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SOURCE

EMISSION

EVALUATION

JANUARY 30, 1990

Prepared For:

**BOEING COMPANY
PLANT 2
CHROMIC ACID ANODIZING TANK 5A
SEATTLE, WASHINGTON
AUGUST-DECEMBER 1989**

Submitted by:

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We certify that the information contained herein is accurate and complete to the best of our knowledge.

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INTRODUCTION

The purpose of this testing program performed at the Boeing Company's Plant No. 2 in Seattle, Washington was to quantify the hexavalent chromium (Cr^{+6}) and total chromium (Cr) emissions exhausted from the #5A chromic acid anodizing tank which is one of the tanks in the 80 anodic tank line located in the 210 Building. The fumes which result from the plating process are controlled by blowing air horizontally across the top of the tank and pulling off the fumes through ductwork with an axial fan to the exhaust stack. The plating cycle takes 55 minutes during which the vat is heated to a temperature of approximately 95° F. Samples were collected over a four (4) month period as coordination would allow.

Three (3) samples were collected while no parts were in the bath (passive or "blank" runs) on August 22, August 29, and September 19, 1989. Eight (8) samples were collected during anodizing cycles on August 22, August 31, September 19, November 30 and December 1, 1990. Three (3) particle size distribution (droplet size) samples were collected during anodizing cycles on August 31 and November 30, 1989. An ambient workroom sample was collected over a 6.5 hour period on August 31, 1989. Samples of the acid in the bath were collected on September 19 and December 1, 1989.

As part of this study, the ventilation system which pulls off air at the surface of the acid bath into vents along one side of the tank was evaluated by measuring the gas velocity at the individual air vents. The velocity was measured on August 22, August 31 and November 30, 1989.

The chromium sample method used is similar to EPA Method 5, which is detailed in the Title 40 Code of Federal Regulations, Part 60 (40 CFR 60), Appendix A. The sample train was modified to exclude the front-half filter and utilized 0.1 N sodium hydroxide (NaOH) solution in the first two (2) impingers, followed by an impinger containing 0.1 N nitric acid (HNO₃), followed by an empty impinger, a final back-half Teflon[®] filter to collect any chromium which might break through the absorbing liquid, and a bubbler containing indicating silica gel desiccant. EPA Methods 1-4 were also performed during each chromium test. Methods 1 and 2 were performed to measure the stack gas velocity, temperature and volumetric flow rate. Method 3 was used to calculate the molecular weight of the stack gas. Method 4 was performed to measure the moisture content of the stack gas.

Mr. Kris A. Hansen, Mr. James A. Guenthoer, Mr. K. Steven Mackey, Ms. Jan M. Widmeyer and Ms. Angela F. Blaisdell of Am Test, Inc.'s Air Quality Division based in Redmond, Washington performed the field sampling, data reduction, and final report preparation. Am Test, Inc.'s Trace Metals Division performed the hexavalent chromium and chromium analysis. Mr. Paul Siebenaler coordinated this project for Boeing Aerospace & Electronics.

PRESENTATION OF RESULTS

This report is divided into separate sections for each type of test conducted. Please refer to the Table of Contents to locate information for a specific type of sample. Within each section a summary sheet is included for each run. On the summary sheet the chromium emission concentration is presented in units of milligrams per dry standard cubic meter (mg/dscm) and in parts per million (ppm). The chromium emission rate is presented in units of pounds per hour (lb/hr) and the chromium emission factor is presented in units of milligrams per ampere-hour (mg/amp-hr). Airflow is also presented in units of dry standard cubic feet per minute (dscf/min). The corresponding computer printout and field data sheet follow each summary sheet for each run. The run numbers indicate the run number on a particular test day, not the total number of runs of a particular sample type. The appropriate process information data sheet follows the field data sheet, where applicable. Laboratory analysis results are included in Appendix A of this report. Example calculations of results are included in Appendix B of this report.

In some cases the hexavalent chromium concentrations were greater than the total chromium concentrations. The explanation is that there is a difference in accuracy between the 2 analytical methods (colorimetric versus ICP). The ICP method would likely be the more accurate method.

A brief summary of the chromium tests conducted without parts in the bath and with parts in the bath is presented in Table 1 below.

Table 1. Summary of results from chromium emissions tests conducted at the #5A chromic acid anodizing tank at Boeing Plant 2.

Date	Time	Condition	Hex. Chromium mg/dscm	Hex. Chromium mg/amp-hr	Total Chromium mg/dscm	Total Chromium mg/amp-hr
8/22	1521-1722	Bath Off	0.109	--	0.094	--
8/29	1008-1209	Bath Off	0.105	--	0.096	--
9/19	1022-1223	Bath Off	0.008	--	0.018	--
8/22	1045-1148	Bath On	1.235	23.8	0.805	15.5
8/22	1401-1503	Bath On	1.389	25.7	0.759	14.0
8/31	1215-1315	Bath On	0.438	33.6	0.431	33.1
8/31	1558-1659	Bath On	0.457	36.4	0.418	33.3
9/19	1300-1401	Bath On	0.947	17.7	0.916	17.1
11/30	0803-0904	Bath On	0.261	6.19	0.280	6.64
11/30	1546-1649	Bath On	0.416	8.23	0.423	8.36
12/1	0729-0831	Bath On	0.263	5.94	0.273	6.17
Average			0.512	19.7	0.410	16.8

SECTION 1
"BLANK" RUNS
(NO PARTS IN BATH)

Sample Type:	Bath Off - Blank Run 1
Sampling Date:	August 22, 1989
Sample Times:	15:21-17:22 (120 minutes)
Run Number:	3
Lab Numbers:	915092, 915095, 915099, 915102
Airflow:	20,499 dscf/min
Hexavalent Chromium	
Concentration:	0.109 mg/dscm
Concentration:	0.05 ppm
Emission Rate:	3802.6 mg/hr
Total Chromium	
Concentration:	0.094 mg/dscm
Concentration:	0.04 ppm
Emission Rate:	3261.7 mg/hr

METHOD 1-5 - HEXAVALENT AND TOTAL CHROMIUM EMISSIONS
AM TEST, INC. - AIR QUALITY DIVISION

FILE NAME: 180M5CR3
CLIENT: BOEING PLANT #2
LOCATION: SEATTLE, WASHINGTON
SAMPLE SITE: BLDG 210/TANK #5
SAMPLE DATE: AUGUST 22, 1989
RUN #: 3-CR+6
OPERATORS: GLEITHNER/MACKAY
CONTACT: P. STEBENALER

LAB #:
START TIME: 915092
STOP TIME: 15:21 O'CLOCK
SAMPLE TIME: 17:22 O'CLOCK
CONDITION: 120.0 MINUTES
BATH OFF

HEXAVALENT CHROMIUM

HEXAVALENT CHROMIUM CONCENTRATION (ug): 332.5
HEXAVALENT CHROMIUM CONCENTRATION (mg/dscm): 0.109
HEXAVALENT CHROMIUM IN SAMPLE (ppm): 0.05
HEXAVALENT CHROMIUM EMISSION RATE (mg/hr): 3802.6

TOTAL CHROMIUM

TOTAL CHROMIUM CONCENTRATION (ug): 285.2
TOTAL CHROMIUM CONC. ON FILTER (ug): < 0.15
TOTAL CHROMIUM CONCENTRATION (mg/dscm): 0.094
TOTAL CHROMIUM IN SAMPLE (ppm): 0.04
TOTAL CHROMIUM EMISSION RATE (mg/hr): 3261.7

FINAL WT. INIT. WT. NET WT.
OF H2O G. OF H2O G. OF H2O G.

905.2 890.8 14.4
381.9 379.7 2.2
473.1 470.2 2.9
745.0 725.6 19.4
TOTAL H2O GAIN: 38.9
TOTAL VOLUME (SCF) 1.83
PERCENT MOISTURE: 1.68
Bws: 0.0168

PITOT Cps: 0.84
NOZZLE DIA INCHES: 0.313
NOZZLE AREA FT^2: 0.0005
STACK DIA. INCHES: 48.00
STACK AREA FT^2: 12.566
METER TEMP. DEG F: 90.9
BAROM. PRES. "HG: 30.04
STATIC PRES. "H2O: 0.00
STACK PRES. "HG: 30.04
ORIFICE PRES "H2O: 1.322
METER PRES. "HG: 30.14

INIT. METER VOL.: 475.221
FINAL METER VOL.: 587.407
VOLUME SAMPLED: 112.186
STD VOLUME (DSCF): 107.545
STD VOLUME (DSCM): 3.046
Y FACTOR: 0.993

AVERAGE % CO2: 0.1
AVERAGE % O2: 20.9
AVERAGE % CO: 0
STACK GAS MW. DRY: 28.85
STACK GAS MW. WET: 28.67

SAMPLE POINT	VELOCITY " OF H2O	TEMPERATURE DEGREES F.	SAMPLE POINT	VELOCITY " OF H2O	TEMPERATURE DEGREES F.
NE 1	0.19	87	NW 1	0.18	87
2	0.27	87	2	0.28	88
3	0.28	87	3	0.32	89
4	0.28	88	4	0.28	88
5	0.26	87	5	0.27	88
6	0.19	87	6	0.21	88

PERCENT ISOkinetics: 103 %
STACK TEMPERATURE: 87.6 DEG. F.
AVERAGE VELOCITY HEAD: 0.249 " OF H2O
STACK GAS VELOCITY: 28.56 FT/SEC.
STACK GAS AIR FLOW: 21535.4 ACF/MIN. 20498.8 DSCF/MIN.

AT

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TRAVERSE SAMPLING DATA

Page 1 of 1

180#50r3 915092

Client Bein-Plant 2
 Date 8-22-89
 Sample Location Bldg 2-10
TANK #5 Exhaust
 Operators JAG-KSW
 Sample Box # C
 Run# 3

EQUIPMENT CHECKS

Initial/Final
 Leak Rate Cfm 4.011
 Leak Test Vac 19
 Pitots, Pretest
 Pitots, Posttest
 Orsat Sampling System
 Tedlar Bag
 Thermocouple @ _____ °F

SCHEMATIC TRAVERSE LAYOUT

Stack Diameter _____
 Distance Upstream _____
 Distance Downstream _____

Filter # _____ tare _____ mgs
 Final Initial Net
 Wt. Wt. Wt.

#1 Bubbler 905.2 - 890.8 =
 #2 Impinger 381.9 - 379.7 =
 #3 Bubbler 473.1 - 470.2 =
 #4 Silica Gel 745.0 - 725.6 =

TOTAL WATER VOLUME _____

Start Time 1521
 Stop Time 1700
 Barometric Pressure "Hg 763
 Static Pres "H₂O _____
 Production Rate BATHOFF

NOMOGRAPH SETUP

% Moisture _____
 Meter Temp. _____
 Stack Temp. _____
 ΔH@ _____ Y _____
 Pitot# _____ Side# _____
 Cp _____
 Nozzle Diameter _____
 K Factor _____
 Reference ΔP _____

Sample Point	Elap Time Min.	Dry Gas Meter Reading Cu. Ft.	Pitot Reading (ΔP), In. H ₂ O	Orifice Setting (ΔH), In H ₂ O	Gas Meter Temp °F	Pump Vacuum In. Hg Gauge	Filter Box Temp °F	Imp. Exit Temp °F	Stack Temp °F	
				Ideal Actual	In Out					
NW 1	0	475.221	.19	.59 .99	87 88	5.6		68	87	
2	10		.27	1.41 1.41	92 88	6.4		67	87	
3	20		.28	1.48 1.48	95 88	7.4		64	87	
4	30		.28	1.48 1.48	92 88	7.4		65	88	
5	40		.26	1.37 1.37	92 89	6.4		66	87	
6	50		.19	1.02 1.02	92 89	6		67	87	
NE 1	60		.18	.95 .95	94 89	6		68	87	
2	70		.28	1.48 1.48	95 89	7.4		66	88	
3	80		.32	1.69 1.69	96 89	8.4		66	89	
4	90		.28	1.48 1.48	95 87	7.4		67	88	
5	100		.27	1.42 1.42	92 85	7		67	88	
6	110		.21	1.11 1.11	91 87	6.4		68	88	
Emp	120	587.407								

1.322 90.9

Sample Type:	Bath Off - Blank Run 2
Sampling Date:	August 29, 1989
Sample Times:	10:08-12:09 (120 minutes)
Run Number:	1
Lab Numbers:	915486, 915487, 915489, 915491
Airflow:	21,403 dscf/min
Hexavalent Chromium	
Concentration:	0.105 mg/dscm
Concentration:	0.05 ppm
Emission Rate:	3818.9 mg/hr
Total Chromium	
Concentration:	0.096 mg/dscm
Concentration:	0.04 ppm
Emission Rate:	3492.5 mg/hr

METHOD 1-5 - HEXAVALENT CHROMIUM EMISSIONS
AM TEST, INC. - AIR QUALITY DIVISION

FILE NAME: 280W5CR1
CLIENT: BOEING PLANT #2
LOCATION: SEATTLE, WASHINGTON
SAMPLE SITE: BLDG 210/TANK #5
SAMPLE DATE: AUGUST 29, 1989
RUN #: 1-CR-6
OPERATORS: GUENTHOER/MACKAY
CONTACT: P. SIEBENALER

LAB #: 915486
START TIME: 10:08 O'CLOCK
STOP TIME: 12:09 O'CLOCK
SAMPLE TIME: 120.0 MINUTES
CONDITION: BATH OFF

HEXAVALENT CHROMIUM

HEXAVALENT CHROMIUM CONCENTRATION (ug): 331.5
HEXAVALENT CHROMIUM CONCENTRATION (mg/dscm): 0.105
HEXAVALENT CHROMIUM IN SAMPLE (ppm): 0.05
HEXAVALENT CHROMIUM EMISSION RATE (mg/hr): 3818.9

TOTAL CHROMIUM

TOTAL CHROMIUM CONCENTRATION (ug): 301.2
TOTAL CHROMIUM CONC. ON FILTER (ug): 2.0
TOTAL CHROMIUM CONCENTRATION (mg/dscm): 0.096
TOTAL CHROMIUM IN SAMPLE (ppm): 0.04
TOTAL CHROMIUM EMISSION RATE (mg/hr): 3492.5

FINAL WT. INIT. WT. NET WT.
OF H2O G. OF H2O G. OF H2O G.

1263.4 1251.8 11.6
634.2 631.9 2.3
478.7 473.9 4.8
772.8 746.1 26.7
TOTAL H2O GAIN: 45.4
TOTAL VOLUME (SCF) 2.14
PERCENT MOISTURE: 1.88
BWS: 0.0188

PITOT Cp: 0.840
NOZZLE DIA INCHES: 0.313
NOZZLE AREA FT^2: 0.0005
STACK DIA. INCHES: 48.00
STACK AREA FT^2: 12.566
METER TEMP. DEG F: 78.5
BAROM. PRES. "HG: 30.04
STATIC PRES. "H2O: 0.00
STACK PRES. "HG: 30.04
ORIFICE PRES "H2O: 1.403
METER PRES. "HG: 30.14

AVERAGE % CO2: 0.1
AVERAGE % O2: 20.9
AVERAGE % CO: 0
STACK GAS MW. DRY: 28.85
STACK GAS MW. NET: 28.65

INIT. METER VOL.: 734.162
FINAL METER VOL.: 847.802
VOLUME SAMPLED: 113.640
STD VOLUME (DSCF): 111.469
STD VOLUME (DSCM): 3.157
Y FACTOR: 0.993

SAMPLE POINT	VELOCITY " OF H2O	TEMPERATURE DEGREES F.	SAMPLE POINT	VELOCITY " OF H2O	TEMPERATURE DEGREES F.
NW 1	0.22	81	NE 1	0.23	82
2	0.27	82	2	0.29	82
3	0.30	82	3	0.33	83
4	0.29	82	4	0.29	84
5	0.26	82	5	0.29	84
6	0.21	83	6	0.27	85
PERCENT ISOKINETICS:					
		102 %			
STACK TEMPERATURE:		82.7 DEG. F.	542.7 DEG. R.		
AVERAGE VELOCITY HEAD:		0.270 " OF H2O			
STACK GAS VELOCITY:			29.62 FT/SEC.		
STACK GAS AIR FLOW:		22330.2 ACF/MIN.	21402.8 DSCF/MIN.		



