples fractions were generated for each sample train:

<u>Fraction</u>	<u>Description</u>
A	Contents of Impinger Nos. 1 & 2 plus applicable distilled deionized water rinses (for HCl and NH ₃)
B	Contents of Impinger No. 3 plus applicable distilled deionized water rinses (for HCl and NH ₃)
C	Contents of Impinger No. 4 plus applicable distilled deionized water rinses (for Cl ₂)
D	Contents of Impinger No. 5 plus applicable distilled deionized water rinses (for Cl ₂)

For each sample train, each of the four fractions were analyzed separately as required by the PA DEP to allow for the calculation of the collection efficiency of the sample train for HCl, Cl₂ and NH₃ collection. The contents of Impinger No. 6 were discarded.

The actual test samples plus field blanks of the impinger scrubbing solutions (0.1 N sulfuric acid and 0.1 N sodium hydroxide) were submitted to the subcontract analytical laboratory for chloride ion analyses using ion chromatographic techniques in accordance with U.S. EPA Reference Method 26A. Sample Fractions A and B and the 0.1 N sulfuric acid solution field blank were also analyzed for ammonium ion concentration using specific ion electrode analysis techniques. The analytical laboratory results showed the following:

- The chloride ion concentrations of the field blanks were less than the analytical detection limit;
- For all three test runs, the HCl collection efficiency of the sample train was calculated to be greater than the minimum collection efficiency specified by the PA DEP (i.e., the chloride catch of the Sample Fraction B was at most 10 percent of the chloride catches from Sample Fraction A plus Sample Fraction B);
- For all three test runs, the Cl₂ collection efficiency of the sample train could not be calculated since the chloride catches of Sample Fractions C and D were less than the analytical detection limit;
- The ammonium ion concentration of the field blank was less than the analytical detection limit; and
- For the first and third test runs, the NH₃ collection efficiency of the sample train was calculated to be greater than the minimum collection efficiency specified by the PA DEP (i.e., the ammonium catch of the Sample Fraction B was at most 10 percent of the ammonium catches from Sample Fraction A plus Sample Fraction B). For the second test run, the NH₃ collection efficiency of the sample train could not be calculated since the ammonium catches in Sample Fractions A and B were very near the analytical detection limit.

Copies of the field data sheets, equipment calibration data, analytical laboratory results and emissions calculations are included in the appendix.

Mr. William C. Graeser

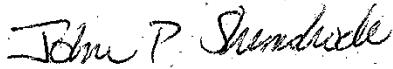
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November 14, 2000

ATS appreciates the opportunity to provide U.S. Steel with process gas testing services.

If you have any questions regarding this letter report, please call Dr. Robinson Khosah or me at (412) 967-1900 or e-mail me at the following address: jshimshock@atsengineers.com.

Very truly yours,



John P. Shimshock, Ph.D.
Senior Project Scientist

Approved by:



Robinson P. Khosah, Ph.D.
Vice President
Science and Technology Division

JPS/blc
Enclosures

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ADVANCED TECHNOLOGY SYSTEMS, INC.

**U.S. STEEL CLAIRTON WORKS
CLAIRTON, PENNSYLVANIA**

TABLE 1

**NO. 20 BATTERY COMBUSTION STACK
HYDROCHLORIC ACID, CHLORINE GAS AND AMMONIA GAS EMISSIONS DATA
OCTOBER 11, 2000**

		<u>Run 1</u>	<u>Run 2</u>	<u>Run 3</u>	<u>Average</u>
<u>Emissions Data</u>					
Hydrochloric Acid (HCl)					
Concentration	(mg/dscm)	8.54E+00	9.11E+00	1.00E+01	9.22E+00
Mass Emission Rate	(lb/hr)	1.70E+00	1.98E+00	2.18E+00	1.95E+00
Chlorine Gas (Cl ₂)					
Concentration	(mg/dscm)	< 1.12E-01	< 1.47E-01	< 7.23E-02	< 1.10E-01
Mass Emission Rate	(lb/hr)	< 2.22E-02	< 3.19E-02	< 1.58E-02	< 2.33E-02
Ammonia Gas (NH ₃)					
Concentration	(mg/dscm)	3.18E-01	4.86E-02	1.53E+00	6.32E-01
Mass Emission Rate	(lb/hr)	6.32E-02	1.06E-02	3.34E-01	1.36E-01
<u>Exhaust Stack Conditions</u>					
Volumetric Flow Rate	(acfm)	1.17E+05	1.28E+05	1.28E+05	1.24E+05
	(scfm)	6.15E+04	6.74E+04	6.72E+04	6.54E+04
	(dscfm)	5.31E+04	5.81E+04	5.83E+04	5.65E+04
Temperature	(°F)	530	531	534	532
Moisture Content	(%)	13.6	13.8	13.3	13.6
<u>Sampling Conditions</u>					
Test Times	(EDT)	0752 to 1004	1037 to 1247	1326 to 1534	
Sampling Time - PM *	(minutes)	120	120	120	
Sample Volume - PM **	(dscf)	62.928	70.785	72.449	
Isokinetic Variation - PM ***	(%)	93.1	95.8	97.8	

mg / dscm = milligrams per dry standard cubic meter

*: Minimum required sampling time is 2 hours (120 minutes)

**: Minimum required sample volume is 50 dscf

***: Acceptable range of values is 90.0% ≤ Isokinetic Variation ≤ 110.0%



ADVANCED TECHNOLOGY SYSTEMS, INC.

**U.S. STEEL CLAIRTON WORKS
CLAIRTON, PENNSYLVANIA**

**Hydrochloric Acid, Chlorine Gas and
Ammonia Gas Emissions Testing Conducted at
No. 20 Battery Combustion Stack
on October 11, 2000**

November 2000

APPENDIX

**Field Data Sheets, Equipment Calibration Data,
Analytical Laboratory Results and Emissions
Calculations**



ADVANCED TECHNOLOGY SYSTEMS, INC.

HIGH FLOW SOURCE SAMPLING DATA SHEET

Page 1 of 2

CLIENT U.S. Steel Clairton Works PLANT SITE Clairton, PA TEST DATE October 11, 2000 APEX-4 HOT/COLD BOX NO. 7
 TEST UNIT No. 20 Battery Combustion Stack B.P. (in. Hg) 29.65 ORIFICE FACTOR (ΔH@) 2.003 FILTER NO. 499
 TEST CREW JL STATIC P. (in. H2O) -1.5 CALIBRATION DATE 9/20/99 NOZZLE DIA. (in.) 0.625
 PROJECT NO. 00-117-P STACK DIA. (in.) 192 PORT SIZE & TYPE 4" Nipples PITOT COEF. 0.84

Test Port	Traverse Point (in.)	Time (EDT)	DGM Reading (def)	Pitot ΔP (in. H2O)	Orifice ΔH Required (in. H2O)	Actual (in. H2O)	Vacuum (in. Hg)	Probe Temp. (°F)	Stack Temp. (°F)	Meter Temp. In (°F) Out (°F)	Filter Temp. (°F)	Exit Temp. (°F)	Comments
A	68.3	7:52	508.141	.01	.70	.70	6	165	558	47	47	46	5 min./pt.
	48.0		510	.02	1.45	1.45	10	175	522	50	47	46	
	34.0			.02	1.45	1.45	17.5	175	529	52	47	47	
	22.7			.02	1.45	1.45	15.5	185	537	51	48	51	
	12.9			.01	.71	.71	7	202	541	51	48	54	
	4.1		523.695	.01	.71	.71	6	257	534	55	48	52	
B	68.3	8:26	523.695	.01	.71	.71	5.5	230	502	52	48	51	
	48.0			.01	.71	.71	6	215	530	55	48	50	
	34.0			.02	1.43	1.43	10	159	538	57	48	50	
	22.7			.02	1.43	1.43	11	158	543	57	49	50	
	12.9			.015	1.07	1.07	10	169	543	57	49	52	
	4.1		538.351	.01	.71	.71	10	179	534	58	49	53	
Page 1	Δ = 60	min	Δ = 30.210	(ΔP) avg =	(ΔH) avg =				(Tstack) avg =	(Tmeter) avg =			
Totals			def	0.014		1.015			534 (°F)	51 (°F)			Estimates:
Test	Δ = 120	min	Δ = 61.632	(ΔP) avg =	(ΔH) avg =				(Tstack) avg =	(Tmeter) avg =			MW = 27.5
Totals			def	0.0145		1.07			536 (°F)	55 (°F)			%H2O = 15

Dry Gas Composition

Run 1	Run 2
CO2	
O2	
CO	
N2	

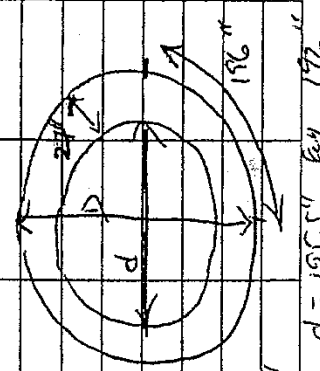
System Leak Check (60 sec)

Vacuum (in. Hg)	DGM Rate (cfm)	Required (cfm)
Before 5.06	0.008	< 0.02
After 17.5	4.45	< 0.02

Pitot Leak Check (15 sec)

Positive	Negative
Before 0.1	0.1
After 0.1	0.1

No.	Impinger Contents	Final	Initial	Δ (g)
1.	50 mL 0.1 N H2SO4			
2.	100 mL 0.1 N H2SO4			
3.	100 mL 0.1 N H2SO4			
4.	100 mL 0.1 N NaOH			
5.	100 mL 0.1 N NaOH			
6.	~ 200 g Silica Gel			
7.				
8.				



