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**Emission Test Report  
Kaiser Steel Corporation, Fontana, Ca.  
Coke Oven Battery "B" Baghouse**

To

**ENVIRONMENTAL PROTECTION AGENCY**

**Contract #68-02-2812  
Work Assignment #43**

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**TRW**  
**ENVIRONMENTAL ENGINEERING DIVISION**

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## SECTION 1

### INTRODUCTION

A test crew from TRW Environmental Engineering Division performed emission testing at Kaiser Steel Corporation's Fontana works between September 17th and 22nd, 1979. The testing was performed simultaneously at the inlet and outlet of a baghouse controlling emissions from Coke oven battery "B". The test results will be used to assist the EPA in establishing performance standards for the iron and steel industry.

The gas constituents monitored included particulates, benzo-a-pyrene, carbon monoxide, oxygen, carbon dioxide, and benzene. Opacity observations of the battery stack were made during the tests. Two engineers monitored the process during the testing to assure normal battery operation.

This report presents the results of the sampling and analysis effort at the Kaiser Steel Corporation Plant in Fontana, California. The following sections of the report contain a summary of the results, description of the process, descriptions of the sampling locations, descriptions of the sampling and analysis procedures, and appendices containing field and laboratory data and example calculations.

## SECTION 2

### SUMMARY AND DISCUSSION OF RESULTS

The results of the test program at Kaiser Steels baghouse "B" are summarized in Tables 1-5 and figures 1-4. The results of simultaneous inlet and outlet particulate tests are summarized in Tables 1 and 2, respectively. The results of simultaneous inlet and outlet benzo-a-pyrene (BaP) tests are summarized in Tables 3 and 4, respectively. The analysis results of the integrated bag samples for benzene, O<sub>2</sub>, CO<sub>2</sub>, and CO are given in Table 5. The results of continuous monitoring of the stack gas for carbon monoxide is presented graphically in Figures 1-4.

The data from particulate test number 2 (Baghouse Inlet) is not presented because this run was terminated at the middle of the test. The probe at the inlet sampling location failed to pass the leak check after changing sampling ports and the glass probe liner was found to be broken.

The BaP and particulate tests were done simultaneously except for test number 2 where the particulate test was aborted. The simultaneous testing was accomplished by operating a BaP train in one sampling port and a particulate sampling train in the other port at both the inlet and outlet locations. Continuous carbon monoxide monitoring and an integrated bag sample (for benzene, CO<sub>2</sub>, CO, and O<sub>2</sub>) were also done simultaneously with the BaP and particulate tests.

Since the baghouse inlet particulate run #2 was aborted, another run was made on Friday. This run (#4) consisted of a particulate sample at both the inlet and outlet. The chart below gives a visual presentation of the sample runs made in order to facilitate the comparison of Inlet and Outlet runs with respect to BAP and particulate testing.

	<u>BAGHOUSE INLET</u>		
<u>Run 1</u>	<u>Run 2</u>	<u>Run 3</u>	<u>Run 4</u>
Particulate and BAP	Particulate Aborted BAP only	Particulate and BAP	Particulate Only
	<u>BAGHOUSE OUTLET</u>		
Particulate and BAP	Particulate and BAP	Particulate and BAP	Particulate Only

Table 1  
Baghouse Inlet Particulate Results

RUN NUMBER	1		3		4		AVERAGE	
	ENGLISH UNITS	METRIC UNITS						
I DATE	9/18/79	9/18/79	9/20/79	9/20/79	9/21/79	9/21/79		
II STACK PARAMETERS								
PST - STATIC PRESSURE, "Hg (mmHg)	-0.132	-3.36	-0.132	-3.36	-0.132	-3.36	-0.132	-3.36
Ps - STACK GAS PRESSURE, "Hg ABSOLUTE (mmHg)	28.44	722.32	28.60	726.38	28.57	725.62	28.54	724.83
% CO <sub>2</sub> - VOLUME % DRY	3.80	3.80	4.35	4.35	4.46	4.46	4.20	4.20
% O <sub>2</sub> - VOLUME % DRY	13.30	18.30	12.00	12.00	12.10	12.10	12.47	12.47
% CO - VOLUME % DRY	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
% N <sub>2</sub> - VOLUME % DRY	82.90	82.90	83.65	83.65	83.44	83.44	83.33	83.33
Ts - AVERAGE STACK TEMPERATURE OF (°C)	482	250	495	257	480	249	486	252
% H <sub>2</sub> O - % MOISTURE IN STACK GAS, BY VOLUME	8.06	8.06	5.49	5.49	6.15	6.15	6.57	6.57
As - STACK AREA, FT <sup>2</sup> (M <sup>2</sup> )	20.63	1.92	20.63	1.92	20.63	1.92	20.63	1.92
Md - MOLECULAR WEIGHT OF STACK GAS, DRY BASIS	29.14	29.14	29.18	29.18	29.20	29.20	29.17	29.17
Ms - MOLECULAR WEIGHT OF STACK GAS, WET BASIS	28.24	28.24	28.56	28.56	28.51	28.51	28.44	28.44
Vs - STACK GAS VELOCITY, FT/SEC. (M/SEC)	58.31	17.77	57.12	17.41	58.03	17.69	57.82	17.62
Qa - STACK GAS VOLUMETRIC FLOW AT STACK CONDITIONS, ACFM (NM <sup>3</sup> /MIN)	72040	2040	70569	1999	71702	2031	71437	2023
Qs - STACK GAS VOLUMETRIC FLOW AT STANDARD CONDITIONS, DSCFM (NM <sup>3</sup> /MIN)	35318	1000	35277	999	36137	1023	35577	1007
III TEST CONDITIONS								
Pb - BAROMETRIC PRESSURE, "Hg (mmHg)	28.57	725.68	28.73	729.74	28.70	728.98	28.67	728.13
Dn - SAMPLING NOZZLE DIAMETER, IN. (MM)	0.25	6.35	0.25	6.35	0.25	6.35	0.25	6.35
T - SAMPLING TIME, MIN	120	120	120	120	120	120	120	120
Vm - SAMPLE VOLUME, ACF (M <sup>3</sup> )	73.30	2.08	79.32	2.25	80.16	2.27	77.59	2.20
Np - NET SAMPLING POINTS	12	12	12	12	12	12	12	12
Cp - PITOT TUBE COEFFICIENT	0.84	0.84	0.84	0.84	0.84	0.84	0.84	0.84
Tm - AVERAGE METER TEMPERATURE OF (°C)	113	45	118	48	102	39	111	44
Pm - AVERAGE ORIFICE PRESSURE DROP, "H <sub>2</sub> O (mmH <sub>2</sub> O)	0.88	22.35	1.19	30.23	1.27	32.26	1.11	28.28
Vlc - CONDENSATE COLLECTED (IMPINGERS AND GEL), MLS	---	123.4	---	88.3	---	103.5	---	105.1
ΔP - STACK VELOCITY HEAD "H <sub>2</sub> O (mmH <sub>2</sub> O)	0.562	14.28	0.540	13.74	0.566	14.38		
IV TEST CALCULATIONS								
Vm - CONDENSED WATER VAPOR, SDCF (NM <sup>3</sup> )	5.91	0.17	4.35	0.12	4.93	0.14	5.06	0.14
Vn - VOLUME OF GAS SAMPLED AT STANDARD CONDITIONS, DSCF (NM <sup>3</sup> )	64.625	1.830	69.802	1.977	72.468	2.052	68.965	1.953
% H <sub>2</sub> O - PERCENT MOISTURE, BY VOLUME	8.06	8.06	5.49	5.49	6.15	6.15	6.57	6.57
Ms - MOLECULAR WEIGHT OF STACK GAS, WET BASIS	28.24	28.24	28.56	28.56	28.51	28.51	28.44	28.44
Vs - STACK VELOCITY, FT/SEC (M/SEC)	58.31	17.77	57.12	17.41	58.03	17.69	57.82	17.62
% I - PERCENT ISOKINETIC	91	91	98	98	99	99	96	96
V ANALYTICAL DATA								
A) PARTICULATES FRONT HALF								
PROBE (HG)		260.9		159.6		126.0		182.2
CYCLONE (HG)								
FILTER (HG)		193.2		162.2		127.0		160.8
PARTICULATES FRONT HALF TOTAL (HG)		454.1		321.8		253.0		343.0
GRS/SDCF, (HG/M <sup>3</sup> )	0.108	248.1	0.071	162.77	0.054	123.29	0.078	178.05
#/HR, (KG/HR)	32.82	14.89	21.47	9.74	16.69	7.57	23.67	10.64
B) PARTICULATED BACK HALF (CONDENSABLES)								
IMPINGERS (HG)		4.70		52.0		45.4		34.03
GRS/SDCF, (HG/M <sup>3</sup> )	0.001	2.56	0.011	26.30	0.01	22.12	0.007	16.99
#/HR, (KG/HR)	0.30	0.14	3.33	1.51	2.99	1.36	2.21	1.00
C) TOTAL PARTICULATE (HG)								
GRS/SDCF, (HG/M <sup>3</sup> )	0.109	458.8	0.082	373.8	0.064	298.4	0.085	377.0
#/HR, (KG/HR)	33.16	250.7	24.79	189.07	19.68	145.41	25.88	195.06
D) SDI FRONT HALF (HG)								
GRS/SDCF, (HG/M <sup>3</sup> )	17.49	17.49	9.47	9.47	6.54	6.54	11.17	11.17
#/HR, (KG/HR)	0.27	71.4	0.017	36.7	0.012	26.7	0.033	45.6
	21.19	9.61	5.08	2.30	3.47	1.64	9.96	4.52

**Table 2**  
**Baghouse Outlet Particulate Results**

RUN NUMBER	1		2		3		4	
	ENGLISH UNITS	METRIC UNITS						
I DATE	9/18/79	9/18/79			9/20/79	9/20/79	9/21/79	9/21/79
II STACK PARAMETERS								
Pst - STATIC PRESSURE, "Hg (mmHg)	-0.61	-15.50	-0.30	-15.50	-0.61	-15.50	-0.61	-15.50
Ps - STACK GAS PRESSURE, "Hg ABSOLUTE (mmHg)	27.96	710.18	27.96	710.18	28.12	714.24	28.09	713.48
% CO <sub>2</sub> - VOLUME % DRY	3.80	3.80	3.03	3.03	4.35	4.35	4.46	4.46
% O <sub>2</sub> - VOLUME % DRY	13.30	13.30	15.1	15.1	12.00	12.00	12.10	12.10
% CO - VOLUME % DRY	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
% N <sub>2</sub> - VOLUME % DRY	82.9	82.9	81.87	81.87	83.65	83.65	83.44	83.44
Ts - AVERAGE STACK TEMPERATURE °F (°C)	442	228	443.3	228.5	443	228	444	229
% H <sub>2</sub> O - % MOISTURE IN STACK GAS, BY VOLUME	9.04	9.04	2.1	2.1	7.47	7.47	6.88	6.88
As - STACK AREA, FT <sup>2</sup> (M <sup>2</sup> )	20.63	1.92	20.6	1.92	20.63	1.92	20.63	1.92
Md - MOLECULAR WEIGHT OF STACK GAS, DRY BASIS	29.14	29.14	29.09	29.09	29.18	29.18	29.20	29.20
Ms - MOLECULAR WEIGHT OF STACK GAS, WET BASIS	28.13	28.13	28.86	28.86	28.34	28.34	28.43	28.43
Vs - STACK GAS VELOCITY, FT/SEC. (M/SEC)	59.27	18.06	58.12	17.71	58.55	17.85	57.24	17.45
Qa - STACK GAS VOLUMETRIC FLOW AT STACK CONDITIONS, ACFM (NM <sup>3</sup> /MIN)	73230	2074	71811	2034	72343	2049	70723	2003
Qs - STACK GAS VOLUMETRIC FLOW AT STANDARD CONDITIONS, DSCFM (NM <sup>3</sup> /MIN)	36472	1033	38433	1088	36839	1043	36136	1023
III TEST CONDITIONS								
Pb - BAROMETRIC PRESSURE, "Hg (mmHg)	28.57	725.68	28.57	725.68	28.73	729.74	28.70	728.98
Dn - SAMPLING NOZZLE DIAMETER, IN. (MM)	0.25	6.35	0.25	6.35	0.25	6.35	0.25	6.35
T - SAMPLING TIME, MIN	120	120	120	120	120	120	120	120
Vn - SAMPLE VOLUME, ACF (M <sup>3</sup> )	78.39	2.22	90.84	2.29	77.76	2.20	75.07	2.13
Np - NET SAMPLING POINTS	12	12	12	12	12	12	12	12
Cp - PITOT TUBE COEFFICIENT	0.84	0.84	0.84	0.84	0.84	0.84	0.84	0.84
Tm - AVERAGE METER TEMPERATURE °F (°C)	105	41	107.58	41.99	104	40	103	40
Pm - AVERAGE ORIFICE PRESSURE DROP, "H <sub>2</sub> O (MMH <sub>2</sub> O)	1.38	35.05	1.42	36.14	1.36	34.44	1.26	31.95
Vlc - CONDENSATE COLLECTED (IMPINGERS AND GELS), MLS	---	151.9	---	33.9	---	123.3	---	108.9
ΔP - STACK VELOCITY HEAD "H <sub>2</sub> O (MMH <sub>2</sub> O)	0.594	15.09	0.585	14.86	0.587	14.91	0.561	14.25
IV TEST CALCULATIONS								
Vm - CONDENSED WATER VAPOR, DSCF (NM <sup>3</sup> )	7.08	0.20	1.70	0.05	5.81	0.165	5.16	0.15
Vn - VOLUME OF GAS SAMPLED AT STANDARD CONDITIONS, DSCF (NM <sup>3</sup> )	70.185	1.988	72.058	2.041	70.082	1.985	67.693	1.917
% H <sub>2</sub> O - PERCENT MOISTURE, BY VOLUME	9.04	9.04	2.1	2.1	7.47	7.47	6.88	6.88
Ms - MOLECULAR WEIGHT OF STACK GAS, WET BASIS	28.13	28.13	28.86	28.86	28.34	28.34	28.43	28.43
Vs - STACK VELOCITY, FT/SEC (M/SEC)	59.27	18.06	58.12	17.71	58.55	17.85	57.24	17.45
% I - PERCENT ISOKINETIC	95	95	92.9	92.9	94	94	93	93
V ANALYTICAL DATA								
A) PARTICULATES FRONT HALF								
Probe (HG)		44.8		16.3		82.4		60.8
Cyclone (HG)				1.6		74.1		1.10
Filter (HG)		79.4		17.9		156.5		61.9
Particulates Front Half Total (HG)		124.2		19.5		230.6		63.0
GRS/SDCF, (HG/M <sup>3</sup> )	0.027	62.47	0.004	8.77	0.034	78.84	0.014	32.29
#/HR, (KG/HR)	8.54	3.87	1.26	0.57	10.88	4.94	4.37	1.98
B) PARTICULATES BACK HALF (CONDENSABLES)								
Impingers (HG)		3.41		6.7		33.4		116.0
GRS/SDCF, (HG/M <sup>3</sup> )	0.007	17.15	0.001	3.28	0.007	16.83	0.026	60.51
#/HR, (KG/HR)	2.34	1.06	0.47	0.21	2.32	1.05	8.19	3.71
C) TOTAL PARTICULATE								
GRS/SDCF, (HG/M <sup>3</sup> )	0.0348	79.64	0.005	12.05	0.041	95.67	0.040	92.80
#/HR, (KG/HR)	10.88	4.94	1.73	0.78	13.20	5.99	12.56	5.70
D) SO <sub>2</sub> FRONT HALF (HG)								
Probe (HG)	6.18	6.18	0.39	0.39	9.32	9.32	6.25	6.25
GRS/SDCF, (HG/M <sup>3</sup> )	0.011	25.22	0.004	1.57	0.017	38.06	0.011	25.50
#/HR, (KG/HR)	3.45	1.56	0.144	0.365	5.26	2.39	3.45	1.56

Table 3  
Baghouse Inlet BaP Results

RUN NUMBER	1		2		3		4	
	ENGLISH UNITS	METRIC UNITS	ENGLISH UNITS	METRIC UNITS	ENGLISH UNITS	METRIC UNITS	ENGLISH UNITS	METRIC UNITS
I. DATE	9/18/79	9/18/79	9/19/79	9/19/79	9/20/79	9/20/79		
II. STACK PARAMETERS								
Pst - STATIC PRESSURE, "Hg (mmHg)	-0.132	-3.36	-0.132	-3.36	-0.132	-3.36	-0.132	-3.36
Ps - STACK GAS PRESSURE, "Hg ABSOLUTE (mmHg)	28.44	722.32	28.44	722.32	28.60	726.38	28.49	723.67
% CO <sub>2</sub> - VOLUME % DRY	3.80	3.80	3.03	3.03	4.35	4.35	3.73	3.73
% O <sub>2</sub> - VOLUME % DRY	13.30	13.30	15.10	15.10	12.00	12.00	13.47	13.47
% CO - VOLUME % DRY	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
% N <sub>2</sub> - VOLUME % DRY	82.90	82.90	81.87	81.87	83.65	83.65	82.81	82.81
Ts - AVERAGE STACK TEMPERATURE °F (°C)	480	249	536	280	495	257	504	262
% H <sub>2</sub> O - % MOISTURE IN STACK GAS, BY VOLUME	8.06	8.06	9.12	9.12	5.49	5.66	7.36	7.61
As - STACK AREA, FT <sup>2</sup> (M <sup>2</sup> )	20.63	1.92	20.63	1.92	20.63	1.92	20.63	1.92
Ms - MOLECULAR WEIGHT OF STACK GAS, DRY BASIS	29.14	29.14	29.09	29.09	29.18	29.18	29.14	29.14
Vs - MOLECULAR WEIGHT OF STACK GAS, MET BASIS	28.24	28.24	28.08	28.08	28.66	28.54	28.33	28.29
Qs - STACK GAS VOLUMETRIC FLOW AT STANDARD CONDITIONS, DSCFM (NM <sup>3</sup> /MIN)	70410	1994	73356	2078	67434	1909	70400	1994
Qs - STACK GAS VOLUMETRIC FLOW AT STANDARD CONDITIONS, DSCFM (NM <sup>3</sup> /MIN)	34592	980	33625	952	33650	953	33956	962
III. TEST CONDITIONS								
Pb - BAROMETRIC PRESSURE, "Hg (mmHg)	28.57	725.68	28.57	725.68	28.73	729.74	28.62	727.03
Dn - SAMPLING NOZZLE DIAMETER, IN. (MM)	0.25	6.35	0.25	6.35	0.25	6.35	0.25	6.35
T - SAMPLING TIME, MIN	120	120	120	120	120	120	120	120
Vm - SAMPLE VOLUME, ACF (M <sup>3</sup> )	82.14	2.33	75.73	2.14	71.18	2.02	76.35	2.16
Np - NET SAMPLING POINTS	12	12	12	12	12	12	12	12
Cp - PITOT TUBE COEFFICIENT	0.84	0.84	0.84	0.84	0.84	0.84	0.84	0.84
Tm - AVERAGE METER TEMPERATURE °F (°C)	113	45	118	48	120	49	117	47
Pm - AVERAGE ORIFICE PRESSURE DROP, "H <sub>2</sub> O (mmH <sub>2</sub> O)	1.24	31.50	1.23	31.24	1.10	27.94	1.19	30.23
VLC - CONDENSATE COLLECTED (IMPINGERS AND GEL), MLS	---	138.4	---	144.9	---	81.5	---	121.6
ΔP - STACK VELOCITY HEAD "H <sub>2</sub> O (mmH <sub>2</sub> O)	0.538	13.67	0.548	13.92	0.494	12.55	0.527	13.38
IV. TEST CALCULATIONS								
Vw - CONDENSED WATER VAPOR, DSCF (NM <sup>3</sup> )	6.62	0.19	6.91	0.20	4.03	0.11	5.85	0.17
Vm - VOLUME OF GAS SAMPLED AT STANDARD CONDITIONS, DSCF (NM <sup>3</sup> )	72.484	2.053	66.253	1.876	62.399	1.766	67.045	1.898
% H <sub>2</sub> O - PERCENT MOISTURE, BY VOLUME	8.06	8.06	9.12	9.12	5.49	5.66	7.61	7.61
Ms - MOLECULAR WEIGHT OF STACK GAS, MET BASIS	28.24	28.24	28.08	28.08	28.66	28.54	28.33	28.29
Vs - STACK VELOCITY, FT/SEC (M/SEC)	56.99	17.37	59.37	18.10	54.60	16.64	56.99	17.37
% I - PERCENT ISOKINETIC	104	104	98	98	93.4	92	98	98
V. ANALYTICAL DATA								
A) BAP FRONT HALF								
PROBE (UG)	---	6.34	---	5.49	---	7.3	---	5.71
CYCLONE (UG)	---	---	---	---	---	---	---	---
FILTER (UG)	---	4.14	---	9.5	---	10.0	---	7.88
BAP FRONT HALF TOTAL (UG)	---	8.48	---	14.99	---	17.3	---	13.59
GRS/DSCF, (UG/M <sup>3</sup> )	1.8 x 10 <sup>-6</sup>	0.004	3.5 x 10 <sup>-6</sup>	0.008	4.3 x 10 <sup>-6</sup>	0.0098	3.2 x 10 <sup>-6</sup>	0.0073
F/DAY (KG/DAY)	0.0128	0.006	0.024	0.011	0.030	0.013	0.022	0.010
B) BAP BACK HALF								
ADSORBENT SAMPLER (UG)	---	1.67	---	2.05	---	2.10	---	1.94
IMPINGERS (UG)	---	---	---	---	---	1.83	---	1.83
BACK HALF TOTAL (UG)	---	1.67	---	2.05	---	3.93	---	---
F/DAY (KG/DAY)	3.56 x 10 <sup>-7</sup>	0.0008	4.8 x 10 <sup>-7</sup>	0.0011	9.7 x 10 <sup>-7</sup>	0.0022	6.0 x 10 <sup>-7</sup>	0.0014
BAP TOTAL (UG)	---	3.0025	---	0.0033	---	0.0067	---	0.0017
GRS/DSCF, (UG/M <sup>3</sup> )	2.16 x 10 <sup>-6</sup>	0.0048	3.98 x 10 <sup>-6</sup>	0.009	5.3 x 10 <sup>-6</sup>	0.012	3.8 x 10 <sup>-6</sup>	0.0086
F/DAY (KG/DAY)	0.015	0.0071	0.027	0.012	0.036	0.016	0.026	0.012

Table 4  
Baghouse Outlet BaP Results

RUN NUMBER	1		2		3		4	
	ENGLISH UNITS	METRIC UNITS	ENGLISH UNITS	METRIC UNITS	ENGLISH UNITS	METRIC UNITS	ENGLISH UNITS	METRIC UNITS
I DATE	9/18/79	9/18/79	9/19/79	9/19/79	9/20/79	9/20/79		
II STACK PARAMETERS								
Pst - STATIC PRESSURE, "Hg (mmHg)	-0.61	-15.50	-0.61	-15.50	-0.61	-15.50	-0.61	-15.50
Ps - STACK GAS PRESSURE, "Hg ABSOLUTE (mmHg)	27.96	710.18	27.96	710.18	28.12	714.24	28.01	711.53
% CO <sub>2</sub> - VOLUME % DRY	3.80	3.80	3.03	3.03	4.35	4.35	3.73	3.73
% O <sub>2</sub> - VOLUME % DRY	13.30	13.30	15.10	15.10	12.00	12.00	13.47	13.47
% CO - VOLUME % DRY	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
% H <sub>2</sub> - VOLUME % DRY	82.90	82.90	81.87	81.87	83.65	83.65	82.81	82.81
Ts - AVERAGE STACK TEMPERATURE OF (°C)	440	227	441	228	443	229	441	228
% H <sub>2</sub> O - % MOISTURE IN STACK GAS, BY VOLUME	9.04	9.04	3.10	2.10	7.47	7.47	6.2	6.54
As - STACK AREA, FT <sup>2</sup> (M <sup>2</sup> )	20.63	1.92	20.63	1.92	20.63	1.92	20.63	1.92
Md - MOLECULAR WEIGHT OF STACK GAS, DRY BASIS	29.14	29.14	29.09	29.09	29.18	29.18	29.14	29.14
Ms - MOLECULAR WEIGHT OF STACK GAS, WET BASIS	28.13	28.13	28.86	28.86	28.34	28.34	28.41	28.41
Vs - STACK GAS VELOCITY, FT/SEC. (M/SEC)	58.35	17.78	57.19	17.43	57.93	17.66	57.82	17.62
Qa - STACK GAS VOLUMETRIC FLOW AT STACK CONDITIONS, ACFM (NM <sup>3</sup> /MIN)	72094	2042	70787	2005	71569	2027	71483	2024
Qs - STACK GAS VOLUMETRIC FLOW AT STANDARD CONDITIONS, DSCFM (NM <sup>3</sup> /MIN)	35986	1019	37598	1065	3641	1031	36666	1038
III TEST CONDITIONS								
Pb - BAROMETRIC PRESSURE, "Hg (mmHg)	28.57	725.68	28.57	725.68	28.73	729.74	28.62	727.03
Dn - SAMPLING NOZZLE DIAMETER, IN. (MM)	0.25	6.35	0.25	6.35	0.25	6.35	0.25	6.35
T - SAMPLING TIME, MIN	120	120	120	120	120	120	120	120
Vn - SAMPLE VOLUME, ACF (M <sup>3</sup> )	74.68	2.11	80.82	2.29	78.82	2.23	78.11	2.21
Np - NET SAMPLING POINTS	12	12	12	12	12	12	12	12
Cp - PITOT TUBE COEFFICIENT	0.84	0.84	0.84	0.84	0.84	0.84	0.84	0.84
Tm - AVERAGE METER TEMPERATURE OF (°C)	107	42	101	38	105	40	104	40
Pm - AVERAGE ORIFICE PRESSURE DROP, "H <sub>2</sub> O (MMH <sub>2</sub> O)	1.41	35.81	1.38	35.05	1.33	33.81	1.37	34.89
Vlc - CONDENSATE COLLECTED (IMPINGERS AND GEL), MLS	---	144.2	---	50.8	---	124.9	---	106.6
ΔP - STACK VELOCITY HEAD "H <sub>2</sub> O (MMH <sub>2</sub> O)	0.577	14.66	0.568	14.43	0.574	14.58	0.573	14.56
IV TEST CALCULATIONS								
Vn - CONDENSED WATER VAPOR, DSCF (NM <sup>3</sup> )	6.75	0.19	2.51	0.07	5.89	0.17	5.05	0.14
Vm - VOLUME OF GAS SAMPLED AT STANDARD CONDITIONS, DSCF (NM <sup>3</sup> )	66.630	1.887	72.862	2.063	71.003	2.011	70.165	1.99
% H <sub>2</sub> O - PERCENT MOISTURE, BY VOLUME	9.04	9.04	3.10	3.10	7.47	7.47	6.54	6.54
Ms - MOLECULAR WEIGHT OF STACK GAS, WET BASIS	28.13	28.13	28.75	28.75	28.34	28.34	28.41	28.41
Vs - STACK VELOCITY, FT/SEC (M/SEC)	58.35	17.78	57.31	17.47	57.93	17.66	57.86	17.64
% I - PERCENT ISOKINETIC	92	92	96.9	96	97	97	95	95
V ANALYTICAL DATA								
A) BAP FRONT HALF								
PROBE (UG)	---	5.0	---	5.42	---	7.76	---	5.92
CYCLONE (UG)	---	---	---	---	---	---	---	---
FILTER (UG)	---	2.20	---	1.12	---	1.25	---	1.19
BAP FRONT HALF TOTAL (UG)	---	7.20	---	6.54	---	7.60	---	7.11
GRS/SDCF, (UG/M <sup>3</sup> )	1.7 x 10 <sup>-6</sup>	0.0038	1.4 x 10 <sup>-6</sup>	0.0032	1.6 x 10 <sup>-6</sup>	0.0038	1.6 x 10 <sup>-6</sup>	0.0036
#/DAY (KG/DAY)	0.012	0.0056	0.011	0.0049	0.012	0.0056	0.012	0.0054
B) BAP BACK HALF								
ABSORBENT SAMPLER (UG)	---	1.12	---	10.60	---	2.75	---	4.82
IMPINGERS (UG)	---	2.28	---	2.56	---	1.91	---	2.26
BACK HALF TOTAL (UG)	---	3.40	---	13.16	---	4.66	---	7.07
GRS/SDCF	7.9 x 10 <sup>-7</sup>	0.0018	2.8 x 10 <sup>-6</sup>	0.0064	1.0 x 10 <sup>-6</sup>	0.0023	1.53 x 10 <sup>-6</sup>	0.0035
#/DAY (KG/DAY)	0.0058	0.0022	0.022	0.0098	0.0075	0.0034	0.0118	0.0053
BAP TOTAL (UG)	---	10.60	---	19.70	---	12.26	---	14.19
GRS/SDCF, (UG/M <sup>3</sup> )	2.5 x 10 <sup>-6</sup>	0.0056	4.2 x 10 <sup>-6</sup>	0.0096	2.6 x 10 <sup>-6</sup>	0.0061	3.1 x 10 <sup>-6</sup>	0.0071
#/DAY (KG/DAY)	0.018	0.0082	0.033	0.0147	0.0196	0.0090	0.0235	0.0106

Table 5  
Gaseous Constituent Concentrations

Test No.	Date	Benzene (ppm)	Carbon Monoxide (ppm)	Carbon Dioxide (%)	Oxygen (%)
1	9/18/79	1.8	153	3.80	13.30
2	9/19/79	2.9	111	3.03	15.10
3	9/20/79	2.5	97	4.35	12.00
4	9/21/79	4.1	139	4.46	12.10

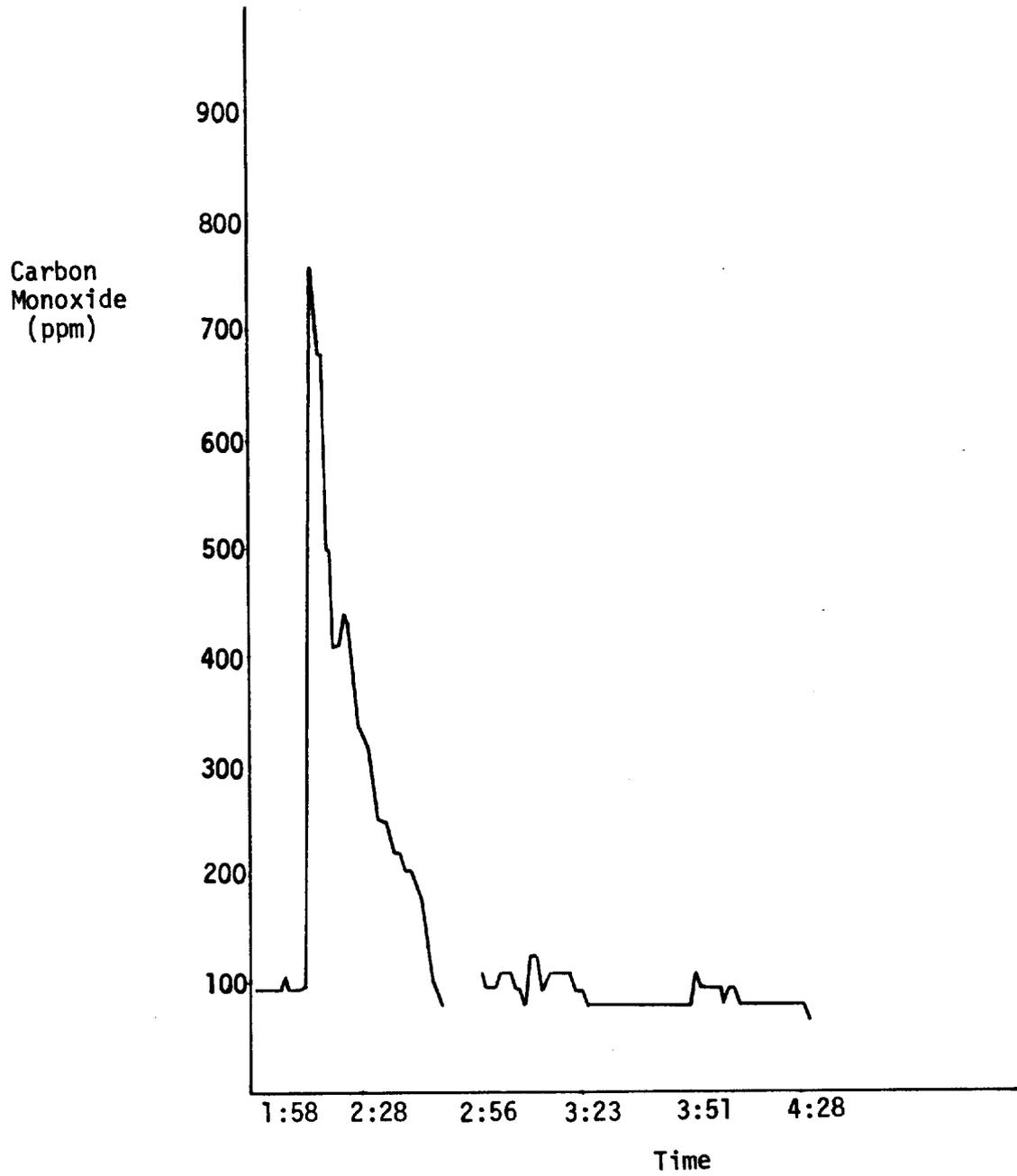


Figure 1  
Carbon Monoxide Concentration, 9/18/79

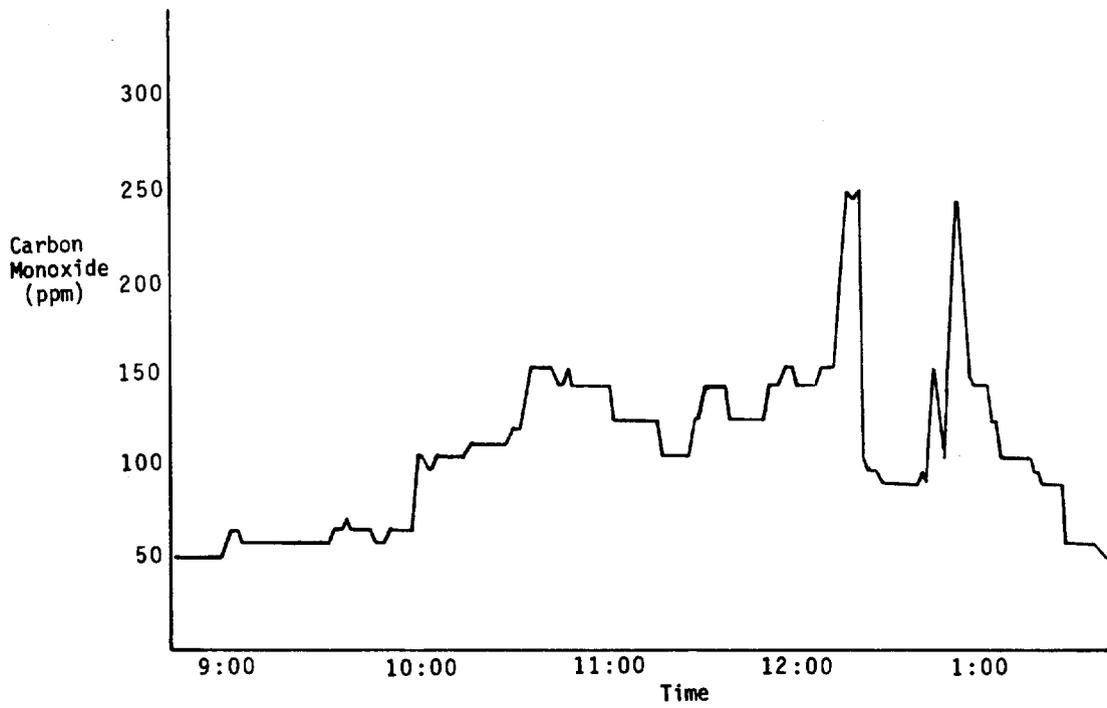
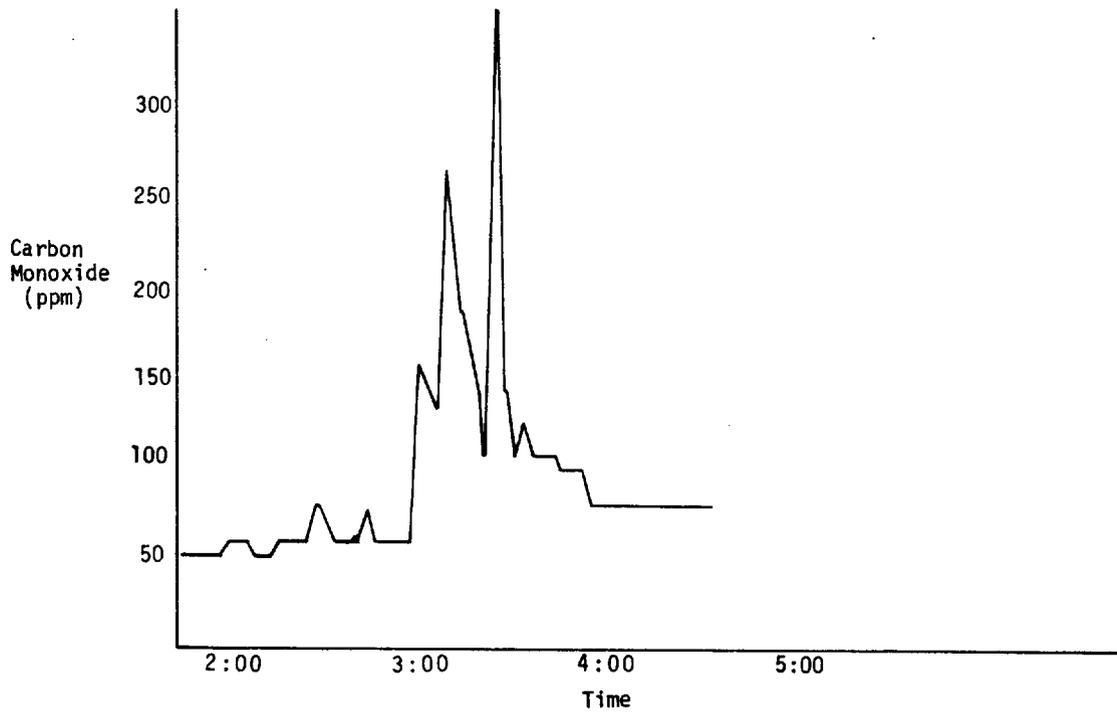