2B-4-01 91548 TRAVERSE SAMPLING DATA

Page 1 of 1

Client Boeing
Date 3-29-89
Sample Location BLDG 2-10
PAV S. TOWER STAIR
Operators CRS & SM
Sample Box # A
Run# 1

SCHEMATIC TRAVERSE LAYOUT

Stack Diameter _____
Distance Upstream _____
Distance Downstream _____

Start Time 1009
Stop Time 1209
Barometric
Pressure "Hg 763
Static Pres "H₂O _____
Production Rate _____
BATH OFF

EQUIPMENT CHECKS

Initial/Final

Leak Rate Cfm 4.01 / .007Leak Test Vac 16 / 17

Pitots, Pretest

Pitots, Posttest

Orsat Sampling System

Tedlar Bag

Thermocouple @ _____ °F

Filter # _____ tare _____ mgs
Final Initial Net
Wt. Wt. Wt.

#1 Bubblers 1263.4 - 1251.2 = _____#2 Impinger 634.2 - 631.9 = _____#3 Bubblers 478.7 - 473.9 = _____#4 Silica
Gel 772.8 - 746.1 = _____

TOTAL WATER VOLUME _____

NOMOGRAPH SETUP

% Moisture 2
Meter Temp. 75
Stack Temp. 80
ΔH @ .943 Y .993
Pitot # AG Side # A
Cp 340
Nozzle Diameter .313
K Factor 5.18
Reference ΔP _____

Sample Point	Elap Time Min.	Dry Gas Meter Reading Cu. Ft.	Pitot Reading (ΔP), In. H ₂ O	Orifice Setting (ΔH), In H ₂ O	Gas Meter Temp °F	Pump Vacuum In. Hg Gauge	Filter Box Temp °F	Imp. Exit Temp °F	Stack Temp °F
NEV 1	0	734.162	.22	1.14	1.14	66 6A	6 1/2	67	81
2	10		.27	1.40	1.40	74 6A	7	61	82
3	20		.30	1.56	1.56	80 70	8 1/2	61	82
4	30		.29	1.50	1.50	83 72	8 1/2	58	82
5	40		.26	1.35	1.35	85 74	7	59	82
6	50		.21	1.09	1.09	85 76	6	59	83
NE 1	60		.23	1.19	1.19	83 76	6 1/2	60	82
2	70		.29	1.50	1.50	85 77	9	61	82
3	80		.33	1.71	1.71	88 79	9 1/2	63	82
4	90		.29	1.50	1.50	89 79	8	64	84
5	100		.29	1.50	1.50	89 80	8	64	84
6	110		.27	1.40	1.40	88 80	7 1/2	65	85
EXP	120	847.802							

1.403 78.5

Sample Type:	Bath Off - Blank Run 3
Sampling Date:	September 19, 1989
Sample Times:	10:22-12:23 (120 minutes)
Run Number:	1
Lab Numbers:	917067, 917068, 917069, 917077
Airflow:	20,651 dscf/min
Hexavalent Chromium	
Concentration:	0.008 mg/dscm
Concentration:	0.004 ppm
Emission Rate:	272.0 mg/hr
Total Chromium	
Concentration:	0.018 mg/dscm
Concentration:	0.009 ppm
Emission Rate:	645.4 mg/hr

METHOD 1-5 - HEXAVALENT CHROMIUM EMISSIONS
AM TEST, INC. - AIR QUALITY DIVISION

FILE NAME: 4805CR1	LAB #: 917077	HEXAVALENT CHROMIUM
CLIENT: BOEING PLANT #2	START TIME: 10:22 O'CLOCK	-----
LOCATION: SEATTLE, WASHINGTON	STOP TIME: 12:23 O'CLOCK	HEXAVALENT CHROMIUM CONCENTRATION (ug): 23.1
SAMPLE SITE: BLDG 210/TANK #5	SAMPLE TIME: 120.0 MINUTES	HEXAVALENT CHROMIUM CONCENTRATION (mg/dscm): 0.008
SAMPLE DATE: SEPTEMBER 19, 1989	CONDITION: BATH OFF	HEXAVALENT CHROMIUM IN SAMPLE (ppm): 0.004
RUN #: 1-CR-6		HEXAVALENT CHROMIUM EMISSION RATE (mg/hr): 272.0
OPERATORS: GUENTHER/MACKAY		-----
CONTACT: P. SIEBENALER		TOTAL CHROMIUM

FINAL WT. INIT. WT. NET WT. OF H2O G. OF H2O G.	PITOT Cp: 0.84	TOTAL CHROMIUM CONCENTRATION (ug): 54.6
448.5 454.9 -6.4	NOZZLE DIA INCHES: 0.313	TOTAL CHROMIUM CONC. ON FILTER (ug): 0.175
480.5 464.0 16.5	NOZZLE AREA FT^2: 0.0005	TOTAL CHROMIUM CONCENTRATION (mg/dscm): 0.018
434.9 429.1 5.8	STACK DIA. INCHES: 48.00	TOTAL CHROMIUM IN SAMPLE (ppm): 0.009
320.1 318.0 2.1	STACK AREA FT^2: 12.566	TOTAL CHROMIUM EMISSION RATE (mg/hr): 645.4
686.0 669.9 16.1	METER TEMP. DEG F: 74.6	
TOTAL H2O GAIN: 34.1	BAROM. PRES. "HG: 30.24	
TOTAL VOLUME (SCF) 1.61	STATIC PRES. "H2O: 0.00	
PERCENT MOISTURE: 1.51	STACK PRES. "HG: 30.24	
Bws: 0.0151	ORIFICE PRES "H2O: 1.255	
	METER PRES. "HG: 30.33	
INIT. METER VOL.: 444.328		
FINAL METER VOL.: 550.148	AVERAGE % CO2: 0.1	
VOLUME SAMPLED: 105.820	AVERAGE % O2: 20.9	
STD VOLUME (DSCF): 105.212	AVERAGE % CO: 0	
STD VOLUME (DSCM): 2.980	STACK GAS MW. DRY: 28.85	
Y FACTOR: 0.993	STACK GAS MW. NET: 28.69	

SAMPLE POINT	VELOCITY " OF H2O	TEMPERATURE DEGREES F.	SAMPLE POINT	VELOCITY " OF H2O	TEMPERATURE DEGREES F.
NV 1	0.20	78	NE 1	0.21	78
2	0.23	78	2	0.27	79
3	0.27	78	3	0.31	80
4	0.27	79	4	0.27	81
5	0.24	79	5	0.26	82
6	0.20	79	6	0.24	83

PERCENT ISOKINETICS:	100 %
STACK TEMPERATURE:	79.5 DEG. F.
AVERAGE VELOCITY HEAD:	0.246 " OF H2O
STACK GAS VELOCITY:	28.11 FT/SEC.
STACK GAS AIR FLOW:	20651.0 DSCF/MIN.



Page 1 of

480A-Cr / 917077

SCHEMATIC TRAVERSE LAYOUT

Start Time 10:22
Stop Time 12:23
Barometric Pressure "Hg 30.24
Static Pres "H₂O -0.02
Production Rate 1274 - O.F.F

NOMOGRAPH SETUP

2 Moisture

Meter Temp.

Stack Temp. 78

ΔΗΘ 943 Υ. 993

Pitot 4' Glass Side A

Cp 84

Nozzle Diameter .313

K Factor _____

Reference ΔP

Filter #	NA	tare	mgs
	Final	Initial	Net
	Wt.	Wt.	Wt.

#1	NaOH Bubbler	448.5	454.9	-
#2	NaOH Impinger	430.5	464.0	-
#3	NaOH Bubbler	434.9	429.1	-
#4	MT Silica Gel	320.1	318.0	
		686.0	669.9	=

TOTAL WATER VOLUME _____

[illegible]

SECTION 2
BATH ON RUNS
(PARTS IN BATH)

Sample Type:	Bath On - Run 1
Sampling Date:	August 22, 1989
Sample Times:	10:45-11:48 (60 minutes)
Run Number:	1
Lab Numbers:	915089, 915090, 915093, 915097 915100
Airflow:	20,704 dscf/min
Process Data	
Bath Amperage:	1825 amp-hr/hr
Voltage:	22.7 volts D.C.
Bath Temperature:	94° F
Ambient Temperature:	74° F
Hexavalent Chromium	
Concentration:	1.235 mg/dscm
Concentration:	0.57 ppm
Emission Rate:	43,457 mg/hr
Emission Factor:	23.8 mg/amp-hr
Total Chromium	
Concentration:	0.805 mg/dscm
Concentration:	0.37 ppm
Emission Rate:	28,305 mg/hr
Emission Factor:	15.5 mg/amp-hr

METHOD 1-5 - HEXAVALENT AND TOTAL CHROMIUM EMISSIONS
AM TEST, INC. - AIR QUALITY DIVISION

FILE NAME: 180W5CR1
CLIENT: BOEING PLANT #2
LOCATION: SEATTLE, WASHINGTON
SAMPLE SITE: BLDG 210/TANK #5
SAMPLE DATE: AUGUST 22, 1989
RUN #: 1-CR-6
OPERATORS: GUENTHER/MACKAY
CONTACT: P. SIEBENALER

LAB #: 915090
START TIME: 10:45 O'CLOCK
STOP TIME: 11:48 O'CLOCK
SAMPLE TIME: 60.0 MINUTES
CONDITION: BATH ON

HEXAVALENT CHROMIUM

HEXAVALENT CHROMIUM CONCENTRATION (ug): 1874.0
HEXAVALENT CHROMIUM IN SAMPLE (mg/dscm): 1.235
HEXAVALENT CHROMIUM EMISSION RATE (mg/hr): 0.57
HEXAVALENT CHROMIUM EMISSION RATE (mg/hr): 43456.5
AMPHERE HOURS PER HOUR (amp-hr/hr): 1825
HEX. CHROMIUM EMISSION FACTOR (mg/amp-hr): 23.8

FINAL WT. INIT. WT. NET WT.
OF H2O G. OF H2O G. OF H2O G.

1252.3 1246.9 5.4
628.3 628.2 0.1
472.5 471.4 1.1
722.0 711.9 10.1
TOTAL H2O GAIN: 16.7
TOTAL VOLUME (SCF) 0.79
PERCENT MOISTURE: 1.45
BWS: 0.0145

PITOT Cp: 0.84
NOZZLE DIA INCHES: 0.313
NOZZLE AREA FT^2: 0.0005
STACK DIA. INCHES: 48.00
STACK AREA FT^2: 12.566
METER TEMP. DEG F: 75.0
BAROM. PRES. "HG: 30.04
STATIC PRES. "H2O: 0.00
STACK PRES. "HG: 30.04
ORIFICE PRES "H2O: 1.278
METER PRES. "HG: 30.13

HEXAVALENT CHROMIUM

TOTAL CHROMIUM CONCENTRATION (ug): 1220.6
TOTAL CHROMIUM CONC. ON FILTER (ug): < 0.15
TOTAL CHROMIUM CONCENTRATION (mg/dscm): 0.805
TOTAL CHROMIUM IN SAMPLE (ppm): 0.37
TOTAL CHROMIUM EMISSION RATE (mg/hr): 28304.7
AMPHERE HOURS PER HOUR (amp-hr/hr): 1825
TOTAL CHROMIUM EMISSION FACTOR (mg/amp-hr): 15.5

INIT. METER VOL.: 364.682
FINAL METER VOL.: 418.957
VOLUME SAMPLED: 54.275
STD VOLUME (DSCF): 53.570
STD VOLUME (DSCM): 1.517
Y FACTOR: 0.993

AVERAGE % CO2: 0.1
AVERAGE % O2: 20.9
AVERAGE % CO: 0
STACK GAS MJ. DRY: 28.85
STACK GAS MJ. WET: 28.69

SAMPLE POINT	VELOCITY " OF H2O	TEMPERATURE DEGREES F.	SAMPLE POINT	VELOCITY " OF H2O	TEMPERATURE DEGREES F.
NW 1	0.20	78	NE 1	0.19	78
2	0.25	79	2	0.27	78
3	0.27	78	3	0.31	78
4	0.28	78	4	0.28	79
5	0.26	78	5	0.26	80
6	0.20	78	6	0.23	80

PERCENT ISOKINETICS: 101 %
STACK TEMPERATURE: 78.5 DEG. F. 538.5 DEG. R.
AVERAGE VELOCITY HEAD: 0.249 " OF H2O
STACK GAS VELOCITY: 28.30 FT/SEC.
STACK GAS AIR FLOW: 21340.7 ACF/MIN. 20704.1 DSCF/MIN.

AT

18

130# Cr 1

915090

TRAVERSE SAMPLING DATA

Page 1 of 1

Client BOEING - PLT #2
 Date 8-22-89
 Sample Location Bldg 2-10
TANK H 5 Exhaust
 Operators JAG - KSM
 Sample Box # A
 Run# 1 - Cr

EQUIPMENT CHECKS

Initial/Final
 Leak Rate Cfm 1.04 / 1.01
 Leak Test Vac 5 / 11"
 Pitots, Pretest
 Pitots, Posttest
 Orsat Sampling System
 Tedlar Bag
 Thermocouple @ _____ °F

SCHEMATIC TRAVERSE LAYOUT

Stack Diameter 48"
 Distance Upstream _____
 Distance Downstream _____

Filter # _____ tare _____ mgs
 Final Initial Net
 Wt. Wt. Wt.
 #1 ^{NACH} Bubblers 1252.3 - 1246.9 = _____
 #2 ^{HU} Impinger 628.3 - 628.2 = _____
 #3 ^{MT} Bubblers 472.5 - 471.4 = _____
 #4 Silica Gel 722.0 - 711.9 = _____
 TOTAL WATER VOLUME 16.7

Start Time 1045
 Stop Time 11:48
 Barometric 30.04"
 Pressure "Hg 763 mm
 Static Pres "H₂O _____
 Production Rate _____
BATH ON

NOMOGRAPH SETUP

% Moisture 2
 Meter Temp. 70
 Stack Temp. 80
 ΔHe .943 y .943
 Pitot# 4 Side# A
 Cp .84
 Nozzle Diameter .313
 K Factor 5.14
 Reference ΔP _____

Sample Point	Elap Time Min.	Dry Gas Meter Reading Cu. Ft.	Pitot Reading (ΔP), In. H ₂ O	Orifice Setting (ΔH), In H ₂ O		Gas Meter Temp °F		Pump Vacuum In. Hg Gauge	Filter Box Temp °F	Imp. Exit Temp °F	Stack Temp °F
				Ideal	Actual	In	Out				
NW 1	0	364.68	.20	1.03	1.03	66	66	5.4		66	78
2	5		.15	1.28	1.28	72	66	6.4	N/A	58	79
3	10		.22	1.39	1.39	74	67	7.4		61	78
4	15		.28	1.43	1.43	78	68	7.4		61	78
5	20		.26	1.34	1.34	80	69	7		61	78
6	25		.20	1.03	1.03	81	70	5.5		60	78
NE 1	30		.19	.98	.98	78	72	5		59	78
2	35		.27	1.39	1.39	82	73	7.0		58	79
3	40		.31	1.59	1.59	84	74	8.5		59	78
4	45		.28	1.43	1.43	85	74	7.5		60	78
5	50		.26	1.34	1.34	85	75	7.0		60	80
6	55		.23	1.18	1.18	85	76	6.0		60	80
END	60	418.957									

24 352

1.278

75.0

August 22, 1989

<u>Time</u>	<u>Amps</u>
<u>Run 1:</u> 1050	200
1055	1820
1100	1820
1105	1820
1110	1820
1115	1820
1120	1820
1145	1820

Cycle is 55 minutes

1825 $\frac{\text{amp-hr}}{\text{hr}}$

ambient temp 74°F

<u>Time</u>	<u>Amps</u>
<u>Run 2:</u> 1400	0
1401	200
1403	1820
1405	1820
1407	1820
1410	1820
1415	1820
1420	1820
1425	1820
1430	1820
1435	1820
1440	1820
1445	1820
1450	1820
1455	1820

3 min.