11120 = 13.6
 1150 = 45.93

11120 = 13.6
 1150 = 45.93

11120 = 13.6
 1150 = 45.93

Page 2 of 2

APEX-4 HOT/COLD BOX NO. 7

2.003 FILTER NO. 499

10-1

9/20/99 NOZZLE DIA (in)

PITOT COEFF

Exit	C
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Temp.	Temp.
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	(F_0)	(F_1)
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15/6/18

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95	67
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17	54
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17	53
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175	66
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15	36
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65	70
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	%

Final

1150	1150
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7	7	7
4	4	4
0	0	0

424	✓	5
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5	488.87	
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647.9	6
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HIGH FLOW SOURCE SAMPLING DATA SHEET

Page 1 of 2

CLIENT U.S. Steel Clairton Works CLAIRTON SITE Clairton, PA
 TEST DATE October 11, 2000 CONTROL BOX NO. 5 APEX-4 HOT/COLD BOX NO. 5
 TEST NO. CLR-#20BS-M26A-2 ORIFICE FACTOR (AH@) 2.003 FILTER NO. 500 QTZ
 B.P. (in. Hg) 29.65 METER CORR. (V) 1.0023 PROBE NO. 10-1
 STATIC P. (in. H2O) -1.50 CALIBRATION DATE 9/20/99 NOZZLE DIA. (in.) 0.625
 STACK DIA. (in.) 192 PORT SIZE & TYPE 4" Nipples PITOT COEF. 0.84

Test Port	Traverse Point (in.)	Time (EDT)	DGM Reading (def)	Pitot ΔP (in. H2O)	Orifice ΔH		Vacuum (in. Hg)	Probe Temp. (°F)	Stack Temp. (°F)	Meter Temp.		Filter Temp. (°F)	Exit Temp. (°F)	Comments
					Required (in. H2O)	Actual (in. H2O)				In (°F)	Out (°F)			
1	68.3	1037	570.247	0.03	2.17	2.17	15	245	543	57	57	248	53	5 min./pt.
	48.0			0.03	2.17	2.17	15	245	547	58	57	248	53	
	34.0			0.03	2.17	2.17	15	245	556	60	57	248	53	
	22.7			0.03	2.14	2.14	15	244	525	62	58	245	53	
	12.9			0.02	1.48	1.48	13	244	523	65	59	245	52	
	4.1	1107	590.915	0.01	0.74	0.74	5	244	520	69	60	244	52	
3	68.3	1110	590.915	0.02	1.48	1.48	15	243	520	67	62	245	51	
	48.0			0.02	1.48	1.48	15	243	548	69	62	245	51	
	34.0			0.03	2.22	2.22	16	243	555	70	63	245	51	
	22.7			0.02	1.45	1.45	15	244	522	70	64	245	51	
	12.9			0.02	1.45	1.45	15	244	522	72	64	244	50	
	4.1	1140	610.660	0.02	1.45	1.45	15	243	524	74	65	244	50	
Page 1	Δ = 60	Δ = 40.413	def	(ΔP) avg =	(ΔH) avg =				(Tstack) avg =	(Tmeter) avg =				
Totals	min	def		0.023		1.67			534 (°F)	64 (°F)				Estimates:
Test	Δ = 120	Δ = 71.173	def	(ΔP) avg =	(ΔH) avg =				(Tstack) avg =	(Tmeter) avg =				MW =
Totals	min	def		0.0175		1.29			534 (°F)	69 (°F)				%H2O =

Dry Gas Composition

Run 1	Run 2
CO2 4.51	
CO 11.6	
NO 84.51	

System Leak Check (60 sec)

Vacuum (in. Hg)	DGM Rate (cfm)	Required (cfm)
Before 5.00	0.007	<0.02
After 16.00	0.010	<0.02

Pitot Leak Check (15 sec)

Positive	Negative
Before OK	OK
After OK	OK

Impinger Contents

No.	Impinger Contents	Final	Initial	Δ (g)
1.	50 mL 0.1 N H2SO4	640.0	495.6	144.4
2.	100 mL 0.1 N H2SO4	581.4	513.4	68.0
3.	100 mL 0.1 N H2SO4	560.7	552.3	8.4
4.	100 mL 0.1 N NaOH	531.8	529.9	1.9
5.	100 mL 0.1 N NaOH	576.4	574.5	1.9
6.	~200 g Silica Gel	611.5	596.1	15.4
7.				
8.			TOTAL	240.0g

Handwritten notes: $1.6 \text{ H}_2\text{O} = 13.8$, $1.150 = 970$

HIGH FLOW SOURCE SAMPLING DATA SHEET

CLIENT	U.S. Steel Clairton Works		TEST DATE	October 11, 2006	CONTROL BOX NO.	APEX-4	HOT/COLD BOX NO.	5
PLANT SITE	Clairton, PA		TEST NO.	CLR - #20BS - M26A - 2	ORIFICE FACTOR (ΔH@)	2.003 FILTER NO.		500 & 17
TEST UNIT	No. 20 Battery Combustion Stack		B.P. (in. Hg)	29.65	METER CORR. (Y)	1.0023 PROBE NO.		10 - 1
TEST CREW	ILJS KA		STATIC P. (in. H2O)	-1.50	CALIBRATION DATE	9/20/99 NOZZLE DIA. (in.)		0.625
PROJECT NO.	00 - 117 - P		STACK DIA. (in.)	192	PORT SIZE & TYPE	4" Nipples		PTOT COEF.
								0.84

[illegible]

Dry Gas Composition

	Run 1	Run 2
CO ₂		
O ₂		
CO		
N ₂		

System Leak Check (60 sec)

	Vacuum (in. Hg)	DGM Rate (cfm)	Required (cfm)
Before	29.98	0.01	< 0.02
After	29.98	0.01	< 0.02

Pitot Leak Check (15 sec)

	Positive	Negative
Before	29.98	0.01
After	29.98	0.01

Impinger Contents

No.	Impinger Contents	Final	Initial	Δ (g)
1.	50 mL 0.1 N H ₂ SO ₄			
2.	100 mL 0.1 N H ₂ SO ₄			
3.	100 mL 0.1 N H ₂ SO ₄			
4.	100 mL 0.1 N NaOH			
5.	100 mL 0.1 N NaOH			
6.	~ 200 g Silica Gel			
7.				
8.				

HIGH FLOW SOURCE SAMPLING DATA SHEET

Page 1 of 2

CLIENT U.S. Steel Clairton Works
 PLANT SITE Clairton, PA
 TEST UNIT No. 20 Battery Combustion Stack
 TEST CREW JL, JS, KA
 PROJECT NO. 00-117-P
 TEST DATE October 11, 2006
 TEST NO. CLR-#20BS-M26A-3
 B.P. (in. Hg) 29.65
 STATIC P. (in. H2O) -1.50
 STACK DIA. (in.) 192
 CONTROL BOX NO. APEX-4
 ORIFICE FACTOR (ΔH@) 2.003
 METER CORR. (Y) 1.0023
 CALIBRATION DATE 9/20/99
 PORT SIZE & TYPE 4" Nipples
 PITOT COEF. 0.625