Figure 2

Carbon Monoxide Concentrations, 9/19/79

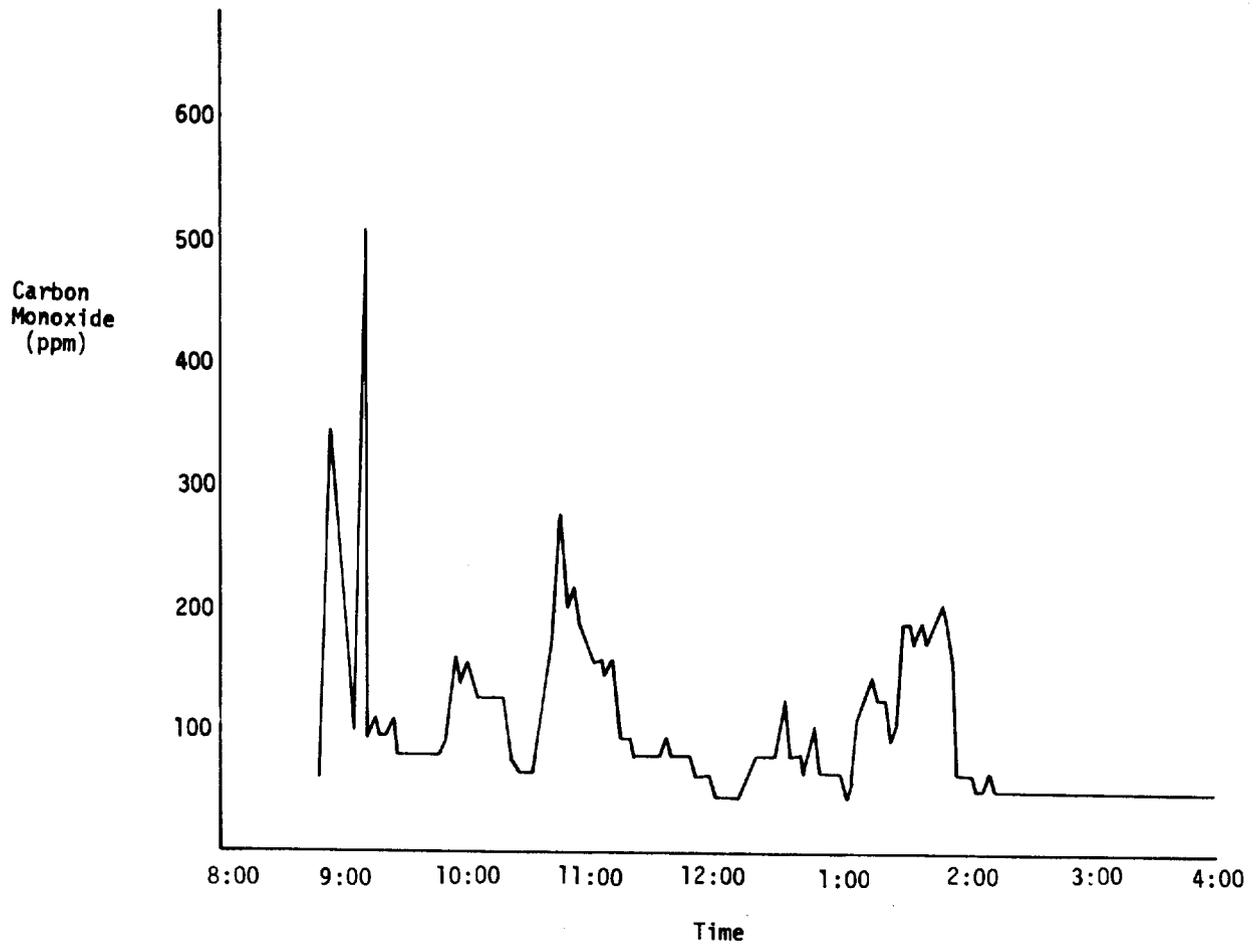


Figure 3  
Carbon Monoxide Concentrations, 9/20/79

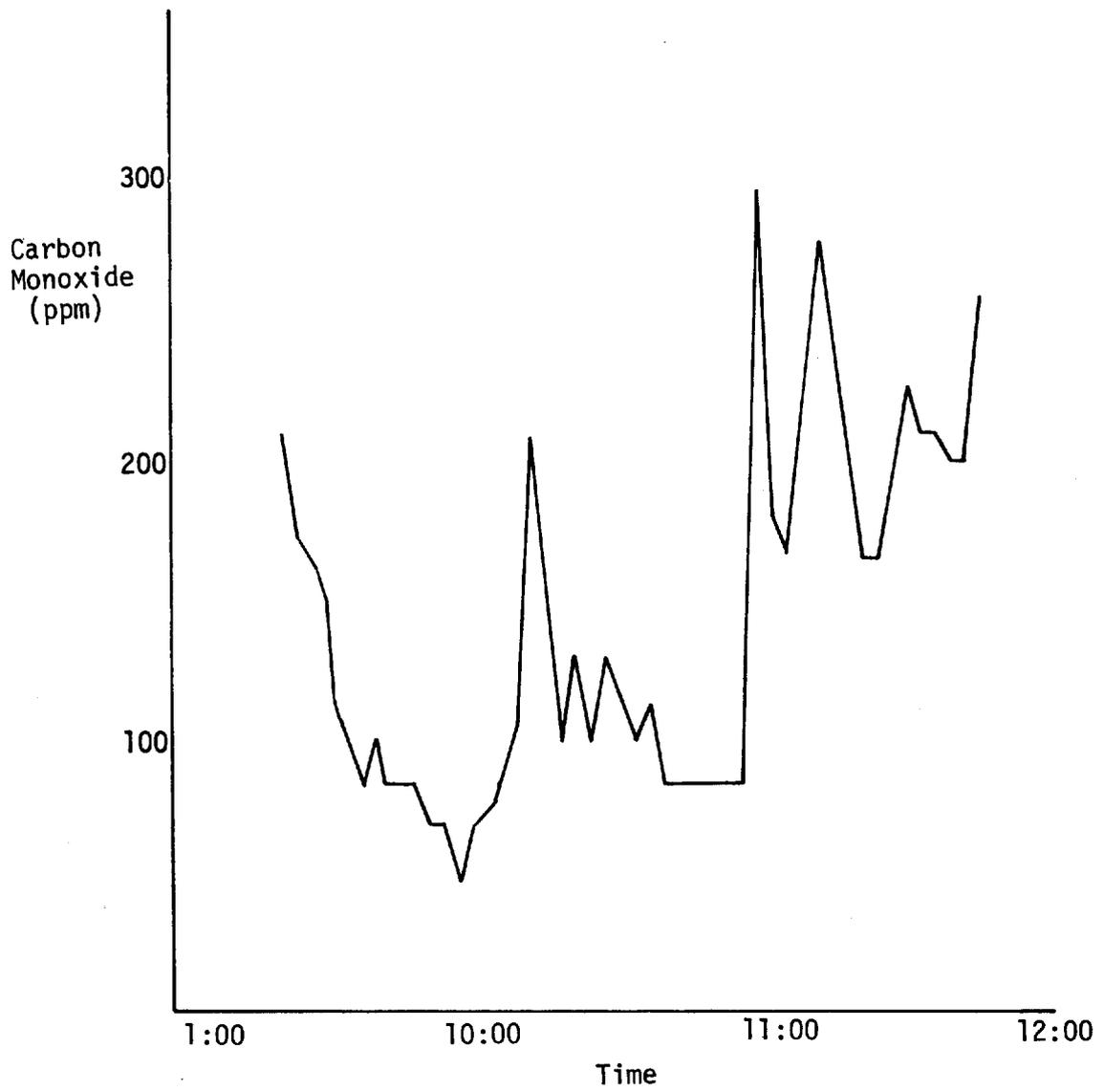


Figure 4  
Carbon Monoxide Concentration, 9/21/79

A TRW crew member certified by the California Air Resources Board to read visible emissions made opacity observations of the coke oven stack during each test. No visible emissions were evident during any of the tests.

### 3. PROCESS DESCRIPTION

Kaiser Steel Corporation operates seven metallurgical coke oven batteries at its steel plant located in Fontana, California. This is the only domestic steel plant which uses fabric filters to control particulate emissions from coke oven battery stacks. Currently, four batteries (B, C, D, and E) are equipped with fabric filter controls. Kaiser plans to install similar controls on the remaining three batteries in the near future (A, F, and G).

Of the four batteries equipped with fabric filter controls, Battery "B" was selected for testing because the duct run configurations to and from the fabric filter were considered more amenable to representative sampling. As discussed previously in Section 2.0 of this report, the emission tests conducted included simultaneous inlet and outlet measurements for mass particulate and benzo-a-pyrene (BaP), continuous carbon monoxide measurements, benzene measurements, and visible emission observations on the battery stack itself. The purpose for these tests was to (a) characterize emissions from battery stacks and (b) assess the performance of a fabric filter on these emissions.

Salient facts on the design and operation of the battery are summarized in Table 3-1. As indicated, the battery is a Koppers-Becker



design and was originally built in 1941. It underwent its most recent rehabilitation, consisting of hot end-flue repairs in 1974. The battery is equipped with double collecting mains and consists of 45 ovens each measuring 4 m (13 ft) in height and capable of coking about 14 tons of coal per charge. During the test period, 12 of the 45 ovens were permanently out of service.

The battery is fired with undesulfurized coke oven gas (COG) using underjet firing. Charging of the ovens is performed by larry car using stage charging techniques. Fuel gas flow was not measurable during the test; however, we were told that the fuel flow rate is generally about 220,000 SCFH. Analysis of the fuel gas and the coal charged to the ovens during the emission tests are included in Appendix D. During the test period, the battery was operated on a 17-hr coking cycle. With 12 ovens out of service, this resulted in a charging frequency of about 1.94 charges per hour.

Normal maintenance practices on the battery include the patching of cracks in the end flues using a hand-held slurry patching gun. Each oven is patched every 30 to 45 days. A complete rebuild of the battery is planned sometime in 1980.

The fabric filter unit used to collect particulate emissions contained in the underfiring exhaust gases was installed in June 1979. The unit is a closed-suction design with reverse air cleaning. It consists of five compartments with a total filtering area of 39,600 sq ft. Each

compartment contains 140 graphite-silicone treated glass fiber bags, each measuring 8 in. in diameter and 22 ft in length. The fabric filter was designed to handle about 88,000 acfm at a net air-to-cloth ratio of 2.76:1 with one compartment isolated for cleaning. The design operating temperature was 450°F. Actual operating conditions are closer to 71,000 acfm at 450°F and the net air-to-cloth ratio nearer 2.23:1. Exhaust gases from the fabric filter are pulled through a 450-hp induced draft fan and are then discharged to the atmosphere through a 225-ft stack.

Each compartment is cleaned automatically at least once every 6 hr for 50 sec or whenever the pressure drop across a compartment exceeds a preset level (about 8.5 in. of water).

It was observed that the total pressure drop across the fabric filter was higher than expected, usually exceeding 8 in. w.c. and that the pressure drop did not decrease by more than 1 in. w.c. after a cleaning cycle. Kaiser engineers were aware of this and were trying to determine the reason for it.

During each of the test periods, the amount of dust captured by the two filters serving Batteries B and C was collected and weighed. Both of these filters are served by one common hopper discharge dust conveyor so it was not possible to separate the dust collected by each filter. Based on the three dust weights most closely associated with each Method 5 test, it was calculated that the dust collection rate was 1.3, 0.2, and < 0.03 kg/hr. These quantities are considerably less

than expected, based on the filter inlet/outlet particulate concentrations. These dust weights may indicate that dust was not being properly discharged from the filter. On the other hand, the weighings were of rather short duration, so the quantities collected may not be representative of longer term operation.

During the periods when the emission testing was conducted, both the battery and fabric filter operations were monitored. The process operating data obtained and observations made are summarized in Appendix D. Tests were conducted only when the battery was operating within normal limits.

## SECTION 4

### LOCATION OF SAMPLING POINTS

- (1) Baghouse inlet - The inlet duct to baghouse "B" is a 5'1" self supported duct connected to an underground duct from the coke ovens. The duct goes up to an elevation of 24 feet above the ground and has a straight run of 128 feet to the baghouse. The sampling location is 63 feet (12.6 diameters) downstream from the nearest bend and 65 feet (13 diameters) upstream from the baghouse. Sampling was done at twelve traverse points. Figures 5 and 6 show this sampling location.
- (2) Baghouse outlet - The duct carrying the treated stack gas from the baghouse to the battery stack is also a 5 feet 1 inch I.D. duct which is 31 feet above the ground at the sampling location. There is a 51 foot (10 diameters) run of straight ducting upstream from the sampling location. The induced draft fan is 44 feet downstream from the sampling location. Samples were taken at twelve traverse points across the duct. Figures 5 and 7 show this sampling location.

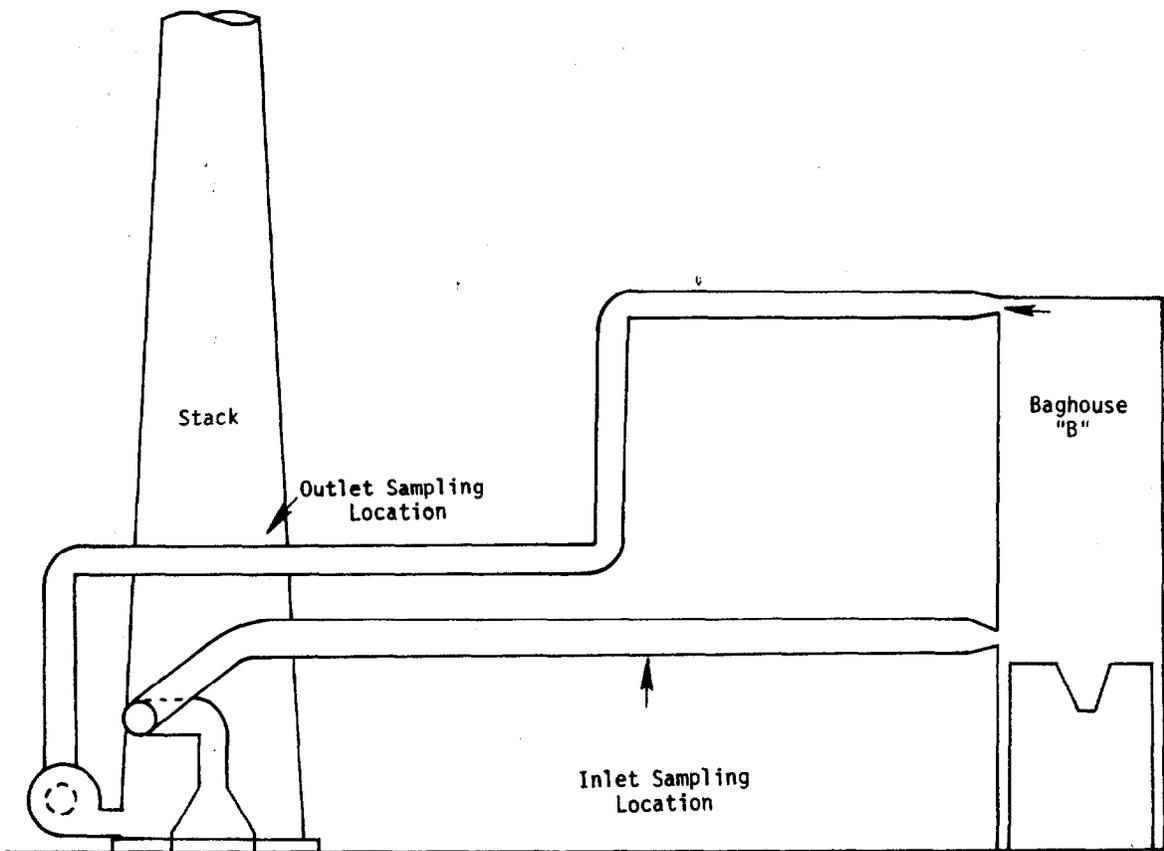
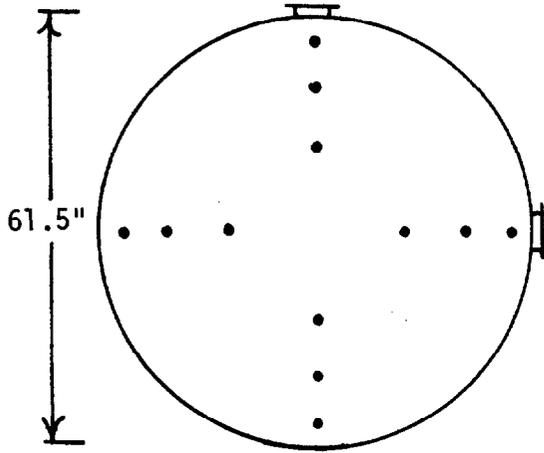


Figure 5 Baghouse "B" Ducting Schematic

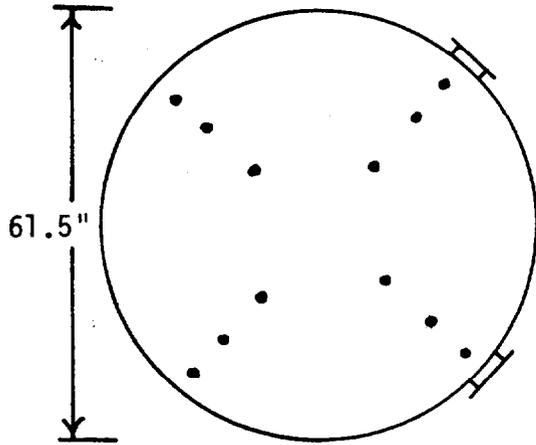
Traverse Point Locations



Traverse Point Number	Percentage of Stack ID	Distance From Inside Wall (inc)
1	4.4	2.71
2	14.6	8.98
3	29.6	18.20
4	70.4	43.30
5	85.4	52.52
6	95.6	58.79

Figure 6 Inlet Sampling Location

Traverse Point Locations



Traverse Point Number	Percentage of Stack I.D.	Distance from Inside Wall (inc)
1	4.4	2.71
2	14.6	8.98
3	29.6	18.98
4	70.4	43.30
5	85.4	52.52
6	95.6	58.79

Figure 7 Outlet Sampling Location

SECTION 5  
SAMPLING AND ANALYSIS PROCEDURES

(A) Particulate Sampling

Particulate sampling was performed according to EPA Method 5 (as revised August 10, 1977). The sampling train varied from the usual Method 5 train in that a flexible teflon line was used between the probe and the filter holder. Figure 8 is a diagram of the sampling train.

The front half of the sampling train consisted of a calibrated nozzle, glass probe liner, flexible teflon line, and heated glass fiber filter. Filterable particulates were collected in the front half of the sampling train.

The back half of the sampling train consisted of four glass impingers in series kept in an ice bath. The first, third and fourth impingers were modified Greenburg-Smith design, with the tip replaced with a  $\frac{1}{2}$  inch I.D. glass tube extending to  $\frac{1}{2}$  inch of the bottom of the flask. The second impinger was the Greenburg-Smith type. The first and second impinger was empty, and the fourth impinger contained 250 grams silica gel. The impingers collected moisture and other gas constituents condensing at 32°F.

Before sampling a velocity traverse was done at each sampling location to determine the average temperature and velocity. A moisture test according to EPA method 4 was done at the inlet to the baghouse before the first test to get an estimate of the stack gas moisture content. These data were used in nozzle size selection and adjustment of nomographs for isokinetic sampling.

After assembling the sampling train it was leak checked at 15 inches of mercury vacuum and sampling was not begun until a leak rate of less than 0.02 cfm was achieved. Leak checks were done before each traverse change, and at the end of each test run at the maximum vacuum encountered during each portion of the test.

Sampling was done at the centers of twelve equal areas within the stack at both the inlet and outlet locations. Inlet and outlet sampling of particulates and BaP (benzo-a-pyrene) were done simultaneously.

Sample Recovery

The sampling nozzle, probe liner, flexible line, and front half of the filter holder were rinsed with acetone and brushed with a nylon probe brush with a polypropylene handle. This acetone rinse was placed in a 250 ml nalgene bottle.

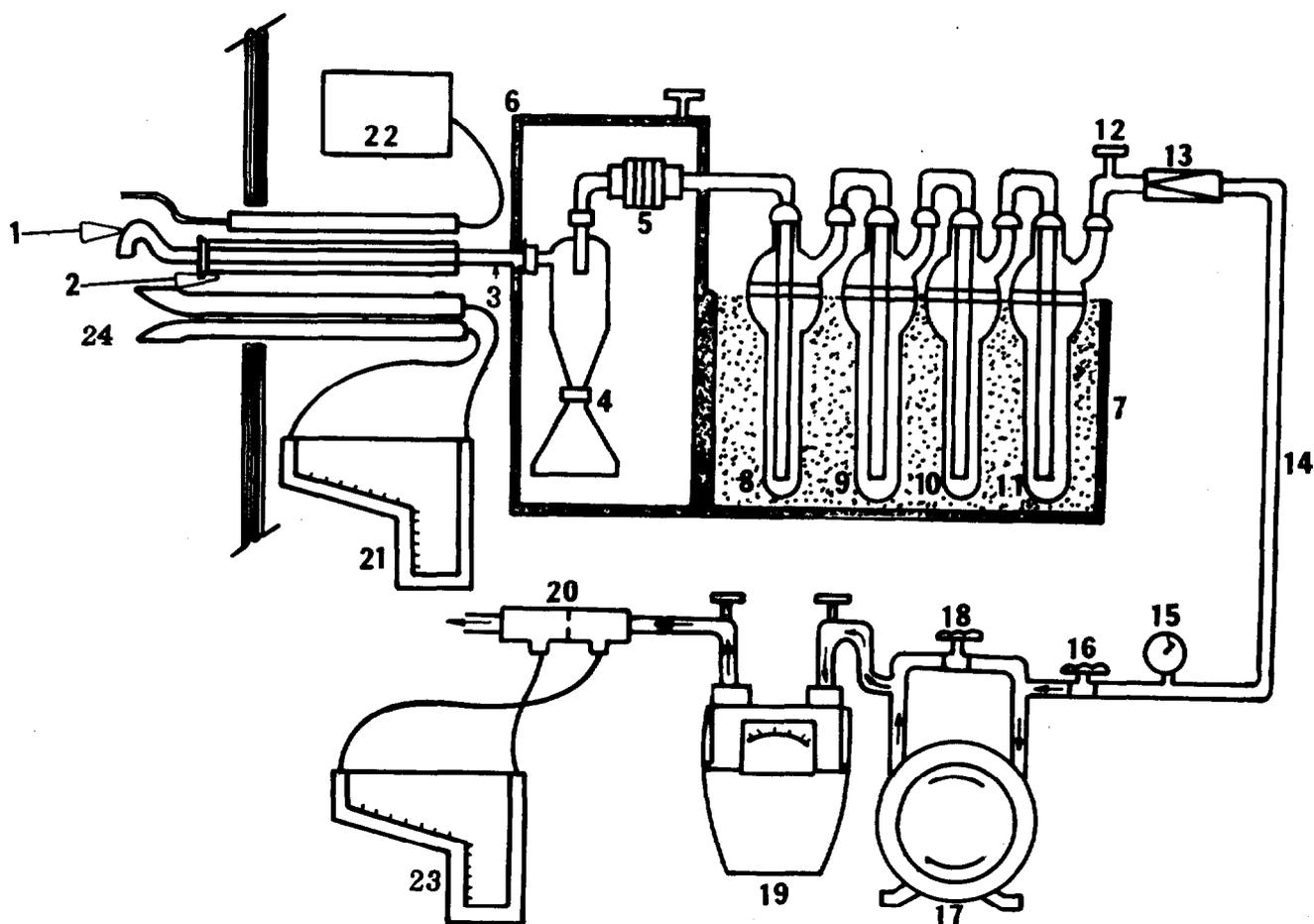


Figure 8. EPA method 5 particulate sampling train

- |                                |                       |
|--------------------------------|-----------------------|
| 1) Calibrated nozzle           | 13) Check valve       |
| 2) Glass lined probe           | 14) Vacuum line       |
| 3) Flexible teflon sample line | 15) Vacuum gauge      |
| 4) Cyclone                     | 16) Main valve        |
| 5) Filter holder               | 17) Air tight pump    |
| 6) Heated box                  | 18) Bypass valve      |
| 7) Ice bath                    | 19) Dry test meter    |
| 8) Impinger (water)            | 20) Orifice           |
| 9) Impinger (water)            | 21) Pitot manometer   |
| 10) Impinger (empty)           | 22) Potentiometer     |
| 11) Impinger (silica gel)      | 23) Orifice manometer |
| 12) Thermometer                | 24) S type pitot tube |

The particulate filter was removed from the filter holder and placed in a sealed polyethylene jar.

The impinger solutions were measured and placed in a glass sample container. The acetone rinse of the impingers, back half of the filter holder, and connecting glassware were placed in a separate glass sample container with a teflon lid liner.

The front half acetone rinses were placed in tared beakers and evaporated. The impinger solutions were placed in tared beakers and dried on a steam bath. The filters and beakers were then placed in a dessicator until they reached a constant weight, and were weighed to within a tenth of a milligram.

After the front half rinses and filters had been weighed to determine the amount of filterable particulate collected, the particulates in the beakers were redissolved with 100 milliliters of 80% isopropanol. The filter for each test was then added to this solution, and macerated to dissolve sulfate collected on it. The resultant solution was then filtered and titrated with standardized barium perchlorate against thornin indicator to determine the amount of sulfate collected.

#### (B) Benzo-a-Pyrene (BaP) Sampling

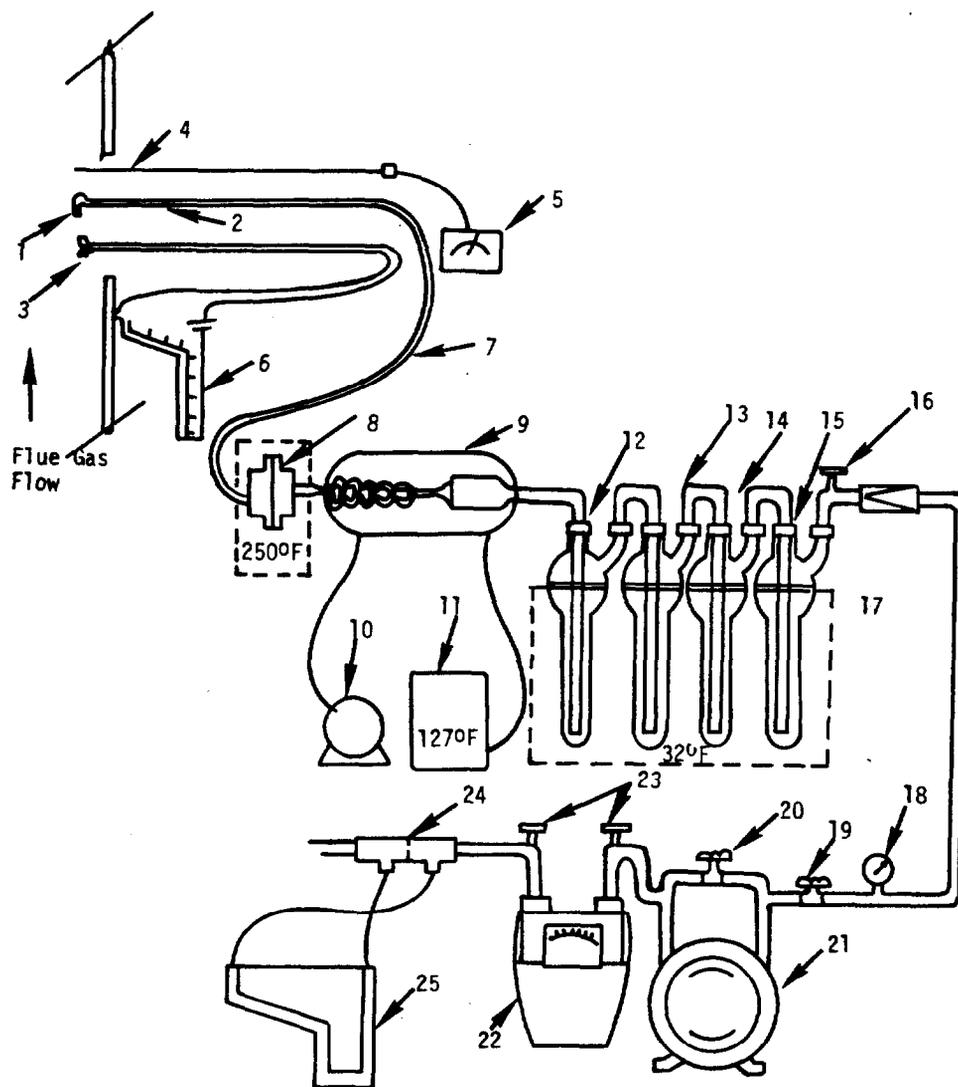
The sampling train used to collect BaP was identical to the train used for particulates except that it contained an adsorbent module between the filter and the first impinger. Figure 9 is a diagram of this sampling train.

A schematic diagram of the BaP adsorbent module is shown in figure 10. The module was packed with XAD-2, (styrene divinyl Benzene) a polymeric adsorbent. The temperature of the water circulating through the cooling jacket was kept at 127°F so that the sampled gas would be cooled to this temperature as it passed through the adsorbent material. The adsorbent module was covered with aluminum foil throughout the testing to prevent deterioration of the sample by exposure to ultraviolet light. Aside from operation of the adsorbent module the BaP train was operated the same as the particulate trains.

Since the BaP adsorbent module is located immediately behind the heated filter, and water cooled to 127°F, some moisture in the stack gas will condense in the module prior to reaching the impingers. Water collected in the impingers and silica gel will not accurately reflect the true moisture content of the stack gas since all the water collected in the BaP train is not accounted for. In operating a BaP train at a source with a high moisture content, either a moisture train or a Method 5 train should be operated during the run for accurate moisture determination. For the purposes of this report, the moisture content determined from the Method 5 train is also used for the BaP train - in data reduction.

#### Sample Extraction

The filter was extracted with 100 milliliters of cyclohexane in a Soxhlet extractor for 7 hours. The probe rinse was agitated in an ultrasonic



- |                               |                                      |                        |
|-------------------------------|--------------------------------------|------------------------|
| 1. Calibrated Nozzle          | 9. Adsorbent Sampler                 | 17. Ice Water Bath     |
| 2. Glass Lined Probe          | 10. Water Pump                       | 18. Vacuum Gauge       |
| 3. S-Type Pitot Tube          | 11. Temperature Controlled Reservoir | 19. Main Valve         |
| 4. Thermocouple               | 12. Modified G-S Impinger-Water      | 20. Bypass Valve       |
| 5. Thermocouple Potentiometer | 13. G-S Impinger-Water               | 21. Vacuum Pump        |
| 6. Pitot Tube Manometer       | 14. Modified G-S Impinger-Empty      | 22. Dry Gas Meter      |
| 7. Teflon Flex Line           | 15. Modified G-S Impinger-Silicagel  | 23. Thermometers       |
| 8. Heated Filter              | 16. Thermometer                      | 24. Calibrated Orifice |
|                               |                                      | 25. Orifice Manometer  |

Figure 9 - BaP Sampling Train

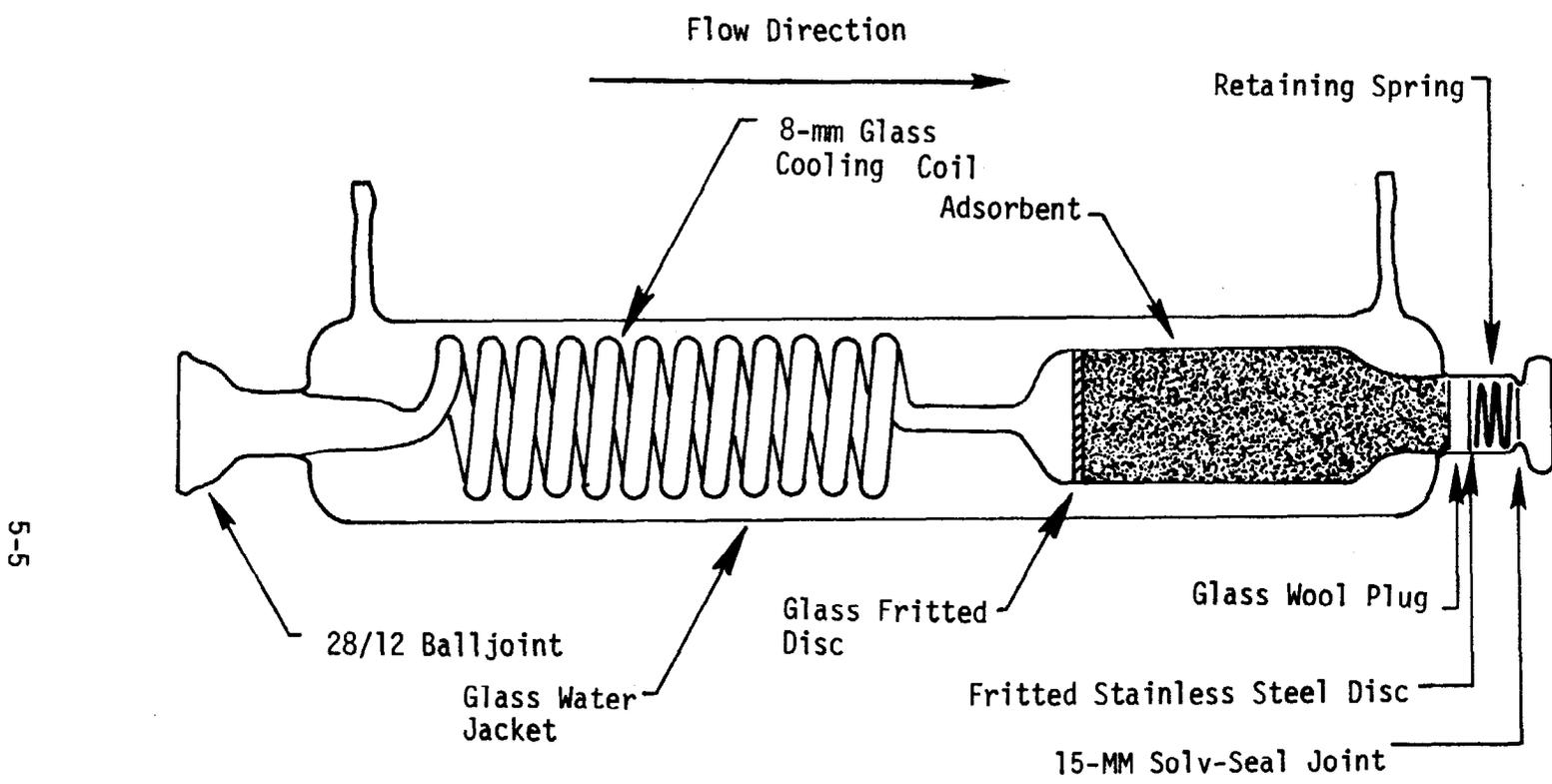


Figure 10 Adsorbent Sampling System

bath for one hour and filtered through a Whatman No. 40 filter. The adsorbent module was extracted with 180 milliliters of cyclohexane for 24 hours in a continuous extraction device. These extraction procedures were done under yellow safe lights and the extract stored in amber glass bottles.