52 min.

Sample Calculation - Run 2

$$(3 \text{ min} * 200 \text{ amps} + 52 \text{ min} * 1820 \text{ amps}) / 55 \text{ min} * \frac{60 \text{ min/hr}}{55 \text{ min}}$$

$$= \underline{\underline{1889}} \text{ amp-hr/hr}$$

Sample Type:	Bath On - Run 2
Sampling Date:	August 22, 1989
Sample Times:	14:01-15:03 (60 minutes)
Run Number:	2
Lab Numbers:	915091, 915094, 915098, 915101
Airflow:	20,555 dscf/min
Process Data	
Bath Amperage:	1889 amp-hr/hr
Voltage:	22.7 volts D.C.
Bath Temperature:	94° F
Ambient Temperature:	83° F
Hexavalent Chromium	
Concentration:	1.389 mg/dscm
Concentration:	0.64 ppm
Emission Rate:	48,503 mg/hr
Emission Factor:	25.7 mg/amp-hr
Total Chromium	
Concentration:	0.759 mg/dscm
Concentration:	0.35 ppm
Emission Rate:	26,494 mg/hr
Emission Factor:	14.0 mg/amp-hr

METHOD 1-5 - HEXAVALENT CHROMIUM EMISSIONS
AM TEST, INC. - AIR QUALITY DIVISION

FILE NAME: 1805CR2 LAB #: 915091
CLIENT: BOEING PLANT #2 START TIME: 14:01 O'CLOCK
LOCATION: SEATTLE, WASHINGTON STOP TIME: 15:03 O'CLOCK
SAMPLE SITE: BLDG 210/TANK #5 SAMPLE TIME: 60.0 MINUTES
SAMPLE DATE: AUGUST 22, 1989 CONDITION: BATH ON
RUN #: 2-CR-6
OPERATORS: GUENTHER/MACKEY
CONTACT: P. STEBENALER

FINAL WT. INIT. WT. NET WT.
OF H2O G. OF H2O G. OF H2O G.
1253.0 1247.1 5.9
624.8 623.6 1.2
532.0 531.5 0.5
833.0 822.8 10.2
TOTAL H2O GAIN: 17.8
TOTAL VOLUME (SCF) 0.84
PERCENT MOISTURE: 1.55
BWS: 0.0155
PITOT CP: 0.84
NOZZLE DIA INCHES: 0.313
NOZZLE AREA FT^2: 0.0005
STACK DIA. INCHES: 48.00
STACK AREA FT^2: 12.566
METER TEMP. DEG F: 85.9
BAROM. PRES. "HG: 30.04
STATIC PRES. "H2O: 0.00
STACK PRES. "HG: 30.04
ORIFICE PRES "H2O: 1.294
METER PRES. "HG: 30.14

INIT. METER VOL.: 419.767
FINAL METER VOL.: 474.771
VOLUME SAMPLED: 55.004
STD VOLUME (DSCF): 53.208
STD VOLUME (DSCM): 1.507
Y FACTOR: 0.993
AVERAGE % CO2: 0.1
AVERAGE % O2: 20.9
AVERAGE % CO: 0
STACK GAS MW. DRY: 28.85
STACK GAS MW. WET: 28.68

SAMPLE POINT	VELOCITY " OF H2O	TEMPERATURE DEGREES F.	SAMPLE POINT	VELOCITY " OF H2O	TEMPERATURE DEGREES F.
NE 1	0.21	86	NW 1	0.18	86
2	0.27	86	2	0.26	86
3	0.31	85	3	0.28	86
4	0.27	85	4	0.27	85
5	0.26	85	5	0.25	85
6	0.24	86	6	0.20	84
PERCENT ISOKINETICS: 102 %					
STACK TEMPERATURE:		85.4 DEG. F.	545.4 DEG. R.		
AVERAGE VELOCITY HEAD:		0.249 " OF H2O	28.49 FT/SEC.		
STACK GAS VELOCITY:		21482.2 ACF/MIN.	20555.4 DSCF/MIN.		

HEXAVALENT CHROMIUM

HEXAVALENT CHROMIUM CONCENTRATION (ug): 2092.5
HEXAVALENT CHROMIUM IN SAMPLE (ppm): 1.389
HEXAVALENT CHROMIUM EMISSION RATE (mg/hr): 0.642
AMPHERE HOURS PER HOUR (amp-hr/hr): 48502.8
HEX. CHROMIUM EMISSION FACTOR (mg/amp-hr): 1889
HEX. CHROMIUM EMISSION FACTOR (mg/amp-hr): 25.7

TOTAL CHROMIUM

TOTAL CHROMIUM CONCENTRATION (ug): 1143.0
TOTAL CHROMIUM CONC. ON FILTER (ug): < 0.18
TOTAL CHROMIUM CONCENTRATION (mg/dscm): 0.759
TOTAL CHROMIUM IN SAMPLE (ppm): 0.35
TOTAL CHROMIUM EMISSION RATE (mg/hr): 26494.0
AMPHERE HOURS PER HOUR (amp-hr/hr): 1889
TOTAL CHROMIUM EMISSION FACTOR (mg/amp-hr): 14.0

TRAVERSE SAMPLING DATA

Page 1 of

1B0#5C72 915091 TRA
Client BOEING-PLNT #2
Date 8-22-89
Sample Location BLDG 2-10
TANK #5 Exhaust
Operators JAG-RSM
Sample Box 1
Run# 2-Cr

EQUIPMENT CHECKS

Initial/Final

Leak Rate Cfm 2.02/2.01

Leak Test Vac 12/18"✓

 Pitots, Pretest

 Pitots, Posttest

 Orsat Sampling System

 Tedlar Bag

 Thermocouple @ °F

SCHEMATIC TRAVERSE LAYOUT

Stack Diameter _____
Distance Upstream _____
Distance Downstream _____

Filter #	Final Wt.	tare Initial Wt.	Net Wt.	mg
#1 ^{NaOH} Bubbler	<u>1253.0</u>	- <u>1247.1</u>	-	
#2 ^{imp} Impinger	<u>624.8</u>	- <u>623.6</u>	-	
#3 ^{mt} Bubbler	<u>532.0</u>	- <u>531.5</u>	-	
#4 ^{Silica} Gel	<u>833.0</u>	- <u>822.8</u>	-	
TOTAL WATER VOLUME				

Start Time 14:21
Stop Time 15:03
Barometric Pressure "Hg 763
Static Pres "H₂O _____
/ Production Rate _____
BATH - ON

NOMOGRAPH SETUP

% Moisture 2
Meter Temp. _____
Stack Temp. _____
ΔH@ M² Y 593
Pitot# Side#
Cp 8d
Nozzle Diameter 3.3
K Factor _____
Reference ΔP _____

[illegible]

August 22, 1989

<u>Time</u>	<u>Amps</u>
<u>Run 1:</u> 1050	200
1055	1820
1100	1820
1105	1820
1110	1820
1115	1820
1120	1820
1145	1820

Cycle is 55 minutes

$$\frac{1825 \text{ amp-hr}}{\text{hr}}$$

<u>Time</u>	<u>Amps</u>
<u>Run 2:</u> 1400	0
1401	200
1403	1820
1405	1820
1407	1820
1410	1820
1415	1820
1420	1820
1425	1820
1430	1820
1435	1820
1440	1820
1445	1820
1450	1820
1455	1820

3 min.

52 min.

Sample Calculation - Run 2

$$(3 \text{ min} * 200 \text{ amps} + 52 \text{ min} * 1820 \text{ amps}) / 55 \text{ min} * \frac{60 \text{ min/hr}}{55 \text{ min}}$$

$$= \underline{\underline{1889}} \text{ amp-hr/hr}$$

ambient temp 83°F
 bath temp 94°F
 temp. above tank 86°F

Sample Type:	Bath On - Run 3
Sampling Date:	August 31, 1989
Sample Times:	12:15-13:15 (60 minutes)
Run Number:	2
Lab Numbers:	915750, 915751, 915752, 915753 915754
Airflow:	21,546 dscf/min
Process Data	
Bath Amperage:	477 amp-hr/hr (small load)
Voltage:	21.8 volts D.C.
Bath Temperature:	94° F
Ambient Temperature:	82° F
Hexavalent Chromium	
Concentration:	0.438 mg/dscm
Concentration:	0.20 ppm
Emission Rate:	16,029 mg/hr
Emission Factor:	33.6 mg/amp-hr
Total Chromium	
Concentration:	0.431 mg/dscm
Concentration:	0.20 ppm
Emission Rate:	15,775 mg/hr
Emission Factor:	33.1 mg/amp-hr

METHOD 1-5 - HEXAVALENT AND TOTAL CHROMIUM EMISSIONS
AM TEST, INC. - AIR QUALITY DIVISION

FILE NAME: 380W5CR2
CLIENT: BOEING PLANT #2
LOCATION: SEATTLE, WASHINGTON
SAMPLE SITE: BLDG 210/TANK #5
SAMPLE DATE: AUGUST 31, 1989
RUN #: 2-CR+6
OPERATORS: GLENTHOER/VIDMEYER
CONTACT: P. SIEBENALER

LAB #: 915750
START TIME: 12:15 O'CLOCK
STOP TIME: 13:15 O'CLOCK
SAMPLE TIME: 60.0 MINUTES
CONDITION: BATH ON

HEXAVALENT CHROMIUM

HEXAVALENT CHROMIUM CONCENTRATION (ug): 689.3
HEXAVALENT CHROMIUM IN SAMPLE (mg/dscm): 0.438
HEXAVALENT CHROMIUM EMISSION RATE (mg/hr): 0.203
AMPHERE HOURS PER HOUR (amp-hr/hr): 16028.6
HEX. CHROMIUM EMISSION FACTOR (mg/amp-hr): 477
33.6

TOTAL CHROMIUM

TOTAL CHROMIUM CONCENTRATION (ug): 678.4
TOTAL CHROMIUM CONC. ON FILTER (ug): < 0.30
TOTAL CHROMIUM IN SAMPLE (mg/dscm): 0.431
TOTAL CHROMIUM EMISSION RATE (mg/hr): 0.20
AMPHERE HOURS PER HOUR (amp-hr/hr): 15774.9
TOTAL CHROMIUM EMISSION FACTOR (mg/amp-hr): 477
33.1

FINAL WT. INIT. WT. NET WT.
OF H2O G. OF H2O G. OF H2O G.
1188.1 1180.1 8.0
570.0 570.2 -0.2
480.6 480.8 -0.2
736.2 724.7 11.5
TOTAL H2O GAIN: 19.1
TOTAL VOLUME (SCF) 0.90
PERCENT MOISTURE: 1.59
BWS: 0.0159

INIT. METER VOL.: 2.263
FINAL METER VOL.: 58.832
VOLUME SAMPLED: 56.569
STD VOLUME (DSCF): 55.594
STD VOLUME (DSCM): 1.574
Y FACTOR: 0.993
AVERAGE % CO2: 0.1
AVERAGE % O2: 20.9
AVERAGE % CO: 0
STACK GAS MW. DRY: 28.85
STACK GAS MW. WET: 28.68

SAMPLE POINT	VELOCITY " OF H2O	TEMPERATURE DEGREES F.	SAMPLE POINT	VELOCITY " OF H2O	TEMPERATURE DEGREES F.
NV 1	0.24	80	NE 1	0.24	83
2	0.30	80	2	0.28	83
3	0.33	81	3	0.31	83
4	0.29	82	4	0.31	84
5	0.26	83	5	0.29	84
6	0.24	83	6	0.19	83

PERCENT ISOKINETICS: 101 %
STACK TEMPERATURE: 82.4 DEG. F.
AVERAGE VELOCITY HEAD: 0.272 " OF H2O
STACK GAS VELOCITY: 29.71 FT/SEC.
STACK GAS AIR FLOW: 22402.8 ACF/MIN.
21545.8 DSCF/MIN.