Test Port	Traverse Point (in.)	Time (EDT)	DGM Reading (def)	Pitot ΔP (in. H2O)	Orifice ΔH Required (in. H2O)	Actual (in. H2O)	Vacuum (in. Hg)	Probe Temp. (°F)	Stack Temp. (°F)	Meter Temp. In (°F)	Out (°F)	Filter Temp. (°F)	Exit Temp. (°F)	Comments
A	68.3	1326	644.465	0.03	2.26	2.26	12	245	525	76	70	245	60	5 min./pt.
	48.0			0.03	2.26	2.26	12	245	528	77	70	245	60	
	34.0			0.03	2.26	2.26	12	244	532	77	70	245	58	
	22.7			0.03	2.26	2.26	12	245	544	80	71	245	56	
	12.9			0.03	2.23	2.23	12	244	547	82	73	244	56	
	4.1	1356	668.178	0.03	2.23	2.23	12	245	531	83	74	245	56	
B	68.3	1358	668.178	0.03	2.28	2.28	12	244	522	80	75	244	54	
	48.0			0.03	2.28	2.28	12	244	530	83	75	244	54	
	34.0			0.02	1.52	1.52	12	245	538	84	77	243	52	
	22.7			0.02	1.52	1.52	12	245	543	85	77	243	52	
	12.9			0.02	1.52	1.52	12	244	549	87	77	243	52	
	4.1	1428	689.302	0.01	0.75	0.75	4	245	519	87	79	243	52	
Page 1	Δ = 60	min	Δ = 689.302	(ΔP) avg = 0.025	(ΔH) avg =			(Tstack) avg =	(Tmeter) avg =					
Totals	min		44.8374	0.025		1.91		534 (°F)	78 (°F)					Estimates:
Test	Δ = 12.0		Δ = 74.480	(ΔP) avg =	(ΔH) avg =			(Tstack) avg =	(Tmeter) avg =					MW = 27.5
Totals	min		def	0.018		1.39		534 (°F)	81 (°F)					%H2O = 15

Dry Gas Composition

Run 1	Run 2
CO2 4.5%	
O2 11.0%	
CO -	
N2 84.5%	

System Leak Check (60 sec)

	Vacuum (in. Hg)	DGM Rate (cfm)	Required (cfm)
Before	5.00	0.004	<0.02
After	12.00	0.006	<0.02

Pitot Leak Check (15 sec)

	Positive	Negative
Before	OK	OK
After	OK	OK

Impinger Contents

No.	Impinger Contents	Final	Initial	Δ (g)
1.	50 mL 0.1 N H2SO4	563.2	419.1	144.1
2.	100 mL 0.1 N H2SO4	575.0	491.9	83.1
3.	100 mL 0.1 N H2SO4	662.3	542.5	119.8
4.	100 mL 0.1 N NaOH	437.2	507.4	-70.2
5.	100 mL 0.1 N NaOH	508.1	549.6	-41.5
6.	~200 g Silica Gel	666.2	647.9	18.3
7.				
8.			TOTAL	235.5g

Δ H2O = 13.3
 Δ H2O = 98

$$= \left[\frac{\sum \Delta H_2O}{n} \right]$$

APEX-4 HOT/COLD BOX NO.

ORIFICE FACTOR (AHQ)

METER CORR. (Y)

CALIBRATION DATE _____

0.625
LA. (in.)[illegible]

4	Supplies	11101	COEF.	0.84
---	----------	-------	-------	------

	No.	Impinger Contents	Final	Initial	A (%)
System Leak Check (60 sec)					
✓ Dry Gas Composition					
✓ Wet Gas Composition					

System Leak Check (60 sec)

Z	Vacuum (in. Hg)	DGM Rate (cfm)	Required (cfm)
Before	26 in. Hg	6	< 0.02
After	26 in. Hg	10	< 0.02

Pitot Leak Check (15 sec)

	Positive	Negative
Before	29	27
After	29	27

APEX GLASS NOZZLE CALIBRATION DATA SHEET

Printed:

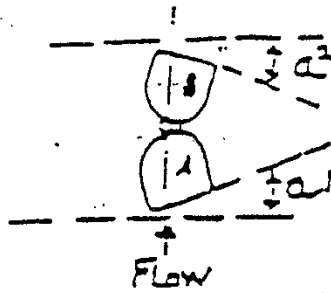
09/18/00

Nozzle No.	Size (inches)					Calibrated	
	Avg.		A	B	C	By	Date
52	0.440		0.440	0.440	0.440	KA	05/01/00
19	0.450		0.450	0.450	0.450	KA	04-14-98
36	0.490		0.490	0.490	0.490	KA	06-10-97
37	0.490		0.490	0.490	0.490	KA	07-05-96
38	0.495		0.495	0.495	0.495	KA	07-05-96
39	0.500		0.500	0.500	0.500	KA	09/18/00
46	0.625		0.625	0.625	0.625	KA	09/18/00
43	0.750		0.750	0.750	0.750	KA	01/05/00

GEOMETRIC PITOT CALIBRATION

Caliper # XFS-59
 Prochert _____
 Post Chart _____

Probe # 10-1
 Date 02-10-00
 Inserter KBA



$$\begin{aligned} \alpha^1 &= \frac{1}{2} \\ \alpha^2 &= \frac{2}{2} \\ \beta^1 &= \frac{1}{2} \\ \beta^2 &= \frac{1}{2} \end{aligned} \quad \begin{aligned} &> \alpha^1, \alpha^2 = < 10^\circ \\ &> \beta^1, \beta^2 = < 5^\circ \end{aligned}$$

$$F = 0.975''$$

$$\mu = 0.017''$$

$$\mu \leq 0.1250'' (\delta \tan \alpha \times F = \mu)$$

$$V = 0.000$$

$$V \leq 0.03125'' (\theta \tan \alpha \times F = V)$$

$$W = 0.195''$$

$$W \geq 0''$$

$$X = 0.321''$$

$$X \geq 0.750''$$

(3/4" using 1/2" scale)

$$Y = 6.215''$$

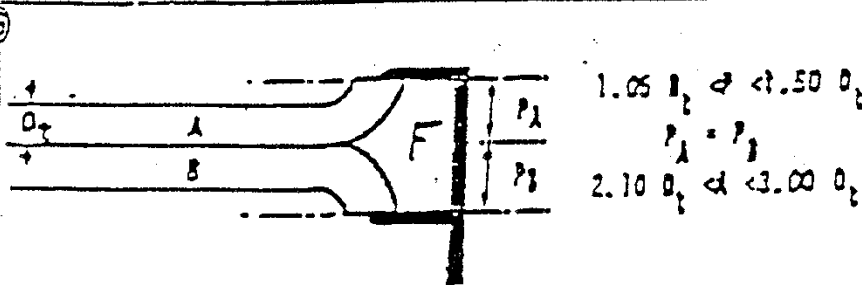
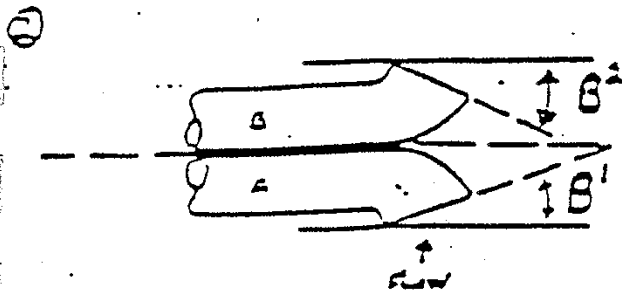
$$Y \geq 3.0''$$