#### BaP Sample Analysis

The sample extract was concentrated in a Kuderna-Danish Concentrator which was heated in a water bath to 50°C. The samples were concentrated to 7 milliliters and brought up to 10 milliliters with washings of the concentrator flask. The concentrated samples were stored in the dark at 1°C until the final analysis step.

Analysis of the BaP samples entailed spotting the concentrate extracts on thin layer chromatography (TLC) plates and reading the fluorescence of the plates with an Aminco 125F spectrofluorometer. The TLC plates were read at an excitation wavelength of 378 nm and an emission wavelength of 403 nm for BaP. Since anthanthrene has an excitation wavelength of 420 nm and an emission wavelength of 430 nm it does not interfere in the analysis. The sample fluorescence was compared with the fluorescence of BaP standard solutions to determine the amount of BaP in the sample.

#### Benzene Sampling

An integrated bag sample of the stack gas was taken during the BaP and particulate test. Figure 11 is a diagram of the integrated-bag sampling train. The contents of the bag were analyzed for benzene with a Shimadzu Mini-1 gas chromatograph equipped with a flame ionization detector, and for fixed gases (O<sub>2</sub>, CO<sub>2</sub>, CO) with a Carle Basic gas chromatograph equipped with a thermal conductivity detector.

#### Benzene Analysis

The sample was injected through a 1 milliliter sample loop into a 6 feet by 1/8 inch stainless steel column containing 5 percent SP 1200 and 1.75 percent Bentone 34 on 100/120 mesh Supelcoport. The column and detector were maintained at 75°C and 225°C, respectively. The peak area was measured with a disc integrator on a Linear Strip chart recorder. Sample values were compared with values obtained from certified standards to calculate sample concentrations.

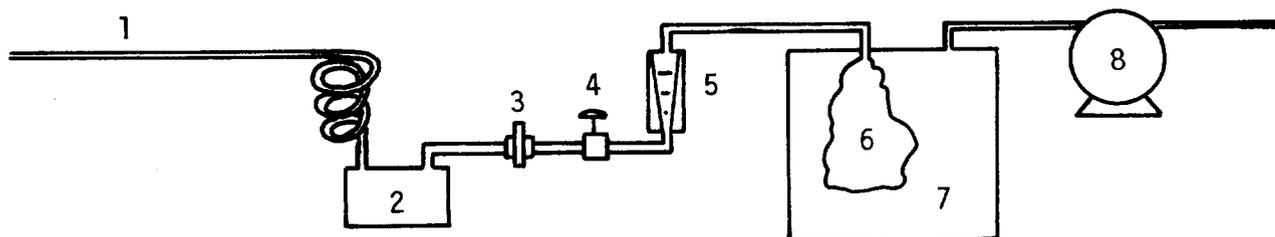
#### Carbon Monoxide Sampling

A sample of the stack gas was extracted continuously from the duct and analyzed for carbon monoxide. The analysis was performed according to EPA method 10, "Determination of Carbon Monoxide Emissions from Stationary Sources". Figure 12 is a schematic diagram of the sampling system used.

#### Carbon Monoxide Analysis

The Continuous analyzer used was an Infrared Industries Model 702-352

nondispersive infrared (NDIR) analyzer with detectors for carbon monoxide and carbon dioxide. The sample gas was drawn through impingers containing ascarite and silica gel to remove carbon dioxide and moisture, respectively, from the sample gas to prevent them from interfering with the carbon monoxide concentration. Quantification of the sample concentration was done by comparison of the response of the analyzer with certified standard gas concentrations.



1) probe

2) air cooled condenser

3) filter

4) needle valve

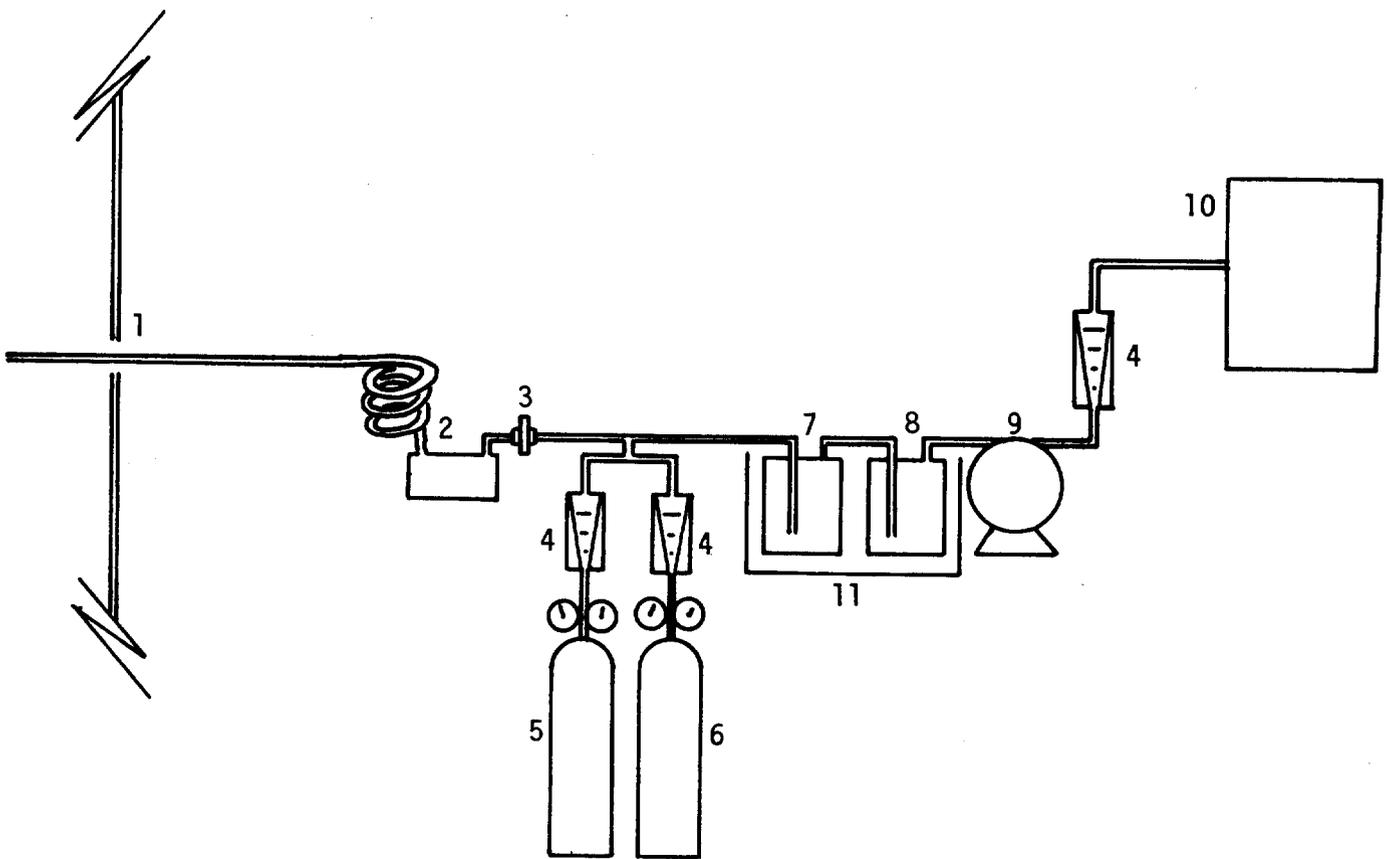
5) flow meter

6) Aluminized Mylar bag

7) Air-tight drum

8) pump

Figure 11 Integrated - Bag Sampling Train



- |                         |               |              |
|-------------------------|---------------|--------------|
| 1) Probe                | 5) Zero gas   | 9) pump      |
| 2) Air-Cooled Condenser | 6) span gas   | 10) NDIR     |
| 3) filter               | 7) Ascarite   | 11) ice bath |
| 4) flow meter           | 8) silica gel |              |

Figure 12 CO Continuous Sampling System

SECTION 6  
APPENDIX A

A. Field and Laboratory Data

1. Traverse Point Location



SECTION 6  
APPENDIX A

2. Field Data Sheets

## Sample Coding System

Test	Sample Code
Particulate - baghouse inlet	KSC-IN-Part-1, KSC-IN-Part-2, KSC-in-Part 3 KSC-IN-Part-4
Particulate - baghouse outlet	KSC-OUT-Part-1, KSC-OUT-Part-2, KSC-OUT-Part-3, KSC-Out-Part-4
BaP - baghouse inlet	KSC-IN-BaP-1, KSC-IN-BaP-2, KSC-In-BaP-3
BaP - baghouse outlet	KSC-OUT-BaP-1, KSC-OUT-BaP-2, KSC-OUT-BaP-3

DR ENT-7  
 TA # A  
 LAST # DM.

FIELD DATA

PLANT KASSER, FONTANA  
 DATE 9-18-79  
 SAMPLING LOCATION INLET  
 SAMPLE TYPE PAPERAL  
 RUN NUMBER 1  
 OPERATOR DESEL  
 AMBIENT TEMPERATURE 10.0  
 BAROMETRIC PRESSURE 29.6 / 29.5  
 STATIC PRESSURE (P<sub>s</sub>) -1.8 / 1.2  
 FILTER NUMBER (s) # 5

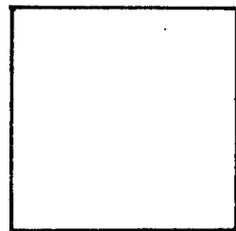
PROBE LENGTH AND TYPE 6'  
 NOZZLE I.D. 1/4"  
 ASSUMED MOISTURE % 6.9%  
 SAMPLE BOX NUMBER 2499  
 METER BOX NUMBER 2499  
 METER ΔH<sub>g</sub>  
 C FACTOR  
 PROBE HEATER SETTING 2.5%  
 HEATER BOX SETTING  
 REFERENCE ΔP .25

SCHMATIC OF TRAVERSE POINT LAYOUT  
 READ AND RECORD ALL DATA EVERY 10 MINUTES

TRAVERSE POINT NUMBER	CLOCK TIME (24-hr CLOCK)	GAS METER READING (V <sub>m</sub> ), ft <sup>3</sup>	VELOCITY HEAD (ΔP <sub>s</sub> ), in. H <sub>2</sub> O	ORIFICE PRESSURE DIFFERENTIAL (ΔH), in. H <sub>2</sub> O		STACK TEMPERATURE (T <sub>s</sub> ), °F	DRY GAS METER TEMPERATURE		PUMP VACUUM, in. Hg	SAMPLE BOX TEMPERATURE, °F	IMPINGER TEMPERATURE, °F
				DESIRED	ACTUAL		INLET (T <sub>m in</sub> ), °F	OUTLET (T <sub>m out</sub> ), °F			
	2:10	382.342									
1	2:10	385.68	1.55	.30	.30	489	110	106	2	250	74
2	2:20	387.90	1.45	.21	.21	435	120	116	2	250	78
3	2:30	390.42	1.45	.21	.21	449	121	108	2	250	77
4	2:40	392.72	1.45	.21	.21	450	124	110	2	250	79
5	2:50	396.42	1.43	.21	.21	453	128	110	2	250	81
6	3:00	402.32	1.45	1.4	1.4	451	134	112	5	250	70
		058.72									
1	4:10		0.58	1.4	1.4	478	110	104	3.5	250	76
2	4:20	066.92	0.58	1.4	1.4	474	120	106	3.5	250	80
3	4:30	074.11	0.65	1.6	1.6	470	124	110	4	250	
		082.15									
1	9:27	082.56									
5	9:40	092.35	0.57	1.4	1.4	535	110	82	7	250	60
6	9:50	102.41	0.52	1.3	1.3	537	120	98	7	250	70
	9:57	112.45	0.40	0.97	0.97	539	128	104	9	250	74
		73.298	0.562	0.88	0.88	482		112			

POINTS 1-5; MONOMETER VALVE # 2 WAS NOT OPEN ALL THE DAY  
 11. STOPPED DUE TO LACK OF FLOW AT POINT 3; 9/18 START OF 9/19

PLANT Kaiser Steel  
 LOCATION outlet  
 OPERATOR Ronell  
 DATE 9/19/79  
 SAMPLE TYPE SAP  
 RUN NO. two  
 SAMPLE BOX NO. \_\_\_\_\_  
 METER BOX NO. \_\_\_\_\_  
 METER  $\Delta H_0$  1.85  
 CORRECTION FACTOR \_\_\_\_\_  
 PITOT TUBE COEFFICIENT,  $C_p$  0.84  
 SAMPLE TYPE \_\_\_\_\_



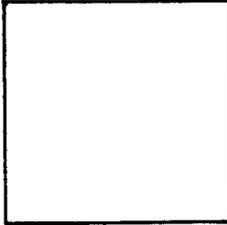
SCHEMATIC OF STACK CROSS SECTION

AMBIENT TEMPERATURE 100  
 BAROMETRIC PRESSURE 28.57  
 ASSUMED MOISTURE, % 8.90  
 PROBE LENGTH, m (FT) 6'  
 NOZZLE IDENTIFICATION NO. 0.25  
 AVERAGE CALIBRATED NOZZLE DIAMETER, CM (IN) 0.25  
 PROBE HEATER SETTING \_\_\_\_\_  
 LEAK RATE, m<sup>3</sup>/MIN. (CFM) \_\_\_\_\_  
 PROBE LINER MATERIAL glass  
 STATIC PRESSURE, mm Hg (IN. Hg) -8.3 in. Hg  
 FILTER NO. # 7

TRAVERSE POINT NUMBER	SAMPLING TIME (O)		VACUUM mm Hg (IN. Hg)	STACK TEMPERATURE (T <sub>s</sub> ) °C (°F)	VELOCITY HEAD ( $\Delta P_s$ ), mm (IN.) H <sub>2</sub> O	PRESSURE DIFFERENTIAL ACROSS ORIFICE METER (IN. H <sub>2</sub> O)	GAS SAMPLE VOLUME m <sup>3</sup> (ft <sup>3</sup> )	GAS SAMPLE TEMPERATURE AT DRY GAS METER		FILTER HOLDER TEMPERATURE °C (°F)	TEMPERATURE OF GAS LEAVING CONDENSER OR LAST IMPINGER	
	MIN.	CLOCK						INLET °C (°F)	OUTLET °C (°F)			
1	1:40		11	440	0.5	1.21	179.533	100	100	250	75	
2	1:50		15	445	0.6	1.45	186.0	118	102	250	75	
3	2:00		17	445	0.62	1.50	194.0	118	102	250	75	
4	2:10		16.5	440	0.57	1.4	199.5	120	105	250	75	
5	2:20		17.0	440	0.62	1.5	206.9	119	105	250	75	
6	2:30		16.0	440	0.55	1.33	213.8	120	106	250	75	
	2:40	leak check & change ports					220.10					
						220.330						
1	3:30		7.0	440	.53	1.28	226.8	100	100	250	75	
2	3:40		9.0	440	.68	1.64	233.94	112	100	250	75	
3	3:50		8.0	445	.59	1.40	240.75	115	102	250	75	
4	4:00		8.0	440	.58	1.40	247.5	115	102	250	75	
5	4:10		8.5	440	0.60	1.45	255.0	115	102	250	75	
6	4:20		6.0	440	0.4	0.97	260.355	115	103	250	75	
	4:30											
TOTAL												
AVERAGE				441	0.568	1.38	30.822	101				

COMMENTS  
 posttest leak check < 0.01 cfm @ 10 in. Hg  
 leak check at port change < 0.02 cfm @ 21 in. Hg.  
 Post test leak check < 0.01 cfm @ 10 in. Hg

PLANT Kaiser Steel  
 LOCATION Outlet  
 OPERATOR Mangum  
 DATE 9/19/79  
 SAMPLE TYPE Particulate  
 RUN NO. Tower (2)  
 SAMPLE BOX NO. \_\_\_\_\_  
 METER BOX NO. \_\_\_\_\_  
 METER  $\Delta Hg$  1.84  
 C FACTOR \_\_\_\_\_  
 PITOT TUBE COEFFICIENT,  $C_p$  0.89  
 SAMPLE TYPE \_\_\_\_\_



SCHEMATIC OF STACK CROSS SECTION

AMBIENT TEMPERATURE 100°F  
 BAROMETRIC PRESSURE 29.57  
 ASSUMED MOISTURE, % 3  
 PROBE LENGTH, m (FT) 6' glass  
 NOZZLE IDENTIFICATION NO. \_\_\_\_\_  
 AVERAGE CALIBRATED NOZZLE DIAMETER, cm (IN) 0.25  
 PROBE HEATER SETTING \_\_\_\_\_  
 LEAK RATE, m<sup>3</sup>/MIN. (CFM) \_\_\_\_\_  
 PROBE LINER MATERIAL glass  
 STATIC PRESSURE, mm Hg (IN. Hg) -3.3 in H<sub>2</sub>O  
 FILTER NO. 8

TRAVERSE POINT NUMBER	SAMPLING TIME (O) CLOCK		VACUUM mm Hg (IN. Hg)	STACK TEMPERATURE (T <sub>g</sub> ) °C (°F)	VELOCITY HEAD ( $\Delta P_s$ ), mm (IN.) H <sub>2</sub> O	PRESSURE DIFFERENTIAL ACROSS ORIFICE METER (IN. H <sub>2</sub> O)	GAS SAMPLE VOLUME m <sup>3</sup> (ft <sup>3</sup> )	GAS SAMPLE TEMPERATURE AT DRY GAS METER		FILTER HOLDER TEMPERATURE °C (°F)	TEMPERATURE OF GAS LEAVING CONDENSER OR LAST IMPINGER
	MIN.	SEC.						INLET °C (°F)	OUTLET °C (°F)		
1	10	1350	4	450	.66	1.6	471.688	100	100		80
2	20	1400	4	445	.69	1.66	478.67	112	103		80
3	30	1410	4	450	.63	1.52	486.35	114	105		80
4	40	1420	4	450	.63	1.52	492.61	116	105		80
5	50	1430	4	445	.63	1.52	499.81	115	107		81
6	60	1440	3	440	.42	1.04	506.55	117	107		81
					Leak check		512.682				
	0	1530					513.007				
1	10	1540	3.5	440	.42	1.02	513.007	100	100		80
2	20	1550	4	440	.63	1.52	518.54	109	101		80
3	30	1600	4	440	.69	1.66	525.12	113	103		79
4	40	1610	4	440	.58	1.5	532.15	113	105		79
5	50	1620	4	440	.58	1.4	539.28	112	105		79
6	60	1630	4	440	.46	1.11	545.85	114	106		79
							552.855				
TOTAL											
AVERAGE	120			443.33	.585	1.423	80.842	107.58			

COMMENTS  
 Pre: Leak Test: .004 cfm Post Leak Test:  
 Leak check at port change < 0.01 @ 5 in Hg.

FIELD DATA

PLANT Kaiser Fontana  
 DATE 9/19/78  
 SAMPLING LOCATION INLET  
 SAMPLE TYPE BAP  
 RUN NUMBER 2  
 OPERATOR Dessa  
 AMBIENT TEMPERATURE 11.0  
 BAROMETRIC PRESSURE 29.50  
 STATIC PRESSURE (P<sub>s</sub>) -1.8440  
 FILTER NUMBER (s) # 6

PROBE LENGTH AND TYPE 6'  
 NOZZLE I.D. 1/4"  
 ASSUMED MOISTURE % 8.70  
 SAMPLE BOX NUMBER 2499  
 METER BOX NUMBER 2499  
 METER AH 0  
 C FACTOR 0  
 PROBE HEATER SETTING 250  
 HEATER BOX SETTING 250  
 REFERENCE Δp 0.83

Schematic of Traverse Point Layout  
 READ AND RECORD ALL DATA EVERY 10 MINUTES

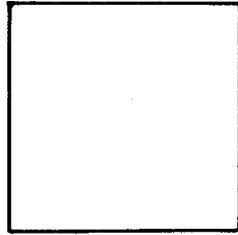
TRAVERSE POINT NUMBER	CLOCK TIME (24-hr CLOCK)	GAS METER READING (V <sub>m</sub> ) ft <sup>3</sup>	VELOCITY HEAD (ΔP <sub>s</sub> ) in. H <sub>2</sub> O	ORIFICE DIFFERENTIAL (ΔH) in. H <sub>2</sub> O		STACK TEMPERATURE (T <sub>s</sub> ) °F	DRY GAS METER TEMPERATURE		PUMP VACUUM in. Hg	SAMPLE BOX TEMPERATURE °F	IMPINGER TEMPERATURE °F
				DESIRED	ACTUAL		INLET (T <sub>m in</sub> ) °F	OUTLET (T <sub>m out</sub> ) °F			
	SEC	120115									
1	10	126.77	.55	1.2	1.2	537	108	106	12	250	80
2	20	133.80	.65	1.4	1.4	541	124	106	15		86
3	30	140.46	.70	1.6	1.6	534	130	108	17		82
4	40	147.51	.58	1.3	1.3	536	130	110	13		88
5	50	151.93	.50	1.1	1.1	539	134	112	10		86
6	60	157.45	.35	.78	.78	533	126	112	7		86
	00	498.152									
1	10	503.52	.35	.78	.78	535	104	104	7	250	98
2	20	509.70	.48	1.1	1.1		126	104	11		67
3	30	516.35	.60	1.4	1.4		136	108	17		70
4	40	523.00	.62	1.4	1.4		138	110	24		72
5	50	529.75	.602	1.4	1.4		136	110	23		72
6	60	536.55	.58	1.3	1.3		138	112	23		71
	120	75.733	.540	1.3	1.3	535.8					

COMMENTS: • STOPPED MOMENTARILY DUE TO POWER FAILURE AT POINT 3  
 • STOPPED " " " " " " POINT 5  
 • STOPPED " " " " " " POINT 6

EPA (80) 235 477



PLANT Kaiser Steel  
 LOCATION outlet  
 OPERATOR Powell  
 DATE 9/18/79  
 SAMPLE TYPE BAP  
 RUN NO. one  
 SAMPLE BOX NO. \_\_\_\_\_  
 METER BOX NO. \_\_\_\_\_  
 METER  $\Delta$ Hg 1.84  
 C FACTOR \_\_\_\_\_  
 PITCT TUBE COEFFICIENT,  $C_p$  0.84  
 SAMPLE TYPE \_\_\_\_\_



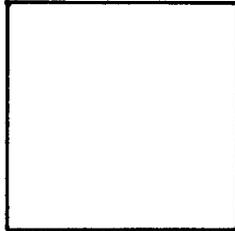
SCHEMATIC OF STACK CROSS SECTION

AMBIENT TEMPERATURE 85  
 BAROMETRIC PRESSURE 29.57  
 ASSUMED MOISTURE, % 6.0  
 PROBE LENGTH, m (FT) 5' glass  
 NOZZLE IDENTIFICATION NO. 075  
 AVERAGE CALIBRATED NOZZLE DIAMETER, CM (IN) 0.25  
 PROBE HEATER SETTING \_\_\_\_\_  
 LEAK RATE, m<sup>3</sup>/MIN. (CFM) <0.01  
 PROBE LINER MATERIAL glass  
 STATIC PRESSURE, mm Hg (IN. Hg) -8.3 in. H<sub>2</sub>O  
 FILTER NO. 4

TRAVERSE POINT NUMBER	SAMPLING TIME (O)		VACUUM mm Hg (IN. Hg)	STACK TEMPERATURE (T <sub>s</sub> ) °C (°F)	VELOCITY HEAD (ΔP <sub>v</sub> ) mm (IN.) H <sub>2</sub> O	PRESSURE DIFFERENTIAL ACROSS ORIFICE METER (IN. H <sub>2</sub> O)	GAS SAMPLE VOLUME m <sup>3</sup> (ft <sup>3</sup> )	GAS SAMPLE TEMPERATURE AT DRY GAS METER		FILTER HOLDER TEMPERATURE °C (°F)	TEMPERATURE OF GAS LEAVING CONDENSER OR LAST IMPINGER
	MIN.	CLOCK						INLET °C (°F)	OUTLET °C (°F)		
1	2:07		4.5	440	0.53	1.30	91.652	102	100	250	70
2	2:09		4.5	440	0.6	1.43	98.218 100.3	112	100	250	70
3	2:27-2:26			power went off			105.05				
3 #	2:27-2:28		5.0	440	0.6	1.43	106.9	116	102	250	70
4 #	2:38		4.8	425	0.57	1.37	114.0	120	106	250	75
5 #	2:48		5.2	440	0.65	1.6	121.2	120	105	250	75
6	2:58		5.0	440	0.6	1.43	128.0	120	107	250	75
	3:08						135.233				
	4:07			leak check			137.857				
1	4:17		6.5	450	0.65	1.6	146.2	110	104	250	75
2	4:27		5.5	445	0.53	1.28	151.353	120	105	250	75
	stopped for night										
3	9:25		4.5	425	0.43	1.06	157.9	90	86	250	75
4	9:35		6.0	445	0.63	1.54	164.8	108	90	250	75
5	9:45		6.0	445	0.59	1.44	171.3	122	95	250	75
TOTAL 6	9:55		6.0	445	0.56	1.39	177.863	126	100	25	75
AVERAGE	10:05			440	0.577	1.41	74.678	107			

COMMENTS pretest leak check <0.01 @ 20 in. Hg.  
power off one minute 2:36-2:38  
leak check at port change <0.02 cfm @ 7 in Hg.  
post test leak check <0.01 cfm @ 8 in. Hg.

PLANT Kaiser Steel  
 LOCATION Outlet  
 OPERATOR H. Morgan  
 DATE 9/18/99  
 SAMPLE TYPE Particulate  
 RUN NO. One  
 SAMPLE BOX NO. \_\_\_\_\_  
 METER BOX NO. \_\_\_\_\_  
 METER  $\Delta H$  1.8  
 C FACTOR \_\_\_\_\_  
 PITOT TUBE COEFFICIENT,  $C_p$  \_\_\_\_\_  
 SAMPLE TYPE \_\_\_\_\_



SCHEMATIC OF STACK CROSS SECTION

AMBIENT TEMPERATURE 85  
 BAROMETRIC PRESSURE 29.57  
 ASSUMED MOISTURE, % 6.0  
 PROBE LENGTH, m (FT) 5' glass  
 NOZZLE IDENTIFICATION NO. \_\_\_\_\_  
 AVERAGE CALIBRATED NOZZLE DIAMETER, CM (IN) 0.25  
 PROBE HEATER SETTING \_\_\_\_\_  
 LEAK RATE, m<sup>3</sup>/MIN. (CFM) <0.02  
 PROBE LINER MATERIAL glass  
 STATIC PRESSURE, mm Hg (IN. Hg) 0 - 8.3 in H<sub>2</sub>O  
 FILTER NO. #1

TRAVERSE POINT NUMBER	SAMPLING TIME (01-108)		VACUUM mm Hg (IN. Hg)	STACK TEMPERATURE (T <sub>s</sub> ) °C (°F)	VELOCITY HEAD (ΔP <sub>s</sub> ) mm (IN.) H <sub>2</sub> O	1.2 PRESSURE DIFFERENTIAL ACROSS ORIFICE METER (IN. H <sub>2</sub> O)	GAS SAMPLE VOLUME m <sup>3</sup> (ft <sup>3</sup> )	GAS SAMPLE TEMPERATURE AT DRY GAS METER		FILTER HOLDER TEMPERATURE °C (°F)	TEMPERATURE OF GAS LEAVING CONDENSER OR LAST IMPINGER
	MIN	CLOCK						INLET °C (°F)	OUTLET °C (°F)		
1	10	14:03	7	440	.49	1.2	392.858	101	101		80
2	20	14:28	7	440	.52	1.2	396.87	108	101		82
3	30	14:55	Power off 2 min. 14:26-14:28 6.5	440	.6	1.43	Power off 2 min. 407.14	118	105		82
4	40	14:55	5	440	.62	1.40	413.37	118	108		82
5	50	14:55	5	440	.65	1.60	422.53	118	108		82
6	60	15:11	5	440	.66	1.60	431.95	118	108		85
	0	4:07					431.547				
1	10	4:07	8	440	.52	1.2	431.547	107	103		85
2	20	4:27	4	440	.5	1.23	438.19	107	103		80
3	30	stopped for night					444.04				
3	30	9:35	4	440	.57	1.06	444.712	90	90		80
4	40	9:45	4	445	.68	1.5	450.99	105	93		80
5	50	9:55	4	450	.67	1.63	457.38	104	98		80
6	60	10:05	4	445	.67	1.49	464.35	120	104		80
							476.346				
TOTAL											
AVERAGE				442	.594	1.38	78.391	105			

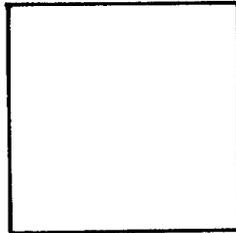
COMMENTS  
 pretest leak check <0.02 cfm @ 15 in Hg  
 post change leak check <0.01 @ 15 in Hg  
 post test leak check <0.02 cfm @ 10 in Hg.







PLANT Kaiser Steel  
 LOCATION outlet  
 OPERATOR M. Mangum  
 DATE 9/20/79  
 SAMPLE TYPE particulate  
 RUN NO. 3  
 SAMPLE BOX NO. \_\_\_\_\_  
 METER BOX NO. \_\_\_\_\_  
 METER  $\Delta H$  1.84  
 C FACTOR 8  
 PITOT TUBE COEFFICIENT,  $C_p$  0.84  
 SAMPLE TYPE \_\_\_\_\_



SCHEMATIC OF STACK CROSS SECTION

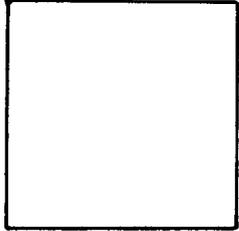
AMBIENT TEMPERATURE 80  
 BAROMETRIC PRESSURE 28.73  
 ASSUMED MOISTURE, % 8  
 PROBE LENGTH, m (FT) 6'  
 NOZZLE IDENTIFICATION NO. \_\_\_\_\_  
 AVERAGE CALIBRATED NOZZLE DIAMETER, CM (IN) 0.25  
 PROBE HEATER SETTING \_\_\_\_\_  
 LEAK RATE, m<sup>3</sup>/MIN. (CFM) \_\_\_\_\_  
 PROBE LINER MATERIAL glass  
 STATIC PRESSURE, mm Hg (IN. Hg) -8.3 in H<sub>2</sub>O  
 FILTER NO. 12

TRAVERSE POINT NUMBER	SAMPLING TIME (CLOCK) MIN. 0	VACUUM mm Hg (IN. Hg)	STACK TEMPERATURE (T <sub>s</sub> ) °C (°F)	VELOCITY HEAD (ΔP <sub>s</sub> ) mm (IN.) H <sub>2</sub> O	PRESSURE DIFFERENTIAL ACROSS ORIFICE METER (IN. H <sub>2</sub> O)	GAS SAMPLE VOLUME m <sup>3</sup> (ft <sup>3</sup> )	GAS SAMPLE TEMPERATURE AT DRY GAS METER		FILTER HOLDER TEMPERATURE °C (°F)	TEMPERATURE OF GAS LEAVING CONDENSER OR LAST IMPINGER
							INLET °C (°F)	OUTLET °C (°F)		
1	10 11:37	6	445	.45	1.07	558.352	95	94		80
2	20 11:59	8	445	.63	1.43	564.96	106	96		80
3	30 12:09	8	450	.66	1.5	571.12	111	99		80
4	12:19	7	440	.53	1.23	578.49	117	101		80
5	12:29	4	440	.61	1.41	585.33	115	103		80
6	12:39	3	440	.54	1.25	592.11	112	104		80
						597.931				
	13:24				Leak Check	598.901				
1	10 13:37	4	440	.59	1.37	598.901	97	96		80
2	20 13:44	4	440	.61	1.41	603.86	106	98		80
3	30 13:54	4.5	440	.65	1.5	610.52	110	100		80
4	40 14:04	4.3	440	.58	1.34	617.74	112	102		80
5	50 14:14	4.5	445	.57	1.34	622.92	112	103		80
6	60 14:24	4.5	445	.63	1.43	630.09	113	104		80
						637.081				
TOTAL	120									
AVERAGE			442.5	.587	1.356	77.765	104.4			

COMMENTS

pretest leak check <0.01 cfm @ 15 in Hg.  
 midtest leak check <0.01 cfm @ 15 in Hg.  
 post test leak check <0.01 cfm @ 10" Hg

PLANT Kaiser Steel  
 LOCATION outlet from BH'B"  
 OPERATOR Powell  
 DATE 9/21/79  
 SAMPLE TYPE particulate  
 RUN NO. 4  
 SAMPLE BOX NO. \_\_\_\_\_  
 METER BOX NO. \_\_\_\_\_  
 METER  $\Delta Hg$  1.84  
 CORRECTION FACTOR \_\_\_\_\_  
 PIVOT TUBE COEFFICIENT,  $C_p$  0.94  
 SAMPLE TYPE \_\_\_\_\_



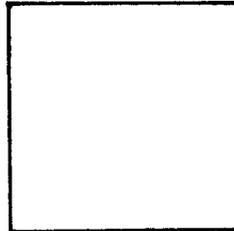
SCHEMATIC OF STACK CROSS SECTION

AMBIENT TEMPERATURE 80  
 BAROMETRIC PRESSURE \_\_\_\_\_  
 ASSUMED MOISTURE, % 8  
 PROBE LENGTH, m (FT) 6'  
 NOZZLE IDENTIFICATION NO. \_\_\_\_\_  
 AVERAGE CALIBRATED NOZZLE DIAMETER, CM (IN) 0.25  
 PROBE HEATER SETTING \_\_\_\_\_  
 LEAK RATE, m<sup>3</sup>/MIN. (CFM) \_\_\_\_\_  
 PROBE LINER MATERIAL glass  
 STATIC PRESSURE, mm Hg (IN. Hg) -8.3 in Hg  
 FILTER NO. 11

TRAVERSE POINT NUMBER	SAMPLING TIME (O)		VACUUM mm Hg (IN. Hg)	STACK TEMPERATURE (T <sub>s</sub> ) °C (°F)	VELOCITY HEAD (ΔP <sub>s</sub> ) mm (IN.) H <sub>2</sub> O	PRESSURE DIFFERENTIAL ACROSS ORIFICE METER (IN. H <sub>2</sub> O)	GAS SAMPLE VOLUME m <sup>3</sup> (ft <sup>3</sup> )	GAS SAMPLE TEMPERATURE AT DRY GAS METER		FILTER HOLDER TEMPERATURE °C (°F)	TEMPERATURE OF GAS LEAVING CONDENSER OR LAST IMPINGER
	MIN.	CLOCK						INLET °C (°F)	OUTLET °C (°F)		
1	9:38		5.0	440	0.50	1.1	638.973	85	85	250	75
2	9:48		5.0	435	0.53	1.17	644.7	98	86	250	70
3	9:58		7.2	445	0.63	1.4	650.5	106	90	250	70
4	10:08		9.0	440	0.70	1.61	656.8	112	98	250	70
5	10:18		8.0	440	0.62	1.42	664.3	120	100	250	70
6	10:28		7.0	440	0.53	1.17	670.9	120	106	250	70
	10:38						676.382				
1	11:00		9.0	450	0.48	1.1	676.618	106	100	250	70
2	11:10		6.0	450	0.50	1.1	683.50	110	100	250	75
3	11:20		7.0	447	0.58	1.33	689.0	112	100	250	75
4	11:30		7.0	445	.53	1.17	696.5	113	101	250	75
5	11:40		7.0	450	0.60	1.35	701.3	112	102	250	75
6	11:50		7.0	450	0.53	1.17	709.3	115	104	250	75
	12:00						714.282				
TOTAL											
AVERAGE	120			444.3	0.561	1.258	75.073		103.375		

COMMENTS  
 pretest leak check < 0.01 cfm @ 10" Hg  
 mid test leak check < 0.02 cfm @ 10" Hg  
 initial leak check < 0.02 cfm @ 12" Hg

PLANT Kaiser Steel  
 LOCATION outlet  
 OPERATOR Amuel  
 DATE 9/20/79  
 SAMPLE TYPE BAP  
 RUN NO. 3  
 SAMPLE BOX NO. \_\_\_\_\_  
 METER BOX NO. \_\_\_\_\_  
 METER  $\Delta H$  1.84  
 C FACTOR \_\_\_\_\_  
 PITOT TUBE COEFFICIENT,  $C_p$  0.84  
 SAMPLE TYPE \_\_\_\_\_



SCHEMATIC OF STACK CROSS SECTION

AMBIENT TEMPERATURE 85  
 BAROMETRIC PRESSURE 28.73  
 ASSUMED MOISTURE, % 8  
 PROBE LENGTH, m (FT) 6'  
 NOZZLE IDENTIFICATION NO. \_\_\_\_\_  
 AVERAGE CALIBRATED NOZZLE DIAMETER, CM (IN) 0.25  
 PROBE HEATER SETTING \_\_\_\_\_  
 LEAK RATE, m<sup>3</sup>/MIN. (CFM) \_\_\_\_\_  
 PROBE LINER MATERIAL glass  
 STATIC PRESSURE, mm Hg (IN. Hg) -8.3 in Hg  
 FILTER NO. 10

TRAVERSE POINT NUMBER	SAMPLING TIME (O)		VACUUM mm Hg (IN. Hg)	STACK TEMPERATURE (T <sub>s</sub> ) °C (°F)	VELOCITY HEAD (ΔP <sub>s</sub> ), mm (IN.) H <sub>2</sub> O	PRESSURE DIFFERENTIAL ACROSS ORIFICE METER (IN. H <sub>2</sub> O)	GAS SAMPLE VOLUME m <sup>3</sup> (ft <sup>3</sup> )	GAS SAMPLE TEMPERATURE AT DRY GAS METER		FILTER HOLDER TEMPERATURE °C (°F)	TEMPERATURE OF GAS LEAVING CONDENSER OR LAST IMPINGER
	MIN.	CLOCK						INLET °C (°F)	OUTLET °C (°F)		
1	11:39		11.0	445	.60	1.42	<del>266.987</del>	92	91	250	69
2	11:49		11.5	445	.66	1.50	274.3	109	92	250	70
3	11:59		12.5	450	.70	1.6	281.1	112	96	250	72
4	12:09		12.3	440	.66	1.5	288.7	118	99	250	72
5	12:19		11.0	450	.6	1.42	295.6	120	102	250	75
6	12:29		8.0	440	.40	.93	302.0	119	102	250	75
	12:39						308.028				
						leak check	308.138	<del>95</del>	<del>95</del>	<del>250</del>	<del>75</del>
1	1:24		8.0	440	.45	1.04	313.5	95	95	250	75
2	1:34		8.5	440	.45	1.04	320.4	108	96	250	75
3	1:44		9.5	440	.57	1.34	327.0	112	100	250	75
4	1:54		12.5	445	.70	1.61	333.0	116	102	250	75
5	2:04		10.5	445	.60	1.42	341.8	116	102	250	75
6	2:14		8.5	440	.5	1.15	345.918	115	102	250	75
	2:24										
TOTAL											
AVERAGE	120			443.6	.574	1.331	78.82	104.62			

COMMENTS

pretest leak check < 0.02 qm @ 15 inHg  
 midtest leak check < 0.02 qm @ 15 inHg  
 post test leak check < 0.02 qm @ 15 inHg

STATE OF CALIFORNIA  
AIR RESOURCES BOARD

This Certifies That

THOMAS ROONEY

Has Attended The

VISIBLE EMISSION EVALUATION

From OCTOBER 25 to OCTOBER 27, 1977



*Stucomben*

Chief, Division of Legal Affairs and Enforcement

*[Signature]*

Chief, Enforcement Branch

44810-110 8-78 900 ① 037

## AIR RESOURCES BOARD

1102 Q STREET  
P.O. BOX 2815  
SACRAMENTO, CA 95812



April 20, 1979

Thomas Rooney, Project Engineer  
TRW  
One Space Park R4/2158  
Redondo Beach, CA 90278

Dear Mr. Rooney:

RE: Visible Emission Evaluation Certification

This is to certify that on April 5, 1979 in Sacramento, California you attended the course "Visible Emissions Evaluation."