415750 TRAVERSE SAMPLING DATA

Page 1 of

Client <u>Boeing</u> Date <u>8-31-87</u> Sample Location <u>TB12-10</u> <u>Tank #4 Exhaust</u> Operators <u>JAB, JMW</u> Sample Box # <u>C</u> Run# <u>2 Cr¹⁰/Cr</u> EQUIPMENT CHECKS Initial/Final Leak Rate Cfm <u>1.07-0.08</u> Leak Test Vac <u>15/20</u> ☒ Pitots, Pretest ☒ Pitots, Posttest ☒ Orsat Sampling System ☒ Tedlar Bag Thermocouple @ _____ °F	SCHEMATIC TRAVERSE LAYOUT Stack Diameter _____ Distance Upstream _____ Distance Downstream _____ <table border="1" style="width:100%; border-collapse: collapse;"> <tr> <th>Filter #</th> <th>tare</th> <th>mgs</th> </tr> <tr> <td></td> <td>Final</td> <td>Initial</td> </tr> <tr> <td></td> <td>Wt.</td> <td>Wt.</td> </tr> <tr> <td>#1 Bubbler</td> <td><u>585.3</u></td> <td><u>1180.1</u></td> </tr> <tr> <td>#2 Impinger</td> <td><u>570.0</u></td> <td><u>570.2</u></td> </tr> <tr> <td>#3 Bubbler</td> <td><u>480.6</u></td> <td><u>480.8</u></td> </tr> <tr> <td>#4 Silica Gel</td> <td><u>736.2</u></td> <td><u>724.7</u></td> </tr> </table> TOTAL WATER VOLUME _____	Filter #	tare	mgs		Final	Initial		Wt.	Wt.	#1 Bubbler	<u>585.3</u>	<u>1180.1</u>	#2 Impinger	<u>570.0</u>	<u>570.2</u>	#3 Bubbler	<u>480.6</u>	<u>480.8</u>	#4 Silica Gel	<u>736.2</u>	<u>724.7</u>	Start Time <u>1215</u> Stop Time <u>1315</u> Barometric Pressure "Hg <u>71.6</u> Static Pres "H₂O _____ Production Rate _____ NOMOGRAPH SETUP % Moisture _____ Meter Temp. _____ Stack Temp. _____ ΔH@ <u>947.5</u> _____ Pitot# _____ Side# _____ Cp <u>0.40</u> Nozzle Diameter <u>3.3</u> K Factor _____ Reference ΔP _____
Filter #	tare	mgs																					
	Final	Initial																					
	Wt.	Wt.																					
#1 Bubbler	<u>585.3</u>	<u>1180.1</u>																					
#2 Impinger	<u>570.0</u>	<u>570.2</u>																					
#3 Bubbler	<u>480.6</u>	<u>480.8</u>																					
#4 Silica Gel	<u>736.2</u>	<u>724.7</u>																					

Sample Point	Elap Time Min.	Dry Gas Meter Reading Cu. Ft.	Pitot Reading (ΔP), In. H ₂ O	Orifice Setting (ΔH), In H ₂ O		Gas Meter Temp °F		Pump Vacuum In. Hg Gauge	Filter Box Temp °F	Imp. Exit Temp °F	Stack Temp °F
				Ideal	Actual	In	Out				
NW 1	0	2.263	.24	1.20	1.20	70	70	6		64	80
2	5		.30	1.54	1.54	74	70	7		58	80
3	10		.33	1.69	1.69	79	71	7.4	NA	63	81
4	15		.27	1.07	1.07	80	72	7		62	82
5	20		.26	1.34	1.34	82	73	6.14		60	82
6	25		.24	1.25	1.25	83	74	6		60	83
NE 1	30		.24	1.25	1.25	82	75	6		61	83
2	35		.28	1.46	1.46	84	76	7		58	83
3	40		.31	1.61	1.61	85	76	7.14		58	83
4	45		.29	1.61	1.61	86	77	7.4		60	84
5	50		.29	1.51	1.51	86	77	7		60	84
6	55		.19	1.99	1.99	85	77	6		60	83
END	60	8.832									

1.418 77.7

8/31/84

27

Run Z
(Method 5A)

Parts into bath @ 12:13
Parts removed @ 1:09

Material into bath is 3 rows of $\frac{3}{8}$ " Tubin. (6 tubes total)

Called Relatively Small Load & this is why Amps

55 min cycle

1 min	12:14	5 V
1 min	12:15	5 V
3 min	12:16	12.0 V
7 min	12:19	22.3 V
	12:26	22.9 V
	12:33	23.2 V
43 min	12:43	23.2 V
	12:53	23.2 V
	1:02	23.3 V
	1:09	0.5 V (off)

200 Amps
250 Amps
550 Amps
680 Amps
450 Amps
450 Amps
400 Amps
400 Amps
400 Amps
0 Amps

$(1 \times 200 + 1 \times 250 + 3 \times 550 + 8 \times 680 + 43 \times 400) / 55 \times \frac{60}{55}$

94.0°F Bath Temp
82°F Ambient

477 Amp-hr / hr
21.8 volts

$$1 \times 5 + 1 \times 5 + 3 \times 12 + 7 \times 22.3 + 7 \times 22.9 + 36 \times 23.2$$

Third Anodic Bath without stack testing:

Parts into bath @ 1:19
Parts removed from bath @ 2:14

23.2V 1820 Amps
94.0°F 84°F Ambient

Velocity Measurements after turn Bath & Before Run #1:

Opening #

- 1
- 6
- 1
- 16
- 2
- 26
- 31
- 36
- 41
- 44
- 51
- 52

ft/min

- 2380
- 2230
- 1650
- 1700
- 1610
- 1390
- 720
- 1000
- 820
- 790
- 720
- 280

Measured 2:40 - 2:50 PM

Sample Type:	Bath On - Run 4
Sampling Date:	August 31, 1989
Sample Times:	15:58-16:59 (60 minutes)
Run Number:	3
Lab Numbers:	915755, 915756, 915757, 915758 915759
Airflow:	21,746 dscf/min
Process Data	
Bath Amperage:	464 amp-hr/hr (small load)
Voltage:	21.5 volts D.C.
Bath Temperature:	94° F
Ambient Temperature:	82° F
Hexavalent Chromium	
Concentration:	0.457 mg/dscm
Concentration:	0.21 ppm
Emission Rate:	16,873 mg/hr
Emission Factor:	36.4 mg/amp-hr
Total Chromium	
Concentration:	0.418 mg/dscm
Concentration:	0.19 ppm
Emission Rate:	15,463 mg/hr
Emission Factor:	33.3 mg/amp-hr

METHOD 1-5 - HEXAVALENT AND TOTAL CHROMIUM EMISSIONS
AM TEST, INC. - AIR QUALITY DIVISION

FILE NAME: 380W5CR3
CLIENT: BOEING PLANT #2
LOCATION: SEATTLE, WASHINGTON
SAMPLE SITE: BLDG 210/TANK #5
SAMPLE DATE: AUGUST 31, 1969
RUN #: 3-CR+6
OPERATORS: GUENTHER/NIDMEYER
CONTACT: P. STEBEMALER

LAB #:
START TIME: 15:58 O'CLOCK
STOP TIME: 16:59 O'CLOCK
SAMPLE TIME: 60.0 MINUTES
CONDITION: BATH ON

FINAL WT. INIT. WT. MET WT. OF H2O G. OF H2O G.
641.6 636.9 4.7
627.4 624.5 2.9
1162.8 1161.6 1.2
812.5 798.6 13.9
TOTAL H2O GAIN: 22.7
TOTAL VOLUME (SCF) 1.07
PERCENT MOISTURE: 1.85
BWS: 0.0185

PITOT CP: 0.840
NOZZLE DIA INCHES: 0.313
NOZZLE AREA FT^2: 0.0005
STACK DIA. INCHES: 48.00
STACK AREA FT^2: 12.566
METER TEMP. DEG F: 79.6
BAROM. PRES. "HG: 30.20
STATIC PRES. "HG: 0.00
STACK PRES. "HG: 30.20
ORIFICE PRES "H2O: 1.447
METER PRES. "HG: 30.31

INIT. METER VOL.: 59.658
FINAL METER VOL.: 117.286
VOLUME SAMPLED: 57.628
STD VOLUME (DSCF): 56.717
STD VOLUME (DSCM): 1.606
Y FACTOR: 0.993

AVERAGE % CO2: 0.1
AVERAGE % O2: 20.9
AVERAGE % CO: 0
STACK GAS MW. DRY: 28.85
STACK GAS MW. WET: 28.65

SAMPLE POINT	VELOCITY " OF H2O	TEMPERATURE DEGREES F.	SAMPLE POINT	VELOCITY " OF H2O	TEMPERATURE DEGREES F.
NW 1	0.22	83	NE 1	0.24	83
2	0.29	83	2	0.31	84
3	0.31	81	3	0.33	84
4	0.31	82	4	0.31	84
5	0.26	83	5	0.29	84
6	0.22	83	6	0.25	84

PERCENT ISO KINETICS: 102 %
STACK TEMPERATURE: 83.2 DEG. F.
AVERAGE VELOCITY HEAD: 0.277 " OF H2O
STACK GAS VELOCITY: 29.95 FT/SEC.
STACK GAS AIR FLOW: 21745.4 DSCF/MIN.

HEXAVALENT CHROMIUM

HEXAVALENT CHROMIUM CONCENTRATION (ug): 733.5
HEXAVALENT CHROMIUM CONCENTRATION (mg/dscm): 0.457
HEXAVALENT CHROMIUM IN SAMPLE (ppm): 0.21
HEXAVALENT CHROMIUM EMISSION RATE (mg/hr): 16873.4
AMPHERE HOURS PER HOUR (amp-hr/hr): 464
HEX. CHROMIUM EMISSION FACTOR (mg/amp-hr): 36.4

TOTAL CHROMIUM

TOTAL CHROMIUM CONCENTRATION (ug): 672.2
TOTAL CHROMIUM CONC. ON FILTER (ug): < 0.30
TOTAL CHROMIUM CONCENTRATION (mg/dscm): 0.418
TOTAL CHROMIUM IN SAMPLE (ppm): 0.19
TOTAL CHROMIUM EMISSION RATE (mg/hr): 15463.3
AMPHERE HOURS PER HOUR (amp-hr/hr): 464
TOTAL CHROMIUM EMISSION FACTOR (mg/amp-hr): 33.3



3 B0#5 Cr 3

915755 TRAVERSE SAMPLING DATA

Page 1 of 1

Client Boeing
Date 8-31-89
Sample Location Bldg 2-10
TANK 5 Exhaust Stack
Operators _____
Sample Box # B
Run# 3

EQUIPMENT CHECKS

Initial/Final

Leak Rate Cfm 1.01 / 1.004Leak Test Vac 20 / 19

Pitots, Pretest

Pitots, Posttest

Orsat Sampling System

Tedlar Bag

Thermocouple @ _____ °F

SCHEMATIC TRAVERSE LAYOUT

Stack Diameter _____

Distance Upstream _____

Distance Downstream _____

Filter # 3 tare _____ mgs
Final Initial Net
Wt. Wt. Wt.

#1 Bubbler 641.6 - 636.9 - _____#2 Impinger 627.4 - 624.5 - _____#3 Bubbler 626.2 - 626.1 - _____#4 Silica 536.6 - 535.5 - _____#4 Gel 812.5 - 799.6 - _____

TOTAL WATER VOLUME _____

Start Time 1558
Stop Time 1659
Barometric 30.20
Pressure "Hg 767
Static Pres "H₂O _____
Production Rate _____
Bath on

NOMOGRAPH SETUP

X Moisture _____

Meter Temp. _____

Stack Temp. _____

ΔH @ .943 y .593

Pitot# _____ Side# _____

Cp .840Nozzle Diameter .313

K Factor _____

Reference ΔP _____

Sample Point	Elap Time Min.	Dry Gas Meter Reading Cu. Ft.	Pitot Reading (ΔP), In. H ₂ O	Orifice Setting (ΔH), In H ₂ O		Gas Meter Temp °F		Pump Vacuum In. Hg Gauge	Filter Box Temp °F	Imp. Exit Temp °F	Stack Temp °F
				Ideal	Actual	In	Out				
NW 1	0	58.658	.27	1.14	1.14	78	71	6.6		65	83
2	3		.29	1.51	1.51	74	72	9		54	83
3	10		.31	1.61	1.61	77	72	9.2	12/17	54	81
4	15		.31	1.61	1.61	79	74	9.4		57	82
5	20		.26	1.35	1.35	80	76	8		59	83
6	25		.22	1.14	1.10	80	77	7		60	83
NW 7	30		.24	1.25	1.25	85	78	7.6		60	83
2	35		.31	1.61	1.61	80	78	9.6		58	84
3	40		.33	1.72	1.72	88	79	10		59	84
4	45		.31	1.61	1.61	89	79	9.6		61	84
5	50		.29	1.51	1.51	88	80	9		61	84
6	55		.25	1.70	1.70	88	80	8		61	84
END	60	112.286									

1.447 79.6

1.00

8/31/81 Boeing Plant 2

31

Run 3

(Method 6) Parts Dipped into Tank 5 @ 3:58 PM

Power On @ 3:59 PM

Parts Removed from Tank @ 4:54 PM

Same Exact Type as Run 2 + all
(40 tubes: 3x22 @ 1/3)

3 min 3:59	5.1V	180 amps
4 min 4:00	17.0V	750 amps
4 min 4:02	22.5V	500 amps
2 min 4:06	22.7V	420 amps
26 4:08	22.8V	420 amps
4:10	23.0V	400 amps
6 min 4:34	23.0V	400 amps
4:37	23.0V	390 amps
7 min 4:40	23.0V	400 amps
7 min 4:47	23.0V	
4:54		

93.5°F Bath

82°F Ambient

$$(3 * 180 + 4 * 750 + 2 * 500 + 26 * 420 + 13 * 400 + 7 * 390) / 55 * 60 / 55 = 464$$

$$(3 * 5.1 + 4 * 17 + 2 * 22.5 + 2 * 22.7 + 24 * 22.8 + 20 * 23) / 55 = 21.5 \text{ V}$$

Sample Type:	Bath On - Run 5
Sampling Date:	September 19, 1989
Sample Times:	13:00-14:01 (60 minutes)
Run Number:	2
Lab Numbers:	917070, 917071, 917072, 917078
Airflow:	20,402 dscf/min
Process Data	
Bath Amperage:	1853 amp-hr/hr
Voltage:	21.1 volts D.C.
Bath Temperature:	94° F
Ambient Temperature:	80° F
Hexavalent Chromium	
Concentration:	0.947 mg/dscm
Concentration:	0.44 ppm
Emission Rate:	32,818 mg/hr
Emission Factor:	17.7 mg/amp-hr
Total Chromium	
Concentration:	0.916 mg/dscm
Concentration:	0.42 ppm
Emission Rate:	31,747 mg/hr
Emission Factor:	17.1 mg/amp-hr



TRAVERSE SAMPLING DATA

480#5Cr2 917078

Client Pan (Plant # 2)
Date 6/19/88
Sample Location Side 2
#5 Chrom TANK Syband
Operators SMG - RSM
Sample Box # Blue 2
Run# 2-10

EQUIPMENT CHECKS

Initial/Final

Leak Rate Cfm 1.005 / 1.002Leak Test Vac 15 / 15☒ Pitots, Pretest☒ Pitots, Posttest☒ Orsat Sampling System☒ Tedlar BagThermocouple @ °F

SCHEMATIC TRAVERSE LAYOUT

Stack Diameter
Distance Upstream
Distance Downstream

Filter #	tare		mgs
	Final Wt.	Initial Wt.	
#1 Bubbler	447.8	445.5	
#2 Impinger	447.4	442.6	
#3 Bubbler	380.4	378.7	
#4 Silica	320.4	319.1	
Gel	608.3	599.6	

TOTAL WATER VOLUME

Start Time 1300
Stop Time 1401
Barometric 30.24"
Pressure "Hg 968mm
Static Pres "H₂O -0.02
Production Rate

NOMOGRAPH SETUP

% Moisture
Meter Temp.
Stack Temp.
ΔH 993 y 993
Pitot# Side#
Cp .84
Nozzle Diameter .312
K Factor
Reference ΔP

Sample Point	Elap Time Min.	Dry Gas Meter Reading Cu. Ft.	Pitot Reading (ΔP), In. H ₂ O	Orifice Setting (ΔH), In H ₂ O		Gas Meter Temp °F		Pump Vacuum In. Hg Gauge	Filter Box Temp °F	Imp. Exit Temp °F	Stack Temp °F
				Ideal	Actual	In	Out				
N 1	0	550.430	.20	1.04	1.04	73	44	4	N/A	63	82
2	5		.25	1.30	1.30	76	74	5		58	82
3	10		.31	1.62	1.62	80	75	6		57	83
4	15		.28	1.46	1.46	83	76	5 1/2		57	83
5	20		.25	1.30	1.30	84	76	5		61	83
6	25		.20	1.15	1.15	84	77	4 1/2		57	84
W 1	30		.22	1.15	1.15	83	78	4 1/2		56	84
2	35		.26	1.36	1.36	86	76	5		56	84
3	40		.29	1.52	1.52	86	79	5 1/2		56	84
4	45		.24	1.52	1.52	87	79	5 1/2		56	84
5	50		.28	1.46	1.46	88	80	5 1/2		58	84
6	55		.22	1.15	1.15	88	80	4 1/2		58	84
END	60	605.566									

1.336 788

Boeing Plant Z

9/19/89

Chronic Acid Bath Tank #5 (Avg. Anodic)

Ambient Temp = 20.0°F

Parts into tank @ 12:59:30

Bath Temp 72.5°F

On @ 1:55 PM (55 minute Anodizing Cycle)

Time	Voltage	Amps	Time	Voltage	Amps
12:58	0.3	0	1:16	22.9	1810
12:59	0.3	0	1:17	22.9	1800
1:00 PM	1.6	150	1:18	22.9	1800
1:01	6.8	1420	1:19	22.9	1810
1:02	11.8	1820	1:20	22.9	1810
1:03	17.0	1820	1:21	23.0	1810
1:04	21.3	1820	1:22	23.0	1810
1:05	22.4	1800	1:23	23.0	1810
1:06	22.5	1760	1:24	23.0	1810
1:07	22.6	1750	1:25	23.0	1820
1:08	22.7	1740	1:26	23.0	1810
1:09	22.7	1740	1:27	23.0	1810
1:10	22.7	1740	1:28	23.1	1810
1:11	22.7	1740	1:29	23.1	1820
1:12	22.8	1760	1:30	23.1	1810
1:13	22.8	1800	↓	↓	↓
1:14	22.8	1800	1:52	23.1	1810
1:15	22.8	1800			

22

1853 amp-hr / hr

21.1 volts

Sample Type:	Bath On - Run 6
Sampling Date:	November 30, 1989
Sample Times:	08:03-09:04 (60 minutes)
Run Number:	1
Lab Numbers:	922093, 922094, 922095
Airflow:	22,740 dscf/min
Process Data	
Bath Amperage:	1628 amp-hr/hr
Voltage:	21.6 volts D.C.
Bath Temperature:	94° F
Ambient Temperature:	76° F
Hexavalent Chromium	
Concentration:	0.261 mg/dscm
Concentration:	0.12 ppm
Emission Rate:	10,077 mg/hr
Emission Factor:	6.19 mg/amp-hr
Total Chromium	
Concentration:	0.280 mg/dscm
Concentration:	0.13 ppm
Emission Rate:	10,813 mg/hr
Emission Factor:	6.64 mg/amp-hr

Note: Acid in bath was drained and replaced prior to this test.