$$Z = 2.417''$$

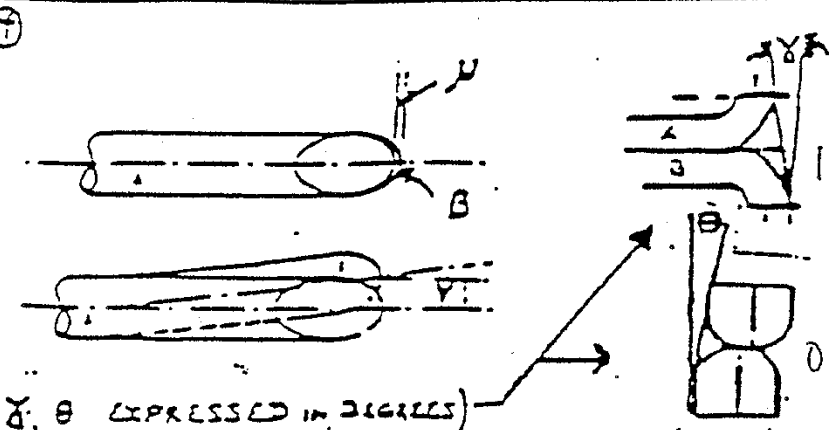
$$Z \geq 2.0''$$

$$D_1 = 0.376''$$

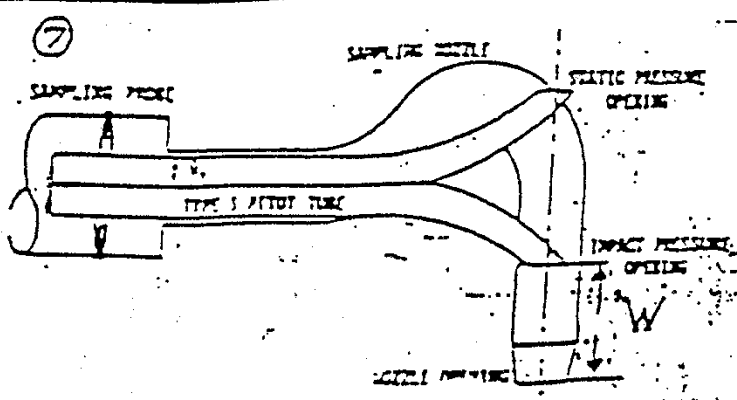
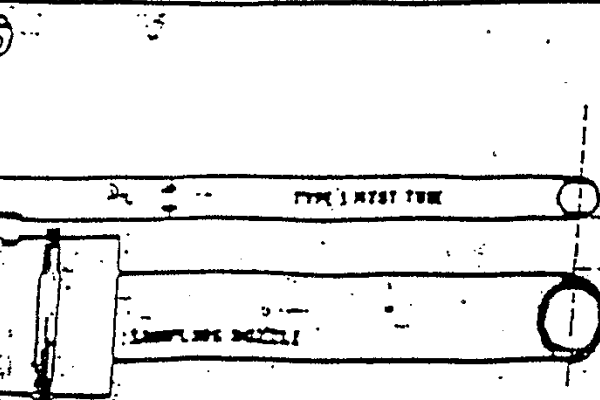
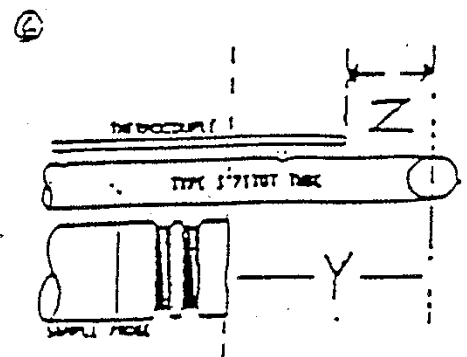
$$D_1 > .1875''$$



$$\begin{aligned} 1.05 \theta_1 &\leq 1.50 \theta_2 \\ 2.10 \theta_1 &\leq 3.00 \theta_2 \end{aligned}$$



δ, θ EXPRESSED IN DEGREES



CERTIFICATE OF CALIBRATION

This certifies that your AL-20 AMERICAN Wet Test gas meter,

serial no. P-1146

has been calibrated with a bell prover.

AMERICAN 16 foot, # 3157

It is traceable to the N.I.S.T., reference no. 1249811.

Calibration by Carl Poe Co., Inc.

99 Reinerman Houston, TX 77007

713-861-3816

2-8-96

Date:

Mark Poe

Signature

DRY GAS METER CALIBRATION DATA SHEET

CONTROL BOX NO.
CALIBRATION DATE
BAROMETRIC PRESSURE (in. Hg)

4221-4
09-24-99
29.10

CHECK PRE-TEST
ONE: POST-TEST
CALIBRATION OFFICER

✓
JPS

RUN NO.		WET TEST METER			DRY GAS METER				
		Gas Volume Vw (cf)	Elapsed Time (min.)	Meter Temp. Tw (°F)	Gas Volume Vd (dcf)	Inlet Temp. Ti (°F)	Outlet Temp. To (°F)	Orifice Diff. Pres. ΔH (in. H2O)	Vacuum (in. H2O)
1	START	0.000	0		318.302			1.0	8.0
	MIDWAY			71		88	78		
	STOP	5.000	9.20		323.417				
	DELTA *	5.000	9.33		5.115				
2	START	0.000	0		324.438			2.0	8.0
	MIDWAY			71		92	79		
	STOP	5.000	6.39		329.522				
	DELTA *	5.000	6.65		5.084				
3	START	0.000	0		331.550			3.0	8.0
	MIDWAY			71		95	80		
	STOP	5.000	5.25		336.644				
	DELTA *	5.000	5.42		5.094				
Dry Gas	START	0.050	0		336.713			0.0	1.0
Meter Leak	STOP	0.358	10:00		337.112				
Check	DELTA *	0.308	10.0		0.399				

{DELTA Vw (cf) - DELTA Vd (dcf)} / 10 (min.) = 0.0091 cfm ≤ 0.02 cfm

*: Express final elapsed time in decimal format

Differential Pressure Gauges (check one):

✓ Inclined Manometers

_____ Magnehelic Gauges

	Run #1	Run #2	Run #3	Avg.
BP (in. Hg)	29.10	29.10	29.10	
Time (min)	9.33	6.65	5.42	
Tw (°F)	71	71	71	
Vw (cf)	5.000	5.000	5.000	
Ti (°F)	88	92	95	
To (°F)	78	79	80	
ΔH (in. H2O)	1.00	2.00	3.00	
Vm (dcf)	5.115	5.084	5.094	
ΔH@ (in. H2O)	1.988	2.016	2.005	2.003
Y (Pre-test)	0.9971	1.0053	1.0044	1.0023

$$\Delta H@ = 0.0317 * \Delta H * [(Tw+460) * Time]^2$$

$$BP * (To + 460) * (Vw)^2$$

$$Y = \frac{Vw * BP * [(Ti+460+To+460)/2]}{Vm * [BP+(\Delta H/13.6)] * (Tw+460)}$$

$$Vm * [BP+(\Delta H/13.6)] * (Tw+460)$$

DRY GAS METER CALIBRATION DATA SHEET

CONTROL BOX NO.
CALIBRATION DATE
BAROMETRIC PRESSURE (in. Hg)

Apex-H
10-20-00
29.24

CHECK PRE-TEST
ONE: POST-TEST
CALIBRATION OFFICER

725

RUN NO.		WET TEST METER			DRY GAS METER				
		Gas Volume Vw (cf)	Elapsed Time (min.)	Meter Temp. Tw (°F)	Gas Volume Vd (dcf)	Inlet Temp. Ti (°F)	Outlet Temp. To (°F)	Orifice Diff. Pres. ΔH (in. H2O)	Vacuum (in. H2O)
1	START	0.000	0		752.023			1.5	18.0
	MIDWAY			67		83	74		
	STOP	5.000	7.43		757.099				
	DELTA *	5.000	7.72		5.076				
2	START	0.000	0		757.099			1.5	18.0
	MIDWAY			67		83	74		
	STOP	5.000	7.43		762.172				
	DELTA *	5.000	7.72		5.073				
3	START	0.000	0		762.172			1.5	18.0
	MIDWAY			67		83	75		
	STOP	5.000	7.43		767.253				
	DELTA *	5.000	7.72		5.081				
Dry Gas	START	0.130	0		767.398			0.0	18.0
Meter Leak	STOP	0.302	10:00		767.658				
Check	DELTA *	0.172	10.0		0.260				
$\{ \text{DELTA Vw (cf)} - \text{DELTA Vd (dcf)} \} / 10 \text{ (min.)} = \underline{0.0088} \text{ cfm} \quad \leq 0.02 \text{ cfm}$									

*: Express final elapsed time in decimal format

Differential Pressure Gauges (check one):



Inclined Manometers

Magnehelic Gauges

	Run #1	Run #2	Run #3	Avg.
BP (in. Hg)	29.24	29.24	29.24	$\Delta H@ = \frac{0.0317 * \Delta H * [(Tw+460) * Time]^2}{BP * (To + 460) * (Vw)^2}$
Time (min)	7.72	7.72	7.72	
Tw (°F)	67	67	67	$Y = \frac{Vw * BP * [(Ti+460+To+460)/2]}{Vm * [BP+(\Delta H/13.6)] * (Tw+460)}$
Vw (cf)	5.000	5.000	5.000	
Ti (°F)	83	83	83	1.0023
To (°F)	74	74	75	
ΔH (in. H2O)	1.50	1.50	1.50	2.015
Vm (dcf)	5.076	5.073	5.081	
Y (Pre-test)				1.0029
ΔH@ (in. H2O)	2.016	2.016	2.012	0.1%
Y (Post-test)	1.0027	1.0033	1.0027	
ΔY (%)				



UEC
USX Engineers
& Consultants, Inc.

RECEIVED NOV 16 2000

October 26, 2000

Advanced Technology Systems, Inc.
ATTN: Mr. John Shimshock
639 Alpha Drive
RIDC Park
Harmarville, PA 15238

Attached are the analytical result(s) of the analysis on sample(s) submitted to the UEC Laboratories on October 12, 2000. Should you have any questions regarding this report, please contact us. An invoice will be issued shortly.

These results are submitted pursuant to USX Engineers & Consultants, Inc.'s current terms and conditions of sale, including the company's standard warranty and limitation of liability provisions, and no responsibility or liability is assumed for the manner in which the results are used or interpreted.

The results were derived with the following methods.

ANALYTE	METHOD
CHLORIDE	EPA 26A

We appreciate the opportunity to be of service and look forward to our continued assistance to you.

NOTE: Samples will be stored for only one month following the report date.

Sincerely,

Stephanie A. Guilyard
Stephanie A. Guilyard, JHIT, Project Manager

Enclosures

USX Engineers & Consultants Inc.