Based on the score you achieved and the criteria established by the Environmental Protection Agency, you are certified as a visible emission evaluator for the following conditions:

- Day Readings  
 Day Readings with Sunglasses  
 Night Readings  
 Night Readings with Starlight Scope

Qualification is based on 50 consecutive readings (25 black or gray readings and 25 white readings) with no reading deviating by more than 3/4 Ringelmann Number or 15 percent opacity and the average deviation for each run of 25 readings not exceeding 7.5 percent.

In accordance with criteria established by EPA, this certification is valid until October 4, 1979. A copy of the certification paper for each condition is attached.

Sincerely,

James J. Morgester, Chief  
Enforcement Branch

Enclosure

WITH SUNGLASSES NO

STATE OF CALIFORNIA - AIR RESOURCES BOARD

VISIBLE EMISSION EVALUATION TRAINING FORM

REV  
MAY

PLEASE PRINT

1. NAME THOMAS ROONEY (PROJECT ENGINEER) DATE 4/5/79

2. AFFILIATION TRW

3. BUSINESS ADDRESS ONE SPACE PARK, REDWOOD BEACH ZIP CODE 90278

RUN NUMBER 2A TIME 1025 CORRECTED BY Tom Armstrong

READING NO.	1	2	3	4	5	6	7	8	9	DW	DW	12	13
OBSERVER READ	35	60	40	30	45	20	40	50	40	65	30	50	30
TRANSMISSIOMETER	40	70	55	35	60	30	45	40	50	65	35	50	45
+ DEVIATION								10		/	/		
- DEVIATION	5	10	15	5	15	10	5		10	/	5	/	15

10  
1  
95  
10  
105

READING NO.	14	15	16	17	DW	DW	20	21	22	23	24	25
OBSERVER READ	20	70	50	25	60	40	50	25	65	50	20	70
TRANSMISSIOMETER	30	70	40	25	55	35	45	30	60	40	25	55
+ DEVIATION		/	10	/	5	5	5		5	10		15
- DEVIATION	10	/		/				5			5	

55  
7  
20  
3  
75

RUN NUMBER 2B TIME 1100 CORRECTED BY Tom Fessler

READING NO.	1	2	3	4	5	6	7	8	9	10	11	12	13
OBSERVER READ	2	1 1/2	3 1/4	2	3 1/2	1 1/4	2 1/2	1	2 3/4	2	2 1/2	1	3 1/4
TRANSMISSIOMETER	2 1/4	1 1/2	3	2	3 1/4	1 1/2	2 3/4	1	3	1 1/2	2 1/2	1 1/2	3 1/2
+ DEVIATION		/	5	/	5		/	/		5	/		
- DEVIATION	5	/		/		5	/	/	5		/	10	5

15  
3  
30  
5

READING NO.	14	15	16	17	18	19	20	21	22	23	24	25
OBSERVER READ	2	2 1/2	1	2 1/2	3 3/4	3	2 1/4	2 3/4	1 1/2	3	2 1/4	2
TRANSMISSIOMETER	2	2 3/4	1	2 1/4	4 1/4	3	1 3/4	2 1/2	1 1/2	3 1/4	2	2
+ DEVIATION	/		/	5		/	5	5	/		10	/
- DEVIATION	/	5	/		10	/			/	5		/

25  
4  
20  
3

4. RUN NUMBER	2	2
5. TOTAL DEVIATION (SUM OF PLUS AND MINUS DEVIATIONS)	180	90
6. AVERAGE DEVIATION (TOTAL DEVIATION DIVIDED BY 25)	7.2	3.6
7. NUMBER OF READINGS 20% DEVIATION OR MORE	0	0



FIGURE 9-2 OBSERVATION RECORD

COMPANY Kaiser Steel  
 LOCATION Fontana Calif  
 TEST NUMBER #4  
 DATE 9/21/79

OBSERVER T. Rooney  
 TYPE FACILITY Calc Over Steel  
 POINT OF EMISSIONS Stack Bathy B

Hr.	Min.	Seconds				STEAM PLUME (check if applicable)		COMMENTS
		0	15	30	45	Attached	Detached	
935	0	0	0	0	0			
936	1	0	0	0	0			
937	2	0	0	0	0			
938	3	0	0	0	0			
939	4	0	0	0	0			
940	5	0	0	0	0			
941	6	0	0	0	0			
942	7	0	0	0	0			
943	8	0	0	0	0			
944	9	0	0	0	0			
945	10	0	0	0	0			
946	11	0	0	0	0			
947	12	0	0	0	0			
948	13	0	0	0	0			
949	14	0	0	0	0			
950	15	0	0	0	0			
951	16	0	0	0	0			
952	17	0	0	0	0			
953	18	0	0	0	0			
954	19	0	0	0	0			
955	20	0	0	0	0			
956	21	0	0	0	0			
957	22	0	0	0	0			
958	23	0	0	0	0			
959	24	0	0	0	0			
1000	25	0	0	0	0			
1001	26	0	0	0	0			
1002	27	0	0	0	0			
1003	28	0	0	0	0			
1004	29	0	0	0	0			

Reference

- 0 = 0% opacity
- 1 = 20% opacity
- 2 = 40% opacity
- 3 = 60% opacity
- 4 = 80% opacity
- 5 = 100% opacity

FIGURE 9-2 OBSERVATION RECORD  
(Continued)

PAGE \_\_\_ OF \_\_\_

COMPANY Kaiser Steel  
 LOCATION Fontana Calif  
 TEST NUMBER 4  
 DATE 9/21/79

OBSERVER T. Reamy  
 TYPE FACILITY Coke Oven  
 POINT OF EMISSIONS Steel Battery **B**

Hr.	Min.	Seconds				STEAM PLUME (check if applicable)		COMMENTS
		0	15	30	45	Attached	Detached	
1005	30	0	0	0	0			
1006	31	0	0	0	0			
1007	32	0	0	0	0			
1008	33	0	0	0	0			
1009	34	0	0	0	0			
1010	35	0	0	0	0			
1011	36	0	0	0	0			
1012	37	0	0	0	0			
1013	38	0	0	0	0			
1014	39	0	0	0	0			
1015	40	0	0	0	0			
1016	41	0	0	0	0			
1017	42	0	0	0	0			
1018	43	0	0	0	0			
1019	44	0	0	0	0			
1020	45	0	0	0	0			
1021	46	0	0	0	0			
1022	47	0	0	0	0			
1023	48	0	0	0	0			
1024	49	0	0	0	0			
1025	50	0	0	0	0			
1026	51	0	0	0	0			
1027	52	0	0	0	0			
1028	53	0	0	0	0			
1029	54	0	0	0	0			
1030	55	0	0	0	0			
1031	56							
1032	57							
1033	58							
1034	59							



4-5

FIGURE 9-2 OBSERVATION RECORD PAGE \_\_\_ OF \_\_\_

COMPANY Kaiser  
 LOCATION Fontana  
 TEST NUMBER #4  
 DATE 9/21/79

OBSERVER T. Rooney  
 TYPE FACILITY Battery #8 Coke Oven  
 POINT OF EMISSIONS Stack

Hr.	Min.	Seconds				STEAM PLUME (check if applicable)		COMMENTS
		0	15	30	45	Attached	Detached	
1100	0	0	0	0	0			NO SMOKE
1101	1	0	0	0	0			
1102	2	0	0	0	0			
1103	3	0	0	0	0			
1104	4	0	0	0	0			
1105	5	0	0	0	0			
1106	6	0	0	0	0			
1107	7	0	0	0	0			
1108	8	0	0	0	0			
1109	9	0	0	0	0			
1110	10	0	0	0	0			
1111	11	0	0	0	0			
1112	12	0	0	0	0			
1113	13	0	0	0	0			
1114	14	0	0	0	0			
1115	15	0	0	0	0			
1116	16	0	0	0	0			
1117	17	0	0	0	0			
1118	18	0	0	0	0			
1119	19	0	0	0	0			
1120	20	0	0	0	0			
1121	21	0	0	0	0			
1122	22	0	0	0	0			
1123	23	0	0	0	0			
1124	24	0	0	0	0			FUGITIVE EMISSIONS FROM BLAST FURNACE BLOCKING STACK FOR READINGS
1125	25	1	1	1	1			
1126	26	1	0	0	0			
1127	27	0	0	0	0			
1128	28	0	0	0	0			
1129	29	0	0	0	0			

Reference  
 0 = 0% Opacity  
 1 = 20% Opacity  
 2 = 40% Opacity  
 3 = 60% Opacity  
 4 = 80% Opacity  
 5 = 100% Opacity

FIGURE 9-2 OBSERVATION RECORD  
(Continued)

COMPANY Kaiser Steel  
 LOCATION Fontana  
 TEST NUMBER # 4  
 DATE 9/21/79

OBSERVER Rooney  
 TYPE FACILITY Hot Open H "B"  
 POINT OF EMISSIONS Stack Betty "B"

Hr.	Min.	Seconds				STEAM PLUME (check if applicable)		COMMENTS
		0	15	30	45	Attached	Detached	
1130	30	0	0	0	0			
1131	31	0	0	0	0			
1132	32	0	0	0	0			
1133	33	0	0	0	0			
1134	34	0	0	0	0			
1135	35	0	0	0	0			
1136	36	0	0	0	0			
1137	37	0	0	0	0			
1138	38	0	0	0	0			
1139	39	0	0	0	0			
1140	40	0	0	0	0			
1141	41	0	0	.5	0			
1142	42	0	0	0	0			
1143	43	0	0	0	0			
1144	44	0	0	0	0			
1145	45	0	0	0	0			
1146	46	0	0	0	0			
1147	47	0	0	0	0			
1148	48	0	0	0	0			
1149	49	0	0	0	0			
1150	50	0	0	0	0			
1151	51	0	0	0	0			
1152	52	0	0	0	0			
1153	53	0	0	0	0			
1154	54	0	0	0	0			
1155	55	0	0	0	0			
	56							
	57							
	58							
	59							



FIGURE 9-2 OBSERVATION RECORD

PAGE \_\_\_ OF \_\_\_

48.  
 COMPANY Kaiser Steel  
 LOCATION Colts Ave. Bldg. B  
 TEST NUMBER #3  
 DATE 9/20/79

OBSERVER Room  
 TYPE FACILITY Colts Oven  
 POINT OF EMISSIONS \_\_\_\_\_

Hr.	Min.	Seconds				STEAM PLUME (check if applicable)		COMMENTS
		0	15	30	45	Attached	Detached	
1340	0	0	0	0	0			
41	1	0	0	0	0			
42	2	0	0	0	0			
43	3	0	0	0	0			
44	4	0	0	0	0			
45	5	0	0	0	0			
46	6	0	0	0	0			
47	7	0	0	0	0			
48	8	0	0	0	0			
49	9	0	0	0	0			
50	10	0	0	0	0			
51	11	0	0	0	0			
52	12	0	0	0	0			
53	13	0	0	0	0			
54	14	0	0	0	0			
55	15	0	0	0	0			
56	16	0	0	0	0			
57	17	0	0	0	0			
58	18	0	0	0	0			
59	19	0	0	0	0			
1400	20	0	0	0	0			
1401	21	0	0	0	0			
1402	22	0	0	0	0			
1403	23	0	0	0	0			
1404	24	0	0	0	0			
1405	25	0	0	0	0			
1406	26	0	0	0	0			
1407	27	0	0	0	0			
1408	28	0	0	0	0			
1409	29	0	0	0	0			

FIGURE 9-2 OBSERVATION RECORD  
(Continued)

PAGE \_\_\_ OF \_\_\_

COMPANY Kaiser Steel  
 LOCATION Fontana, Calif  
 TEST NUMBER #3  
 DATE 9/20/79

OBSERVER T. Rooney  
 TYPE FACILITY Coke Oven & Charge 'B'  
 POINT OF EMISSIONS Stack

Hr.	Min.	Seconds				STEAM PLUME (check if applicable)		COMMENTS
		0	15	30	45	Attached	Detached	
1410	30	0	0	0	0			
1411	31	0	0	0	0			
1412	32	0	0	0	0			
1413	33	0	0	0	0			
1414	34	0	0	0	0			
1415	35	0	0	0	0			
1416	36	0	0	0	0			
1417	37	0	0	0	0			
1418	38	0	0	0	0			
1419	39	0	0	0	0			
1420	40	0	0	0	0			
1421	41	0	0	0	0			
1422	42	0	0	0	0			
1423	43	0	0	0	0			
1424	44	0	0	0	0			
1425	45	0	0	0	0			
1426	46	0	0	0	0			
1427	47	0	0	0	0			
1428	48	0	0	0	0			
1429	49	0	0	0	0			
1430	50	0	0	0	0			
	51							
	52							
	53							
	54							
	55							
	56							
	57							
	58							
	59							



FIGURE 9-2 OBSERVATION RECORD

PAGE \_\_\_ OF \_\_\_

COMPANY Kaiser Steel  
 LOCATION Pintura  
 TEST NUMBER #3  
 DATE 9/20/79

OBSERVER T. Ramsey  
 TYPE FACILITY Coal Oven  
 POINT OF EMISSIONS Stack 100'

Hr.	Min.	Seconds				STEAM PLUME (check if applicable)		COMMENTS
		0	15	30	45	Attached	Detached	
1200	0	0	0	0	0			
1201	1	0	0	0	0			
2	2	0	0	0	0			
3	3	0	0	0	0			
4	4	0	0	0	0			
5	5	0	0	0	0			
6	6	0	0	0	0			
7	7	0	0	0	0			
8	8	0	0	0	0			
9	9	0	0	0	0			
10	10	0	0	0	0			
11	11	0	0	0	0			
12	12	0	0	0	0			
13	13	0	0	0	0			
14	14	0	0	0	0			
15	15	0	0	0	0			
16	16	0	0	0	0			
17	17	0	0	0	0			
18	18	0	0	0	0			
19	19	0	0	0	0			
20	20	0	0	0	0			
21	21	0	0	0	0			
22	22	0	0	0	0			
23	23	0	0	0	0			
24	24	0	0	0	0			
25	25	0	0	0	0			
26	26	0	0	0	0			
27	27	0	0	0	0			
28	28	0	0	0	0			
29	29	0	0	0	0			

FIGURE 9-2 OBSERVATION RECORD  
(Continued)

PAGE \_\_\_ OF \_\_\_

COMPANY Kaiser Steel  
 LOCATION Fontana  
 TEST NUMBER 3  
 DATE 9/20/79

OBSERVER T. Brown  
 TYPE FACILITY Slab Mill "Coke Area B"  
 POINT OF EMISSIONS Stack after Dry Line

Hr.	Min.	Seconds				STEAM PLUME (check if applicable)		COMMENTS
		0	15	30	45	Attached	Detached	
30	30	0	0	0	0			
31	31	0	0	0	0			
32	32	0	0	0	0			
33	33	0	0	0	0			
34	34	0	0	0	0			
35	35	0	0	0	0			
36	36	0	0	0	0			
37	37	0	0	0	0			
38	38	0	0	0	0			
39	39	0	0	0	0			
40	40	0	0	0	0			
41	41	0	0	0	0			
42	42	0	0	0	0			
43	43	0	0	0	0			
44	44	0	0	0	0			
45	45	0	0	0	0			
46	46							
47	47							
48	48							
49	49							
50	50							
51	51							
52	52							
53	53							
54	54							
55	55							
56	56							
57	57							
58	58							
59	59							





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OBSERVATION RECORD PAGE \_\_\_ OF \_\_\_

COMPANY KAISER STEEL  
 LOCATION BATTERY # 5 "STACK"  
 TEST NUMBER 111114  
 DATE 11/11/74

OBSERVER J. Rogers  
 TYPE FACILITY Steel Mill  
 POINT OF EMISSIONS Battery # 5 "Stack"

934 Stack

Hr.	Min.	Seconds			STEAM PLUME (check if applicable)		COMMENTS
		0	15	30	45	Attached	
9	1	0	0	0	0		
	2	0	0	0	0		
	3	0	0	0	0		
	4	0	0	0	0		
	5	0	0	0	0		
	6	0	0	0	0		
	7	0	0	0	0		
	8	0	0	0	0		
	9	0	0	0	0		
	10	0	0	0	0		
	11	0	0	0	0		
	12	0	0	0	0		
	13	0	0	0	0		
	14	0	0	0	0		
	15	0	0	0	0		
	16	0	0	0	0		
	17	0	0	0	0		
	18	0	0	0	0		
	19	0	0	0	0		
	20	0	0	0	0		
	21	0	0	0	0		
	22	0	0	0	0		
	23	0	0	0	0		
	24	0	0	0	0		
	25	0	0	0	0		
	26	0	0	0	0		
	27	0	0	0	0		
	28	0	0	0	0		
	29	0	0	0	0		

Wind 0-5  
 WD W  
 T 95  
 Ambient Smoggy  
 Smoke Black

OBSERVATION RECORD PAGE \_\_\_ OF \_\_\_

COMPANY KAISER STEEL  
 LOCATION BATTERY # 6 STACK  
 TEST NUMBER 111114  
 DATE 9/18/74

OBSERVER J. Rogers  
 TYPE FACILITY Steel Mill  
 POINT OF EMISSIONS Battery # 6 "Stack"

416

Hr.	Min.	Seconds			STEAM PLUME (check if applicable)		COMMENTS
		0	15	30	45	Attached	
	0	0	0	0	0		
	1	0	0	0	0		
	2	0	0	0	0		
	3	0	0	0	0		
	4	0	0	0	0		
	5	0	0	0	0		
	6	0	0	0	0		
	7	0	0	0	0		
	8	0	0	0	0		
	9	0	0	0	0		
	10	0	0	0	0		
	11	0	0	0	0		
	12	0	0	0	0		
	13	0	0	0	0		
	14	0	0	0	0		
	15	0	0	0	0		
	16	0	0	0	0		
	17	0	0	0	0		
	18	0	0	0	0		
	19	0	0	0	0		
	20	0	0	0	0		
	21	0	0	0	0		
	22	0	0	0	0		
	23	0	0	0	0		
	24	0	0	0	0		
	25	0	0	0	0		
	26	0	0	0	0		
	27	0	0	0	0		
	28	0	0	0	0		
	29	0	0	0	0		

A-35

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OBSERVATION RECORD PAGE \_\_\_ OF \_\_\_

COMPANY KAISER STEEL  
LOCATION BATTERY 3  
TEST NUMBER 9  
DATE 9/18/79

OBSERVER T. ROONEY  
TYPE FACILITY COKE OVEN  
POINT OF EMISSIONS BATTERY B

Hr.	Min.	Seconds					STEAM PLUME (check if applicable)		COMMENTS
		0	15	30	45	Attached	Detached		
	0	0	0	0	0				
	1	0	0	0	0				
	2	0	0	0	0				
	3	0	0	0	0				
	4	0	0	0	0				
	5	0	0	0	0				
	6	0	0	0	0				
	7	0	0	0	0				
	8	0	0	0	0				
	9	0	0	0	0				
	10	0	0	0	0				
	11	0	0	0	0				
	12	0	0	0	0				
	13	0	0	0	0				
	14	0	0	0	0				
	15	0	0	0	0				
	16	0	0	0	0				
	17	0	0	0	0				
	18	0	0	0	0				
	19	0	0	0	0				
	20	0	0	0	0				
	21	0	0	0	0				
	22	0	0	0	0				
	23	0	0	0	0				
	24	0	0	0	0				
	25	0	0	0	0				
	26	0	0	0	0				
	27	0	0	0	0				
	28	0	0	0	0				
	29	0	0	0	0				
	30	0	0	0	0				

OBSERVATION RECORD PAGE \_\_\_ OF \_\_\_

COMPANY \_\_\_\_\_  
LOCATION \_\_\_\_\_  
TEST NUMBER \_\_\_\_\_  
DATE \_\_\_\_\_

OBSERVER \_\_\_\_\_  
TYPE FACILITY \_\_\_\_\_  
POINT OF EMISSIONS \_\_\_\_\_

Hr.	Min.	Seconds					STEAM PLUME (check if applicable)		COMMENTS
		0	15	30	45	Attached	Detached		
	30	0	0	0	0				
	31	0	0	0	0				
	32	0	0	0	0				
	33	0	0	0	0				
	34	0	0	0	0				
	35	0	0	0	0				
	36	0	0	0	0				
	37	0	0	0	0				
	38	0	0	0	0				
	39	0	0	0	0				
	40	0	0	0	0				
	41	0	0	0	0				
	42	0	0	0	0				
	43	0	0	0	0				
	44	0	0	0	0				
	45	0	0	0	0				
	46	0	0	0	0				
	47								
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	59								





SECTION 6  
APPENDIX A

3. Analytical Data Sheets

	<u>ug/ml</u>	<u>VOL</u>	<u>ug</u>
KSC-IN-1 rinse	.0362	120	4.344g
KSC-IN-1 filter	.0414	100	14.14g
KSC-IN-1 impinger	—	—	—
KSC-IN-1 XAD-2	.0067	250	1.67
KSC-OUT-1-rinse	.0424	118	5.00
OUT-1 filter	.022	100	2.20
OUT-1 impinger	.0055	415	2.28
OUT-1 XAD-2	.0045	250	1.12
KSC-IN-2 rinse	.0352	156	5.49
filter	.095	100	9.5
impinger	—	—	—
XAD-2	.0082	250	2.05
KSC-OUT-2 rinse	.0352	154	5.42
filter	.0062	100	.62
impinger	.0064	400	2.56
XAD-2	.0425	250	10.6
filter/rinse	.05	—	.5
KSC-IN-3 rinse	.0280	262	7.3
filter	.1	100	10.0
impinger	.0042	435	1.83
XAD-2	.0084	250	2.1
KSC-OUT-3 rinse	.0350	210	7.35
filter	.0025	100	.25
impinger	.0045	425	1.91
XAD-2	.011	250	2.75

DO NOT WRITE IN THESE SPACES  
A-40

WITNESS: RA Rm 2158 DATE: \_\_\_\_\_ SIGNED: \_\_\_\_\_  
 WITNESS: \_\_\_\_\_ DATE: \_\_\_\_\_ SIGNED: \_\_\_\_\_

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run #1

replicate	stack gas		5ppm benzene std	
	int. area	height x width <sup>h</sup> (at $\frac{1}{2}$ ht)	int. area	ht x width <sup>h</sup> (at $\frac{1}{2}$ ht)
1	28	52.5	60	105
2	18	41.3	57	99
3	16	36.0	58	104
avg	20.7	43.3	58.3	102.7
std. dev.	6.43	8.42	1.53	2.95

conc benzene by int. area = 1.8 ppm  $\pm$  0.6  
 by ht x width<sup>h</sup> ( $\frac{1}{2}$ ht) = 2.1 ppm  $\pm$  0.4 \*

run #2

replicate	Stack gas		5ppm benzene std.	
	int. area	height x width <sup>h</sup> (@ $\frac{1}{2}$ ht)	int. area	height x width <sup>h</sup> (@ $\frac{1}{2}$ ht)
1	28.0	60.0	39.0	81.0
2	23.0	48.0	38.0	72.5
3	18.0	42.0	40.0	78.0
avg	23.0	50.0	39.0	77.2
std dev.	5.00	9.16	1.00	4.31

conc benzene by int. area = 2.9  $\pm$  0.6  
 by ht x width<sup>h</sup> ( $\frac{1}{2}$ ht) = 3.2  $\pm$  0.6

3/8

run #3

replicate	stack gas		5ppm benzene std	
	int. area	height x width @ $\frac{1}{2}$ ht	int. area	height x width @ $\frac{1}{2}$ ht
1	42.5	74.8	21.0	38.5
2	38.0	77.0	21.0	32.5
3			18.0	27.0
avg	40.3	75.9	20.0	32.7
std. dev.			1.73	5.75

conc. benzene by int. area =  $2.5 \pm 0.2$  \*

by ht x width @  $\frac{1}{2}$ ht =  $2.2 \pm 0.4$

run #4

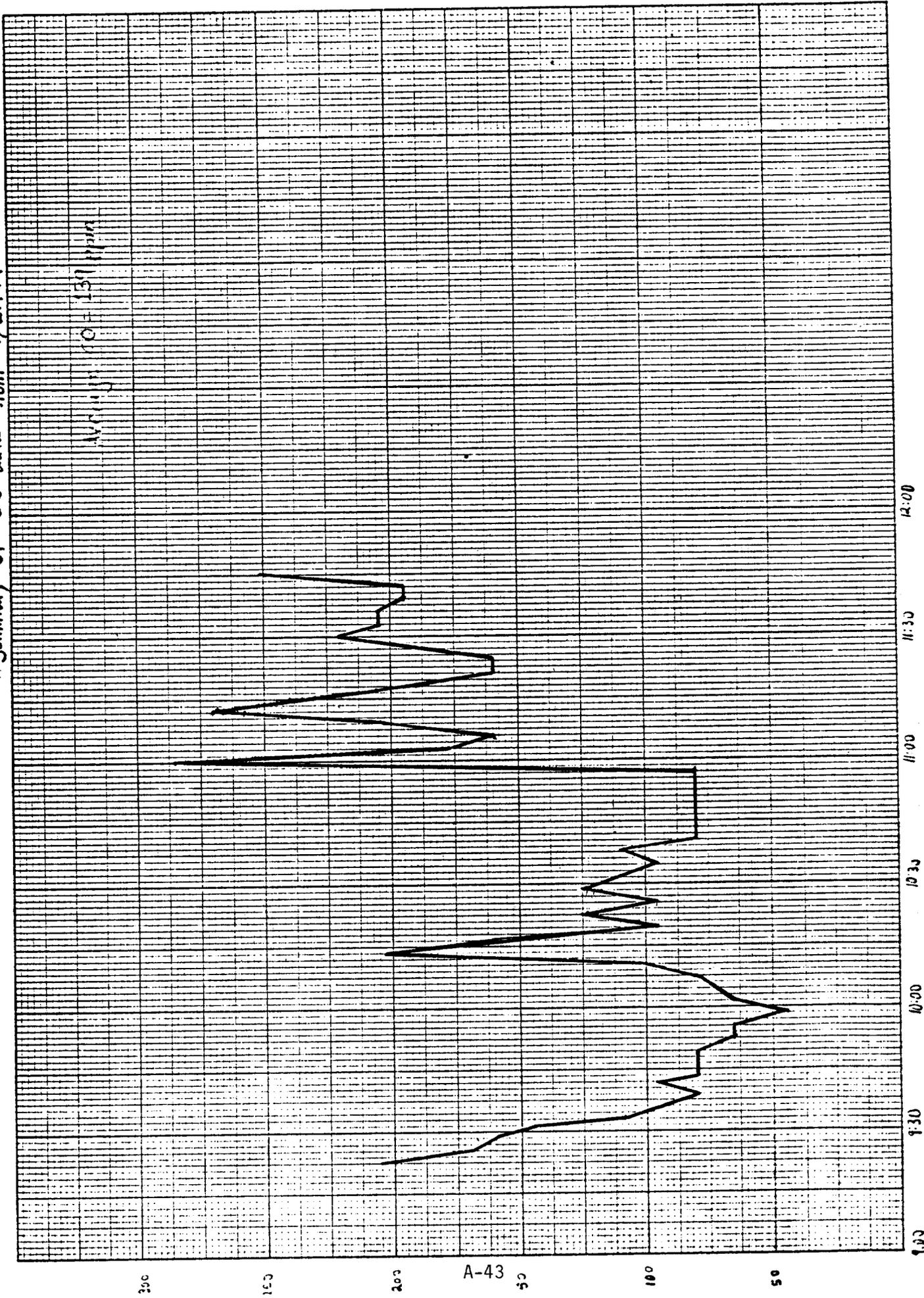
replicate	stack gas		5ppm benzene std	
	int. area	height x width @ $\frac{1}{2}$ ht	int. area	height x width @ $\frac{1}{2}$ ht
1	38.7	71.5	45.4	81.0
2	35.5	57.0	44.2	91.0
3	33.4	49.5	41.8	84.0
avg.	35.9	59.3	43.8	85.3
std. dev.	2.67	11.25	1.84	5.13