METHOD 1-5 - HEXAVALENT CHROMIUM EMISSIONS
AM TEST, INC. - AIR QUALITY DIVISION

FILE NAME: 580W5GR1
CLIENT: BOEING PLANT #2
LOCATION: SEATTLE, WASHINGTON
SAMPLE SITE: BLDG 210/TANK #5
SAMPLE DATE: NOVEMBER 30, 1989
RUN #: 1-CR+6
OPERATORS: S. MACKAY
CONTACT: P. STEBENALER

LAB #: 922094
START TIME: 8:03 O'CLOCK
STOP TIME: 9:04 O'CLOCK
SAMPLE TIME: 60.0 MINUTES
CONDITION: BATH ON

HEXAVALENT CHROMIUM

HEXAVALENT CHROMIUM CONCENTRATION (ug): 438
HEXAVALENT CHROMIUM CONCENTRATION (mg/dscm): 0.261
HEXAVALENT CHROMIUM IN SAMPLE (ppm): 0.121
HEXAVALENT CHROMIUM EMISSION RATE (mg/hr): 10077.1
AMPHERE HOURS PER HOUR (amp-hr/hr): 1628
HEX. CHROMIUM EMISSION FACTOR (mg/amp-hr): 6.19

FINAL WT. INIT. WT. NET WT.
OF H2O G. OF H2O G. OF H2O G.

1225.8 1245.5 -19.7
558.2 565.3 -7.1
515.4 514.0 1.4
756.9 749.7 7.2
TOTAL H2O GAIN: -18.2
TOTAL VOLUME (SCF) -0.86
PERCENT MOISTURE: -1.47
Bias: -0.0147

PITOT Cp: 0.842
NOZZLE DIA INCHES: 0.313
NOZZLE AREA FT^2: 0.0005
STACK DIA. INCHES: 48.00
STACK AREA FT^2: 12.566
METER TEMP. DEG F: 74.5
BAROM. PRES. "HG: 30.40
STATIC PRES. "H2O: -0.02
STACK PRES. "HG: 30.40
ORIFICE PRES "H2O: 3.078
METER PRES. "HG: 30.63

TOTAL CHROMIUM

TOTAL CHROMIUM CONCENTRATION (ug): 470
TOTAL CHROMIUM CONC. ON FILTER (ug): < 0.15
TOTAL CHROMIUM CONCENTRATION (mg/dscm): 0.280
TOTAL CHROMIUM IN SAMPLE (ppm): 0.129
TOTAL CHROMIUM EMISSION RATE (mg/hr): 10813.3
AMPHERE HOURS PER HOUR (amp-hr/hr): 1628
TOTAL CHROMIUM EMISSION FACTOR (mg/amp-hr): 6.64

INIT. METER VOL.: 843.639
FINAL METER VOL.: 901.593
VOLUME SAMPLED: 57.954
STD VOLUME (DSCF): 59.304
VOLUME (DSCM): 1.680
Y FACTOR: 1.012

AVERAGE % CO2: 0.1
AVERAGE % O2: 20.9
AVERAGE % CO: 0
STACK GAS MW DRY: 28.85
STACK GAS MW WET: 29.01

SAMPLE POINT	VELOCITY " OF H2O	TEMPERATURE DEGREES F.	SAMPLE POINT	VELOCITY " OF H2O	TEMPERATURE DEGREES F.
NW 1	0.20	72	NE 1	0.18	73
2	0.28	73	2	0.30	74
3	0.31	73	3	0.35	74
4	0.31	73	4	0.31	74
5	0.30	73	5	0.30	74
6	0.25	73	6	0.28	74

PERCENT ISOKINETICS: 102 %
STACK TEMPERATURE: 73.3 DEG. F.
AVERAGE VELOCITY HEAD: 0.279 " OF H2O
STACK GAS VELOCITY: 29.55 FT/SEC.
STACK GAS AIR FLOW: 22740.0 DSCF/MIN.



922094 TRAVERSE SAMPLING DATA

Page 1 of 1

Client <u> </u> Date <u> </u> Sample Location <u> </u> Operators <u> </u> Sample Box # <u> </u> Run# <u>1</u> <u>Cr# / Teller</u>	SCHEMATIC TRAVERSE LAYOUT Stack Diameter <u>48"</u> Distance Upstream <u> </u> Distance Downstream <u> </u> Filter # <u>Teller</u> tare <u> </u> mgs Final Initial Net Wt. Wt. Wt. <u>3-NaOH</u> #1 Bubbler <u>1225.8 - 1245.5</u> <u>1-HNO3</u> #2 Impinger <u>558.2 - 565.3</u> #3 Bubbler <u>515.4 - 514.0</u> #4 Silica Gel <u>756.9 - 749.7</u> TOTAL WATER VOLUME <u> </u>	Start Time <u> </u> Stop Time <u>7:00</u> Barometric Pressure "Hg <u> </u> Static Pres "H2O <u>-</u> Production Rate <u> </u> NOMOGRAPH SETUP % Moisture <u> </u> Meter Temp. <u> </u> Stack Temp. <u> </u> ΔH_e <u>1.9</u> Y <u>1.1</u> Pitot# <u> </u> Side# <u> </u> Cp <u>0.84</u> Nozzle Diameter <u>0.315</u> K Factor <u>13.9</u> Reference ΔP <u> </u>
EQUIPMENT CHECKS Initial/Final Leak Rate Cfm <u>0.15 / 0.1</u> Leak Test Vac <u>15" / 15"</u> Pitots, Pretest <u> </u> Pitots, Postest <u> </u> Orsat Sampling System <u> </u> Tedlar Bag <u> </u> Thermocouple @ <u> </u> °F		

Sample Point	Elap Time Min.	Dry Gas Meter Reading Cu. Ft.	Pitot Reading (ΔP), In. H2O	Orifice Setting (ΔH), In H2O		Gas Meter Temp °F		Pump Vacuum In. Hg Gauge	Filter Box Temp °F	Imp. Exit Temp °F	Stack Temp °F	
				Ideal	Actual	In	Out					
1	0	843.639	.20	2.10	2.10	51	47	11	110	36	72	
2	5		.29	3.10	3.10	76	41	12		36	73	
3	10		.31	3.10	3.40	85	42	12		37	73	
4	15		.31	3.10	3.40	95	45	12		40	73	
5	20		.30	3.10	3.20	95	45	12		40	73	
6	25		.25	2.74	2.74	100	52	11		40	73	
7	30		.18	1.97	1.97	100	55	10		41	73	
8	35		.30	3.29	3.29	109	56	12		42	74	
9	40		.35	3.80	3.80	109	57	13		43	74	
10	45		.31	3.40	3.40	111	62	12		42	74	
11	50		.30	3.29	3.29	113	60	12		42	74	
12	55		.29	3.07	3.50	116	66	12		40	74	
13	60	901.593										
14												
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3.078 74.5

✓

Prime version - 055 1844
Arthur Holm

39

11/30/89

Chronic Acid Bath 5

Bath Temp. - 94°

Parts descrip. - Clips, fittings, filters, Angles, chords

Path ON

Run 1

Parts in -

Time	Volts	Amperes	(FPM) Velocity (Velometer)
0806	23.0	100 1 min	Pt. 5 2400
0807	21.6	500 1	
0808	20.0	950 1	10 1790
0809	13.0	1000 1	
0810	17.5	1800 3	15 1690
0811	20.0	1800	
0812	22.0	1800	20 1560
0813	22.0	1500 2	
0814	22.5	1500	25 960
0815	22.5	1550 1	
0816	22.5	1500 9	30 1010
0817	22.5	1500	
0818			35 970
0819	22.5	1500	
0820	22.5	1500	40 750
0825	22.5	1550 26	45 950
0830	22.5	1550	50 460
0835	22.6	1550	
0840	22.6	1550	55 260
0845			
0850	22.6	1575 11	60 600
0855	22.9	1575	
0900	22.9	1575	

Amb. Temp. 76°F

1100 - 1105

Path OFF

0901

Parts out

0902

21.6 V

1628 amp-hr/hr

(over time)

Sample Type:	Bath On - Run 7
Sampling Date:	November 30, 1989
Sample Times:	15:46-16:49 (60 minutes)
Run Number:	4
Lab Numbers:	922106, 922107, 922108
Airflow:	22,084 dscf/min
Process Data	
Bath Amperage:	1896 amp-hr/hr
Voltage:	21.2 volts D.C.
Bath Temperature:	94.5° F
Ambient Temperature:	77° F
Hexavalent Chromium	
Concentration:	0.416 mg/dscm
Concentration:	0.19 ppm
Emission Rate:	15,601 mg/hr
Emission Factor:	8.23 mg/amp-hr
Total Chromium	
Concentration:	0.423 mg/dscm
Concentration:	0.20 ppm
Emission Rate:	15,853 mg/hr
Emission Factor:	8.36 mg/amp-hr

Note: Acid in bath was drained and replaced prior to this test.

METHOD 1-5 - HEXAVALENT CHROMIUM EMISSIONS AM TEST, INC. - AIR QUALITY DIVISION

FILE NAME: 580W5CR4
 CLIENT: BOEING PLANT #2
 LOCATION: SEATTLE, WASHINGTON
 SAMPLE SITE: BLDG 210/TANK #5
 SAMPLE DATE: NOVEMBER 30, 1989
 RUN #: 4-CR-6
 OPERATORS: S. MACEY
 CONTACT: P. STEBEMALER

LAB #: 922107
 START TIME: 15:46 O'CLOCK
 STOP TIME: 16:49 O'CLOCK
 SAMPLE TIME: 60.0 MINUTES
 CONDITION: BATH ON

HEXAVALENT CHROMIUM

 HEXAVALENT CHROMIUM CONCENTRATION (ug): 679
 HEXAVALENT CHROMIUM CONCENTRATION (mg/dscm): 0.416
 HEXAVALENT CHROMIUM IN SAMPLE (ppm): 0.193
 HEXAVALENT CHROMIUM EMISSION RATE (mg/hr): 15600.6
 AMPHIRE HOURS PER HOUR (amp-hr/hr): 1896
 HEX. CHROMIUM EMISSION FACTOR (mg/amp-hr): 8.23

FINAL WT. INIT. WT. NET WT.
 OF H2O G. OF H2O G. OF H2O G.

1255.5 1254.3 1.2
 570.1 568.3 1.8
 518.0 517.6 0.4
 771.7 762.6 9.1
 TOTAL H2O GAIN: 12.5
 TOTAL VOLUME (SCF) 0.59
 PERCENT MOISTURE: 1.01
 BWS: 0.0101

PITOT Cp: 0.842
 NOZZLE DIA. INCHES: 0.313
 NOZZLE AREA FT^2: 0.0005
 STACK DIA. INCHES: 48.00
 STACK AREA FT^2: 12.566
 METER TEMP. DEG F: 91.8
 BAROM. PRES. "HG: 30.48
 STATIC PRES. "H2O: 0.00
 STACK PRES. "HG: 30.48
 ORIFICE PRES "H2O: 2.977
 METER PRES. "HG: 30.70

HEXAVALENT CHROMIUM

 TOTAL CHROMIUM CONCENTRATION (ug): 690
 TOTAL CHROMIUM CONC. ON FILTER (ug): < 0.15
 TOTAL CHROMIUM CONCENTRATION (mg/dscm): 0.423
 TOTAL CHROMIUM IN SAMPLE (ppm): 0.196
 TOTAL CHROMIUM EMISSION RATE (mg/hr): 15853.3
 AMPHIRE HOURS PER HOUR (amp-hr/hr): 1896
 TOTAL CHROMIUM EMISSION FACTOR (mg/amp-hr): 8.36

INIT. METER VOL.: 946.900
 FINAL METER VOL.: 1004.859
 VOLUME SAMPLED: 57.959
 STD VOLUME (DSCF): 57.586
 STD VOLUME (DSCM): 1.631
 Y FACTOR: 1.012

AVERAGE % CO2: 0.1
 AVERAGE % O2: 20.9
 AVERAGE % CO: 0
 STACK GAS MW. DRY: 28.85
 STACK GAS MW. WET: 28.74

SAMPLE POINT	VELOCITY " OF H2O	TEMPERATURE DEGREES F.	SAMPLE POINT	VELOCITY " OF H2O	TEMPERATURE DEGREES F.
NE 1	0.21	79	NW 1	0.22	78
2	0.30	79	2	0.27	78
3	0.33	80	3	0.30	78
4	0.30	79	4	0.30	78
5	0.29	79	5	0.29	78
6	0.26	78	6	0.24	77
PERCENT ISOKINETICS:					
		102 %			
STACK TEMPERATURE:		78.4 DEG. F.	538.4 DEG. R.		
AVERAGE VELOCITY HEAD:		0.275 " OF H2O			
STACK GAS VELOCITY:		2299.1 ACF/MIN.	29.58 FT/SEC.		
STACK GAS AIR FLOW:		22051.3 DSCF/MIN.			