4000 Tech Center Drive
Monroeville, PA 15146
PHONE: (412)825-2400 FAX: (412)825-2407
AIHA Accreditation #322

REPORT OF TEST RESULTS

DATE - 10/19/2000
PAGE - 1

Customer:	CD-002D	ATTENTION: Mr. John Shimshock
Advanced Technology Systems, Inc. 639 Alpha Drive RDC Park		Work Requested by : Mr. John Shimshock Phone No. : 412-967-1900
Harmarville, PA 15238		CUSTOMER P.O. # : 3872 SITE LOCATION : US STEEL CLAIRTON WORKS
TRACKING NUMBER: 4545 A		

UEC ID	CLIENT ID	ANALYTE	DATE SAMPLED	SAMPLE TIME (min)	PUMP RATE (LPM)	AIR VOL. SAMPLED (L)	ANALYSIS DATE	mg/L	mg/Kg	PPM	µg/L	µg/Kg	pH	%	LOD
39235	CLR-24BS-M26A-1A	CHLORIDE	10/11/00	*	*	*	10/18/00	33							2.0 mg/L
39236	CLR-24BS-M26A-1B	CHLORIDE	10/11/00	*	*	*	10/18/00	<2.0							2.0 mg/L
39237	CLR-24BS-M26A-1C	CHLORIDE	10/11/00	*	*	*	10/18/00	<2.0							2.0 mg/L
39238	CLR-24BS-M26A-1D	CHLORIDE	10/11/00	*	*	*	10/18/00	<2.0							2.0 mg/L
39239	CLR-24BS-M26A-2A	CHLORIDE	10/11/00	*	*	*	10/18/00	41							2.0 mg/L
39240	CLR-24BS-M26A-2B	CHLORIDE	10/11/00	*	*	*	10/18/00	<2.0							2.0 mg/L
39241	CLR-24BS-M26A-2C	CHLORIDE	10/11/00	*	*	*	10/18/00	<2.0							2.0 mg/L
39242	CLR-24BS-M26A-2D	CHLORIDE	10/11/00	*	*	*	10/18/00	<2.0							2.0 mg/L
39243	CLR-24BS-M26A-3A	CHLORIDE	10/11/00	*	*	*	10/18/00	47							2.0 mg/L
39244	CLR-24BS-M26A-3B	CHLORIDE	10/11/00	*	*	*	10/18/00	<2.0							2.0 mg/L
39245	CLR-24BS-M26A-3C	CHLORIDE	10/11/00	*	*	*	10/18/00	<2.0							2.0 mg/L
39246	CLR-24BS-M26A-3D	CHLORIDE	10/11/00	*	*	*	10/18/00	<2.0							2.0 mg/L
39247	CLR-H2S04-BLK	CHLORIDE	10/12/00	*	*	*	10/18/00	<2.0							2.0 mg/L

COMMENTS: SAMPLES ARE BLANK CORRECTED.

NOTES: * = Information not supplied by client. < = less than.
= Information not requested by client. N/A = Not Applicable. B - TUBE
Time, flow rate and/or sample volume data are based on client supplied information, unless otherwise noted.
A - FILTER OR SINGLE STAGE MONITOR C - TUBE OR 2 STAGE MONITOR E - LIQUIDS OR SOLIDS J - FILTER + TUBE
D - BULK MATERIALS OR WIPES I - FILTER + TUBE

USX Engineers & Consultants Inc.
 Environmental Laboratories
 4000 Tech Center Drive
 Monroeville, PA 15146
 PHONE: (412)825-2400 FAX: (412)825-2407
 AHA Accreditation #322

REPORT OF TEST RESULTS

DATE - 10/19/2000
 PAGE - 2

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Advanced Technology Systems, Inc. 639 Alpha Drive RDC Park Harmarville, PA 15238		Work Requested by : Mr. John Shimshock Phone No. : 412-967-1900 CUSTOMER P.O. # : 3872 SITE LOCATION : US STEEL CLAIRTON WORKS

TRACKING NUMBER: 4545 A

UEC ID	CLIENT ID	ANALYTE	DATE SAMPLED	SAMPLE TIME (min)	PUMP RATE (LPM)	AIR VOL. SAMPLED (L)	ANALYSIS DATE	mg/L	mg/Kg	PPM	µg/L	µg/Kg	pH	%	LOD
39248	CLR-NAOH-BLK	CHLORIDE	10/12/00	*	*	*	10/18/00	<2.0							2.0 mg/L
															E

COMMENTS: SAMPLES ARE BLANK CORRECTED.

ANALYST : N.K. [Signature]
 APPROVED: Stephanie [Signature]
 Date: 10-19-00
 Date: 10/30/00
 NOTES: * = Information not supplied by client. # = Information not requested by client. N/A = Not Applicable.
 Time, flow rate and/or sample volume data are based on client supplied information, unless otherwise noted.

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 B - TUBE D - BULK MATERIALS OR WIPES I - FILTER + TUBE



UEC
USX Engineers
& Consultants, Inc.

October 26, 2000

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RIDC Park
Harmarville, PA 15238

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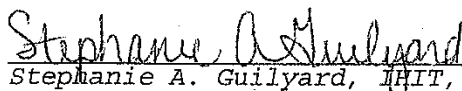
The results were derived with the following methods.

ANALYTE	METHOD
AMMONIUM-WATER	EPA 350.2 (MOD)
CHLORIDE	EPA 26A

We appreciate the opportunity to be of service and look forward to our continued assistance to you.

NOTE: Samples will be stored for only one month following the report date.

Sincerely,



Stephanie A. Guilyard, IHIT, Project Manager

Enclosures



ADVANCED TECHNOLOGY SYSTEMS, INC.
639 ALPHA DRIVE, R.I.D.C. PARK
PITTSBURGH, PA 15238
(412)967-1900 FAX (412)967-1911

CHAIN OF CUSTODY RECORD

PROJECT NUMBER 44-117-P; P.O. # 3872				ANALYSES TO BE CONDUCTED								
PROJECT NAME U.S. Steel Clanton Works				Legend:								
ANALYTICAL LAB USE IIT and Environmental Laboratories				A= Impinger 1+2								
DELIVER TO Sample Receiving				B= Impinger 3								
COMMENTS				C= Impinger 4								
No. 2 & Battery Combustion Stack				D= Impinger 5								
SAMPLE IDENTIFICATION NUMBER	SAMPLE COLLECTION DATE	SAMPLE COLLECTION TIME	NUMBER OF CONTAINERS	COMPOSITE OR GRAB	Chloride ion v/c	Iron Chromatography	Ammonium ion v/c	Net Chloride ion v/c	REMARKS OR OBSERVATIONS			
CLR-#24BS-N2GA-1A	10-11-00	0552 →	1	Comp.	✓		✓		0.1N H ₂ SO ₄ -Sample Volume = 448.7			
CLR-#24BS-N2GA-1B		1404 EDT	1	Comp.	✓		✓		0.1N H ₂ SO ₄ -Sample Volume = 305.7			
CLR-#24BS-N2GA-1C		↓	1	Comp.	✓				0.1N NaOH-Sample Volume = 99.6			
CLR-#24BS-N2GA-1D		↓	1	Comp.	✓				0.1N NaOH-Sample Volume = 105.4			
CLR-#24BS-N2GA-2A	10-11-00	1057 →	1	Comp.	✓		✓		0.1N H ₂ SO ₄ -Sample Volume = 433.4			
CLR-#24BS-N2GA-2B		1247 EDT	1	Comp.	✓		✓		0.1N H ₂ SO ₄ -Sample Volume = 165.0			
CLR-#24BS-N2GA-2C		↓	1	Comp.	✓				0.1N NaOH-Sample Volume = 147.0			
CLR-#24BS-N2GA-2D		↓	1	Comp.	✓				0.1N NaOH-Sample Volume = 132.7			
RELINQUISHED BY (SIGNATURE)				DATE	TIME	RECEIVED BY (SIGNATURE)				DATE	TIME	ICE CHEST #
John P. Simms				10-12-00	1118 EDT	K. L. G. G.				10-12-00	1115	
Judy Atchell				10-13-00		D. J. M. M.				10-12-00	1215	CHEST TEMP.
						James G. Miller				10-18-2000	1230	
												TAG #

USX Engineers & Consultants Inc.
 IH & Environmental Laboratories
 4000 Tech Center Drive
 Monroeville, PA 15146
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 ALHA Accreditation #322

REPORT OF TEST RESULTS

DATE - 10/20/2000
 PAGE - 1

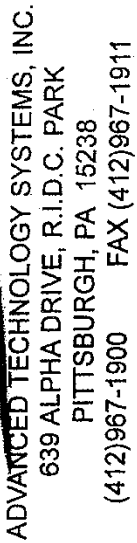
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Harmarville, PA 15238		CUSTOMER P.O. # : 3872 SITE LOCATION : US STEEL CLAIRTON WORKS
TRACKING NUMBER: 4545		