conc. benzene by int. area =  $4.1 \pm 0.3$  \*

by ht x width @  $\frac{1}{2}$ ht =  $3.5 \pm 0.7$

Summary of CO data from 9/21/79

Velocity = 139 ft/min

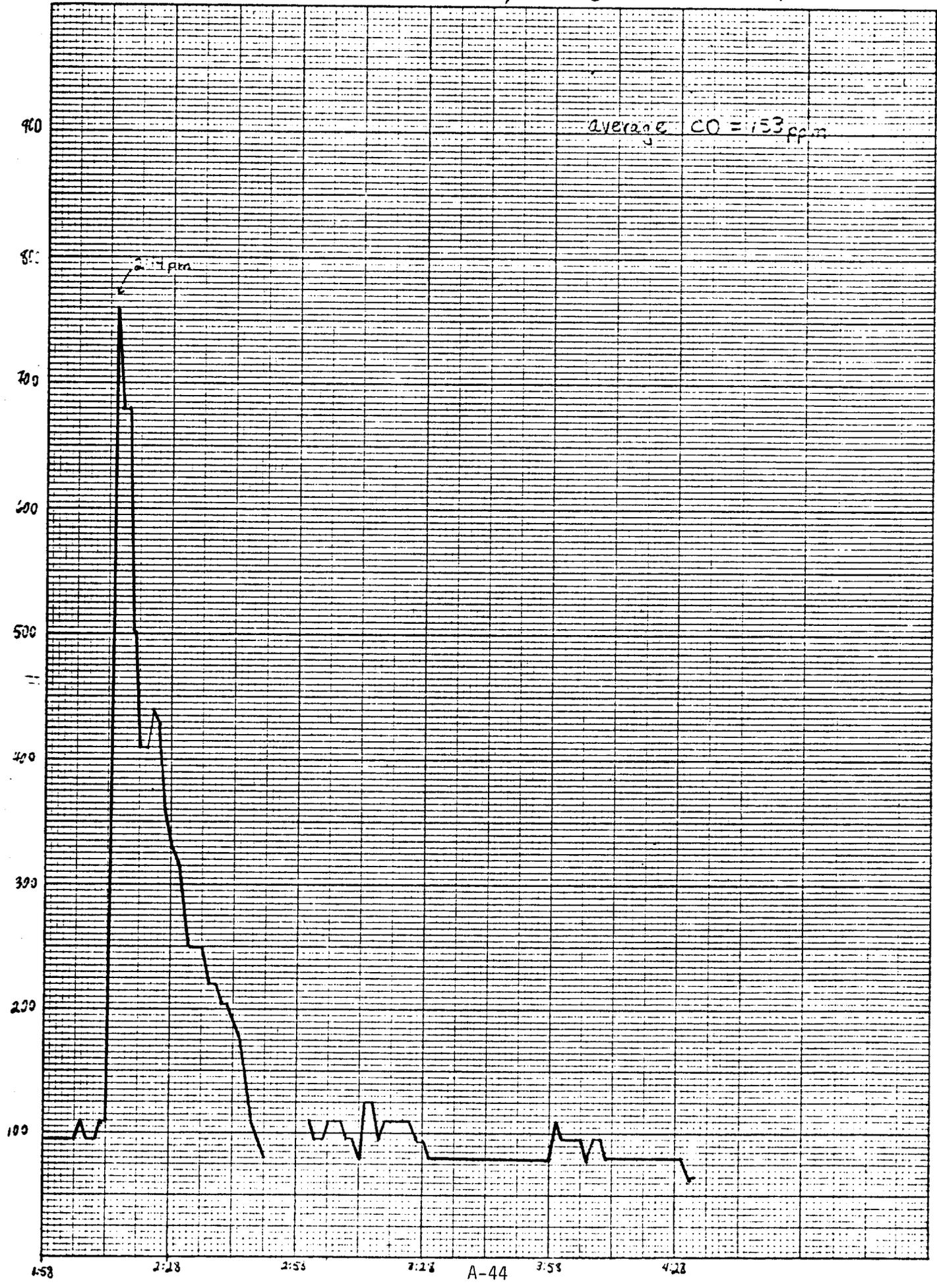


Summary of CO data from 1/18/74

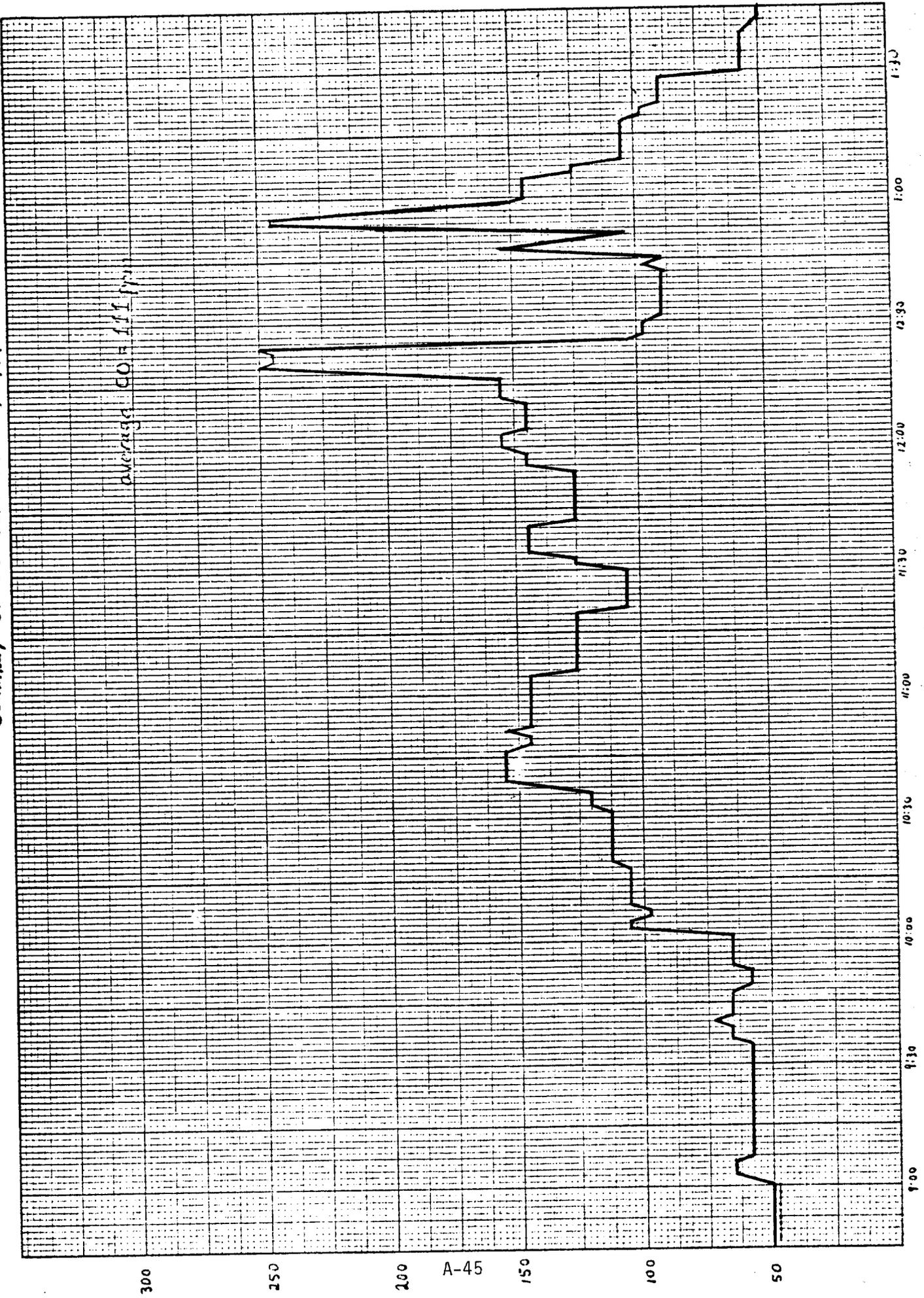
46 1242  
ppm CO

average CO = 153 ppm

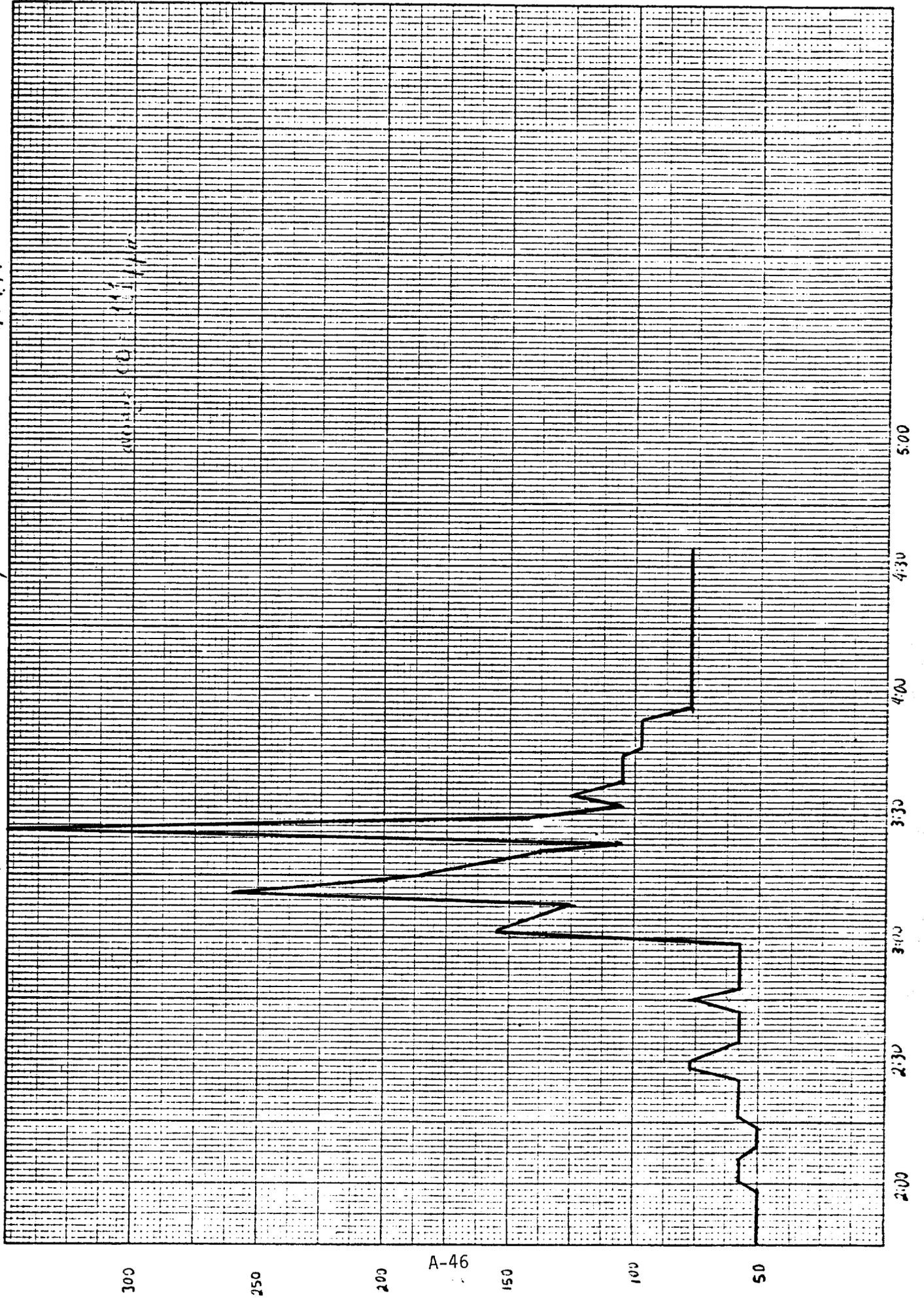
K&E  
20 X 20 TO THE INCH • 7 X 10 INCHES  
KLUFFEL & ESSLER CO. MADE IN U.S.A.



Summary of CO Data from 9/19/79



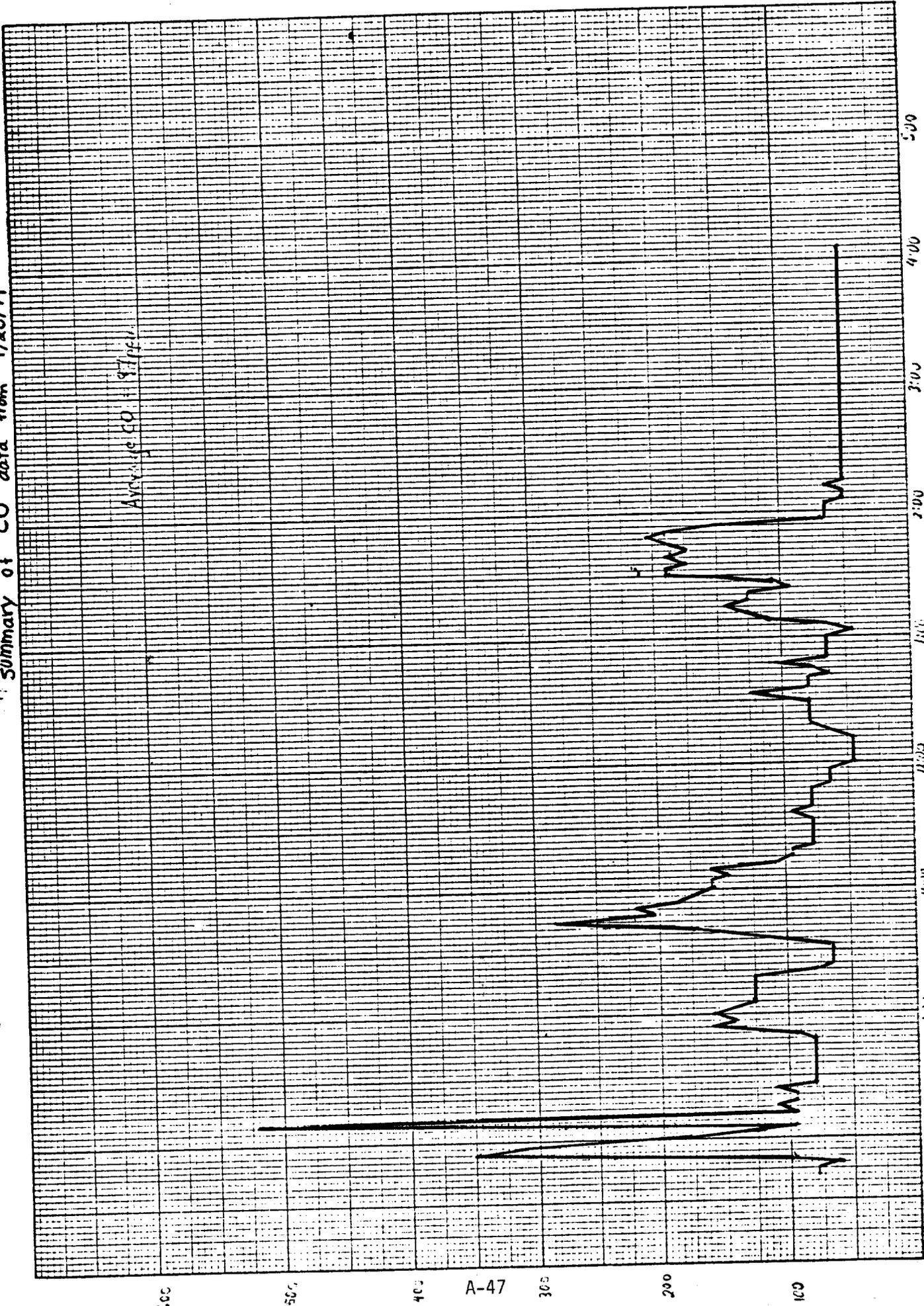
Summary of CO data from 9/19/79



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Summary of CO data from 9/20/79

Average CO = 87 ppm



SECTION 6  
APPENDIX A

4. Meter Box Calibration Data Sheets

DATE 19 Nov 79

BOX # 2343

BAROMETRIC PRESSURE  $P_b$  30.10 in. Hg

DRY GASMETER # \_\_\_\_\_

*Wally Murphy*

Orifice Manometer Settling H (in. H <sub>2</sub> O)	Gas Volume Wet Test Meter V <sub>w</sub> (ft <sup>3</sup> )	Gas Volume Dry Gas Meter V <sub>d</sub> (ft <sup>3</sup> )	Temperature				Time θ (min.)	γ	ΔHθ
			Wet Test Meter T <sub>w</sub> (°F)	Dry Gas Meter					
				Inlet T <sub>d</sub> (°F)	Outlet T <sub>do</sub> (°F)	Average T <sub>d</sub> (°F)			
0.5	3.820	4.010	65	98	84	91	10	.999	1.805
<del>1.0</del>	3.802	4.029	66	98	88	93	10	.991	1.823
<del>2.0</del>	5.165	5.617	66	104	90	97	10	.991	1.961
<del>4.0</del>	5.181	5.528	66	104	92	98	10	.990	1.953
6.0									
8.0									
Average								<del>.988</del> .993	1.886

Calculations

ΔH	$\frac{\Delta H}{13.6}$	γ	ΔHθ
		$\frac{V_w P_b (T_d + 460)}{V_d (P_b + \frac{H}{13.6} (T_w + 460))}$	$\frac{0.0317 \Delta H}{P_b (T_d + 460)} \left[ \frac{(T_w + 460) \theta^2}{V_w} \right]$
0.5	0.0368		
1.0	0.0737		
2.0	0.147		
4.0	0.294		
6.0	0.431		
8.0	0.588		

DATE 16 Nov 79

BOX # 2315

BAROMETRIC PRESSURE  $P_b$  30.03 in. Hg

DRY GASMETER # " "

*Wally Murphy*

Orifice Manometer Settling H (in. H <sub>2</sub> O)	Gas Volume Wet Test Meter V <sub>w</sub> (ft <sup>3</sup> )	Gas Volume Dry Gas Meter V <sub>d</sub> (ft <sup>3</sup> )	Temperature				Time $\theta$ (min.)	$\gamma$	$\Delta H\theta$
			Wet Test Meter T <sub>w</sub> (°F)	Dry Gas Meter					
				Inlet T <sub>d</sub> (°F)	Outlet T <sub>do</sub> (°F)	Average T <sub>d</sub> (°F)			
0.5	4.010	4.148	66	98	78	88.0	10	1.006	1.657
1.0	3.910	4.077	67	104	83	93.5	10	1.006	1.732
2.0	5.404	5.715	67	112	88	100	10	1.002	1.793
4.0	5.414	5.619	68	112	87	99.5	10	1.002	1.797
6.0									
8.0									
Average								1.004	1.745

Calculations

$\Delta H$	$\frac{\Delta H}{13.6}$	$\gamma$	$\Delta H\theta$
		$\frac{V_w P_b (T_d + 460)}{V_d (P_b + \frac{H}{13.6} (T_w + 460))}$	$\frac{0.0317 \Delta H}{P_b (T_d + 460)} \left[ \frac{(T_w + 460)\theta^2}{V_w} \right]$
0.5	0.0368		
1.0	0.0737		
2.0	0.147		
4.0	0.294		
6.0	0.431		
8.0	0.588		

DATE 16 Nov. 79

BOX # 2363

BAROMETRIC PRESSURE  $P_b$  30.05 in. Hg

DRY GASMETER # 1111

*Wally Murphy*

Orifice Manometer Settling H (in. H <sub>2</sub> O)	Gas Volume Wet Test Meter V <sub>w</sub> (ft <sup>3</sup> )	Gas Volume Dry Gas Meter V <sub>d</sub> (ft <sup>3</sup> )	Temperature				Time θ (min.)	Y	ΔHθ
			Wet Test Meter T <sub>w</sub> (°F)	Dry Gas Meter					
				Inlet T <sub>d</sub> (°F)	Outlet T <sub>do</sub> (°F)	Average T <sub>d</sub> (°F)			
0.5	3.937	4.061	66	96	79	85.0	10	.992	1.686
1.0	3.973	4.171	66	98	79	88.5	10	1.003	1.728
2.0	5.303	5.610	66	110	84	97.0	10	.999	1.863
4.0	5.297	5.639	66	110	88	99.0	10	.996	1.861
6.0									
8.0									
Average								.9975	1.784

Calculations

ΔH	$\frac{\Delta H}{13.6}$	Y	ΔHθ
		$\frac{V_w P_b (T_d + 460)}{V_d (P_b + \frac{H}{13.6} (T_w + 460))}$	$\frac{0.0317 \Delta H}{P_b (T_d + 460)} \left[ \frac{(T_w + 460) \theta}{V_w} \right]^2$
0.5	0.0368		
1.0	0.0737		
2.0	0.147		
4.0	0.294		
6.0	0.431		
8.0	0.588		

DATE 26 nov 79

BOX # 2499

BAROMETRIC PRESSURE  $P_b$  50.01 in. Hg

DRY GASMETER # 11 11

*Walby Murphy*

Orifice Manometer Settling H (in. H <sub>2</sub> O)	Gas Volume Wet Test Meter V <sub>w</sub> (ft <sup>3</sup> )	Gas Volume Dry Gas Meter V <sub>d</sub> (ft <sup>3</sup> )	Temperature				Time $\theta$ (min.)	$\gamma$	$\Delta H\theta$
			Wet Test Meter T <sub>w</sub> (°F)	Dry Gas Meter					
				Inlet T <sub>d</sub> (°F)	Outlet T <sub>do</sub> (°F)	Average T <sub>d</sub> (°F)			
0.5	<del>4.052</del> 4.43	4.431	68	108	79	93.5	11	.957	1.960
1.0	4.307	4.451	68	106	82	94.0	11	1.014	1.734
2.0	6.181	6.434	69	106	86	96.0	11	1.008	1.684
4.0	6.092	6.345	69	109	86	97.5	11	1.011	1.728
6.0									
8.0									
Average								998	1.777

Calculations

$\Delta H$	$\frac{\Delta H}{13.6}$	$\gamma$	$\Delta H\theta$
		$\frac{V_w P_b (T_d + 460)}{V_d (P_b + \frac{H}{13.6} (T_w + 460))}$	$\frac{0.0317 \Delta H}{P_b (T_d + 460)} \left( \frac{(T_w + 460)\theta}{V_w} \right)^2$
0.5	0.0368		
1.0	0.0737		
2.0	0.147		
4.0	0.294		
6.0	0.431		
8.0	0.588		

SECTION 6

APPENDIX B

Sample Calculations

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### Nomenclature

$P_b$	Barometric Pressure, mm. Hg.
$P_m$	Average Orifice Pressure Drop, mm. H <sub>2</sub> O
$T_m$	Average Dry Gas Meter Temperature, °C
$V_m$	Volume of Dry Gas Sampled at Meter Conditions, Am <sup>3</sup>
$V_{m\text{std}}$	Volume of Dry Gas Sampled at Standard Conditions <sup>(1)</sup> , Nm <sup>3</sup>
$V_w$	Total H <sub>2</sub> O Collected in Impingers and Silica Gel, ml
$V_{w\text{std}}$	Volume of Water Vapor Collected at Standard Conditions <sup>(1)</sup> , Nm <sup>3</sup>
%M	Percent Moisture in Stack Gas, by Volume
$M_d$	Mole Fraction Dry Stack Gas
%CO <sub>2</sub>	Percent CO <sub>2</sub> by volume, dry
%O <sub>2</sub>	Percent O <sub>2</sub> by volume, dry
%CO	Percent CO by volume, dry
%N <sub>2</sub>	Percent N <sub>2</sub> by volume, dry
MW <sub>d</sub>	Molecular Weight of Dry Stack Gas, gm/gm-mole
MW	Molecular Weight of Wet Stack Gas, gm/gm-mole
MW <sub>c</sub>	Molecular Weight of Chemical
C <sub>p</sub>	Pitot Tube Coefficient
P <sub>s</sub>	Stack Gas Pressure, mm. Hg., absolute
PPM	Parts per million
T <sub>s</sub>	Stack Gas Temperature, °C
$\bar{T}_s$	Average Stack Gas Temperature, °C
$\Delta P_s$	Velocity head, mm. H <sub>2</sub> O
V <sub>s</sub>	Average Stack Gas Velocity, Stack Conditions, Am/s
A <sub>s</sub>	Stack Area, m <sup>2</sup>
Q <sub>s</sub>	Stack Gas Flow Rate at Standard Conditions <sup>(1)</sup> , dry Nm <sup>3</sup> /min.

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$Q_a$	Stack gas flow rate at stack conditions, $\text{Am}^3/\text{min}$ .
$T_t$	Net time of test, min.
$D_n$	Sampling nozzle diameter, mm.
%I	Percent isokinetic
$m_f$	Particulate collected in probe, cyclone and filter, mg.
$m_t$	Total particulate collected, mg.
$I_c$	Percent of particulate caught in impingers
$C_{sf}$	Particulate concentrations at standard conditions <sup>(1)</sup> , dry, based on probe, cyclone and filter catch, $\text{mg}/\text{Nm}^3$
$C_{st}$	Particulate concentration at standard conditions <sup>(1)</sup> , dry, based on total catch, $\text{mg}/\text{Nm}^3$
$C_{af}$	Particulate concentration at stack conditions, based on probe, cyclone and filter catch, $\text{mg}/\text{Am}^3$
$C_{at}$	Particulate concentration at stack conditions, based on total catch, $\text{mg}/\text{Am}^3$
$E_f$	Particulate emission rate, based on probe, cyclone and filter catch, kg/hr.
$E_t$	Particulate emission rate; based on total particulate catch, kg/hr.
$P_u$	Unit process rate, _____
$PE_f$	Particulate emission rate on a process basis, probe, cyclone and filter catch, kg/_____
$PE_t$	Particulate emission rate on a process basis, total catch kg/_____
%EA	Percent excess air in stack gas

Calculations

1. Volume of dry gas sampled at standard conditions<sup>(1)</sup>

$$V_{m_{std}} = \frac{0.3855 \times V_m \times (P_b + \frac{P_m}{13.6})}{(T_m + 273)} = N_m^3$$

2. Volume of water vapor at standard conditions<sup>(1)</sup>

$$V_{w_{gas}} + 0.0013 \times V_w = N_m^3$$

3. Percent moisture in stack gas by volume

$$\%M = \frac{100 \times V_{w_{gas}}}{V_{w_{gas}} + V_{m_{std}}} = \%$$

4. Mole fraction dry stack gas

$$M_s = \frac{100 - \%M}{100} = \%$$

5. Molecular weight of dry stack gas

$$MW_d = (\%CO \times \frac{44}{100}) + (\%O_2 \times \frac{32}{100}) + [\%CO + \%N_2 \times \frac{28}{100}]$$

= gm/gm-mole

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Calculations

1. Volume of dry gas sampled at standard conditions<sup>(1)</sup>

$$V_{m_{std}} = \frac{0.3855 \times V_m \times (P_b + \frac{P_m}{13.6})}{(T_m + 273)} - \text{volume of SO}_2 \text{ collected} = \text{Nm}^3$$

2. Volume of water vapor at standard conditions<sup>(1)</sup>

$$V_{w_{gas}} + 0.0013 \times V_w = \text{Nm}^3$$

3. Percent moisture in stack gas by volume

$$\%M = \frac{100 \times V_{w_{gas}}}{V_{w_{gas}} + V_{m_{std}}} = \%$$

4. Mole fraction dry stack gas

$$M_s = \frac{100 - \%M}{100} = \%$$

5. Molecular weight of dry stack gas

$$\begin{aligned} MW_d &= (\%CO \times \frac{44}{100}) + (\%O_2 \times \frac{32}{100}) + [\%CO + \%N_2 \times \frac{28}{100}] \\ &= \text{gm/gm-mole} \end{aligned}$$

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6. Molecular weight of wet stack gas

$$MW = MW_d \times M_d + 18(1-M_d) = \text{gm/gm-mole}$$

7. Stack gas velocity at stack conditions<sup>(2)</sup>

$$V_s = 34.97 \times C_p \times \sqrt{\Delta P_s \times (T_s + 273)} \frac{1}{P_s \times MW}^{\frac{1}{2}} = \text{Am/sec.}$$

8. Stack gas volumetric flow rate at standard conditions<sup>(1)</sup>, dry

$$Q_s = \frac{2.325 \times V_s \times A_s \times M_d \times P_s}{1} = \text{Nm}^3/\text{min.}$$

9. Stack gas volumetric flow rate at stack conditions

$$Q_a = \frac{2.59 \times Q_s (T_s + 273)}{P_s \times M_d} = \text{Am}^3/\text{min.}$$

10. Percent isokinetic

$$\%I = \frac{54,120 \times (\bar{T}_s + 273) \times V_{m\text{std}}}{V_s \times T_t \times P_s \times M_d \times (D_n)^2} = \%$$

11. Particulate concentration at standard conditions<sup>(1)</sup>, dry,  
based on probe, cyclone and filter catch

$$C_{sf} = \frac{m_f}{V_{m\text{std}}} = \text{mg/Nm}^3$$

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12. Particulate concentration at standard conditions (1), dry, based on total catch

$$C_{st} = \frac{m_t}{V_{m_{std}}} = \text{mg/Nm}^3$$

13. Particulate concentration at stack conditions, based on probe, cyclone, and filter catch

$$C_{af} = \frac{0.3855 \times C_{sf} \times P_s \times M_d}{T_s + 273} = \text{mg/Am}^3$$

14. Particulate concentration at stack conditions, based on total catch

$$C_{at} = \frac{0.3855 \times C_{sf} \times P_s \times M_d}{T_s + 273} = \text{mg/Am}^3$$

15. Particulate emission rate, based on probe, cyclone, and filter catch

$$E_f = 1,000,000 \times C_{sf} \times Q_s = \text{kg/hr.}$$

16. Particulate emission rate, based on total catch

$$E_t = 1,000,000 \times C_{st} \times Q_s = \text{kg/hr.}$$

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- 17. Particulate emission rate on a process basis, probe, cyclone, and filter catch

$$PF_f = \frac{E_f}{P_u}$$

- 18. Particulate emission rate on a process basis, total catch

$$PE_t = \frac{E_t}{P_u}$$

- 19. Particulate emission rate, part per million

$$PPM = \frac{M_t}{V_{m_{std}}(NM^3)} \times \frac{22,0226}{MW(c)}$$

---

(1) Standard conditions: 20 C, 760 mm. Hg.

(2)  $\sqrt{\Delta P_s \times (T_s + 273)}$  is determined by averaging the square root of the product of the velocity head ( $\Delta P_s$ ) and the absolute stack temperature ( $T_s + 273$ ) at each sampling point.

SECTION 6  
APPENDIX C

Daily Activity Log

5

## Daily Activity Log

9/17/79 - Arrived on site. Met with plant personnel. Were briefed on safety and security. Began setting up equipment.

9/18/79 - Ran test number one for Particulates, BaP, Benzene, and CO.

9/19/79 - Ran test number two for Particulate, BaP, Benzene, and CO. Had trouble with particulate test. Broken probe liner in middle of inlet particulate test.

9/20/79 Ran test number three for Particulate, BaP, Benzene, and CO.

9/21/79 Ran fourth test for particulates to replace test aborted on 9/19/79. Also ran Benzene and Co. packed up equipment and left site.

## APPENDIX D

### PROCESS DATA \*

\* Note - Data is grouped by Date (Test Number). For each data, the information is presented in the following order:

#### Tables

1. Record of Pushes and Charges
2. Process Operating Data
3. Filter Operating Data
4. Notes
5. Analysis of Coal and COG fuel gas
6. Battery Temperature Record

#### Figures (Circular Charts)

1. Fuel Gas Pressure (Reading x 4 = mm H<sub>2</sub>O)
2. C.S. Stack Draft (mm H<sub>2</sub>O)
3. P.S. Stack Draft (mm H<sub>2</sub>O)
4. P.S. Collecting Main Pressure (mm H<sub>2</sub>O)
5. C.S. Collecting Main Pressure (mm H<sub>2</sub>O)

TEST NO. 1

September 18, 1979 (and September 19, 1979)\*

\* Note - Test No. 1 was conducted on the afternoon of 9/18/79, and continued the morning of 9/19/79. See charts for 9/19/79 in the next section (Test No. 2).



Facility  
 Dates: 7/15/79

Heater Room

Time	Stack Draft mm H <sub>2</sub> O	Fuel Press. mm H <sub>2</sub> O	Temperatures °C				Oxygen Collector Analysis				
			PreHT		Washit		Cell Moist				
			After boiler Hot in service	Before	PS	CS	PS	CS	PS	CS	
10:47	22	26	170	40	41	270	265	85	83	7.0	7.0
			<i>Lowest pressure during lunch break</i>								
11:57	22	25	170	40	41	270	270	85	84	7.0	7.0
12:57	22	25	352	41	41	260	270	84	82	7.0	7.0
1:53	22	25	352	41	41	265	267	85	83	7.5	7.0
2:56	22	25	352	41	41	270	270	88	85	7.5	7.0
3:55	22	26	352	41	41	269	270	88	82	7.5	7.0
4:35	22	25	352	41	42	280	270	90	84	7.5	7.0
7:45 am	21	27	352	41	41	270	267	90	87	8.0	7.0
				7/19/79 Commissioning of Run No. 1							
11:50	22	26	352	44	45	270	268	91	86	8.0	7.0
12:55	22	25	352	45	45	272	271	96	86	8.0	7.5

Run on 7 min + 37 min per the hour

D-4

Note, Fuel Gas Flowmeter was being bypassed - No Readings

4/18/79

Filter Instruments

Time	Manometers, in.w.c.					Total ΔP in.w.c.	Inlet Temp °F	Inlet Draft mm H <sub>2</sub> O	Fan Load amps	Trans P. Log C. 11
	1	2	3	4	5					
1:05	cand bleed - condense gel in 20 like readings									
1:50	5.6	5.0	4.6	5.5	4.1	8.2	47.5	31	20	11
2:50	5.4	5.3	4.8	5.8	4.4	8.5	47.5	31	20	11
<del>1:50</del> 1:50	5.6	<del>5.0</del> 5.2	4.8	5.7	4.4	8.6	47.5	32	20	11
2:50	6.0	5.4	4.9	5.8	4.5	8.5	47.5	29	20	11
3:50	6.0	5.4	4.9	5.9	4.5	8.8	47.5	31	20	11
4:30	5.4	5.3	4.9	5.8	4.5	8.4	47.5	30	20	11
	7/19/79 Continuation of Run 461									
8:45 am	6.1	5.5	5.1	6.0	4.7	8.5	47.5	29	20	11
9:45 am	5.7	5.1	4.8	5.7	4.5	8.4	480	30	20	11
10:50 am	5.4	5.3	4.9	5.8	4.6	8.4	480	29	20	11

Date: June 9/18/79

Notes

This is supposed to be the first test day.

Ovens are numbered 51-59, 61-69, 71-79, 81-89, 91-99

Ovens permanently out of service are:

83, 85, 95, 87, 97, 92, 64, 74, 94, 86, 68, 98

9:10 am - Filter is in a cleaning cycle.

Checked the dust discharge chute and can see more dust being discharged into collecting bin.

10:20 am Put box under <sup>dust</sup> discharge chute for B-C filter  
next cleaning cycle is at 11:00 am for B filter  
Removed box at 3:10 weighed 14 lbs of dust.  
(2.9 lbs/hr)

1:45 Filter is in a cleaning cycle

3:00 Looked in flue caps on No 89 oven  
Flue 13<sup>th</sup> PS, <sup>in</sup> wall 89, were already leaking

See Mike Gardner or Mr. Biddlow for copies of charts

4:30 pm Frank Clay says he has decided to stop the run  
about 3/4 done, and finish it up tomorrow morning

8:30 am 7/19/79 In for continuation of Run No 1

9:00 am 7/19 Put dust bucket under B-C filter dust discharge line

9:30 am Restarted continuation of No 1 run

10:05 am Finished " " "

6 ovens are out of service <sup>D-6</sup> on C battery  
Fuel gas meter is also bypassed

Heater room operator estimates that fuel gas usage would  
be 220,000 SCFH which is the max that they can get regardless  
of how many ovens are in service

Sample #1  
Sample #2

9/18/79

Coke Oven Gas Analysis.

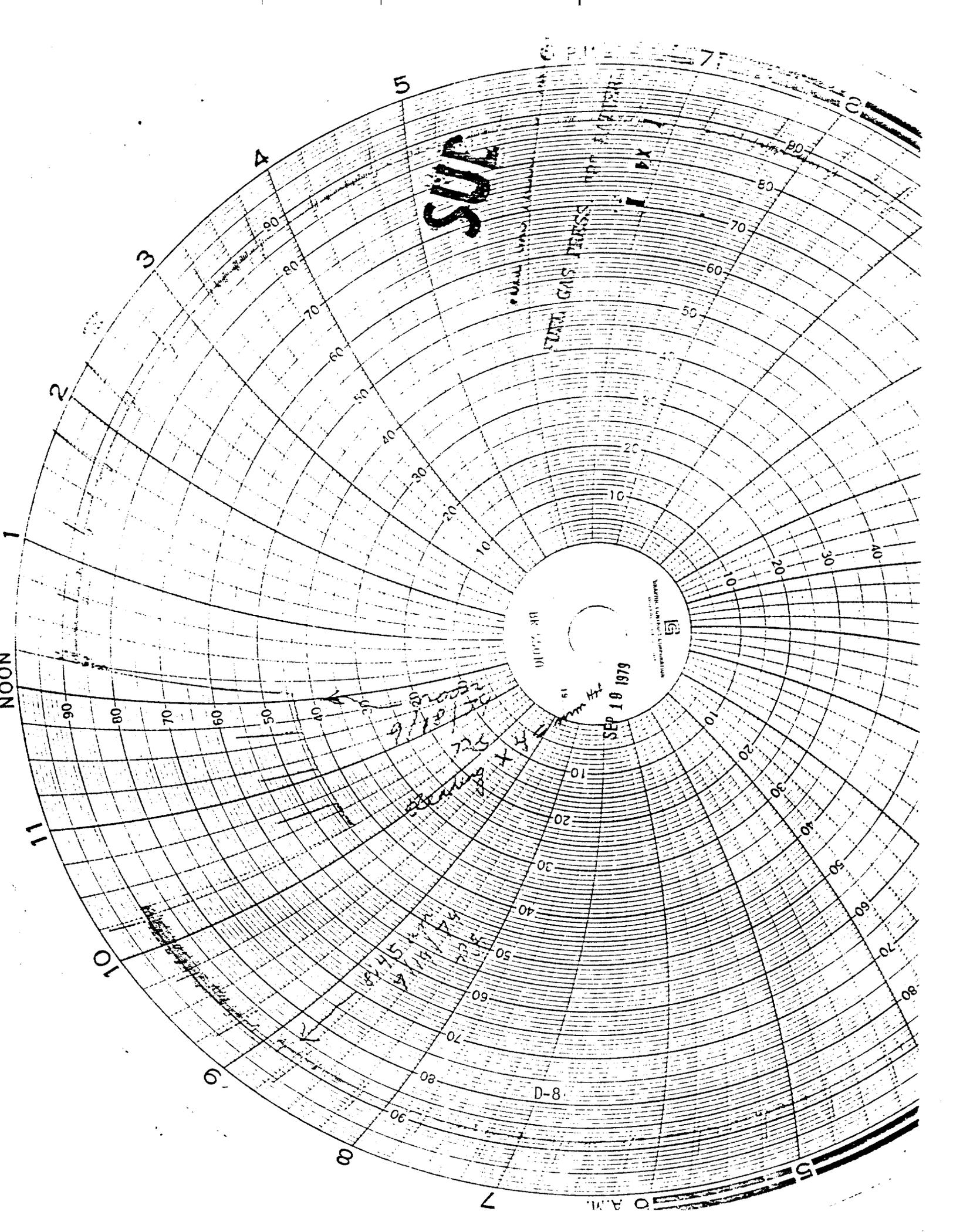
- CO<sub>2</sub> = 2.8%
- Hydrocarbons = 4.4%
- O<sub>2</sub> = 1.8%
- CO = 8.4%
- H<sub>2</sub> = 41.0%
- CH<sub>4</sub> = 25.6%
- N<sub>2</sub> = 16.0%

9/18/79 Coal Mix for Battery "B"

1975 avg.