11/30/89
Chromic Acid Bath 5

R4-MS Bath Temp. 94.5

Parts descrip. -

Ambient Temp. 77°

Parts In - 15 54
~~Parts In~~ 15 53
Bath on - 15 56
15 57
15 58
15 59
16 00
16 01
16 02
16 03
16 04
16 05
16 06
16 07
16 08
16 09
16 10
16 15
~~Parts out~~ 16 18
16 20
16 25
16 30
16 40
16 50
Bath off 16 51
Parts out 16 53

Volts

0.5

~~2.1~~

2.1

5.0

8.5

13.5

17.7

21.5

22.0

22.0

22.0

22.5

22.5

21.2 V

~~Ampere~~
~~Ampere~~

Ampere

~~100~~

100

100

1800

1800

1800

1800

1800

1800

1800

1800

1800

1896 amp-hr/hr

Sample Type:	Bath On - Run 8
Sampling Date:	December 1, 1989
Sample Times:	07:29-08:31 (60 minutes)
Run Number:	5
Lab Numbers:	922114, 922115, 922116
Airflow:	22,318 dscf/min
Process Data	
Bath Amperage:	1680 amp-hr/hr
Voltage:	20.8 volts D.C.
Bath Temperature:	93.5° F
Ambient Temperature:	70° F
Hexavalent Chromium	
Concentration:	0.263 mg/dscm
Concentration:	0.12 ppm
Emission Rate:	9,982 mg/hr
Emission Factor:	5.94 mg/amp-hr
Total Chromium	
Concentration:	0.273 mg/dscm
Concentration:	0.13 ppm
Emission Rate:	10,371 mg/hr
Emission Factor:	6.17 mg/amp-hr

Note: Acid in bath was drained and replaced prior to this test.

METHOD 1-5 - HEXAVALENT CHROMIUM EMISSIONS
AM TEST, INC. - AIR QUALITY DIVISION

FILE NAME: 5805CR5
CLIENT: BOEING PLANT #2
LOCATION: SEATTLE, WASHINGTON
SAMPLE SITE: BLDG 210/TANK #5
SAMPLE DATE: DECEMBER 1, 1989
RUN #: 5-CR+6
OPERATORS: S. MCKEY
CONTACT: P. STEBENALER

LAB #: 922114
START TIME: 07:29 O'CLOCK
STOP TIME: 08:31 O'CLOCK
SAMPLE TIME: 60.0 MINUTES
CONDITION: BATH ON

HEXAVALENT CHROMIUM

HEXAVALENT CHROMIUM CONCENTRATION (ug): 442.00
HEXAVALENT CHROMIUM CONCENTRATION (mg/dscm): 0.263
HEXAVALENT CHROMIUM IN SAMPLE (ppm): 0.122
HEXAVALENT CHROMIUM EMISSION RATE (mg/hr): 9982.0
AMPHERE HOURS PER HOUR (amp-hr/hr): 1680
HEX. CHROMIUM EMISSION FACTOR (mg/amp-hr): 5.94

TOTAL CHROMIUM

TOTAL CHROMIUM CONCENTRATION (ug): 459.2
TOTAL CHROMIUM CONC. ON FILTER (ug): < 0.15
TOTAL CHROMIUM CONCENTRATION (mg/dscm): 0.273
TOTAL CHROMIUM IN SAMPLE (ppm): 0.127
TOTAL CHROMIUM EMISSION RATE (mg/hr): 10370.5
AMPHERE HOURS PER HOUR (amp-hr/hr): 1680
TOTAL CHROMIUM EMISSION FACTOR (mg/amp-hr): 6.17

FINAL WT. INIT. WT. NET WT.
OF H2O G. OF H2O G. OF H2O G.

1176.0 1175.6 0.4
628.0 627.2 0.8
479.2 478.5 0.7
801.9 791.0 10.9
TOTAL H2O GAIN: 12.8
TOTAL VOLUME (SCF) 0.60
PERCENT MOISTURE: 1.01
Bws: 0.0101

PITOT Cp: 0.842
NOZZLE DIA INCHES: 0.313
NOZZLE AREA FT^2: 0.0005
STACK DIA. INCHES: 48.00
STACK AREA FT^2: 12.566
METER TEMP. DEG F: 72.5
BAROM. PRES. "HG: 30.50
STATIC PRES. "H2O: 0.00
STACK PRES. "HG: 30.50
ORIFICE PRES "H2O: 3.045
METER PRES. "HG: 30.72

INIT. METER VOL.: 5.482
FINAL METER VOL.: 63.027
VOLUME SAMPLED: 57.545
STD VOLUME (DSCF): 59.295
STD VOLUME (DSCM): 1.679
Y FACTOR: 1.012

AVERAGE % CO2: 0.1
AVERAGE % O2: 20.9
AVERAGE % CO: 0
STACK GAS MW. DRY: 28.85
STACK GAS MW. WET: 28.74

SAMPLE POINT	VELOCITY " OF H2O	TEMPERATURE DEGREES F.	SAMPLE POINT	VELOCITY " OF H2O	TEMPERATURE DEGREES F.
NV 1	0.20	71	NE 1	0.22	71
2	0.27	72	2	0.30	72
3	0.30	73	3	0.34	72
4	0.31	72	4	0.30	72
5	0.30	72	5	0.30	72
6	0.24	71	6	0.27	72

PERCENT ISOCHINETICS: 104 %
STACK TEMPERATURE: 71.8 DEG. F.
AVERAGE VELOCITY HEAD: 0.278 " OF H2O
STACK GAS VELOCITY: 29.55 FT/SEC.
STACK GAS AIR FLOW: 22277.4 ACF/MIN. 22318.3 DSCF/MIN.

531.8 DEG. R.



922114 TRAVERSE SAMPLING DATA

Page 1 of 1

Client Bogal
Date 12/1/80
Sample Location Town
Operators YCH
Sample Box # 6
Run# 5

EQUIPMENT CHECKS

Initial/Final

Leak Rate Cfm 0.01 / 0.01
Leak Test Vac 10 / 10
✓ Pitots, Pretest
✓ Pitots, Posttest
✓ Orsat Sampling System
✓ Tedlar Bag
✓ Thermocouple @ °F

SCHEMATIC TRAVERSE LAYOUT

Stack Diameter
Distance Upstream
Distance Downstream

Filter #	tare		mgs
	Final Wt.	Initial Wt.	
#1 Bubbler	1176.0	1175.6	-
#2 Impinger	628.0	627.2	-
#3 Bubbler	479.2	478.5	-
#4 Silica Gel	801.9	791.0	-

TOTAL WATER VOLUME

Start Time 07:00
Stop Time 08:00
Barometric Pressure "Hg
Static Pres "H₂O
Production Rate

NOMOGRAPH SETUP

% Moisture
Meter Temp.
Stack Temp.
 $\Delta H @$ Y
Pitot# Side#
Cp
Nozzle Diameter
K Factor
Reference ΔP

Sample Point	Elap Time Min.	Dry Gas Meter Reading Cu. Ft.	Pitot Reading (ΔP), In. H ₂ O	Orifice Setting (ΔH), In H ₂ O		Gas Meter Temp °F		Pump Vacuum In. Hg Gauge	Filter Box Temp °F	Imp. Exit Temp °F	Stack Temp °F
				Ideal	Actual	In	Out				
1	0	005.48	.20	2.18	2.18	42	42	11	N/A	38	71
2	5		.27	2.25	2.25	65	45	12		36	72
3	10		.30	3.27	3.27	92	41	12		30	72
4	15		.31	3.38	3.37	90	47	13		40	72
5	20		.30	3.31	3.27	95	40	13		41	72
	25		.34	2.62	2.62	101	50	12		41	71
			.27	2.40	2.40	96	54	12		41	71
	30		.30	3.27	3.27	105	54	12		41	70
			.34	3.71	3.71	100	59	14		41	72
U	40		.26	3.27	3.27	105	60	12		41	71
			.31	3.27	3.27	102	61	12		41	72
	50		.27	2.25	2.25	110	61	12		40	72
		063.027									

3.045 72.5

12-1-89

Chromic Acid Bath #5

Bath Temp. 93.5°F Ambient - 70°F

Parts Descrip. - supports, stiffeners

Run 5

Plots In

~~Plots In~~

Bath ON

Time	Volts	Ampere
0730	0.6	0
0731	0.4	0
0732	3.0	100 1
0733	6.0	100 1
0734	11.5	800 1
0735	15.5	1800 2
0736	21.8	1800
0737	21.8	1600 23+25
0738	22.0	1600
0739	22.0	1600
0740	22.0	1600
0741	22.2	1600
0742	22.5	1600
0743	22.6	1600
0744	22.6	1600
0745	22.6	1600
0750	↓ 10	↓
0751	22.7	1600
0753	↓ 16	↓
0800	22.6	1600
0805	↓ 20	↓
0810	22.6	1650 2
0820	↓	↓
0825	22.6	1650 2
Bath off	1.0	0
Parts out	0.8	0

Set B 1176.0
 Run 5 → 628.0
 final → 479.2
 801.9

$$(2 \times 100 + 800 + 48 \times 1600 + 2 \times 1650)$$

20.8 v

1680 amp-hr/hr

SECTION 3
PARTICLE SIZE DISTRIBUTION RUNS
BATH ON

The results of the particle size distribution tests are presented graphically in Figures 1 and 2. Figure 1 is a plot of the distribution based on chemical analysis for total chromium of each filter which lined each stage of the Cascade impactor. Figure 2 is a plot of the distribution based on the gravimetric weight gain on each filter prior to chemical analysis. The detailed results are presented on computer printouts titled "Pilat (U of W) Mark 5 Particle Size Analysis Results" and computer printouts titled "Particle Size Analysis" which are included for each run. The column titled "aerodynamic diameter" (in micrometers) was plotted against the column titled "percent less than" on semi-log versus probability graph paper to illustrate the particle size distributions.

The aerodynamic mass mean diameter (MMD) value represents the size (in micrometers - microns) at which fifty percent of the particulate matter collected was composed of particles of less than that value. The average MMD based on chemical analysis of the progressive size ranges was 4.9 microns. The average MMD based on gravimetric (weight) analysis of the cut sizes was 3.0 microns.

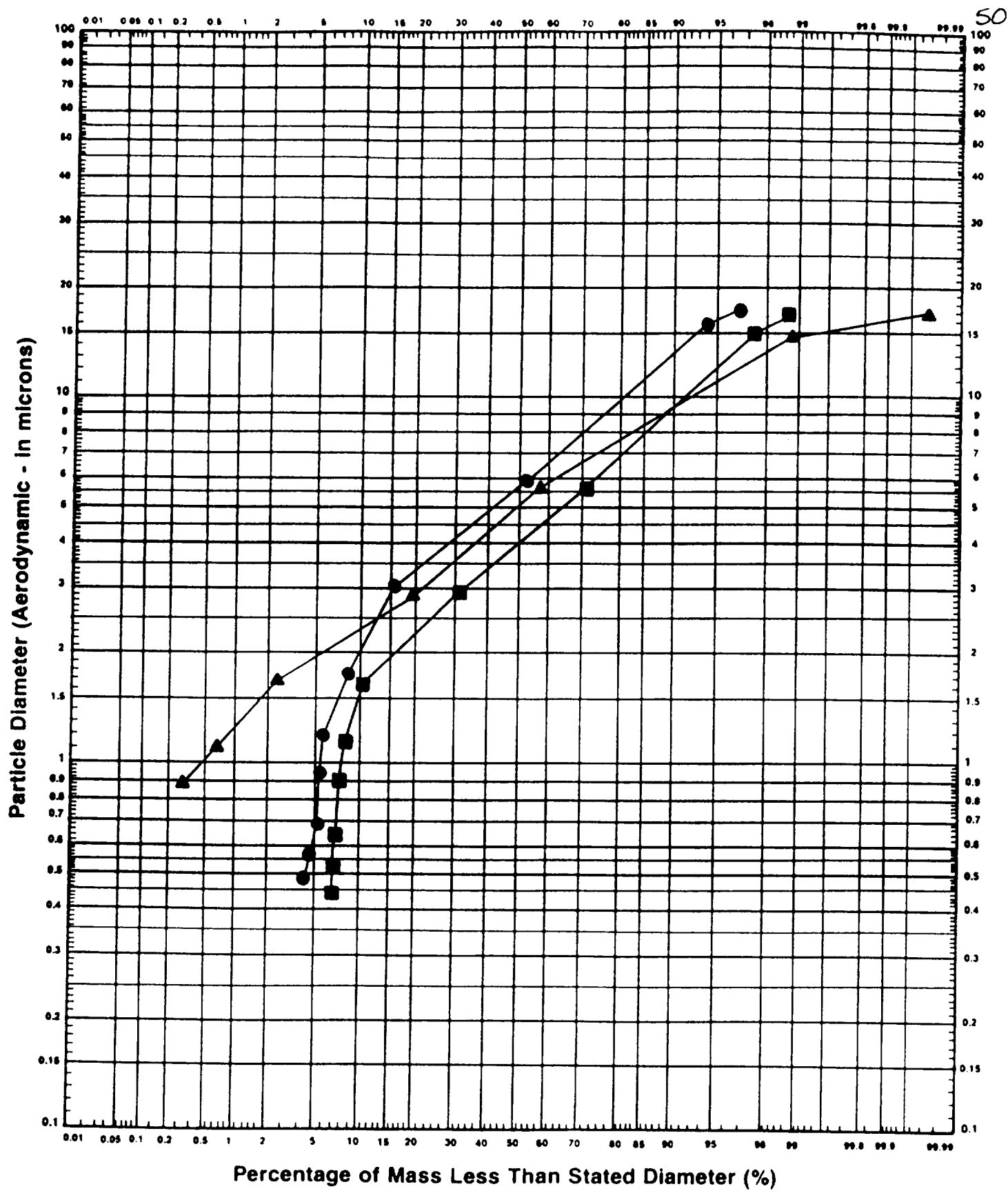


Figure 1.



Plot of particle size versus chromium concentration at the #5A chromic acid anodizing tank at Boeing Plant 2 in Seattle, Washington.

Symbol	Run #	MMD microns
●	1	5.7
■	2	4.0
▲	3	5.1
	Average	4.9

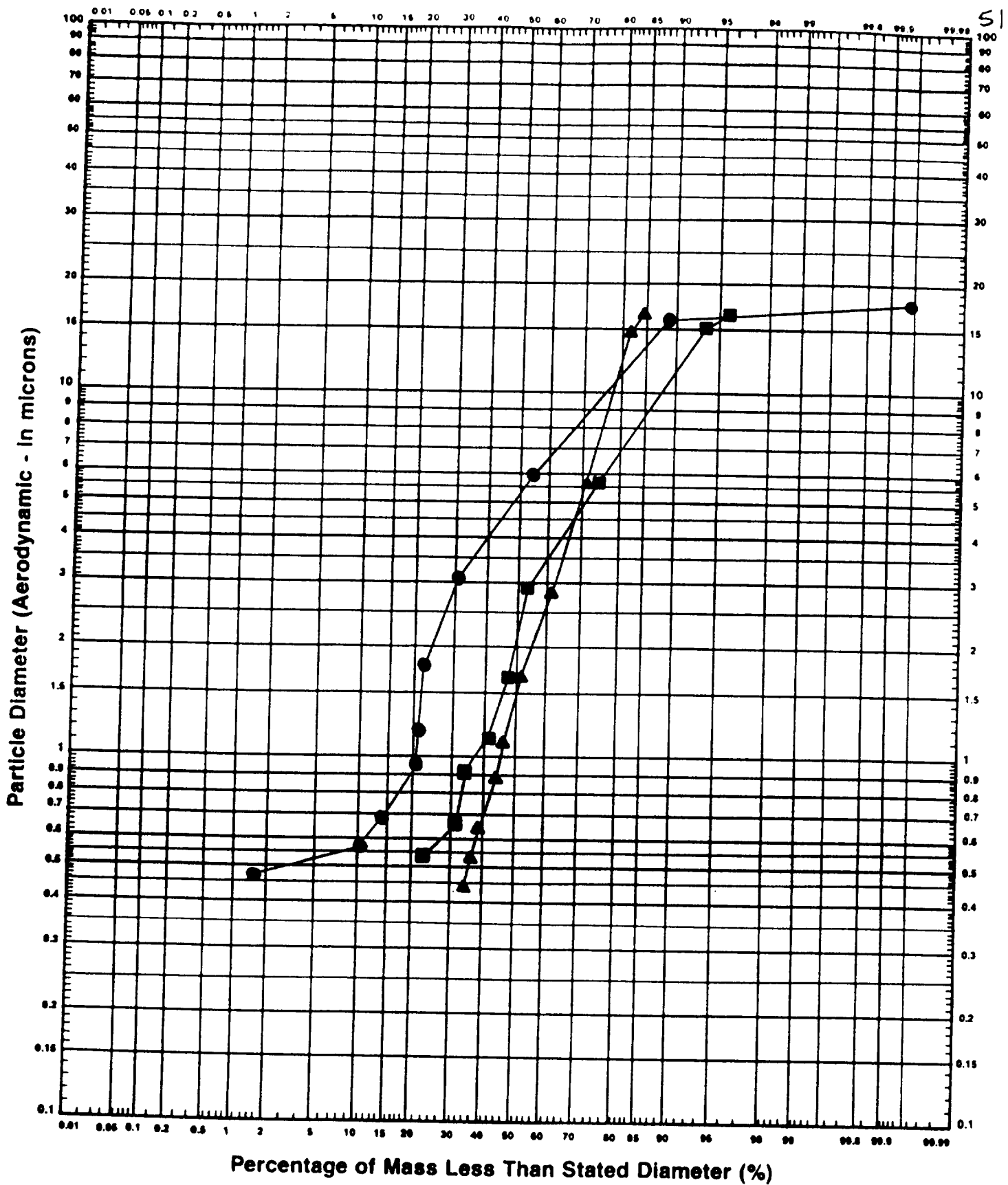


Figure 2.