UEC ID	CLIENT ID	ANALYTE	DATE SAMPLED	SAMPLE TIME (min)	PUMP RATE (LPM)	AIR VOL. SAMPLED (L)	ANALYSIS DATE	mg/L	mg/Kg	PPM	µg/L	µg/Kg	pH	%	LOD
39235	CLR-24BS-M26A-1A	AMMONIUM-WATER	10/11/00	*	*	*	10/19/00			1.2				0.1	E
39236	CLR-24BS-M26A-1B	AMMONIUM-WATER	10/11/00	*	*	*	10/19/00			0.2				0.1	E
39239	CLR-24BS-M26A-2A	AMMONIUM-WATER	10/11/00	*	*	*	10/19/00			0.2				0.1	E
39240	CLR-24BS-M26A-2B	AMMONIUM-WATER	10/11/00	*	*	*	10/19/00			0.1				0.1	E
39243	CLR-24BS-M26A-3A	AMMONIUM-WATER	10/11/00	*	*	*	10/19/00			7.7				0.1	E
39244	CLR-24BS-M26A-3B	AMMONIUM-WATER	10/11/00	*	*	*	10/19/00			0.2				0.1	E
39247	CLR-H2S04-BLK	AMMONIUM-WATER	10/12/00	*	*	*	10/19/00			< 0.1				0.1	E

ANALYST: James J. Miller Date: 10-20-2000
 APPROVED: Stephanie A. Guitard Date: 10/30/00

Stephanie A. Guitard, IHT, Project Manager
 NOTES: * = Information not supplied by client < = less than.
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 B - TUBE D - BULK MATERIALS OR WIPES I - FILTER + TUBE



PROJECT NUMBER 00-117P ; P.O. # 3872

PROJECT NAME U.S. Steel Clinton Works

ANALYTICAL LAB SET IIT and Environmental Laboratories

DELIVER TO	Sample	Receiving
COMMENTS		

21/11/2000

No. 26 Betty's Combustion Stack	
SAMPLE	SAMPLE
1	2
3	4
5	6
7	8
9	10
11	12
13	14
15	16
17	18
19	20
21	22
23	24
25	26
27	28
29	30
31	32
33	34
35	36
37	38
39	40
41	42
43	44
45	46
47	48
49	50
51	52
53	54
55	56
57	58
59	60
61	62
63	64
65	66
67	68
69	70
71	72
73	74
75	76
77	78
79	80
81	82
83	84
85	86
87	88
89	90
91	92
93	94
95	96
97	98
99	100

IDENTIFICATION

NUMBER

IL-#2485-M26A-3A

CU2-#2485-M26A-3B

CLP-#2485-M264-3C

LR-#2685-M264-3D

10

UL-12804-BLK

CLP-NACHBEK

10

1

1

SECRET

RELINQUISHED BY
J A D

Sam P. Stewart

②

July 1964

—

100

ATS 10/98

PAGE 2 OF 2

Please take 25 mg
sodium thiosulfate
 $\text{Na}_2\text{S}_2\text{O}_3 \cdot 3.5\text{H}_2\text{O}$
prior to analysis

Legend:

$$A = \text{Empirical } 1 + 2$$

3 = Impinger 3

2-Impringer &

1 - American 5

REMARKS OR OBSERVATIONS

0.1N H_2SO_4 - Sample Volume =

$$3.1 \text{ N H}_2\text{SO}_4 - \text{Sample Volume} =$$
$$1 \text{ N } \text{H}^+ - \text{Sample Volume} =$$

1/1N NaOH - Sample Volume =

 $\text{Dil N H}_2\text{SO}_4$

5.1N Ngoff

ICE CHEST #

TIME

DATE _____

CHEST TEMP.

vi

2-00

TAG #

U.S. STEEL CLAIRTON WORKS - CLAIRTON, PA
 NO. 20 BATTERY COMBUSTION STACK
 OCTOBER 11, 2000
 U.S. EPA REFERENCE METHOD 26A SAMPLING
 CALCULATION OF THE IMPINGER COLLECTION EFFICIENCIES

Test No.	Sample ID (CLR-#20BS -M26A-)	Sample Type	Chloride Conc. (mg / L)	Sample Volume (mL)	Chloride Catch (mg)	Collection Efficiency (%)
1	1A	0.1 N H ₂ SO ₄ - Impingers 1 & 2	33	448.7	14.81	100.0
	1B	0.1 N H ₂ SO ₄ - Impinger 3	< 2.0	305.7	< 0.61	
	1C	0.1 N NaOH - Impinger 4	< 2.0	99.6	< 0.20	NA
	1D	0.1 N NaOH - Impinger 5	< 2.0	105.4	< 0.21	
2	2A	0.1 N H ₂ SO ₄ - Impingers 1 & 2	41	433.4	17.77	100.0
	2B	0.1 N H ₂ SO ₄ - Impinger 3	< 2.0	165.0	< 0.33	
	2C	0.1 N NaOH - Impinger 4	< 2.0	147.0	< 0.29	NA
	2D	0.1 N NaOH - Impinger 5	< 2.0	132.7	< 0.27	
3	3A	0.1 N H ₂ SO ₄ - Impingers 1 & 2	47	425.0	19.98	100.0
	3B	0.1 N H ₂ SO ₄ - Impinger 3	< 2.0	265.0	< 0.53	
	3C	0.1 N NaOH - Impinger 4	< 2.0	74.2	< 0.15	NA
	3D	0.1 N NaOH - Impinger 5	< 2.0	112.4	< 0.22	
Blank	Blank	0.1 N H ₂ SO ₄	< 2.0			
Blank	Blank	0.1 N NaOH	< 2.0			

0.1 N H₂SO₄

Collection Eff. = $100 * \{1 - [\text{XB Chloride Catch (mg)} / \text{XA Chloride Catch (mg)}]\}$
 (%) where X = 1, 2 or 3

0.1 N NaOH

Collection Eff. = $100 * \{1 - [\text{XD Chloride Catch (mg)} / \text{XC Chloride Catch (mg)}]\}$
 (%) where X = 1, 2 or 3

For chloride concentrations less than the analytical detection limit (< 2.0) ---->
 Chloride catch = 0

U.S. STEEL CLAIRTON WORKS - CLAIRTON, PA

NO. 20 BATTERY COMBUSTION STACK

OCTOBER 11, 2000

U.S. EPA CONDITIONAL TEST METHOD 027 SAMPLING

CALCULATION OF THE IMPINGER COLLECTION EFFICIENCIES

Test No.	Sample ID (CLR-#20BS -M26A-)	Sample Type	Ammonium Conc. (mg / L)	Sample Volume (mL)	Ammonium Catch (mg)	Collection Efficiency (%)
1	1A	0.1 N H2SO4 - Impingers 1 & 2	1.2	448.7	0.54	88.6
	1B	0.1 N H2SO4 - Impinger 3	0.2	305.7	0.06	
2	2A	0.1 N H2SO4 - Impingers 1 & 2	0.2	433.4	0.09	81.0
	2B	0.1 N H2SO4 - Impinger 3	0.1	165.0	0.02	
3	3A	0.1 N H2SO4 - Impingers 1 & 2	7.7	425.0	3.27	98.4
	3B	0.1 N H2SO4 - Impinger 3	0.2	265.0	0.05	
Blank Blank		0.1 N H2SO4	< 0.1			

0.1 N H₂SO₄

Collection Eff. = $100 * \{1 - [\text{XB Ammonium Catch (mg)} / \text{XA Ammonium Catch (mg)}]\}$
 (%) where X = 1, 2 or 3

For ammonium concentrations less than the analytical detection limit (< 0.1) ----->

Ammonium catch = 0

PROCESS GAS TESTING CALCULATIONS - ISOKINETIC SAMPLING

CLIENT: U.S. STEEL CLAIRTON WORKS - CLAIRTON, PA

TEST DATE: 10/11/00

TEST SITE: NO. 20 BATTERY COMBUSTION STACK

TEST NO.: CLR- #20BS-M26A-1

Input Parameters (excluding analytical data)