- Sunnyside = 30% H.V.C. 2.67 d, 46.7 VM, 6.2 A, 7.2 H<sub>2</sub>
- York Canyon = 41% H.V.C. 2.47 d, 36.9 VM, 8.1 A, 6.3 H<sub>2</sub>
- Coal Basin = 21% H.V.C. 0.54 d, 34.4 VM, 7.5 A, 6.4 H<sub>2</sub>
- Petrochem Coke = 8% H.V.C. 1.66 d, 11.3 VM, 6.3 A, 8.4 H<sub>2</sub>

No analysis of mix available for 9/18/79  
due to equipment failure.



**SUR**

BR 25010

SEP 10 1979

D-8

NOON

2

3

4

5

6

7

8

11

10

9

8

7

6

0 A.M.

90

80

70

60

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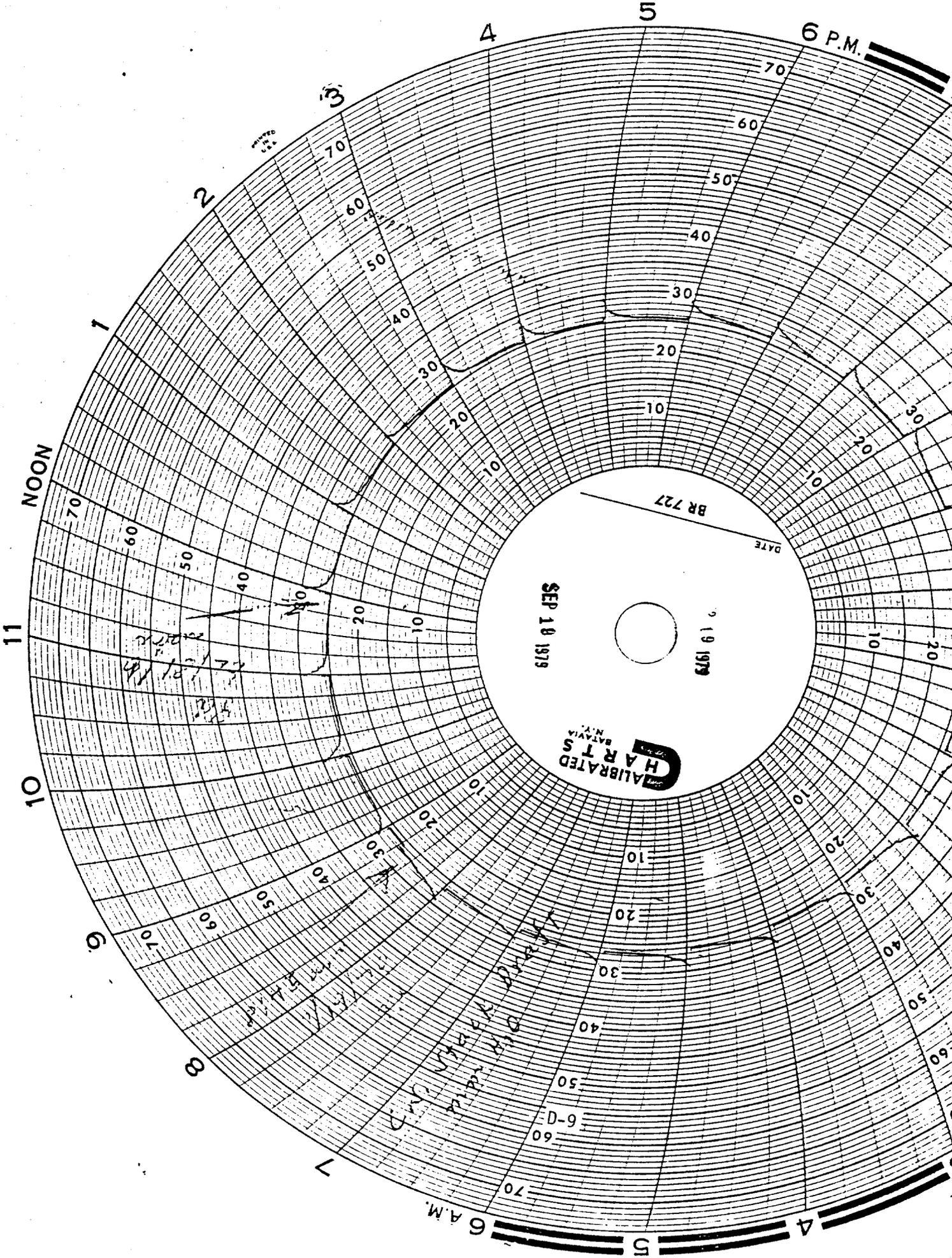
20

30

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50

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6 P.M.

4

5

3

2

1

NOON

11

10

9

8

7

6 A.M.

DATE

BR 727

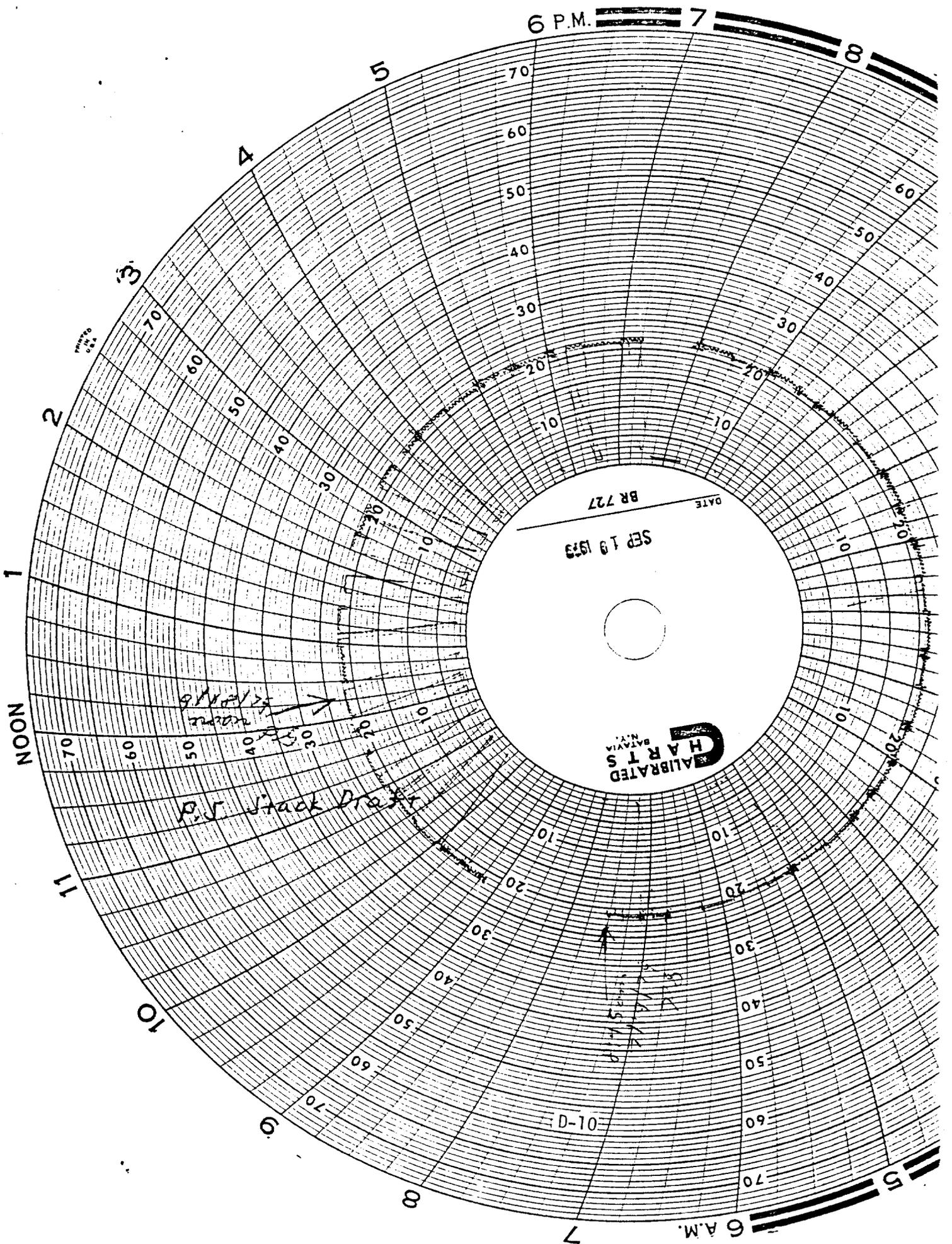
SEP 18 1979

9 19 1979

CALIBRATED CHARTS BATAVIA N.Y.

Handwritten notes: 22/21/18, 22/21/18, 22/21/18

Handwritten notes: 22/21/18, 22/21/18, 22/21/18



6 P.M. 7 8

1 2 3 4 5

NOON

11

10

9

8

7

6 A.M.

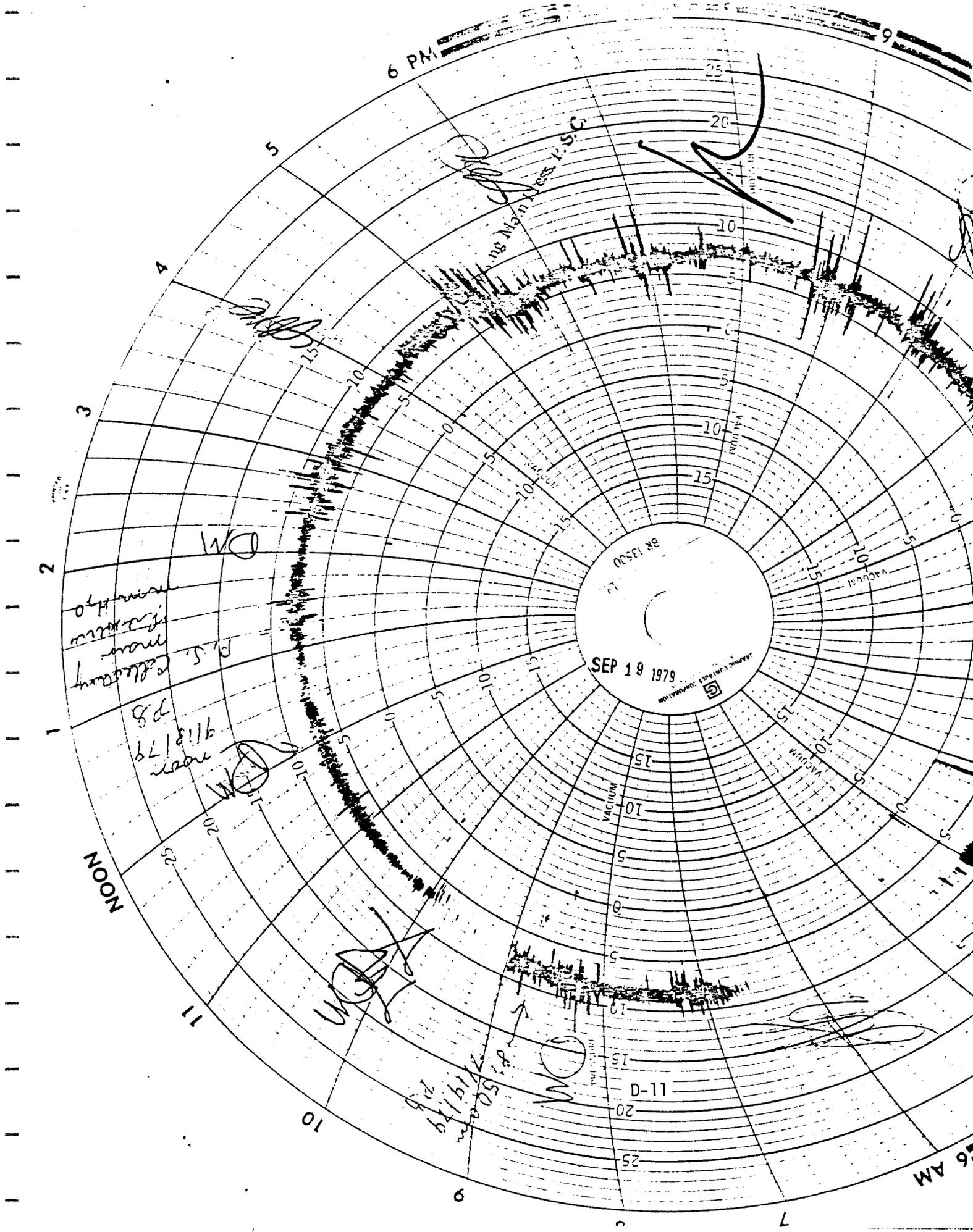
DATE  
SEP 19 1953  
BR 727

CALIBRATED  
HARTS  
PATENT

P.S. Stack Draft

9.11/18  
10.00/18

D-10



6 PM

9

5

4

3

2

1

NOON

11

10

9

7

6 AM

25

20

10

10

15

15

10

15

10

5

5

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10

15

20

25

10g Alum Press P-5C

DM

P.S. Cellulose  
more  
9/18/79

more  
9/18/79

DM

DM

9/20/79  
9/21/79  
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12/29/79  
12/30/79

SEP 19 1979

EX 13500

VACUUM GAUGE  
MILITARY GRADE  
EX 13500

11-D



COPE OVEN SPAN AND BATTERY CROSS ALL TEMPERATURES

READER: *Martin*

DATE: *9-18-79*

TIME: *2:15*

"A" BATTERY FLUE TEMPERATURES				"B" BATTERY FLUE TEMPERATURES				WALL NUMBER		WALL NUMBER	
PUSHER SIDE		Wall No.	COKE SIDE		PUSHER SIDE		Wall No.	COKE SIDE		PS	PS
24		T	34		50		51	10		27	28
xxx	25	2	xxx	31	xxx	29	52	xxx	25	SM	SM
		3		35		29			29	09	85
24		4	26		32		54	30	xxx	14	90
32	xxx	5	23	xxx	28	xxx	55			15	93
		6		22		34				DUT	98
xxx	32	7	xxx	27	xxx	30	56	xxx	32	20	75
		8		26		33			26	20	96
35		9	15		37		58	26	xxx	22	94
16	xxx	10	xxx	03	xxx	33	59	30		25	96
		11		26		27				28	98
xxx	25	12	xxx	26	xxx	27	61	xxx	28	31	00
		13		22		27			28	31	00
24		14	22		22		63	26	xxx	31	00
27	xxx	15	30	xxx	20	xxx	64	3		31	00
		16		33		23			23	31	00
xxx	31	17	xxx	33	xxx	20	66	xxx	23	31	00
19		18	27		25		67	31	xxx	31	00
04	xxx	19	10	xxx	25	xxx	68	14		31	00
		20		33		22			19	31	00
xxx	34	21	xxx	28	xxx	15	71	xxx	21	31	00
		22		31		15			31	31	00
35		23	29		15		72	31	xxx	30	00
32	xxx	24	xxx	34	xxx	23	73	23		27	01
		25		24		31			14	27	01
xxx	25	26	xxx	24	xxx	31	75	xxx	22	28	02
		27		30		30			27	28	02
14		28	25		35		77	32	xxx	28	05
		29		09		25			20	TAR	02
xxx	90	30	xxx	95	xxx	29	79	20	20	TAR	05
		31		00		25			20	TAR	05
88		32	xxx	08	xxx	19	81	xxx	xxx	27	08
10	xxx	33		16	xxx	24	82	15		27	08
		34		21		31			26	24	98
xxx	14	35	xxx	21	xxx	31	84	xxx	38	21	92
		36		24		10			21	20	89
28		37	24		92		86	19	xxx	15	75
18	xxx	38	15	xxx	20	xxx	87	xxx	90	12	59
		39		20		90			31	01	63
xxx	20	40	NIA	1090	xxx	30	88	xxx	31		
		41	SM			25			29		
16	xxx	42	xxx		xxx	30	89	29	xxx		
		43		31		30		32	xxx		
xxx	98	44	xxx	31	xxx	55	91	xxx	33		
		45		02		32			25		
20	xxx	46	21	xxx	24	xxx	92	xxx	xxx		
25		47	18		09		93	24			
		48		16		28		06			
xxx	27	49	xxx	12	xxx	28	94	xxx	28		
		50		01		25			24		
00	xxx	51	01	xxx	95	xxx	95	D-13	xxx		
92		52	96		20		96	03	xxx		
		53		70		30		22			
280	273	"A"	260	260	263	264	"B"	261	278		
2276 (2248)			2260		2263 (2266)		2269				

REMARKS:

COKE OVEN SPAN AND BATTERY CROSSWALL TEMPERATURES

MARKING: *Marking*

DATE: *9-19-79*

TIME: *1:45 AM '79*

"A" BATTERY FLUE TEMPERATURES					"B" BATTERY FLUE TEMPERATURES					WALL NUMBER	
PUSHER SIDE	Wall No.	COKE SIDE	PUSHER SIDE	Wall No.	COKE SIDE	PS #29	PS 31				
29	T	24	25	15		1 OUT	1 OUT				
xxx	2	xxx	26	22		2 62	2 OUT				
	3	30	27	34	chxxx	3 77	3 63				
32	Q	xxx	SM	54	55	4 82	4 78				
39	T	27	27	55	56	5 85	5 85				
xxx	4	22	xxx	56	36	6 90	6 90				
	5	23	xxx	57	31	7 95	7 95				
34	5	23	32	58	20	8 93	8 12				
19	6	17	34	59	30	9 85	9 90				
xxx	7	xxx	xxx	60	xxx	10 85	10 93				
	8	04	xxx	61	34	11 92	11 94				
21	T	29	23	62	31	12 75	12 96				
xxx	9	36	xxx	63	xxx	13 95	13 97				
35	10	30	28	64	27	14 97	14 95				
xxx	11	37	xxx	65	34	15 98	15 98				
17	12	24	xxx	66	29	16 98	16 02				
02	13	09	xxx	67	xxx	17 97	17 00				
xxx	14	31	xxx	68	15	18 01	18 01				
	15	25	xxx	69	35	19 00	19 00				
35	16	33	15	70	xxx	20 01	20 01				
29	17	27	19	71	24	21 97	21 97				
xxx	18	23	xxx	72	21	22 97	22 97				
25	19	24	xxx	73	19	23 92	23 92				
19	20	25	29	74	xxx	24 58	24 88				
xxx	21	xxx	30	75	26	25 75	25 80				
95	22	01	xxx	76	24	26 58	26 14				
SM	23	10	30	77	26	27 45	27 60				
xxx	24	03	25	78	xxx						
	25	11	xxx	79	24						
01	26	22	30	80	20						
SM	27	xxx	20	81	20						
10	28	05	xxx	82	20						
xxx	29	25	80	83	20						
	30	2	58	84	20						
22	31	30	23	85	20						
20	32	xxx	31	86	20						
xxx	33	27	xxx	87	20						
	34	07	xxx	88	20						
15	35	20	26	89	20						
26	36	26	03	90	20						
xxx	37	24	14	91	20						
	38	23	01	92	20						
95	39	98	98	93	20						
85	40	85	18	94	20						
	41	80	32	95	20						
297	232	247	252	262	260	"B"	255 278				
2264	(2256)	2249	2261	(2263)	2266						

REMARKS:

Both walls off

ONE GIVEN SPAN AND BATTERY CROSSL WALL TEMPERATURES

W.M.H

DATE: 9-18-79

TIME: 8:15 AM

"A" BATTERY FLUE TEMPERATURES					"B" BATTERY FLUE TEMPERATURES					WALL NUMBER		WALL NUMBER	
70	68	Wall No.	47	79	70		Wall No.	50		PS	73	PS	74
PUSHER SIDE			COKE SIDE		PUSHER SIDE			COKE SIDE					
20		1	34		90		(5)	17		1	65	1	80
xxx	25	2	xxx	32	xxx	07	52	xxx	29	2	80	2	90
	7	3		28		37	(53)		42	3	84	3	06
22	xxx	(4)	20	xxx	28	xxx	54	38	xxx	4	82	4	15
45		5	31		37		55	44		5	86	5	21
xxx	43	6	xxx	26	xxx	41	56	xxx	43	6	02	6	21
	25	7				33	57		29	7	03	7	25
38	xxx	8	22	xxx	31	xxx	58	15	xxx	8	05	8	26
03		(9)	05		38		59	33		9	07	9	26
xxx	95	(10)	xxx	95	xxx	38	61	xxx	35	10	10	10	25
	23	12		33		25	62		35	11	95	11	27
27	xxx	13	25	xxx	20	xxx	63	25	xxx	12	93	12	28
26		14	28		15		(64)	22		13	96	13	29
xxx	37	15	xxx	37	xxx	17	65	xxx	36	14	03	14	29
	36	16		35		21	66		26	15	96	15	
13	xxx	(17)	18	xxx	30	xxx	67	15	xxx	16	96	16	
90		(18)	00		27		(68)	10		17	03	17	
xxx	26	19	xxx	35	xxx	23	69	xxx	10	18	96	18	
	34	21		29		19	71		35	19	03	19	
33	xxx	22	27	xxx	13	xxx	72	37	xxx	20	96	20	25
92		(23)	42		03		73	21		21	92	21	23
xxx	43	24	xxx	42	xxx	25	(74)	xxx	15	22	92	22	
	33	25		28		47			31	23	96	23	21
28	xxx	26	29	xxx	35	xxx	76	21	xxx	24	73	24	16
17		27	21		35		77	34		25	86	25	00
xxx	43	(28)	xxx	28	xxx	30	78	xxx	37	26	06	26	05
	97	(29)		07		25	79		14	27	92	27	14
95	xxx	(30)	07	xxx	22	xxx	81	10	xxx	28	92	28	14
04		32	13		18		82	10		29	12	29	18
xxx	15	33	xxx	31	xxx	36	(83)	xxx	30	30	15	30	22
	28	34		37		37	84		42	31	15	31	22
26	xxx	(35)	28	xxx	05	xxx	(85)	22	xxx	32	10	32	22
11		(36)	07		95		(86)	00		33	14	33	26
xxx	21	37	xxx	15	xxx	47	(87)	xxx	00	34	19	34	25
	36	38		30		25	88		27	35	14	35	26
25	xxx	(39)	38	xxx	19	xxx	89	29	xxx	36	14	36	26
16		41	36		28		91	32		37	11	37	18
xxx	28	(42)	xxx	32	xxx	36	(92)	xxx	32	38	11	38	
	27	(43)		06		37	93		28	39	14	39	
18	xxx	44	20	xxx	24	xxx	(94)	25	xxx	40	14	40	
28		45	25		00		(95)	98		41	19	41	
xxx	31	46	xxx	14	xxx	22	96	23		42	19	42	
	18	(47)		05		22	(97)	D-15	32	43	19	43	
06	xxx	(48)	02	xxx	92	xxx	(98)	97	xxx	44	86	44	
86		(49)	93		13		99	24		45	76	45	
	76	(50)		80		36	(10)		31	46	76	46	
254	319	"A"	252	297	253	285	"B"	253	307				
2287			2275		2269			2280					

REMARKS:

COKE OVEN SPAN AND BATTERY CROSSWALL TEMPERATURES

REG. 1048 F-1

READER: TATUM

DATE: 9-18-79

TIME: 10:45

"A" BATTERY FLUE TEMPERATURES				"B" BATTERY FLUE TEMPERATURES				WALL NUMBER		WALL NUMBER	
PUSHER SIDE	Wall No.	COKE SIDE		PUSHER SIDE	Wall No.	COKE SIDE		PS #2	PS #13		
27		32		14	51	07		1 15'	1 FIRE		
xxx	31	xxx	38	xxx	21	xxx	22	2 23	2 FIRE		
	28		27		30		34	3 20	3 17		
23	xxx	23	xxx	30	xxx	41	xxx	4 99	4 23		
24		23		17	xxx	21		5 21	5 26		
xxx	34	xxx	34	xxx	41	xxx	41	6 28	6 26		
	34		33		35		30	7 28	7 24		
33	xxx	24	xxx	36	xxx	21	xxx	8 33	8 26		
15		10		42	xxx	35		9 33	9 28		
xxx	94	xxx	90	xxx	35	xxx	30	10 33	10 25		
	21		31		40		31	11 28	11 25		
24	xxx	25	xxx	18	xxx	28	xxx	12 11	12 25		
34		32		10	xxx	15		13 33	13 22		
xxx	31	xxx	32	xxx	05	xxx	23	14 33	14 20		
	31		32		20		23	CS	CS		
21	xxx	20	xxx	27	xxx	17	xxx	14 34	14 20		
90		08		17	xxx	05		13 34	13 98		
xxx	20	xxx	28	xxx	10	xxx	06	12 36	12 17		
	31		28		10		32	11 36	11 25		
34	xxx	30	xxx	17	xxx	43	xxx	10 38	10 26		
	34		35		09			9 38	9 28		
xxx	39	xxx	40	xxx	14	xxx	09	8 24	8 29		
	31		25		20		13	7 04	7 25		
24	xxx	26	xxx	37	xxx	24	xxx	6 95	6 26		
24		29		45	xxx	33		5 21	5 28		
xxx	23	xxx	34	xxx	30	xxx	35	4 27	4 31		
	90		93		29		17	3 27	3 32		
75	xxx	90	xxx	23	xxx	09	xxx	2 10	2 30		
08		11		23	xxx	15		1 95	1 FROZE		
xxx	98	xxx	99	xxx	33	xxx	29	REMARKS:			
	18		19		33		47				
32	xxx	24	xxx	15	xxx	23	xxx				
06		01		75	xxx	94					
xxx	11	xxx	08	xxx	25	xxx	90				
	18		18		29		29				
27	xxx	29	xxx	23	xxx	31	xxx				
17		27		25	xxx	23					
xxx	00	xxx	30	xxx	28	xxx	26				
	90		94		24		20				
19	xxx	21	xxx	17	xxx	12	xxx				
35		21		94	xxx	97					
xxx	21	xxx	09	xxx	22		22				
	21		12		22	D-16	14				
80	xxx	90	xxx	94	xxx	01	xxx				
75		80		13	xxx	20					
	75		72		29		24				
260	274	"A"	255 260	261 290	"B"	255 304					
2268			2258	2276		2280					

TEST NO. 2 \*

September 19, 1979 \*

\* Note - Test No. 2 on 9/19/79 did not produce a valid method 5 test due to a broken probe liner, although other tests (e.g., BaP) were successfully completed. Therefore, the No.2 Method 5 test was carried out on 9/21/79.

Test No 2 \*

Sept 19, 1979 \*

\* NO. 2 - Test No 2 on 9/19/79 did not produce a valid method 5 test due to a broken probe lens, although observations (e.g. FAT) were successfully completed. Therefore, the No 2 method 5 test was carried out on 9/21/79.



Date: <sup>Wed</sup> 9/14/74

Heater Room

Time	Stack Draft		Fuel Press. mm H <sub>2</sub> O	Temperatures °C						Oxygen Collector	
	mm H <sub>2</sub> O			PreHT		Warr HT		Cell Man		Pressure	
	PS	CS		After	Before	FS	CS	FS	CS	PS	CS
2:57	25	25	352	47	47	271	270	102	84	7.5	7.5
3:00	<sup>max</sup> 22	25	352	47	47	275	273	97	82	8.0	5.0
3:53	22	25	352	47	47	271	270	105	84	Not Read	
4:00	22	27	352	47	47	272	270	105	85	8.0	-7.5
4:40	<sup>min</sup> 22	26	352	47	47	280	272	110	90	8.0	7.0

Below data is for 9/14/74  
 Test No. 2 (incl. including marked 5) - see notes

Note: Fuel Gas Flowmeter was being bypassed - No Readings

W. M.  
Date - 9/14/74

FILTER INSTRUMENTS

Time	Manometers, in. w.c.					Total LP in. w.c.	Inlet Temp °F	Inlet Draft in. w.c.	Fan Load amps	Fan % Output
	1	2	3	4	5					
12:47	5.8	5.2	4.9	5.7	4.5	8.4	480	29	20	11
1:45	5.8	5.3	4.8	5.7	4.4	8.3	480	28	20	11
2:48	5.7	5.1	4.7	5.6	4.2	8.3	480	29	20	11
3:55	6.0	5.4	4.9	5.9	4.5	8.4	480	30	20	11
4:50 pm	6.0	5.3	4.9	5.9	4.4	8.3	480	30	20	11

above data is for 9/14/74  
Test No 2 (incl. including method 5) see notes

Notes  
Run No. 2

Wed  
Date: 9/19/79

- Finished No. 1 run up this morning. Getting ready to start No. 2
- 1:45 pm Getting some visible gray emissions from C stack
- 1:50 Approx start of Run No. 2
- 2:15 pm Slight visible emissions from B stack
- 2:43 pm B baghouse is in a cleaning cycle
- 3:45 pm Had open pull flue caps in both walls of #96 oven wall #96 had ~~had~~ had leaks in #1 & #2 flues P.S. Also, several of the burners in the flues were plugged up and not burning or burning very weakly.
- 4:20 Removed dust collection bucket. Only collected a very small amount (less than 1 lb)

For this test on 9/19/79, it was found that the method 5 test was invalid (~~at~~ broken probe lines). Therefore, the data is for test No. 2 "Bu?", but not method 5. Tomorrow 9/20/79 will be test No. 3. The No. 2 method 5 test will be done on Fri 9/21/79

73

# Coke Gas Analysis - 9/19/79

	%
CO <sub>2</sub>	2.2
H <sub>2</sub>	3.6
O <sub>2</sub>	2.4
CO	4.8
H <sub>2</sub>	?
CH <sub>4</sub>	25.4
N <sub>2</sub>	?

(Reported 56.0% but suspect in error)

Analyses	% -	VM	FC	Ash	Sulf.
Coke	0.9	88.3	10.8	0.72	
Petroleum Coke	11.9	87.8	0.3	1.51	
Sunnyside	39.3	54.0	6.7	1.26	
Coal Basin	24.3	69.4	6.3	0.59	
York	36.1	56.5	7.4	0.44	
Coal Mix	32.3	61.2	6.5	0.79	

Coal Mix\* by % → 30% Sunnyside, 41% York, 21% Coal Basin, 8% Pet Coke.

D-23

\* Trying for this mix may not hit it exactly.



COKE OVEN SPAN AND BATTERY CROSSWALL TEMPERATURES

KS60 1043 R-2

FEADER:

K. SIMPSON

DATE:

9-19-79

TIME:

9:15 AM

"A" BATTERY FLUE TEMPERATURES				"B" BATTERY FLUE TEMPERATURES				WALL NUMBER		
PUSHER SIDE		Wall No.	COKE SIDE		PUSHER SIDE		COKE SIDE		PS	PS
40	77		59	50	77	103	51	70	PS	PS
28		(1)	41	<del>82</del>	34		(51)	22	75	1
xxx	25	2	NIA	(92)	xxx	32	xxx	36		2
	33	3	xxx	35	xxx	32	xxx	39		3
02		(4)	28		37		54	38		4
28	xxx	5	24	xxx	41	xxx	55	42	xxx	4
1	34	6	xxx	17	xxx	38	xxx	42	xxx	5
xxx	33	7	20		xxx	36	xxx	33		5
22	xxx	8	24	xxx	35	xxx	58	25	xxx	6
21		(9)	21		40		59	36		6
xxx	08	(11)	xxx	08	xxx	35	xxx	33		7
	29	12	xxx	41	xxx	28	xxx	41		7
33	xxx	13	27	xxx	25	xxx	63	32		8
37		14	38	xxx	16	xxx	(64)	17	xxx	8
xxx	35	15	xxx	32	xxx	08	xxx	32		9
	24	16	xxx	24	xxx	18	xxx	22		9
20	xxx	(17)	34	xxx	26	xxx	67	18	xxx	10
02		(18)	09		21		(68)	12		10
xxx	24	19	xxx	21	xxx	27	xxx	28		11
	34	21	xxx	24	xxx	22	xxx	34		11
39	xxx	22	27	xxx	24	xxx	72	43	xxx	12
40		(23)	38		24		73	28		12
xxx	34	24	xxx	28	xxx	24	(74)	xxx	21	13
	32	25	xxx	21	xxx	29	75	21	21	13
22	xxx	26	25	xxx	38	xxx	76	21	xxx	14
23		(27)	25		29		77	30		14
xxx	95	(28)	xxx	13	xxx	33	78	xxx	32	10
	94	(29)	xxx	04	xxx	35	79	xxx	20	9
84	xxx	(31)	14	xxx	25	xxx	81	43	xxx	9
20		32	18	xxx	31	xxx	82	21	xxx	8
xxx	19	33	xxx	27	xxx	45	(83)	xxx	36	7
	24	34	xxx	27	xxx	27	84	xxx	38	7
31	xxx	(35)	25	xxx	02	xxx	(85)	18	xxx	6
98		(36)	03		82		(86)	26		6
xxx	17	37	xxx	16	xxx	28	(87)	xxx	28	5
	33	38	xxx	20	xxx	26	(88)	xxx	29	5
42	xxx	39	36	xxx	24	xxx	89	40	xxx	4
21		41	32		29		91	23		4
xxx	96	(42)	xxx	26	xxx	35	(92)	xxx	28	3
	91	(43)	xxx	06	xxx	29	93	xxx	24	3
32	xxx	44	06	xxx	15	xxx	(94)	25	xxx	2
34		45	22		92	D-25	(95)	27		2
xxx	27	46	xxx	02	xxx	18	96	xxx	16	1
	31	(47)	xxx	12	xxx	13	(97)	xxx	04	1
96	xxx	(48)	93	xxx	86	xxx	(98)	94	xxx	
76		(49)	77		22		99	31		
	68	(51)	67		41		(100)	32		
300	292	"A"	245	240	300	278	"B"	316	306	
2296			2242		2289			2311		

REMARKS:

COKE OVEN SPAN AND BATTERY CROSS ALL TEMPERATURES

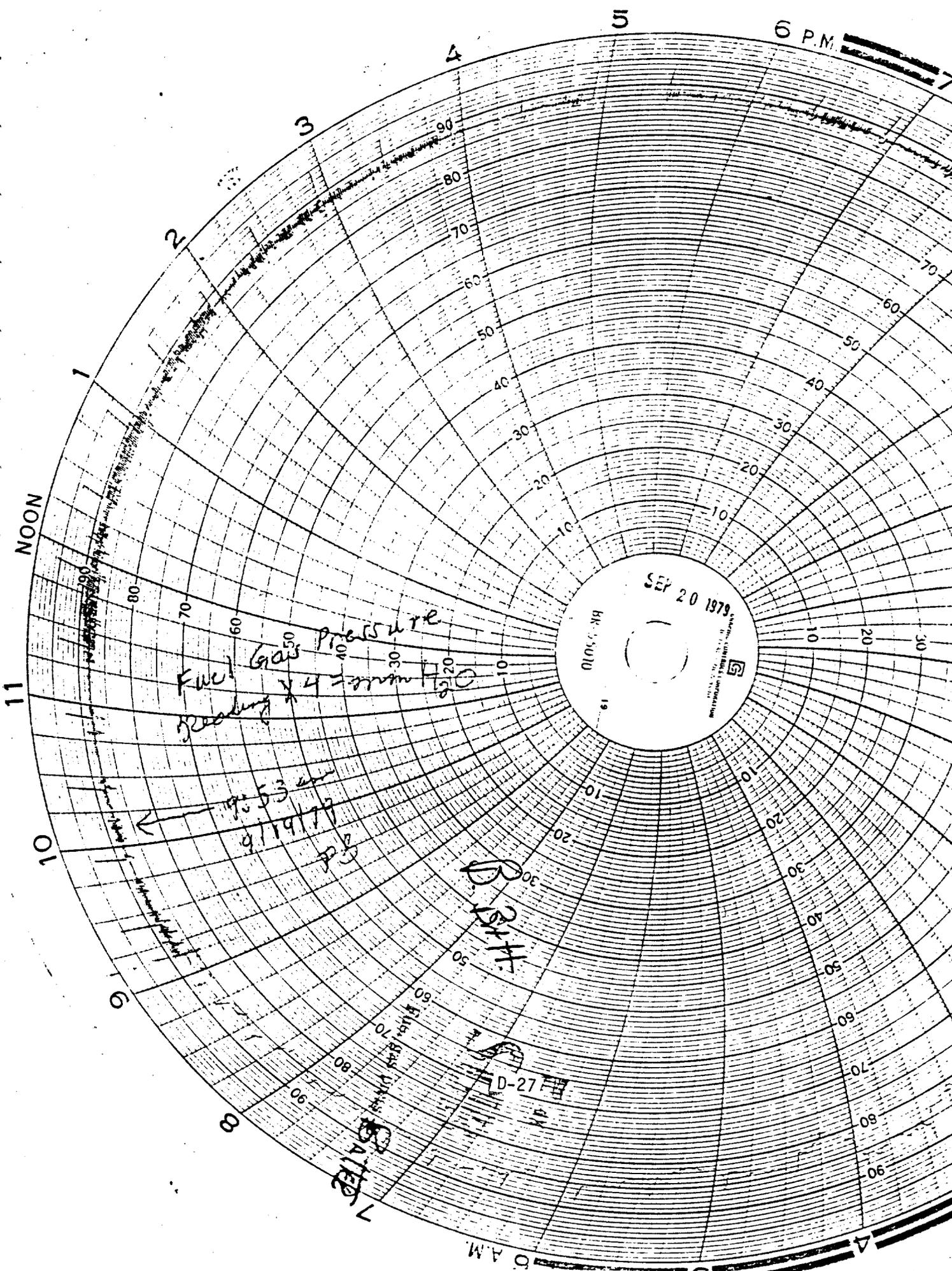
KS60 1043 R-2

READER: Martin

DATE: 9-20-79

TIME: 1:15

"A" BATTERY FLUE TEMPERATURES				"B" BATTERY FLUE TEMPERATURES				WALL NUMBER		WALL NUMBER	
PS	WALL No.	PUSHER SIDE	COKE SIDE	PS	WALL No.	PUSHER SIDE	COKE SIDE	PS	WALL No.	PUSHER SIDE	COKE SIDE
45	42	T	33	182	101	51	28	#38	38	PS	38
28	2	xxx	34	39	52	xxx	33	1	2	1	LEAK
xxx	3	xxx	31	xxx	53	xxx	37	2	2	2	76
26	4	xxx	31	25	54	xxx	32	3	3	3	90
36	5	xxx	27	28	55	xxx	34	4	4	4	00
xxx	6	xxx	28	xxx	56	xxx	36	5	5	5	09
35	7	xxx	25	32	57	xxx	26	6	6	6	14
11	8	xxx	17	39	58	xxx	76	7	7	7	19
xxx	9	xxx	13	xxx	59	xxx	37	8	8	8	17
28	10	xxx	34	41	61	xxx	34	9	9	9	16
36	11	xxx	35	25	62	xxx	25	10	10	10	10
xxx	12	xxx	30	19	63	xxx	36	11	11	11	16
27	13	xxx	26	24	64	xxx	22	12	12	12	12
07	14	xxx	19	29	65	xxx	17	13	13	13	16
xxx	15	xxx	26	xxx	66	xxx	23	14	14	14	20
35	16	xxx	33	30	67	xxx	38	CS	CS	CS	22
54	17	xxx	33	28	68	xxx	27	14	14	14	20
35	18	xxx	25	28	69	xxx	27	13	13	13	17
xxx	19	xxx	23	30	70	xxx	24	12	12	12	20
19	20	xxx	23	30	71	xxx	29	11	11	11	20
03	21	xxx	25	35	72	xxx	36	10	10	10	24
xxx	22	xxx	11	xxx	73	xxx	37	9	9	9	25
95	23	xxx	98	xxx	74	xxx	15	8	8	8	23
12	24	xxx	10	xxx	75	xxx	18	7	7	7	22
92	25	xxx	98	18	76	xxx	18	6	6	6	20
21	26	xxx	22	19	77	xxx	17	5	5	5	17
xxx	27	xxx	26	30	78	xxx	20	4	4	4	17
24	28	xxx	23	17	79	xxx	94	3	3	3	16
07	29	xxx	21	92	80	xxx	08	2	2	2	10
xxx	30	xxx	19	xxx	81	xxx	08	1	1	1	85
40	31	xxx	23	23	82	xxx	20	REMARKS:			
43	32	xxx	23	23	83	xxx	26				
98	33	xxx	03	29	84	xxx	26				
10	34	xxx	15	xxx	85	xxx	21				
xxx	35	xxx	26	23	86	xxx	01				
21	36	xxx	13	23	87	xxx	10				
xxx	37	xxx	28	99	88	xxx	07				
27	38	xxx	20	xxx	89	xxx	31				
23	39	xxx	18	85	90	xxx	27				
95	40	xxx	05	82	91	xxx	27				
85	41	xxx	82	27	92	xxx	27				
48	42	xxx	75	32	93	xxx	27				
285	311	"A"	248	274	268	284	"B"	273	301		
2298			2261		2276			2287			



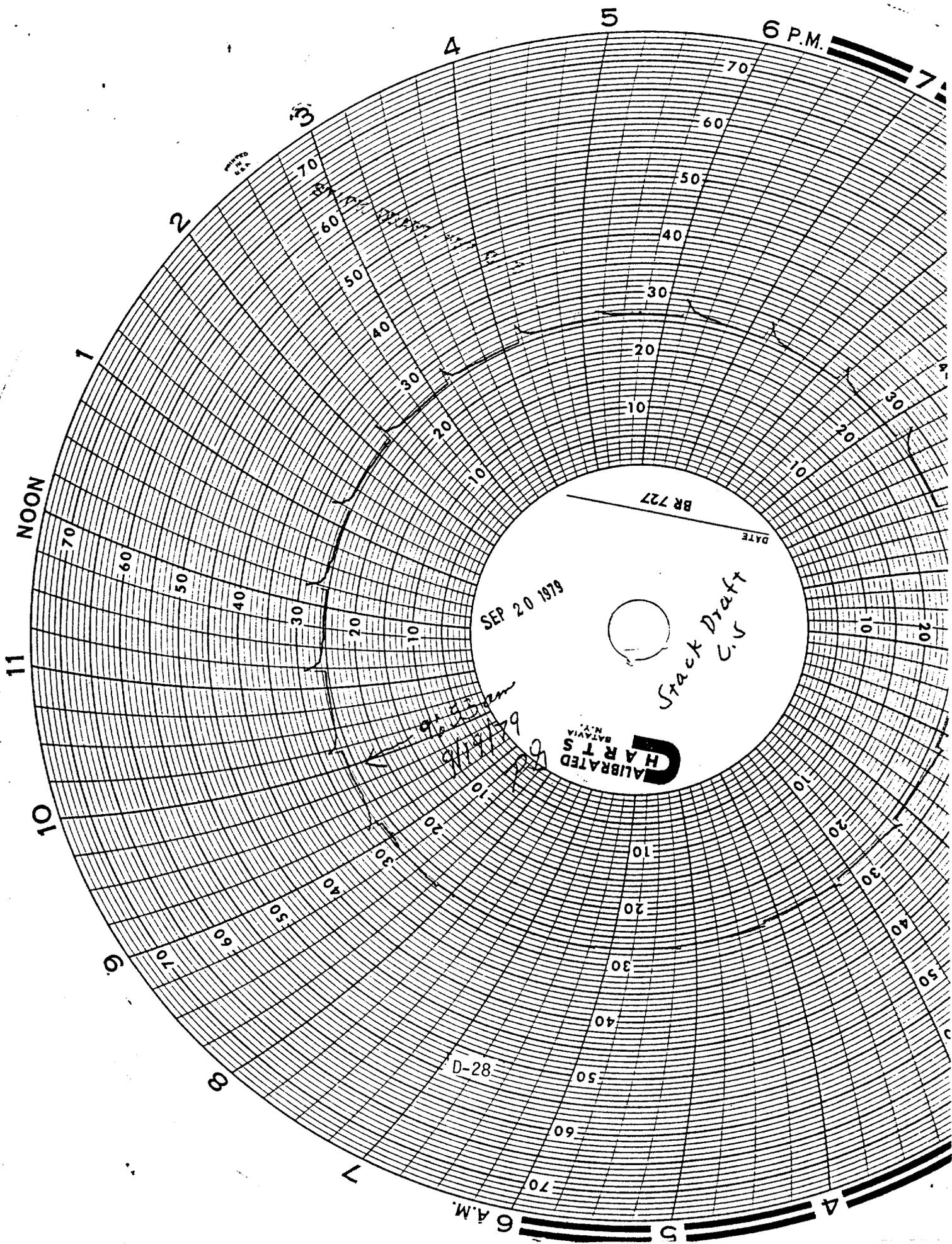
Fuel Gas Pressure  
Reading  $\times 4 = \text{mm H}_2\text{O}$

9:53 am  
9/19/79  
PB

RETT

D-27

DATA



6 A.M.

5

4

6 P.M.

7

4

5

3

2

1

NOON

11

10

9

8

7

SEP 20 1979

BR 727

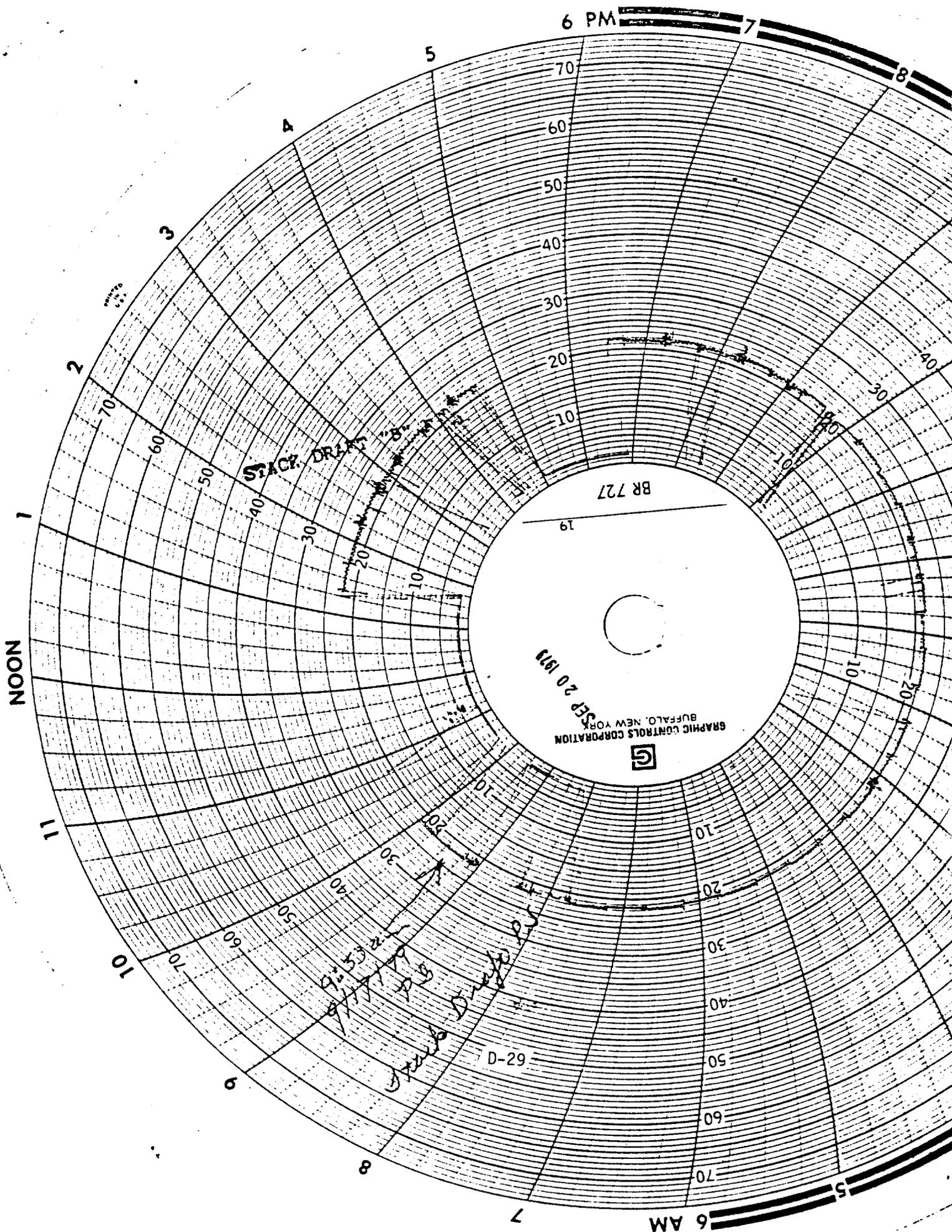
DATE

Stack Draft  
C.V.

CALIBRATED  
HARTS  
BATAVIA  
N.Y.

67-1016  
9/20/79

8-28



NOON

6 PM

6 AM

BR 727

19

SEP 20 1979

GRAPHIC CONTROLS CORPORATION

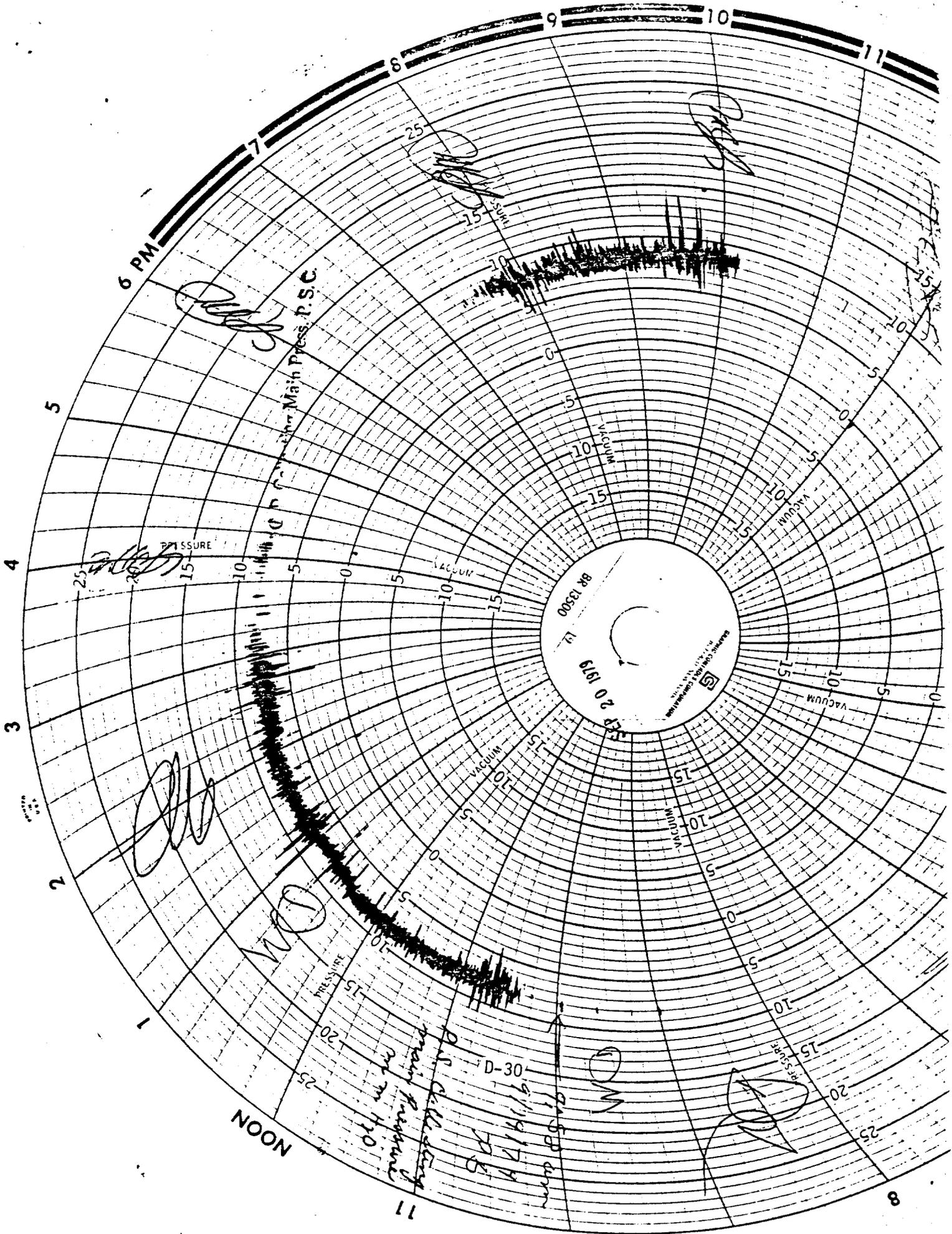
BUFFALO, NEW YORK

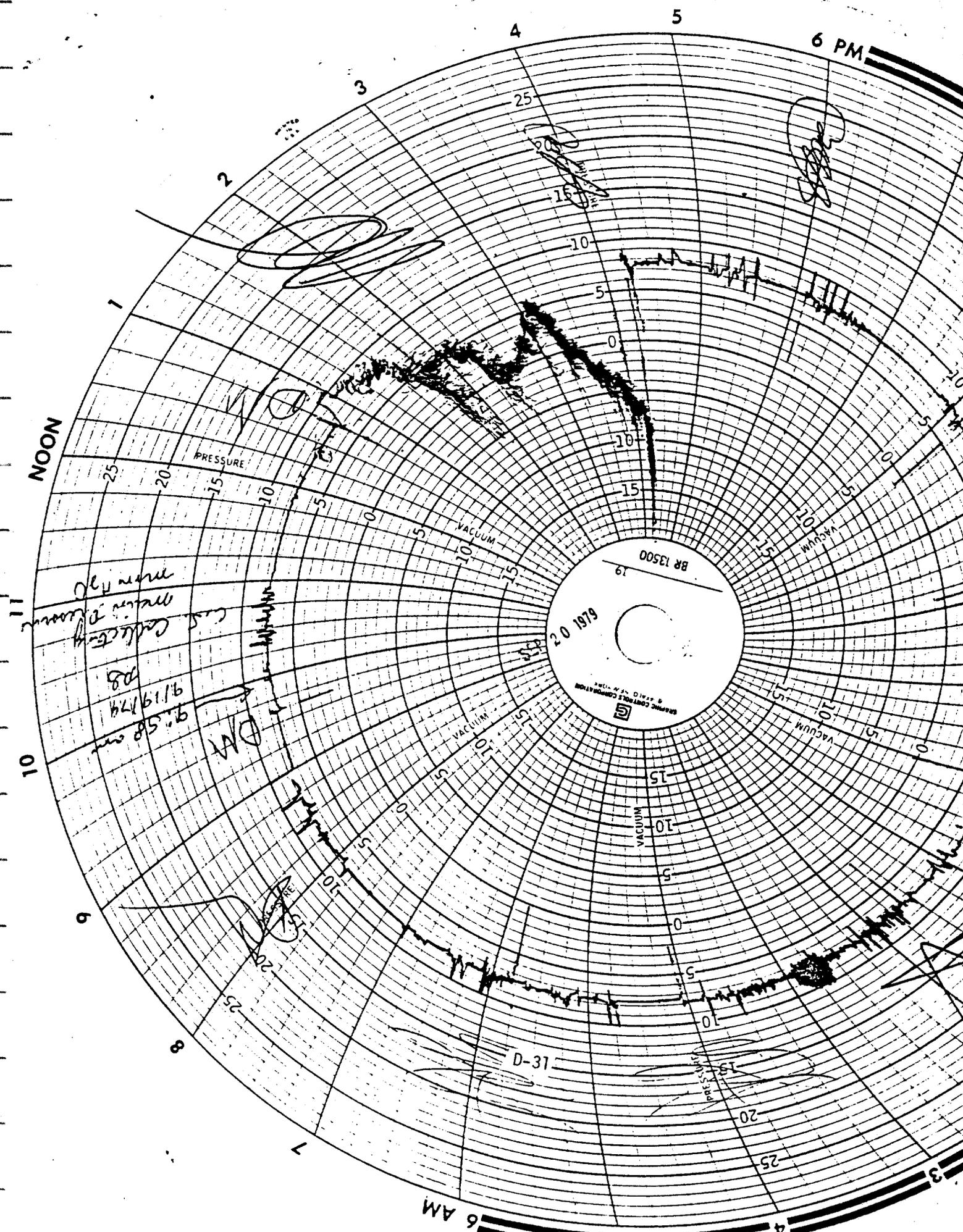


D-29

STOCK DRUGS

D-29





6 PM

5

4

3

2

1

NOON

PRESSURE

VACUUM

BR 13500

6/19/02

VACUUM

VACUUM

C/S Collecting  
main room

9/19/74

9:58 am

D-31

D-37

PRESSURE

6 AM

4

3

7

8

9

10

11

TEST NO. 3

September 20, 1979



Thurs  
Date: 4/26/74

Heater Room

manometer

Time	Stack Draft			Fuel Press. mm H <sub>2</sub> O	Temperatures °C						Oxygen			
	mm H <sub>2</sub> O				PreHT		Waste HT		Cell Man		PS	C		
	PS	CS			After	Before	PS	CS	PS	CS	PS	C		
<del>1:03</del>	PS	CS												
1:03	21	22	20	3.52	41	42	276	274	87	85			PS ↓	C ↓
2:04	22	25	20	3.52	41	42	274	271	86	85 17:25			Not P.C	Read P.C
1:06	22	25	18	3.52	42	43	271	269	86	86			4.0	8.0
1:58	22	25	19	3.52	44	44	270	268	84	85			8.5	7.0
2:50	22	25	19	3.52	43	43	268	265	83	84			8.5	8.

D-34

Note: Fuel Gas Flowmeter was being bypassed - No Readings

Thru  
 1000 - 9/20/79

Filter Instruments

Time	Manometers, in. w.c. Compartment					Total ΔP in. w.c.	Inlet Temp °F	Inlet Draft -mm H <sub>2</sub> O	Fan Load amps	Trans P <sub>o</sub> P <sub>o</sub> Outlet
	1	2	3	4	5					
10:48 am	6.1	5.5	5.1	6.1	4.7	8.6	480	30	20	11
11:00	5.7	5.1	4.7	5.7	4.3	8.2	480	30	20	11
11:53	5.8	5.2	4.8	5.8	4.4	8.3	480	29	20	11
12:50	5.8	5.2	4.7	5.7	4.2	8.2	480	30	20	11
1:45	5.8	5.2	4.7	5.7	4.3	8.2	480	29	20	11

Notes  
Run No 3

Thurs  
Date; 9/20/74

This is to be Run No 3. (method 5 test for Run No 2 is planned for tomorrow 9/21/74)

2:48 am - Put dust collection bucket under dust discharge chute from B+C filter, removed bucket at 3:05. Too little dust to weigh. Estimate 0.2-0.5 lbs

Operator says they cleared nozzles on No 96 oven last night. Watched push at 4:02 am. No improvement in push greenness from yesterday. Report is that ~~there~~ there was a fire in the byproducts plant early this morning. Mainly in the Cottrell precipitator

11:45 Test started

2:45 Test over.

Did not do any fine inspections today

DATA FOR COKE PLANT BATTERY "B" - TRW - EPA - MRI TESTS.

COKE OVEN GAS  
9/20/79

	%
CO <sub>2</sub>	2.4
Ill.	4.0
O <sub>2</sub>	1.2
CO	4.6
H <sub>2</sub>	52.4
CH <sub>4</sub>	26.6
N <sub>2</sub>	8.8

COKE OVEN GAS  
9/21/79

	%
CO <sub>2</sub>	2.6
Ill.	3.8
O <sub>2</sub>	1.4
CO	4.6
H <sub>2</sub>	48.4
CH <sub>4</sub>	25.0
N <sub>2</sub>	14.2

Gross heating value = 535 BTU/cf.  
Net heating value = 482 BTU/cf.

Gross heating value = 501 BTU/cf.  
Net heating value = 452 BTU/cf.

Coal and Coke Analysis - 9/20/79

Item	%VM	%FC	%Ash	%Sulf.
Coke	1.9	87.4	10.7	0.74
Petroleum Coke	11.8	88.1	0.1	1.87
Sunnyside Coal	40.4	52.8	6.8	1.22
Coal Basin	24.6	68.2	7.2	0.62
York Canyon	36.2	56.2	7.5	0.45
Coal Mix	32.9	60.4	6.7	0.84

Coal Mix by % → 30% Sunnyside, 41% York Canyon, 21% Coal Basin  
(Aim) 8% Petroleum Coke

Coal and Coke Analysis - 9/21/79

Item	%VM	%FC	%Ash	%Sulf.
Coke	1.4	88.2	10.4	0.75
Petroleum Coke	10.8	89.1	0.1	1.85
Sunnyside Coal	39.0	54.1	6.9	1.20
Coal Basin		-----Lost Sample-----		
York Canyon	36.4	D-37 55.8	7.8	0.44
Coal Mix	32.3	60.8	6.9	0.88

Coal Mix by % → 30% Sunnyside, 41% York Canyon, 21% Coal Basin  
(Aim) and 8% Petroleum Coke

OVEN PAN AND BATTERY CROSS-ALL TEMPERATURES

OPERATOR: HARTMAN

DATE: 9-20

TIME: 8:50 AM

"A" BATTERY FLUE TEMPERATURES					"B" BATTERY FLUE TEMPERATURES					WALL NUMBER		
PUSHER SIDE		Wall No.	COKE SIDE		PUSHER SIDE		COKE SIDE		PS	B	PS	B
39		1	46		<del>48</del>	30			1	24	04	
xxx	36	2	xxx	31	xxx	48	xxx	39	2	37	14	
	31	3		32		34		32	3	45	33	
28	xxx	4	34	xxx	33	xxx	35	xxx	4	49	36	
38		5	29		45		35		5	44	42	
xxx	29	6	xxx	19	xxx	40	xxx	45	6	56	42	
	21	7		21		50		50	7	56	48	
210	xxx	8	26	xxx	57	xxx	41	xxx	8	2600	50	
58		9	11		48		42		9	2610	49	
xxx	95	11	xxx	01	xxx	36	xxx	36	10	62	49	
	21	12		29		35		42	11	60	45	
30	xxx	13	22	xxx	25	xxx	24	xxx	12	50	44	
32		14	35		21		20		13	35		
xxx	38	15	xxx	31	xxx	16	xxx	36	14	22		
	34	16		30		2		23	15			
31	xxx	17	30	xxx	38	xxx	59	xxx	16			
05		18	18		28		09		17			
xxx	20	19	xxx	31	xxx	26	xxx	09	18			
	26	21		30		25		41	19			
40	xxx	22	31	xxx	25	xxx	41	xxx	20			
23		23	26		25		27		21			
xxx	23	24	xxx	30	xxx	32	xxx	25	22			
	22	25		21		25		25	23			
28	xxx	26	27	xxx	50	xxx	29	xxx	24			
06		27	24		50		40		25			
xxx	90	28	xxx	90	xxx	39	xxx	34	26			
	75	29		95		35		13	27			
95	xxx	31	08	xxx	29	xxx	17	xxx	28			
31		32	18		49		32		29			
xxx	25	33	xxx	33	xxx	45	xxx	44	30			
	25	34		30		40		40	31			
26	xxx	35	13	xxx	96	xxx	22	xxx	32			
97		36	00		95		99		33			
xxx	08	37	xxx	32	xxx	03	xxx	85	34			
	31	38		20		38		32	35			
99	xxx	39	14	xxx	18	xxx	31	xxx	36			
13		40	16		24		28		37			
xxx	06	41	xxx	30	xxx	35	xxx	28	38			
	06	42		00		14		23	39			
23	xxx	43	19	xxx	97	xxx	02	xxx	40			
34		44	01		96		45		41			
xxx	30	45	xxx	23	xxx	19	xxx	17	42			
	38	46		24		10		97	43			
01	xxx	47	02	xxx	01	xxx	97	xxx	44			
35		48	14		17		26		45			
	64	49	80		35		27		46			
271	475	"A"	244	276	346	325	"B"	320	317			
22-3			2260		2335			2319				

REMARKS:

SOAK  
A  
L

COKE OVEN SPAN AND BATTERY CROSS-ALL TEMPERATURES

REF: 1043 P-1

READER: O.J

DATE: 9-20-79

TIME: 6:45

"A" BATTERY FLUE TEMPERATURES					"B" BATTERY FLUE TEMPERATURES					WALL NUMBER			
PUSHER SIDE		Wall No.	COKE SIDE		PUSHER SIDE		Wall No.	COKE SIDE		PS	WALL NUMBER	PS	WALL NUMBER
28		1	36		31		51	11		97		98	
xxx	39	2	xxx	32	xxx	37	52	xxx	27	50		50	
	39	3		27		42	53		39				
14		4	13		34		54	32		88		67	
36	xxx	5	22	xxx	42	xxx	55	40	xxx	95		71	
xxx	27	6	xxx	11	xxx	41	56	xxx	40	74		79	
	30	7		07		08	57		05				
31		8	15		95		58	98		82		76	
94	xxx	9	97	xxx	23	xxx	59	20	xxx	02		86	
xxx	83	10	xxx	88	xxx	33	61	xxx	28	04		90	
	22	11		33		22	62		34	02		89	
38		12	20		21		63	37		83		83	
33	xxx	13	xxx		14	xxx	64	19	xxx	83		83	
xxx	23	14	30	xxx	xxx	17	65	xxx	36	83		85	
	23	15		24		17	66		23	87		88	
13		16	18		25		67	07		81		97	
92	xxx	17	00	xxx	26	xxx	68	01	xxx	81		97	
xxx	23	18	xxx	31	xxx	25	69	xxx	11	86		90	
	32	19		24		23	71		31				
33		20	20		07		72	28		CS		CS	
22	xxx	21	23	xxx	18	xxx	73	18	xxx	14	96	14	90
xxx	17	22	xxx	15	xxx	24	74	xxx	16	13	01	13	90
	20	23		15		46	75		24	12	10	12	91
19		24	24		33		76	23		11	09	11	91
02	xxx	25	08	xxx	42	xxx	77	32	xxx	10	98	10	90
xxx	80	26	xxx	80	xxx	33	78	xxx	45	9	96	9	93
	66	27		78		25	79		00	8	96	8	85
72		28	85		24		81	05		7	83	7	89
12	xxx	29	17	xxx	17	xxx	82	14	xxx	6	83	6	83
xxx	29	30	xxx	22	xxx	31	83	xxx	26	5	85	5	81
	30	31		24		19	84		24	4	88	4	91
29		32	18		91		85	12		3	85	3	84
88	xxx	33	87	xxx	72	xxx	86	74	xxx	2	73	2	73
xxx	03	34	xxx	13	xxx	76	87	xxx	77	1	45	1	58
	24	35		12		10	88		06				
96		36	78		17		89	25					
99	xxx	37	02	xxx	26	xxx	91	34	xxx				
xxx	92	38	xxx	20	xxx	18		xxx	12				
	85	39		88		14			10				
12		40	13		87								
33	xxx	41	31	xxx	80	D-39		00	xxx				
xxx	28	42	xxx	14	xxx	07		77					
	24	43		09		02		xxx	99				
83		44	85		86			89	83				
60	xxx	45	58	xxx	21			28	xxx				
xxx	51	46	1480		40				29				
265	270	"A"	233	243	295	287	"B"	274	299				
2268			2238	2291				2288					

Wall throtled - coke pushed on west side of wall on  
 Wall is off: No coke

REMARKS:

COKE OVEN SPAN AND BATTERY CROSS-ALL TEMPERATURES

MSCO 1-43 P-2

READER: MARSCHIEDER

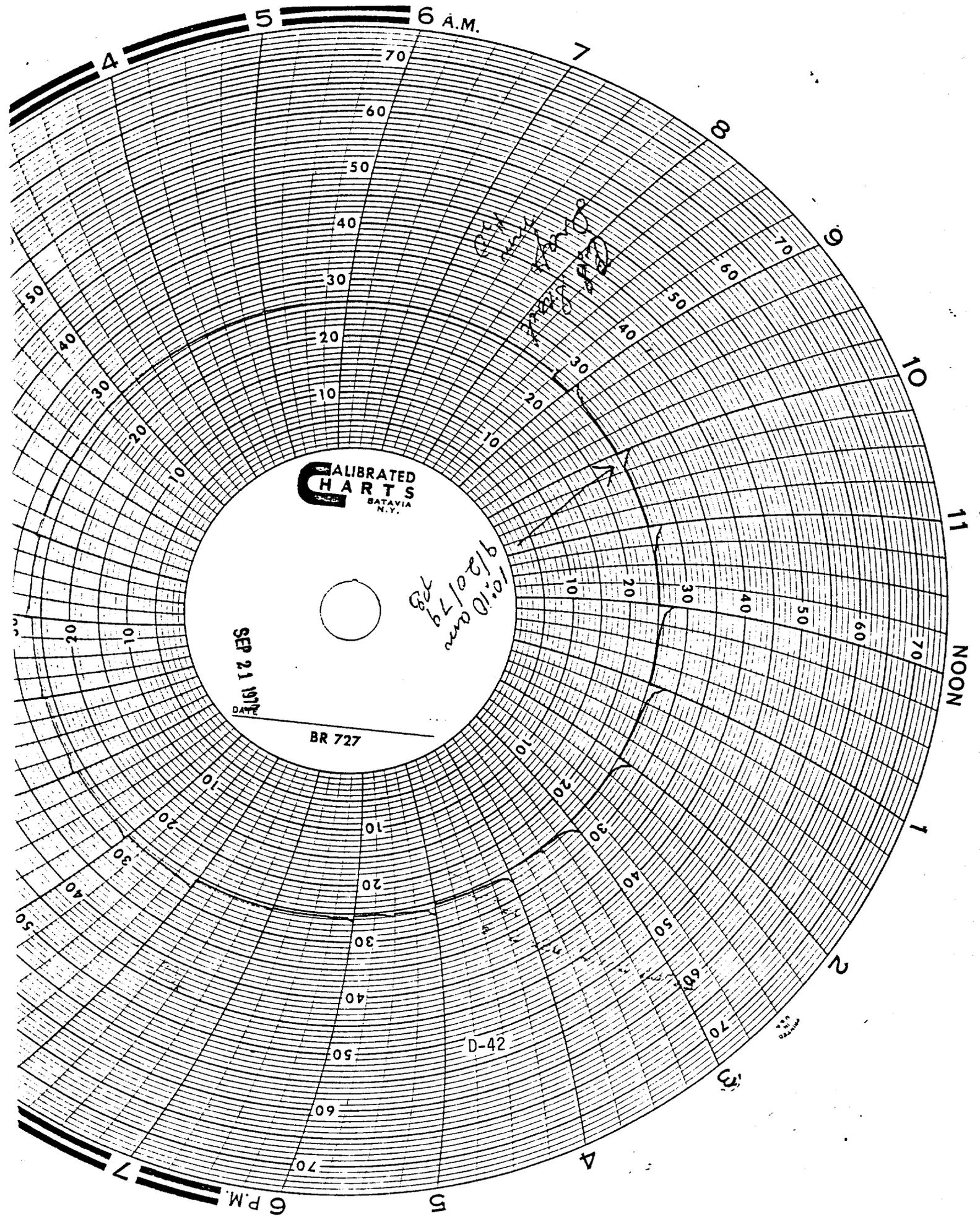
DATE: 9-21

TIME: 1:45 A

"A" BATTERY FLUE TEMPERATURES				"B" BATTERY FLUE TEMPERATURES				WALL NUMBER		WALL NUMBER		
PUSHER SIDE		Wall No.	COKE SIDE		PUSHER SIDE		COKE SIDE		PS	CS	PS	CS
<del>34</del>	<del>33</del>	1	<del>45</del>	<del>13</del>	1	10	1	BURIED				
xxx	29	2	xxx	33	xxx	45	xxx	33				
	30	3		26		37		35				
14	xxx	4	17	xxx	40	xxx	34	xxx				
35		5	26		12		41					
xxx	23	6	xxx	14	xxx	26	xxx	28				
	32	7		15		30		31				
28	xxx	8	16	xxx	27	xxx	15	xxx				
10		9	27		31		22					
xxx	95	10	xxx	04	xxx	29	xxx	22				
	24	12		30		32		39				
23	xxx	13	17	xxx	23	xxx	26	xxx				
37		14	39		14		19					
xxx	34	15	xxx	73	xxx	09	xxx	27				
	26	16		30		15		21				
27	xxx	17	30	xxx	26	xxx	10	xxx				
03		18	13		20		05					
xxx	18	19	xxx	25	xxx	17	xxx	07				
	30	21		28		19		26				
34	xxx	22	26	xxx	25	xxx	34	xxx				
25		23	20		22		26					
xxx	33	24	xxx	31	xxx	23	xxx	15				
	27	25		23		12		02				
19	xxx	26	18	xxx	36	xxx	20	xxx				
11		27	12		44		35					
xxx	75	28	xxx	20	xxx	33	xxx	29				
	72	29		82		28		10				
23	xxx	30	99	xxx	23	xxx	10	xxx				
26		31	27		25		19					
xxx	20	32	xxx	22	xxx	14	xxx	18				
	32	33		37		34		42				
31	xxx	34	28	xxx	08	xxx	27	xxx				
91		35	93		26		95					
xxx	90	36	xxx	15	xxx	17	xxx	95				
	24	37		13		23		25				
93	xxx	38	75	xxx	18	xxx	26	xxx				
00		39	09		21		19					
xxx	94	40	xxx	26	xxx	27	xxx	26				
	33	41		99		26		41				
21	xxx	42	27	xxx	15	xxx	16	xxx				
41		43	34		96	D-40	81					
xxx	20	44	xxx	17	xxx	15	xxx	17				
	33	45		20		14		08				
94	xxx	46	02	xxx	87	xxx	00	xxx				
07		47	69		28		32					
xxx	57	48	xxx	62	xxx	38	xxx	33				
269	275	49	236	253	287	248	246	228				
2272	xxx	50	2245	xxx	2268	xxx	2237	xxx				

REMARKS:





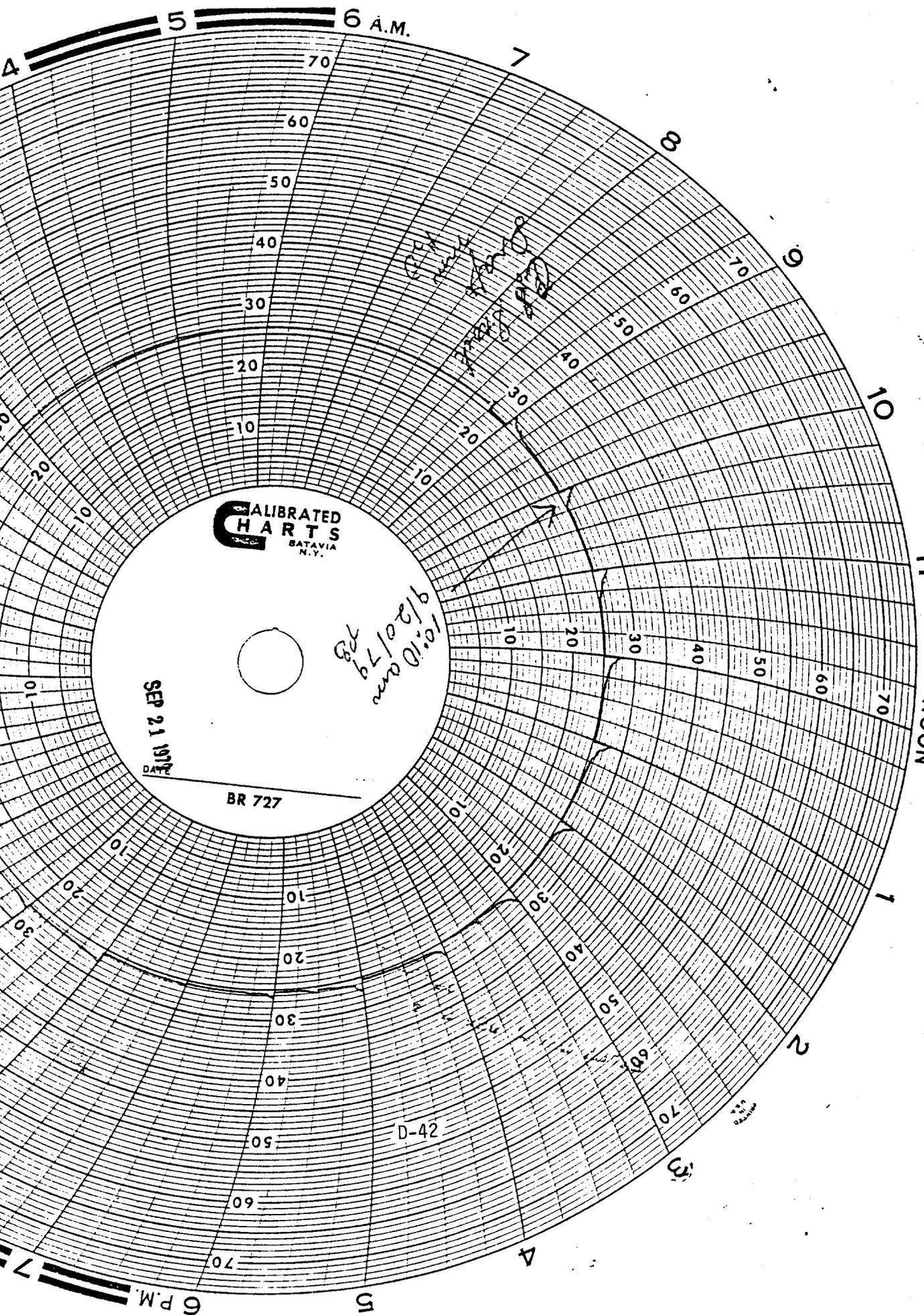
CALIBRATED  
CHARTS  
BATAVIA  
N.Y.