Plot of particle size versus particle mass (weight) at the #5A chromic acid anodizing tank at Boeing Plant 2 in Seattle, Washington.



Symbol	Run #	MMD microns
●	1	5.3
■	2	2.2
▲	3	1.5
	Average	3.0

Sample Type:		Particle Size Distribution Bath On - Run 1	
Sampling Date:		August 31, 1989	
Sample Times:		10:26-11:26 (60 minutes)	
Run Number:		1	
Lab Numbers:		915962-915976, 915744-915749	
Airflow:		21,696 dscf/min	
Process Data			
Bath Amperage:		1892 amp-hr/hr	
Voltage:		22.4 volts D.C.	
Bath Temperature:		94.5° F	
Ambient Temperature:		78° F	
Stage #	Distribution d50's (microns)	Cumulative Cr % Less Than Stated Diameter	Chromium Concentration (mg/dscm)
1	17.54	96.85	0.009
2	15.87	94.54	0.007
3	5.90	52.90	0.117
4	3.07	15.90	0.104
5	1.76	7.93	0.022
6	1.18	5.74	0.006
7	0.95	5.29	0.001
8	0.68	5.01	0.001
9	0.56	4.72	0.001
10	0.47	4.45	0.001
final	<0.47	0.00	0.013
TOTAL			0.280

PILAT (U of W) MARK 5 PARTICLE SIZE ANALYSIS RESULTS
AM TEST, INC. - AIR QUALITY DIVISION

FILE NAME	A:BOH5CR1	Y FACTOR	0.993	mls	0.1
CLIENT	BOEING AEROSPACE	VOLUME H2O	N/A	SCF	20.9
LOCATION	SEATTLE, WASHINGTON	PERCENT MOISTURE	0.81	%	Percent
SAMPLE SITE	PLANT NO. 2, BLDG. 2-10	METER TEMP	67.5	Deg. F.	Percent
SAMPLE DATE	CHRONIC TANK #5 EXHAUST	STACK TEMP	80.2	Deg. F.	gm/mole
OPERATOR	AUGUST 31, 1999	MARK 5 TEMP	80.2	Deg. F.	gm/mole
	GUENTHER/WIDMEYER	BAROMETRIC PRESSURE	30.16	" of Hg	inches
RUN #	1-MCS/CF	STATIC PRESSURE	0.00	" of H2O	sq. ft.
LAB #	915744	ORIFICE PRESSURE	30.16	" of Hg	inches
START TIME	10:26	MARK 5 OUTLET ABS. PRES	0.17	" of H2O	sq. ft.
STOP TIME	11:26	AVG. MARK 5 PRESSURE	1.00	" of Hg	" H2O
SAMPLE TIME	60.00 MINUTES	SAMPLE RATE	30.06	cf/min	ft/sec
INITIAL METER VOL	982.904	SAMPLE RATE (STD)	0.32	dscf/min	ft/min
FINAL METER VOL	1001.815	SAMPLE RATE (MKS)	0.32	dscf/min	dscf/min
VOLUME SAMPLED	18.911	SAMPLE RATE (MKS)	8.95	liter/min	%
VOLUME (STACK COND)	19.40				
STD VOLUME	18.955				
STD VOLUME	0.537				
SET ID #	WH-QUARTZ 8-T1R1-TANK 5-OUT				
CONFIGURATION:	1,6,12,90,110,110,105,105,78,FINAL FILTER				

STAGE #	CHROMIUM ON FILTERS micrograms	CHROMIUM ON FILTERS milligrams	FRACTIONAL %	PERCENT < than	AERODYNAMIC DIAMETER microns	CHROMIUM CONC. mg/dscm
NOZZLE:						
1	0.00	0.00000				
2	4.75	0.00475	3.15	96.85	17.54	0.0085
3	3.47	0.00347	2.30	94.54	15.87	0.0065
4	62.70	0.06270	41.64	52.90	5.90	0.1168
5	55.70	0.05570	37.00	15.90	3.07	0.1037
6	12.00	0.01200	7.97	7.93	1.76	0.0223
7	3.30	0.00330	2.19	5.74	1.18	0.0061
8	0.67	0.00067	0.45	5.29	0.95	0.0012
9	0.42	0.00042	0.28	5.01	0.68	0.0008
10	0.45	0.00045	0.30	4.72	0.56	0.0008
FILTER	0.40	0.00040	0.27	4.45	0.47	0.0007
	6.70	0.00670	4.45	0.00	<.47	0.0125
TOTAL:	150.56	0.15056	100.00			0.2804

BACKHALF ANALYSIS

RINSE OF SUBSTRATES	0.75
POST IMPACTOR RINSE	4.45
IMPINGER #1	< 0.90
IMPINGER #2	< 0.79
IMPINGER #3 & 4	< 0.83
FILTER	< 0.30

TOTAL: 5.20 ug

**** INPUT DATA ****

DATE OF TEST AUGUST 31, 1989
 TIME OF TEST 10:26-11:26
 LOCATION OF TEST BOEING PLANT NO. 2, BLDG. 2-10
 TEST NUMBER 1
 PART. DIAM. TYPE C (I=IMP AERO, C=CLAS AERO, P=PHYSICAL)
 TEST TYPE OUTLET
 RUN NUMBER 1-TANK 5 - FILE NAME: B:T1R1-TANK 5.OUT
 REMARKS:
 IMPACTOR TYPE MK5-78
 MARK 5 IMPACTOR WITH A 78 HOLE FINAL STAGE

WATER VAPOR 0.81%
 CARBON DIOXIDE 0.10%
 CARBON MONOXIDE 0.00%
 OXYGEN 20.90%
 SULFUR DIOXIDE 0.00%
 NITROGEN 79.00%
 PARTICLE DENSITY 1.00 GRAMS/CM³

GAS METER VOLUME 18.911 CUBIC FEET
 IMPACTOR DELTA P 1.00 INCHES HG
 ORIFICE DELTA P 0.17 INCHES H2O
 STACK PRESS. (BELOW ATMOS.) 0.00 INCHES H2O
 BAROMETRIC PRESS. 30.16 INCHES HG
 STACK TEMPERATURE 80.2 DEGREES F
 METER TEMPERATURE 67.5 DEGREES F
 IMPACTOR TEMPERATURE 80.2 DEGREES F
 SAMPLE TIME 60.00 MINUTES
 AV. VELOCITY OF STACK GAS 1766.70 FEET/MINUTE
 GAS METER PRESSURE 0.00 IN HG
 NOZZLE DIAMETER 0.19 INCHES
 MAXIMUM AERODYN. DIAMETER 60.00 MICRONS

MASS GAIN ON STAGE 1 0.01 MG
 MASS GAIN ON STAGE 2 0.22 MG
 MASS GAIN ON STAGE 3 0.57 MG
 MASS GAIN ON STAGE 4 0.43 MG
 MASS GAIN ON STAGE 5 0.14 MG
 MASS GAIN ON STAGE 6 0.03 MG
 MASS GAIN ON STAGE 7 0.01 MG
 MASS GAIN ON STAGE 8 0.12 MG
 MASS GAIN ON STAGE 9 0.06 MG
 MASS GAIN ON STAGE 10 0.16 MG
 MASS GAIN ON FINAL FILTER 0.03 MG

RESULTS

56

DATE OF TEST AUGUST 31, 1989
 TIME OF TEST 10:26-11:26
 LOCATION OF TEST BOEING PLANT NO. 2, BLDG. 2-10
 TEST NUMBER 1 -
 RUN NUMBER 1-TANK 5
 ACTUAL FLOW RATE (STACK CONDITIONS) 0.325 CFM
 FLOW RATE (STANDARD CONDITIONS) 0.318 CFM
 PERCENT ISOKINETIC SAMPLING 95.55 %

VISCOSITY OF GAS STREAM		0.0001830 GRAMS/CM-SEC		
STAGE	CCF	DP(CLAS AERO)	DP(IMP AERO)	CUM FRACTION
1	1.009	17.538	17.621	0.9944
2	1.010	15.865	15.948	0.8708
3	1.028	5.896	5.978	0.5506
4	1.054	3.074	3.155	0.3090
5	1.094	1.758	1.839	0.2303
6	1.140	1.179	1.259	0.2135
7	1.175	0.952	1.031	0.2079
8	1.248	0.676	0.755	0.1404
9	1.306	0.555	0.634	0.1067
10	1.372	0.467	0.547	0.0169

TOTAL MASS PER DRY NORMAL CUBIC METER 3.2958 MG/CUBIC METER

PART. DIAM. PARTICLE SIZE (MICRONS)	TYPE C CUMFR (STD. DEV.)	(I=IMP AERO, C=CLAS AERO, P=PHYSICAL)		
		CUMFR (PER CENT)	CUM.MASS (MG/DRY N.CU.METER)	dM/dLOG D
0.20	-9.8170	0.0	0.000	0.000
0.25	-7.7933	0.0	0.000	0.000
0.40	-3.5306	0.0	0.001	0.054
0.50	-1.7166	4.3	0.142	3.926
0.75	-1.0210	15.4	0.506	1.489
1.00	-0.7962	21.3	0.702	0.488
1.50	-0.7653	22.2	0.732	0.444
2.00	-0.7254	23.4	0.772	0.213
2.50	-0.6733	25.0	0.825	1.127
4.00	-0.0619	47.5	1.567	5.061
5.00	0.1987	57.9	1.908	1.252
7.50	0.3707	64.5	2.124	2.865
10.00	0.6623	74.6	2.459	2.464
15.00	1.0733	85.8	2.829	1.725
20.00	4.9321	100.0	3.296	0.000
25.00	9.0597	100.0	3.296	0.000
40.00	19.2740	100.0	3.296	0.000
50.00	29.4350	100.0	3.296	0.000

***** RESULTS (CONTINUED) *****

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TIME OF TEST 10:26-11:26
 LOCATION OF TEST BOEING PLANT NO. 2, BLDG. 2-10
 TEST NUMBER 1
 RUN NUMBER 1-TANK 5

*** INHALABLE PARTICULATE MATTER ***

(M. MASS LESS THAN 2.5 MICRON: 0.83 MG/DRY NORMAL CU.METER (25.0 %)
 (M. MASS LESS THAN 5.0 MICRON: 1.91 MG/DRY NORMAL CU.METER (57.9 %)
 CUM. MASS LESS THAN 10.0 MICRON: 2.46 MG/DRY NORMAL CU.METER (74.6 %)
 CUM. MASS LESS THAN 15.0 MICRON: 2.83 MG/DRY NORMAL CU.METER (85.8 %)

NOTE: DIAMETERS FOR INHALABLE PARTICULATE ARE CLASSICAL AERODYNAMIC DIAMETERS.

LOG-NORMAL SIZE DISTRIBUTION PARAMETERS

LEAST SQUARES LINE : $Y = -1.04 + 2.13X$
 MASS GEOMETRIC MEAN DIAMETER 3.077
 GEOMETRIC STANDARD DEVIATION 2.942
 CORRELATION COEFFICIENT 0.875

Page 1 of

[illegible]

6.1.5

80.2

8/31/89

Boeing Plant 2

Run 1
(Particle Sealing)Started with Parts into back @ 10:26 AM
Removed Parts 11:21 AM

Readings during Test:

10:26
10:27
10:295
12
23.01
20
200
2

10:45

23.0 Volts 26

1830

1830 Amps 34

94.5° Bath Temperature

10:55

23.0 Volts

1830 Amps

11:03

23.1 Volts 8

1830 Amps

11:11

23.2 Volts 18

1820 Amps 18

78°F ambient

11:20

23.2 Volts

1820 Amps

11:21

23.2 Volts

1820 Amps

11:22

23.2 Volts

1820 Amps

Velocity Measurements between Run 1 & 2:
Opening # 14/min reading1
6
11
16
21
26
31
36
41
46
51
56
612270
1810
1740
1640
1650
1220
730
1060
730
820
680
340
620(Reading from 11:35 - 11:50)
(Empty Bath)

$$(1 \times 0 + 2 \times 200 + 34 \times 1830 + 18 \times 1820) / 55 = 69 / 55$$

1892 amperes
22.4 volt

← Workroom Air Sample Here; Wet Surfaces Too

Sample Type:		Particle Size Distribution Bath On - Run 2	
Sampling Date:		November 30, 1989	
Sample Times:		12:02-13:07 (65 minutes)	
Run Number:		2	
Lab Numbers:		922208-922219, 922096-922100	
Airflow:		22,576 dscf/min	
Process Data			
Bath Amperage:		1883 amp-hr/hr	
Voltage:		21.5 volts D.C.	
Bath Temperature:		93.0° F	
Ambient Temperature:		73° F	
Stage #	Distribution d50's (microns)	Cumulative Cr % Less Than Stated Diameter	Chromium Concentration (mg/dscm)
1	16.58	98.61	0.003
2	15.00	97.65	0.002
3	5.57	70.65	0.052
4	2.91	30.51	0.077
5	1.66	11.16	0.037
6	1.11	8.26	0.006
7	0.90	7.79	0.001
8	0.64	7.54	0.001
9	0.52	7.25	0.001
10	0.44	7.25	0.000
final	<0.44	0.00	0.014
TOTAL			0.196

PILAT (U of W) MARK 5 PARTICLE SIZE ANALYSIS RESULTS
AM TEST, INC. - AIR QUALITY DIVISION

FILE NAME
CLIENT
LOCATION
SAMPLE SITE
SAMPLE DATE
OPERATOR
A: BOWKSCR2
BOEING AEROSPACE
SEATTLE, WASHINGTON
PLANT NO. 2, BLDG. 2-10
CHROMIUM TANK #5 EXHAUST
NOVEMBER 30, 1989
MACKEY