A.	Barometric Pressure (in. Hg)	29.65
B.	Process Gas Static Pressure (in. H2O)	-1.50
C.	Pitot Tube Coefficient	0.84
D.	Dry Gas Meter Calibration Factor	1.0023
»»»	Is the Duct Round (Y/N)?	Y
E.	Duct Diameter (in.) - for round duct	192
F.	Duct Width (in.) - for rectangular duct	0
G.	Duct Depth (in.) - for rectangular duct	0
H.	Nozzle Diameter (in.)	0.625
I.	Average ΔP (in. H2O) = $[(\Delta P^{0.5})_{avg}]^2$ - for flows	0.015
J.	Average ΔP (in. H2O) = $[(\Delta P^{0.5})_{avg}]^2$ - for isokinetic	0.015
K.	Average ΔH (in. H2O) variation	1.07
L.	Average Process Gas Temperature (°F)	530
M.	Average Dry Gas Meter Temperature (°F)	55
N.	Dry Gas Composition (should total to 100%)	
	Carbon Dioxide (%)	4.5
	Oxygen (%)	11.0
	Nitrogen (%)	84.5
	Carbon Monoxide (%)	0.0
	Hydrogen (%)	0.0
	Methane (%)	0.0
	Ethane (%)	0.0
	Argon (%)	0.0
O.	Sample Time (min)	120
P.	Total H2O Mass Collected in Impingers (g)	210.6
Q.	Metered Gas Volume (dcf)	61.632

Calculated Parameters (excluding analytical data)

R.	Absolute Process Gas Pressure (in. Hg)	29.54	[A+(B/13.6)]
S.	Absolute Meter Pressure (in. Hg)	29.73	[A+(K/13.6)]
T.	Duct Area (ft.^2)	2.01E+02	[Pi*E^2/(4*144) or F*G/144]
U.	Nozzle Area (ft.^2)	2.13E-03	[Pi*H^2/(4*144)]
V.	Average Absolute Process Gas Temperature (R)	990	[L+460]
W.	Average Absolute Dry Gas Meter Temperature (R)	515	[M+460]
X.	Dry Gas Volume Sampled (dscf)	62.928	[Q*D*(528/W)*(S/29.92)]
Y.	H2O Vapor Condensed (scf)	9.930	[P*0.04715]
Z.	Calculated Percent H2O in Gas Stream (%)	13.6	[100*Y/(X+Y)]
AA.	Theoretical Maximum Percent H2O in Gas Stream (%)	#N/A	[100*Saturated Water Vapor Pressure / Stack Pressure]
BB.	Actual Percent H2O in Gas Stream (%)	13.6	[Calculated %H2O <= Theoretical Max. %H2O]
CC.	Process Gas Molecular Weight:		

Gas	% Volume / 100	* (1 - %H2O/100)	* Mol. Weight	= Wt./Mol
H2O	0.136		18	2.453
CO2	0.045	0.864	44	1.710
O2	0.110	0.864	32	3.040
N2	0.845	0.864	28	20.435
CO	0.000	0.864	28	0.000
H2	0.000	0.864	2	0.000
CH4	0.000	0.864	16	0.000
C2H6	0.000	0.864	30	0.000
Ar	0.000	0.864	40	0.000

	Process Gas Molecular Weight (lb/lb-mol)	27.64	
DD.	Average Process Gas Velocity (ft/sec)	9.68E+00	$[85.49 * C * [(I * V) / (R * CC)]^{0.5}]$
EE.	Process Gas Volumetric Flow Rate (acfm)	1.17E+05	$[DD * T * 60]$
FF.	Process Gas Volumetric Flow Rate (scfm)	6.15E+04	$[EE * (528 / V) * (R / 29.92)]$
GG.	Process Gas Volumetric Flow Rate (dscfm)	5.31E+04	$[FF * (1 - (BB / 100))]$
HH.	Isokinetic Variation (%)	93.1	$[100 * V * \{(0.002669 * P) + (O * D * S / W)\}] /$

Particulate Matter Results (corrected for blank)

II.	Filter Weight (g)	0.0076	
JJ.	Front-Half Residue Weight (g)	0.0213	
KK.	Back-Half H2O-Condensibles Weight (g)	0.0000	
LL.	Total Weight (g)	0.0289	[II+JJ+KK]
NN.	Concentration (gr/dscf)	0.0071	[(7000/454)*LL/X]
OO.	Mass Flow Rate (lb/hr)	3.23E+00	[NN*GG*60/7000]

PROCESS GAS TESTING CALCULATIONS - ISOKINETIC SAMPLING

CLIENT: U.S. STEEL CLAIRTON WORKS - CLAIRTON, PA

TEST DATE: 10/11/00

TEST SITE: NO. 20 BATTERY COMBUSTION STACK

TEST NO.: CLR- #20BS-M26A-1

Hydrochloric Acid (corrected for blank)

PP.	Total Catch (mg)	15.22	
QQ.	Concentration (mg/dscm)	8.54E+00	[PP/(X*0.02832)]
RR.	Mass Flow Rate (lb/hr)	1.70E+00	[QQ*0.02832*GG*60/454000]

Chlorine Gas Acid (corrected for blank)

SS.	Total Catch (mg)	<	0.20	
TT.	Concentration (mg/dscm)	<	1.12E-01	[SS/(X*0.02832)]
UU.	Mass Flow Rate (lb/hr)	<	2.22E-02	[TT*0.02832*GG*60/454000]

Ammonia Gas Acid (corrected for blank)

VV.	Total Catch (mg)		0.57	
WW.	Concentration (mg/dscm)		3.18E-01	[VV/(X*0.02832)]
XX.	Mass Flow Rate (lb/hr)		6.32E-02	[WW*0.02832*GG*60/454000]

PROCESS GAS TESTING CALCULATIONS - ISOKINETIC SAMPLING

CLIENT: U.S. STEEL CLAIRTON WORKS - CLAIRTON, PA

TEST DATE: 10/11/00

TEST SITE: NO. 20 BATTERY COMBUSTION STACK

TEST NO.: CLR- #20BS-M26A-2

Input Parameters (excluding analytical data)

A.	Barometric Pressure (in. Hg)	29.65
B.	Process Gas Static Pressure (in. H2O)	-1.50
C.	Pitot Tube Coefficient	0.84
D.	Dry Gas Meter Calibration Factor	1.0023
»»»	Is the Duct Round (Y/N)?	Y
E.	Duct Diameter (in.) - for round duct	192
F.	Duct Width (in.) - for rectangular duct	0
G.	Duct Depth (in.) - for rectangular duct	0
H.	Nozzle Diameter (in.)	0.625
I.	Average ΔP (in. H2O) = $[(\Delta P^{0.5})_{avg}]^2$ - for flows	0.018
J.	Average ΔP (in. H2O) = $[(\Delta P^{0.5})_{avg}]^2$ - for isokinetic	0.018
K.	Average ΔH (in. H2O) variation	1.29
L.	Average Process Gas Temperature (°F)	531
M.	Average Dry Gas Meter Temperature (°F)	69
N.	Dry Gas Composition (should total to 100%)	
	Carbon Dioxide (%)	4.5
	Oxygen (%)	11.0
	Nitrogen (%)	84.5
	Carbon Monoxide (%)	0.0
	Hydrogen (%)	0.0
	Methane (%)	0.0
	Ethane (%)	0.0
	Argon (%)	0.0
O.	Sample Time (min)	120
P.	Total H2O Mass Collected in Impingers (g)	240.0
Q.	Metered Gas Volume (dcf)	71.173

Calculated Parameters (excluding analytical data)

R.	Absolute Process Gas Pressure (in. Hg)	29.54	[A+(B/13.6)]
S.	Absolute Meter Pressure (in. Hg)	29.74	[A+(K/13.6)]
T.	Duct Area (ft.^2)	2.01E+02	[Pi*E^2/(4*144) or F*G/144]
U.	Nozzle Area (ft.^2)	2.13E-03	[Pi*H^2/(4*144)]
V.	Average Absolute Process Gas Temperature (R)	991	[L+460]
W.	Average Absolute Dry Gas Meter Temperature (R)	529	[M+460]
X.	Dry Gas Volume Sampled (dscf)	70.785	[Q*D*(528/W)*(S/29.92)]
Y.	H2O Vapor Condensed (scf)	11.316	[P*0.04715]
Z.	Calculated Percent H2O in Gas Stream (%)	13.8	[100*Y/(X+Y)]
AA.	Theoretical Maximum Percent H2O in Gas Stream (%)	#N/A	[100*Saturated Water Vapor Pressure / Stack Pressure]
BB.	Actual Percent H2O in Gas Stream (%)	13.8	[Calculated %H2O <= Theoretical Max. %H2O]
CC.	Process Gas Molecular Weight:		

Gas	% Volume / 100	* (1 - %H2O/100)	* Mol. Weight	= Wt./Mol
H2O	0.138		18	2.481
CO2	0.045	0.862	44	1.707
O2	0.110	0.862	32	3.035
N2	0.845	0.862	28	20.399
CO	0.000	0.862	28	0.000
H2	0.000	0.862	2	0.000
CH4	0.000	0.862	16	0.000
C2H6	0.000	0.862	30	0.000
Ar	0.000	0.862	40	0.000