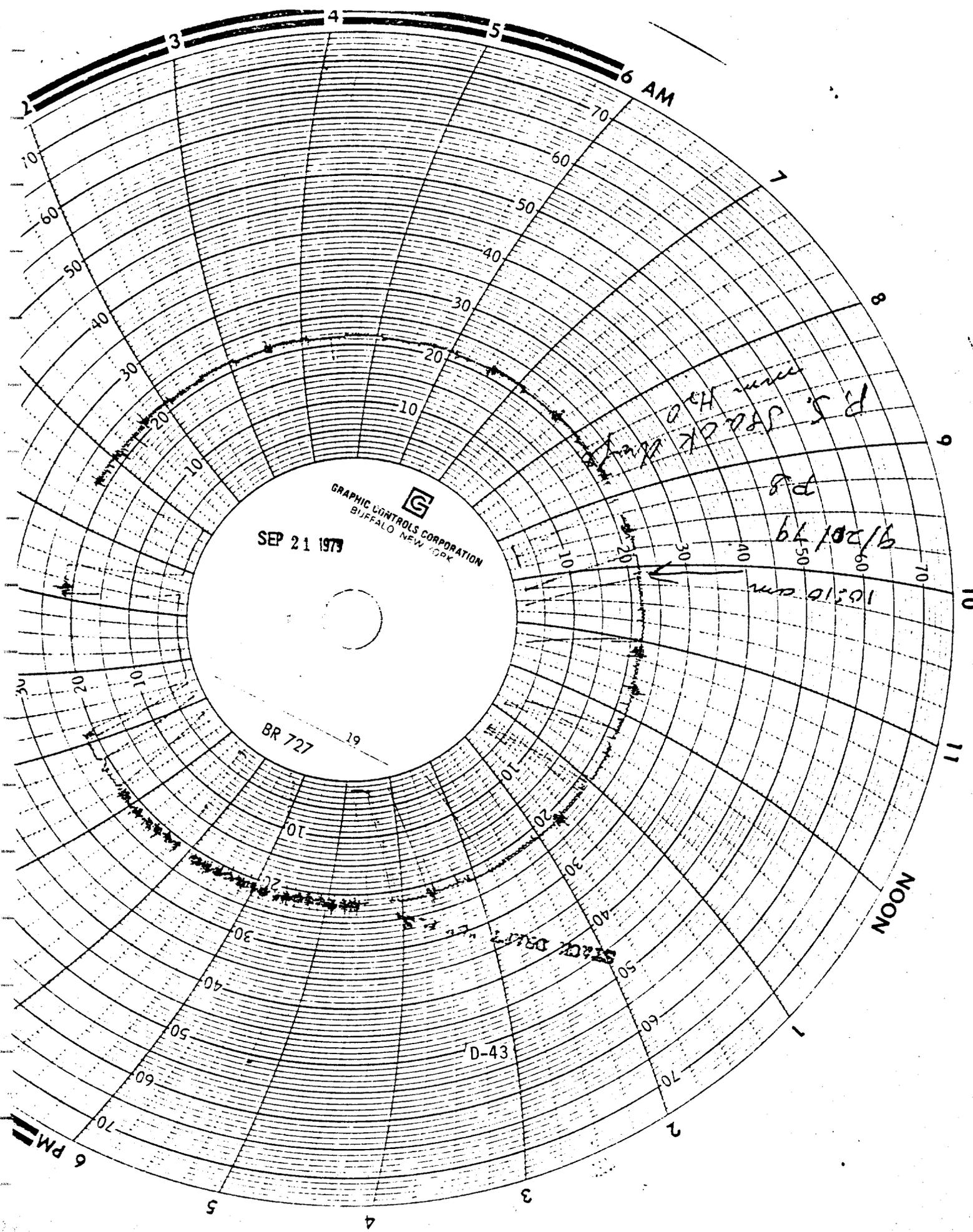
SEP 21 1978

BR 727

10:10 am  
9/20/79  
798

D-42





SEP 21 1979

GRAPHIC CONTROLS CORPORATION  
BUFFALO NEW YORK

BR 727

D-43

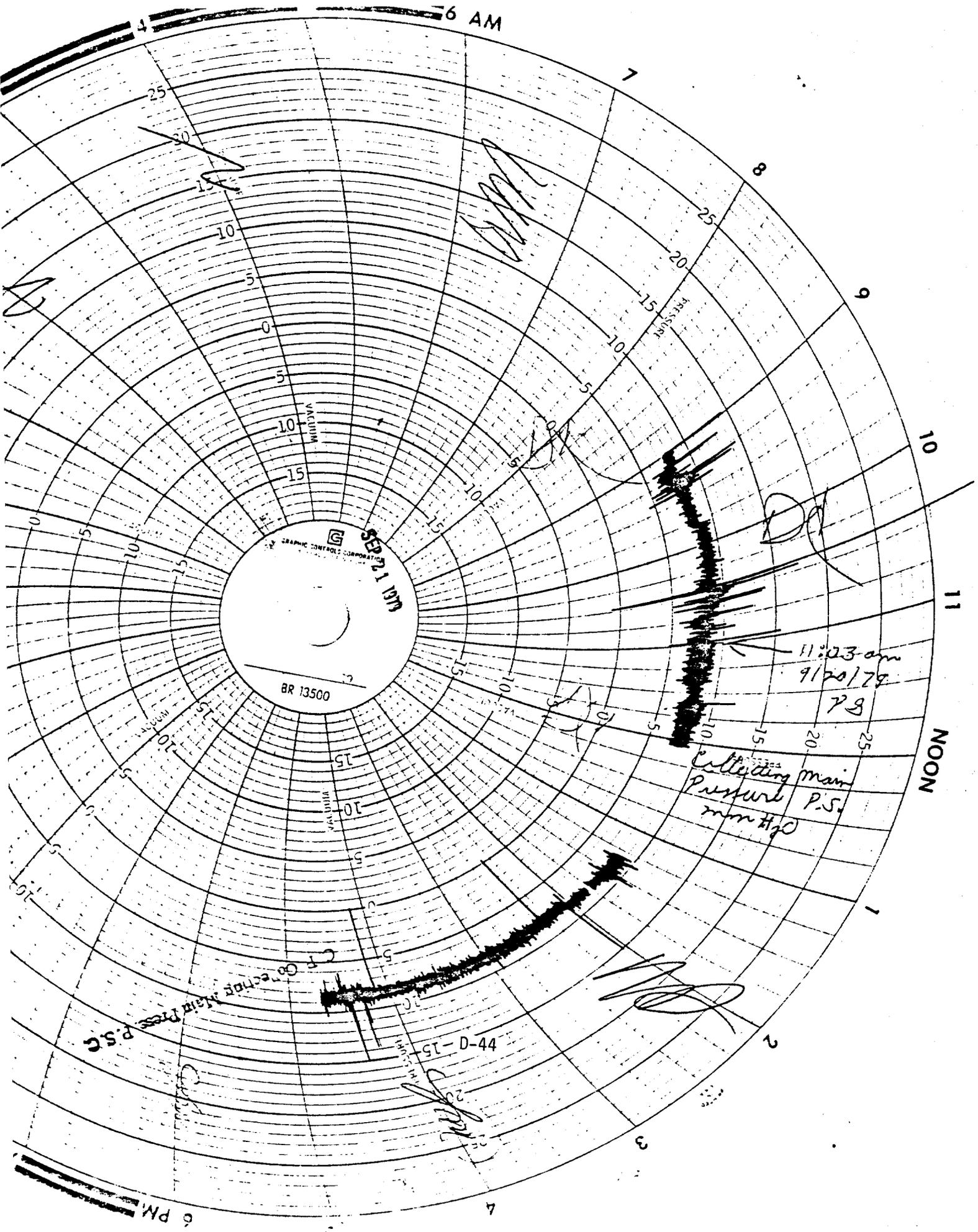
P.S. JACK  
D-43  
9/20/79

10:30 am

NOON

6 AM

6 PM



6 AM

NOON

6 PM

G  
GRAPHIC CONTROLS CORPORATION  
SEP 21 1979  
BR 13500

11:03 am  
9/20/79  
78

Collecting main  
Pressure P.S.  
mm H<sub>2</sub>O

CT Collecting main Press. P.S.C.

44-D-15



TEST NO. 2 (EPA Method 5 only) \*

September 21, 1979

\* Note - The Method 5 test on 9/19/79 (Test No. 2) was invalid.  
Therefore, it was re-run on 9/21/79.

D-46



Friday  
Date: 7/21/74

Heater Room

Time	Stack Draft			Fuel Press. mm H <sub>2</sub> O	Temperatures °C				Current Corrected Manifold Pressure			
	mm H <sub>2</sub> O				Picht		Wet Bulb		Cell Manif.			
	PS	CS	Manif. meter		After	Before	FS	CS	PS	CS	PS	CS
5:22	26	19		352	40	40	274	270	78	80	7.5	7.0
35	22	26	NR	376	41	41	273	263	86	85	8.5	8.0
1:00	22	26	19	352	41	42	273	264	84	86	8.0	8.0

D-48

Note: Fuel Gas Flowmeter was being bypassed - No Readings

Friday  
7/21/79

Filter Instruments

Time	Manometers, in. w.c. Compartment					Total ΔP in. w.c.	Inlet Temp °F	Inlet Draft -mm H <sub>2</sub> O	Fan Load amps	Total % ΔP Outlet
	1	2	3	4	5					
9:30 am	5.1	4.7	4.3	5.1	3.8	7.6	480	29	20	11
10:55	5.3	4.9	4.4	5.2	3.4	8.0	480	29	20	10
11:50	5.7	5.1	4.7	5.6	4.2	Sump reading - cleaning cycle started				
12:15	5.0	4.6	4.1	5.0	3.6	7.5	480	27	19	11



DATA FOR COKE PLANT BATTERY "B" - TRW - EPA - MRI TESTS.

COKE OVEN GAS  
9/20/79

	%
CO <sub>2</sub>	2.4
Ill.	4.0
O <sub>2</sub>	1.2
CO	4.6
H <sub>2</sub>	52.4
CH <sub>4</sub>	26.6
N <sub>2</sub>	8.8

COKE OVEN GAS  
9/21/79

	%
CO <sub>2</sub>	2.6
Ill.	3.8
O <sub>2</sub>	1.4
CO	4.6
H <sub>2</sub>	48.4
CH <sub>4</sub>	25.0
N <sub>2</sub>	14.2

Gross heating value = 535 BTU/cf.  
Net heating value = 482 BTU/cf.

Gross heating value = 501 BTU/cf.  
Net heating value = 452 BTU/cf.

Coal and Coke Analysis - 9/20/79

Item	%VM	%FC	%Ash	%Sulf.
Coke	1.9	87.4	10.7	0.74
Petroleum Coke	11.8	88.1	0.1	1.87
Sunnyside Coal	40.4	52.8	6.8	1.22
Coal Basin	24.6	68.2	7.2	0.62
York Canyon	36.2	56.2	7.5	0.45
Coal Mix	32.9	60.4	6.7	0.84

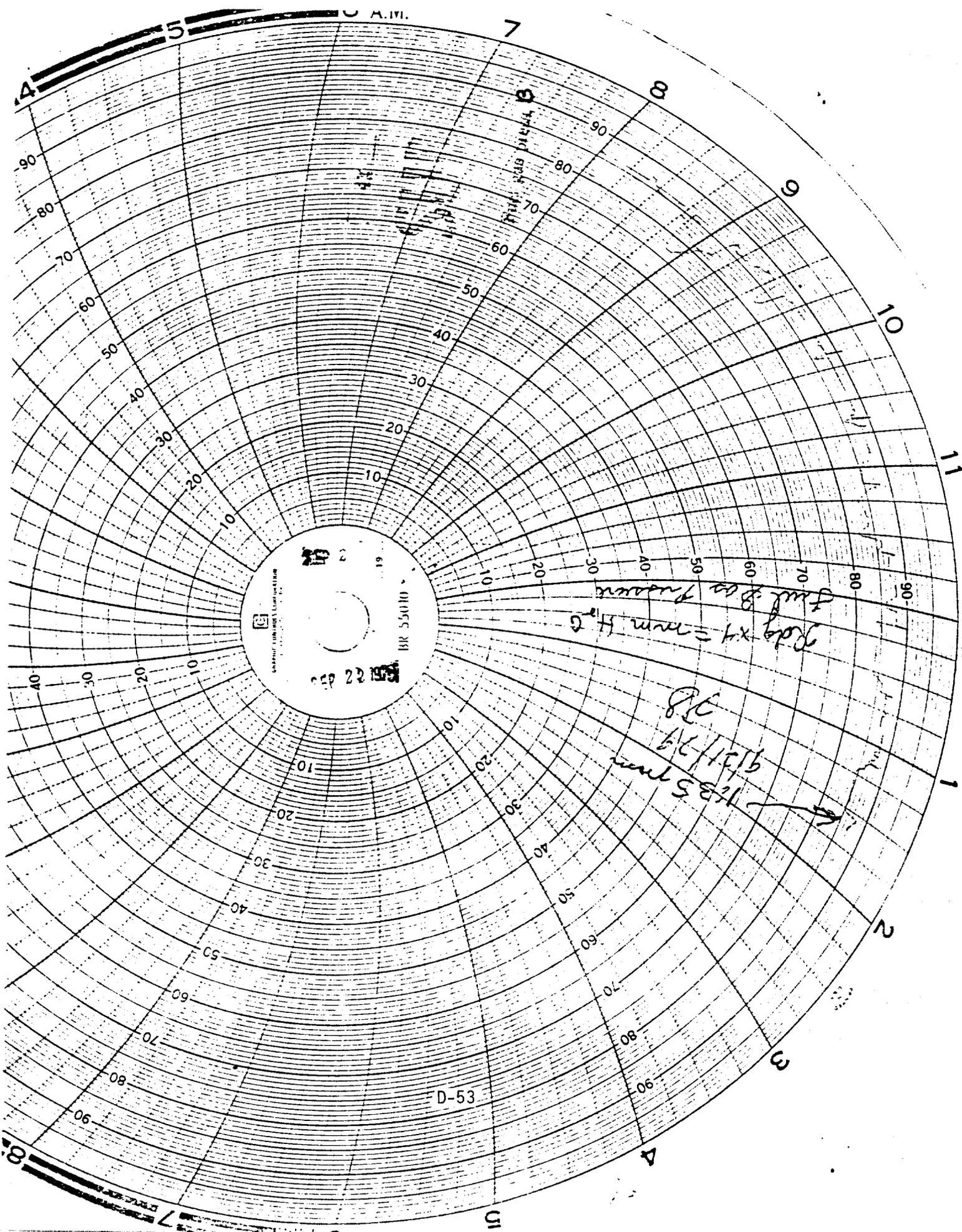
Coal Mix by % → 30% Sunnyside, 41% York Canyon, 21% Coal Basin  
(Aim) 8% Petroleum Coke

Coal and Coke Analysis - 9/21/79

Item	%VM	%FC	%Ash	%Sulf.
Coke	1.4	88.2	10.4	0.75
Petroleum Coke	10.8	89.1	0.1	1.85
Sunnyside Coal	39.0	54.1	6.9	1.20
Coal Basin	-----Lost Sample-----			
York Canyon	36.4	D-51 55.8	7.8	0.44
Coal Mix	32.3	60.8	6.9	0.88

Coal Mix by % → 30% Sunnyside, 41% York Canyon, 21% Coal Basin  
(Aim) and 8% Petroleum Coke

Battery temperature record for ~~ST~~ 8-4 ship  
on 9/21/79 was not available.



C.A.M.

4

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NOON

1

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U.I.

8

7

BR 55010

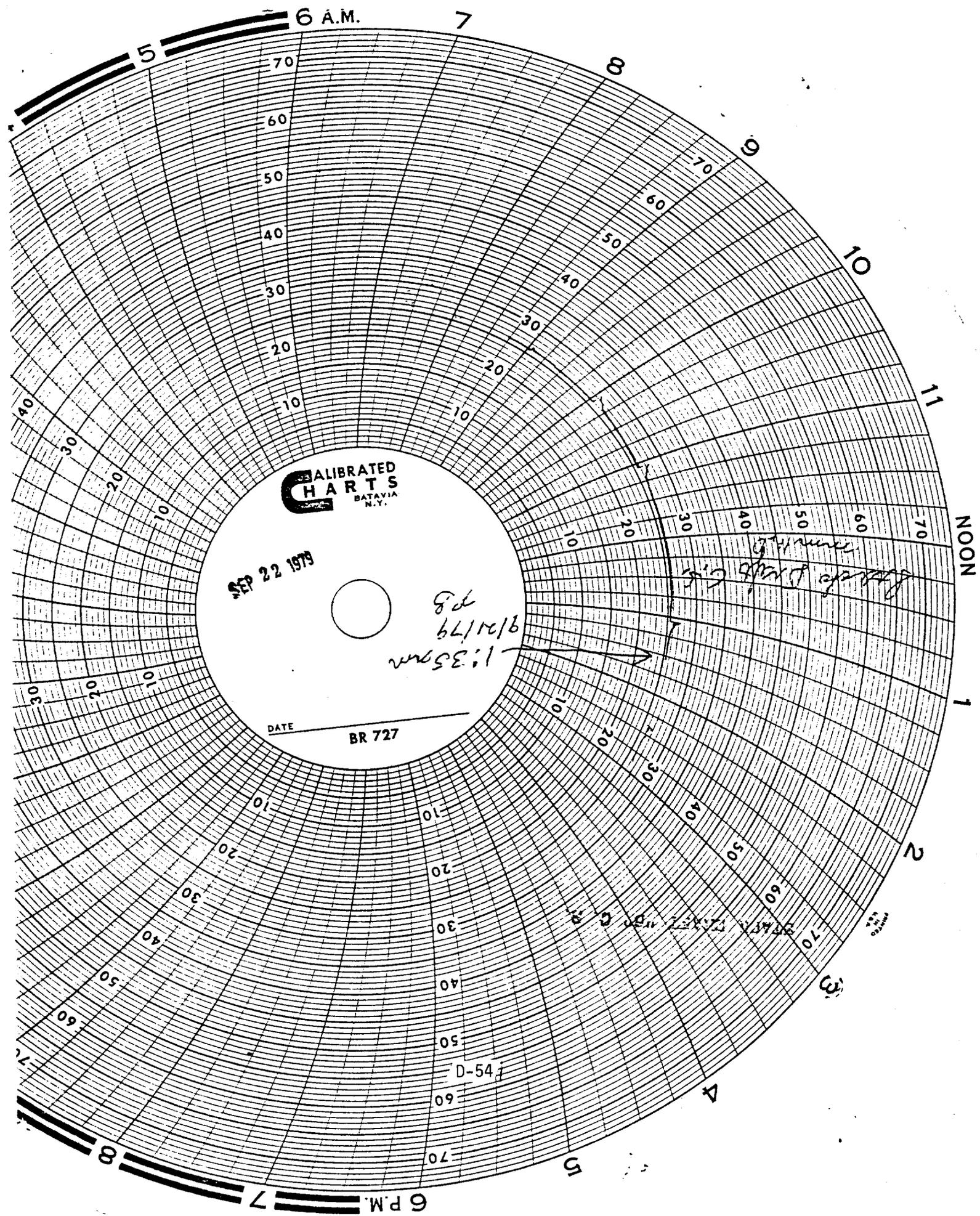
BR 55010

BR 55010

Redy x4 = 3mm H<sub>2</sub>O  
Full 200 Pressure

1235 mm  
9/21/79  
JCB

D-53



**CALIBRATED  
CHARTS**  
BATAVIA  
N.Y.

SEP 22 1979

1:35 pm  
D-54  
BR 727

DATE  
BR 727

*Handwritten notes on the right side of the chart, including '1:35 pm' and other illegible text.*

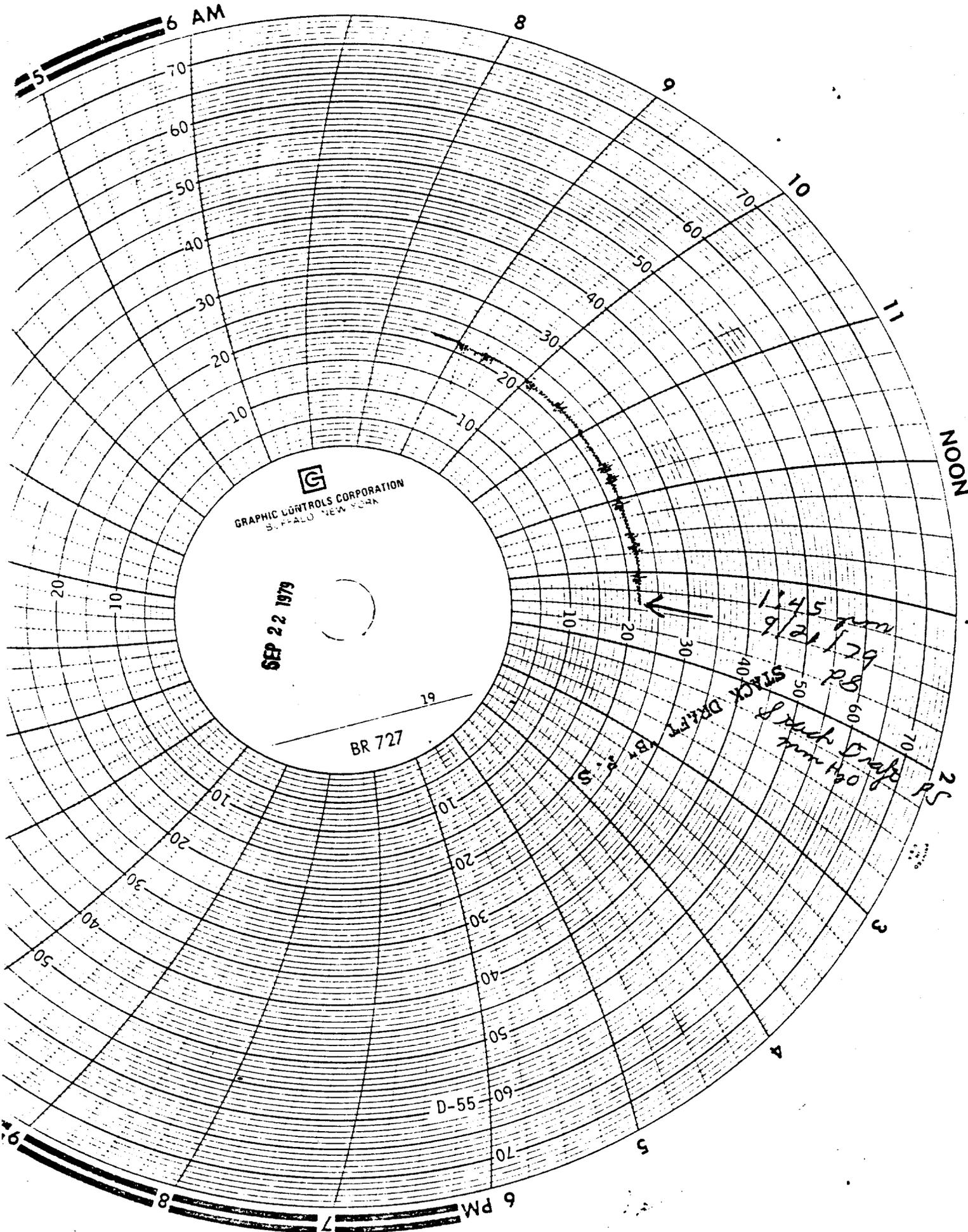
*Handwritten notes at the bottom of the chart, including 'D-54' and 'BR 727'.*

D-54

6 P.M.

6 A.M.

NOON



**G**  
GRAPHIC CONTROLS CORPORATION  
BUFFALO, NEW YORK

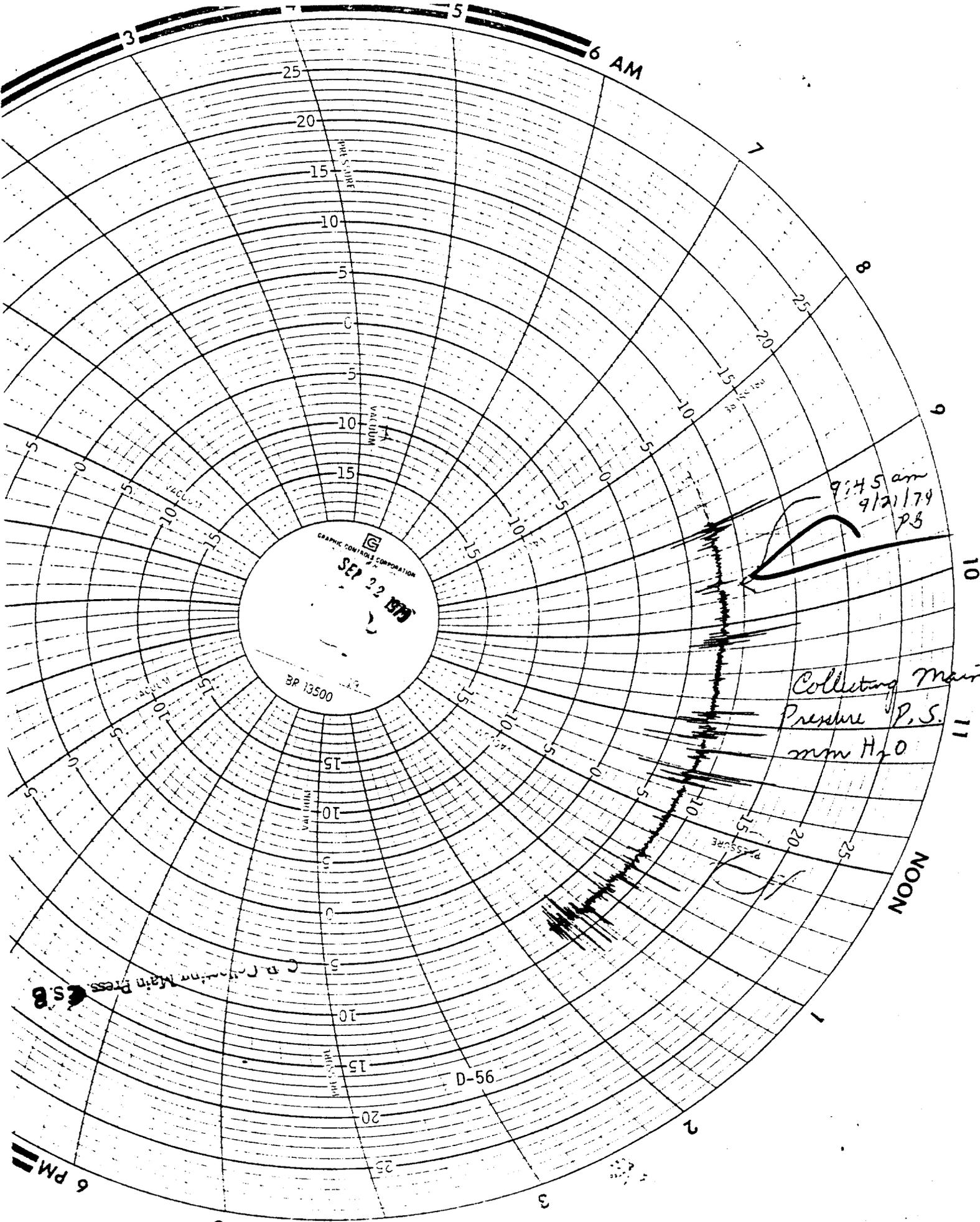
SEP 22 1979

BR 727

D-55-09

1345 run  
9/21/79  
STACK DRIFT 18" p.p.s.  
8 Stack Drift  
run 100 p.p.s.





3 5 6 AM

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GRAPHIC CONTROLS CORPORATION  
SEP 22 1974  
BR 13500

9:45 am  
9/21/74  
PB

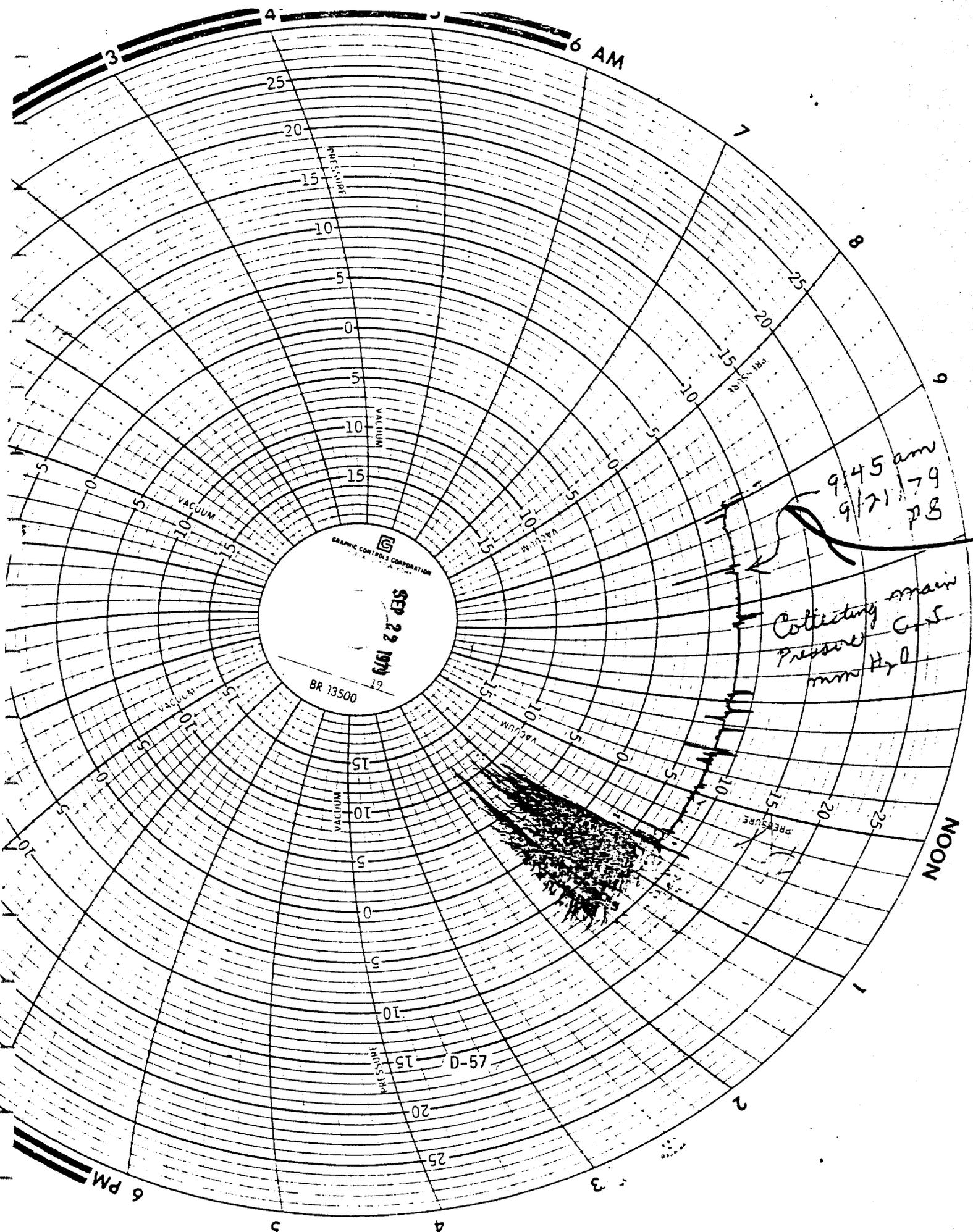
Collecting Main  
Pressure P.S.  
mm H<sub>2</sub>O

D-56

C.P. Collecting Main Press

6 PM

NOON



6 AM

9:45 am  
9/21/79  
p8

Collecting main  
pressure G.S.  
mm Hg

GRAPHIC CONTROLS CORPORATION  
SEP 22 1979  
BR 13500

NOON

6 PM

65-D