	Process Gas Molecular Weight (lb/lb-mol)	27.62	
DD.	Average Process Gas Velocity (ft/sec)	1.06E+01	$[85.49 \cdot C^* [(T^*V)/(R^*CC)]^{0.5}]$
EE.	Process Gas Volumetric Flow Rate (acfm)	1.28E+05	$[DD \cdot T^*60]$
FF.	Process Gas Volumetric Flow Rate (scfm)	6.74E+04	$[EE \cdot (528/V) \cdot (R/29.92)]$
GG.	Process Gas Volumetric Flow Rate (dscfm)	5.81E+04	$[FF \cdot (1-(BB/100))]$
HH.	Isokinetic Variation (%)	95.8	$[100 \cdot V^* \{ (0.002669 \cdot P) + (Q \cdot D^*S/W) \}] /$

Particulate Matter Results (corrected for blank)

<u>Analysis of Filter Results (Corrected for Blank)</u>			
II.	Filter Weight (g)	0.0099	
JJ.	Front-Half Residue Weight (g)	0.0196	
KK.	Back-Half H2O-Condensibles Weight (g)	0.0000	
LL.	Total Weight (g)	0.0295	[II+JJ+KK]
NN.	Concentration (gr/dscf)	0.0064	[(7000/454)*LL/X]
OO.	Mass Flow Rate (lb/hr)	3.20E+00	[NN*GG*60/7000]

PROCESS GAS TESTING CALCULATIONS - ISOKINETIC SAMPLING

CLIENT: U.S. STEEL CLAIRTON WORKS - CLAIRTON, PA

TEST DATE: 10/11/00

TEST SITE: NO. 20 BATTERY COMBUSTION STACK

TEST NO.: CLR- #20BS-M26A-2

Hydrochloric Acid (corrected for blank)

PP.	Total Catch (mg)	18.27	
QQ.	Concentration (mg/dscm)	9.11E+00	[PP/(X*0.02832)]
RR.	Mass Flow Rate (lb/hr)	1.98E+00	[QQ*0.02832*GG*60/454000]

Chlorine Gas Acid (corrected for blank)

SS.	Total Catch (mg)	<	0.29	
TT.	Concentration (mg/dscm)	<	1.47E-01	[SS/(X*0.02832)]
UU.	Mass Flow Rate (lb/hr)	<	3.19E-02	[TT*0.02832*GG*60/454000]

Ammonia Gas Acid (corrected for blank)

VV.	Total Catch (mg)		0.10	
WW.	Concentration (mg/dscm)		4.86E-02	[VV/(X*0.02832)]
XX.	Mass Flow Rate (lb/hr)		1.06E-02	[WW*0.02832*GG*60/454000]

PROCESS GAS TESTING CALCULATIONS - ISOKINETIC SAMPLING

CLIENT: U.S. STEEL CLAIRTON WORKS - CLAIRTON, PA

TEST DATE: 10/11/00

TEST SITE: NO. 20 BATTERY COMBUSTION STACK

TEST NO.: CLR- #20BS-M26A-3

Input Parameters (excluding analytical data)

A.	Barometric Pressure (in. Hg)	29.65
B.	Process Gas Static Pressure (in. H ₂ O)	-1.50
C.	Pitot Tube Coefficient	0.84
D.	Dry Gas Meter Calibration Factor	1.0023
»»»	Is the Duct Round (Y/N)?	Y
E.	Duct Diameter (in.) - for round duct	192
F.	Duct Width (in.) - for rectangular duct	0
G.	Duct Depth (in.) - for rectangular duct	0
H.	Nozzle Diameter (in.)	0.625
I.	Average ΔP (in. H ₂ O) = $[(\Delta P^{0.5})_{avg}]^2$ - for flows	0.018
J.	Average ΔP (in. H ₂ O) = $[(\Delta P^{0.5})_{avg}]^2$ - for isokinetic	0.018
K.	Average ΔH (in. H ₂ O) variation	1.39
L.	Average Process Gas Temperature (°F)	534
M.	Average Dry Gas Meter Temperature (°F)	81
N.	Dry Gas Composition (should total to 100%)	
	Carbon Dioxide (%)	4.5
	Oxygen (%)	11.0
	Nitrogen (%)	84.5
	Carbon Monoxide (%)	0.0
	Hydrogen (%)	0.0
	Methane (%)	0.0
	Ethane (%)	0.0
	Argon (%)	0.0
O.	Sample Time (min)	120
P.	Total H ₂ O Mass Collected in Impingers (g)	235.5
Q.	Metered Gas Volume (dscf)	74.480

Calculated Parameters (excluding analytical data)

R.	Absolute Process Gas Pressure (in. Hg)	29.54	[A+(B/13.6)]
S.	Absolute Meter Pressure (in. Hg)	29.75	[A+(K/13.6)]
T.	Duct Area (ft. ²)	2.01E+02	[Pi*E ² /(4*144) or F*G/144]
U.	Nozzle Area (ft. ²)	2.13E-03	[Pi*H ² /(4*144)]
V.	Average Absolute Process Gas Temperature (R)	994	[L+460]
W.	Average Absolute Dry Gas Meter Temperature (R)	541	[M+460]
X.	Dry Gas Volume Sampled (dscf)	72.449	[Q*D*(528/W)*(S/29.92)]
Y.	H ₂ O Vapor Condensed (scf)	11.104	[P*0.04715]
Z.	Calculated Percent H ₂ O in Gas Stream (%)	13.3	[100*Y/(X+Y)]
AA.	Theoretical Maximum Percent H ₂ O in Gas Stream (%)	#N/A	[100*Saturated Water Vapor Pressure / Stack Pressure]
BB.	Actual Percent H ₂ O in Gas Stream (%)	13.3	[Calculated %H ₂ O <= Theoretical Max. %H ₂ O]
CC.	Process Gas Molecular Weight:		

Gas	% Volume / 100	* (1 - %H ₂ O/100)	* Mol. Weight	= Wt./Mol
H ₂ O	0.133		18	2.392
CO ₂	0.045	0.867	44	1.717
O ₂	0.110	0.867	32	3.052
N ₂	0.845	0.867	28	20.516
CO	0.000	0.867	28	0.000
H ₂	0.000	0.867	2	0.000
CH ₄	0.000	0.867	16	0.000
C ₂ H ₆	0.000	0.867	30	0.000
Ar	0.000	0.867	40	0.000

	Process Gas Molecular Weight (lb/lb-mol)	27.68	
DD.	Average Process Gas Velocity (ft/sec)	1.06E+01	[85.49*C*[(I*V)/(R*CC)]^0.5]
EE.	Process Gas Volumetric Flow Rate (acfm)	1.28E+05	[DD*T*60]
FF.	Process Gas Volumetric Flow Rate (scfm)	6.72E+04	[EE*(528/V)*(R/29.92)]
GG.	Process Gas Volumetric Flow Rate (dscfm)	5.83E+04	[FF*(1-(BB/100))]
HH.	Isokinetic Variation (%)	97.8	[100*V*{(0.002669*P)+(Q*D*S/W)}]

Particulate Matter Results (corrected for blank)

II.	Filter Weight (g)	0.0050	
JJ.	Front-Half Residue Weight (g)	0.0240	
KK.	Back-Half H2O-Condensibles Weight (g)	0.0000	
LL.	Total Weight (g)	0.0290	[II+JJ+KK]
NN.	Concentration (gr/dscf)	0.0062	[(7000/454)*LL/X]
OO.	Mass Flow Rate (lb/hr)	3.08E+00	[NN*GG*60/7000]

PROCESS GAS TESTING CALCULATIONS - ISOKINETIC SAMPLING

CLIENT: U.S. STEEL CLAIRTON WORKS - CLAIRTON, PA

TEST DATE: 10/11/00

TEST SITE: NO. 20 BATTERY COMBUSTION STACK

TEST NO.: CLR- #20BS-M26A-3

Hydrochloric Acid (corrected for blank)

PP.	Total Catch (mg)	20.54	
QQ.	Concentration (mg/dscm)	1.00E+01	[PP/(X*0.02832)]
RR.	Mass Flow Rate (lb/hr)	2.18E+00	[QQ*0.02832*GG*60/454000]

Chlorine Gas Acid (corrected for blank)

SS.	Total Catch (mg)	< 0.15	
TT.	Concentration (mg/dscm)	< 7.23E-02	[SS/(X*0.02832)]
UU.	Mass Flow Rate (lb/hr)	< 1.58E-02	[TT*0.02832*GG*60/454000]

Ammonia Gas Acid (corrected for blank)

VV.	Total Catch (mg)	3.14	
WW.	Concentration (mg/dscm)	1.53E+00	[VV/(X*0.02832)]
XX.	Mass Flow Rate (lb/hr)	3.34E-01	[WW*0.02832*GG*60/454000]