Y FACTOR
VOLUME H2O
VOLUME H2O
PERCENT MOISTURE
METER TEMP
STACK TEMP
MARK 5 TEMP
BAROMETRIC PRESSURE
STATIC PRESSURE
ORIFICE PRESSURE
MKS OUTLET ABS. PRES
MKS DELTA P
AVG. MARK 5 PRESSURE
SAMPLE RATE (STD)
SAMPLE RATE (MKS)
SAMPLE RATE (MKS)

1.012
N/A
N/A
3.54
88.7
76.8
76.8
30.42
-0.02
30.42
0.43
29.42
1.00
30.32
0.35
0.35
0.36
9.90

mls
SCF
%
Deg. F.
Deg. F.
Deg. F.
" of Hg
" of Hg
" of Hg
" of Hg
" of Hg
" of Hg
cf/min
acfm/min
liter/min

0.1
20.9
0.0
28.85
28.47
0.842
0.188
0.0002
48.00
12.566
0.30
31.0
1862.5
23405.2
22575.7
101

Percent
Percent
Percent
gm/mole
gm/mole
inches
sq. ft.
inches
sq. ft.
" H2O
ft/sec
ft/min
acfm/min
dscf/min
%

2-MKS/CF
922208
12:02
13:07
65.00 MINUTES
902.199 CU FEET
925.122 CU FEET
22.923 CU FEET
23.55 ACTUAL CU FT
22.719 DSCF
0.644 DSCF
SET ID # RB-QUARTZ B:T1R2-TANK 5.0UT
CONFIGURATION: 1,6,12,90,110,110,105,105,78,FINAL FILTER

STAGE #	CHROMIUM ON FILTERS micrograms	CHROMIUM ON FILTERS milligrams	FRACTIONAL %	PERCENT < than	AERODYNAMIC DIAMETER microns	CHROMIUM CONC. mg/dscm
NOZZLE:	0.00	0.00000				
1	1.72	0.00172	1.39	98.61	16.58	0.0027
2	1.20	0.00120	0.97	97.65	15.00	0.0019
3	33.50	0.03350	27.00	70.65	5.57	0.0521
4	49.80	0.04980	40.14	30.51	2.91	0.0774
5	24.00	0.02400	19.34	11.16	1.66	0.0373
6	3.60	0.00360	2.90	8.26	1.11	0.0056
7	0.58	0.00058	0.47	7.79	0.90	0.0009
8	0.32	0.00032	0.26	7.54	0.64	0.0005
9	0.35	0.00035	0.28	7.25	0.52	0.0005
10	0.00	0.00000	0.00	7.25	0.44	0.0000
FILTER	9.00	0.00900	7.25	0.00	<.44	0.0140
TOTAL:	124.07	0.12407	100.00			0.1928

BACKHALF ANALYSIS

RINSE OF SUBSTRATES 1.62
RINSE OF IMPACTOR 24.2
IMPINGER #1 & #2 6.08
IMPINGER #3 & 4 < 0.8
FILTER < 0.15

TOTAL: 31.9 ug

PILAT (U of W) MARK 5 PARTICLE SIZE ANALYSIS RESULTS
AM TEST, INC. - AIR QUALITY DIVISION

FILE NAME	A:BOEMKSR2	Y FACTOR	1.012	mls	Percent
CLIENT	BOEING AEROSPACE	VOLUME H2O	N/A	SCF	Percent
LOCATION	SEATTLE, WASHINGTON	VOLUME H2O	N/A	%	Percent
SAMPLE SITE	PLANT NO. 2, BLDG. 2-10	PERCENT MOISTURE	3.54		gm/mole
SAMPLE DATE	CHRONIC TANK #5 EXHAUST	METER TEMP	88.7	Deg. F.	gm/mole
OPERATOR	NOVEMBER 30, 1989	STACK TEMP	76.8	Deg. F.	
	S. MACKEY	MARK 5 TEMP	76.8	Deg. F.	
RUN #	2-MKS/CF	BAROMETRIC PRESSURE	30.42	" of Hg	inches
LAB #	922208	STATIC PRESSURE	-0.02	" of H2O	sq. ft.
START TIME	12:02	ORIFICE PRESSURE	30.42	" of Hg	inches
STOP TIME	13:07	MKS OUTLET ABS. PRES	0.43	" of H2O	sq. ft.
SAMPLE TIME	65.00	MKS DELTA P	29.42	" of Hg	" H2O
INITIAL METER VOL	902.199	AVG. MARK 5 PRESSURE	1.00	" of Hg	ft/sec
FINAL METER VOL	925.122	SAMPLE RATE	30.32	" of Hg	ft/min
VOLUME SAMPLED	22.923	SAMPLE RATE (STD)	0.35	cf/min	acf/min
VOLUME (STACK COND)	23.55	SAMPLE RATE (MKS)	0.36	acf/min	dscf/min
STD VOLUME	22.719	SAMPLE RATE (MKS)	9.90	liter/min	% ISO KINETICS
STD VOLUME	0.644				101

CONFIGURATION: 1,6,12,90,110,110,110,105,105,76, FINAL FILTER
SET ID # RB-QUARTZ B-T1R2-TANK 5 OUT

STAGE #	TARE WT. Gms.	FINAL WT. Gms.	NET WT. Gms.	NET WT. Mgs.	FRACTIONAL %	PERCENT < than	AERODYN. DIAMETER um	PARTIC. CONC. Gr/DSCF	PARTIC. @ STACK CONDITIONS Gr/ACF	PARTIC. CONC. Mg/DSCM
NOZZLE:	0.00000	0.00000	0.00000	0.00						
1	0.79516	0.79520	0.00004	0.04	4.08	95.92	16.58	2.7E-05	2.6E-05	0.06
2	1.20263	1.20265	0.00002	0.02	2.04	93.88	15.00	1.4E-05	1.3E-05	0.03
3	1.19687	1.19705	0.00018	0.18	18.37	75.51	5.57	1.2E-04	1.2E-04	0.28
4	1.27910	1.27931	0.00021	0.21	21.43	54.08	2.91	1.4E-04	1.4E-04	0.33
5	1.19856	1.19862	0.00006	0.06	6.12	47.96	1.66	4.1E-05	3.9E-05	0.09
6	1.19888	1.19894	0.00006	0.06	6.12	41.84	1.11	4.1E-05	3.9E-05	0.09
7	1.29744	1.29751	0.00007	0.07	7.14	34.69	0.90	4.6E-05	4.6E-05	0.11
8	1.29010	1.29013	0.00003	0.03	3.06	31.63	0.64	2.0E-05	2.0E-05	0.05
9	1.29562	1.29570	0.00008	0.08	8.16	23.47	0.52	5.4E-05	5.2E-05	0.12
10	1.28629	1.28652	0.00023	0.23	23.47	0.00	0.44	1.6E-04	1.5E-04	0.36
FILTER	0.43523	0.43523	0.00000	0.00	0.00	0.00	<.44	0.0E+00	0.0E+00	0.00
TOTAL:			0.00098	0.98	100.00			0.0007	0.0006	1.52

BLANK #1: 1.20388 1.20393 0.00005 PM10: 85.3 % < 10 Microns
BLANK #2: 1.23287 1.23290 0.00003 MMD: 2.19 Microns @ 50%
AVERAGE BLANK: 0.00004

***** P A R T I C L E S I Z E A N A L Y S I S *****

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**** INPUT DATA ****

DATE OF TEST NOVEMBER 30, 1989
 TIME OF TEST 12:02-13:07
 LOCATION OF TEST BOEING PLANT NO. 2, BLDG. 2-10
 TEST NUMBER 1
 PART. DIAM. TYPE C (I=IMP AERO, C=CLAS AERO, P=PHYSICAL)
 TEST TYPE OUTLET
 RUN NUMBER 2-TANK 5 - FILE NAME: B:T1R2-TANK 5.OUT
 REMARKS:
 IMPACTOR TYPE MK5-78
 MARK 5 IMPACTOR WITH A 78 HOLE FINAL STAGE

WATER VAPOR 3.54%
 CARBON DIOXIDE 0.10%
 CARBON MONOXIDE 0.00%
 OXYGEN 20.90%
 SULFUR DIOXIDE 0.00%
 NITROGEN 79.00%
 PARTICLE DENSITY 1.00 GRAMS/CM³

GAS METER VOLUME 22.923 CUBIC FEET
 IMPACTOR DELTA P 1.00 INCHES HG
 ORIFICE DELTA P 0.43 INCHES H2O
 STACK PRESS. (BELOW ATMOS.) -0.02 INCHES H2O
 BAROMETRIC PRESS. 30.42 INCHES HG
 STACK TEMPERATURE 76.8 DEGREES F
 METER TEMPERATURE 88.7 DEGREES F
 IMPACTOR TEMPERATURE 76.8 DEGREES F
 SAMPLE TIME 65.00 MINUTES
 AV. VELOCITY OF STACK GAS 1862.50 FEET/MINUTE
 GAS METER PRESSURE 0.00 IN HG
 NOZZLE DIAMETER 0.19 INCHES
 MAXIMUM AERODYN. DIAMETER 60.00 MICRONS

MASS GAIN ON STAGE 1 0.04 MG
 MASS GAIN ON STAGE 2 0.02 MG
 MASS GAIN ON STAGE 3 0.18 MG
 MASS GAIN ON STAGE 4 0.21 MG
 MASS GAIN ON STAGE 5 0.06 MG
 MASS GAIN ON STAGE 6 0.06 MG
 MASS GAIN ON STAGE 7 0.07 MG
 MASS GAIN ON STAGE 8 0.03 MG
 MASS GAIN ON STAGE 9 0.08 MG
 MASS GAIN ON STAGE 10 0.23 MG
 MASS GAIN ON FINAL FILTER 0.00 MG

RESULTS

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DATE OF TEST NOVEMBER 30, 1989
 TIME OF TEST 12:02-13:07
 LOCATION OF TEST BOEING PLANT NO. 2, BLDG. 2-10
 TEST NUMBER 1 -
 RUN NUMBER 2-TANK 5
 ACTUAL FLOW RATE (STACK CONDITIONS) 0.358 CFM
 FLOW RATE (STANDARD CONDITIONS) 0.345 CFM
 PERCENT ISOKINETIC SAMPLING 99.62 %

VISCOSITY OF GAS STREAM		0.0001798 GRAMS/CM-SEC		
STAGE	CCF	DP(CLAS AERO)	DP(IMP AERO)	CUM FRACTION
1	1.010	16.580	16.659	0.9592
2	1.011	14.998	15.077	0.9388
3	1.029	5.573	5.652	0.7554
4	1.055	2.905	2.983	0.5413
5	1.096	1.661	1.738	0.4801
6	1.143	1.113	1.191	0.4190
7	1.178	0.898	0.975	0.3476
8	1.253	0.638	0.714	0.3170
9	1.312	0.524	0.600	0.2355
10	1.380	0.440	0.517	0.0010

TOTAL MASS PER DRY NORMAL CUBIC METER 1.5454 MG/CUBIC METER

PART. DIAM. PARTICLE SIZE (MICRONS)	TYPE C CUMFR (STD. DEV.)	(I=IMP AERO, C=CLAS AERO, P=PHYSICAL)		
		CUMFR (PER CENT)	CUM.MASS (MG/DRY N.CU.METER)	dM/dLOG D
0.20	-23.0317	0.0	0.000	0.000
0.25	-17.3927	0.0	0.000	0.000
0.40	-5.5153	0.0	0.000	0.000
0.50	-1.1746	12.0	0.186	8.410
0.75	-0.5342	29.7	0.458	0.472
1.00	-0.2907	38.6	0.596	1.209
1.50	-0.0709	47.2	0.729	0.352
2.00	-0.0213	49.2	0.760	0.225
2.50	0.0317	51.3	0.792	0.504
4.00	0.3785	64.7	1.001	1.324
5.00	0.5984	72.5	1.121	1.093
7.50	0.8744	80.9	1.250	0.519
10.00	1.0497	85.3	1.318	0.620
15.00	1.5456	93.9	1.451	0.790
20.00	2.1875	98.6	1.523	0.318
25.00	2.7887	99.7	1.541	0.089
40.00	5.6261	100.0	1.545	0.000
50.00	12.3087	100.0	1.545	0.000

**** RESULTS (CONTINUED) ****

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TIME OF TEST 12:02-13:07
 LOCATION OF TEST BOEING PLANT NO. 2, BLDG. 2-10
 TEST NUMBER 1
 RUN NUMBER 2-TANK 5

*** INHALABLE PARTICULATE MATTER ***

UM. MASS LESS THAN 2.5 MICRON: 0.79 MG/DRY NORMAL CU.METER (51.3 %)
 UM. MASS LESS THAN 5.0 MICRON: 1.12 MG/DRY NORMAL CU.METER (72.5 %)
 CUM. MASS LESS THAN 10.0 MICRON: 1.32 MG/DRY NORMAL CU.METER (85.3 %)
 UM. MASS LESS THAN 15.0 MICRON: 1.45 MG/DRY NORMAL CU.METER (93.9 %)

NOTE: DIAMETERS FOR INHALABLE PARTICULATE ARE CLASSICAL AERODYNAMIC DIAMETERS.

LOG-NORMAL SIZE DISTRIBUTION PARAMETERS

LEAST SQUARES LINE : $Y = -0.69 + 2.02X$
 MASS GEOMETRIC MEAN DIAMETER 2.193
 GEOMETRIC STANDARD DEVIATION 3.124
 CORRELATION COEFFICIENT 0.763

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[illegible]

.428 88.7

76.8

11/30/89

Chromic Acid Bath 5

Bath Temp. 93 °F Ambient 73°F

Parts descrip. - fittings etc., stringers mostly

Run 2 - Particle Sizing

<u>Time</u>	<u>Volts</u>	<u>Amps</u>
-------------	--------------	-------------

1200
1201
1202
1203
1204
1205
1206
1207
1208

$$(2 \times 150 + 1100 + 1750 \times 51 \times 1800) / 55$$

Parts In
Bath ON

1209
1210
1211
1212
1213
1214
1215
1216
1217
1218
1219
1220
1221
1222
1223
1224
1225
1230
1235
1240
1245
1255
1300
1305
1306

0.7

2.5

7.0

16.0

14.0

19.0

21.5

22.0

22.2

22.2

22.2

22.3

22.3

22.3

22.4

22.6

22.6

22.6

22.7

22.8

22.8

22.8

0.7

0

150

1100

1750

1800

1800

1800

1800

1800

1800

1800

1800

1800

1800

1800

1800

1800

1800

1800

1800

1800

1800

0

1883 amp-hr/hr

21.5 Volts

Parts out
BATH OFF

Note: Chromic Acid has been drained & replaced with new since last testing (Because of repairs)

Sample Type:		Particle Size Distribution Bath On - Run 3	
Sampling Date:		November 30, 1990	
Sample Times:		14:15-15:15 (60 minutes)	
Run Number:		3	
Lab Numbers:		922220, 922223-922233, 922101-922105	
Airflow:		22,433 dscf/min	
Process Data			
Bath Amperage:		1920 amp-hr/hr	
Voltage:		20.8 volts D.C.	
Bath Temperature:		94.0° F	
Ambient Temperature:		78° F	
Stage #	Distribution d50's (microns)	Cumulative Cr % Less Than Stated Diameter	Chromium Concentration (mg/dscm)
1	16.44	99.67	0.001
2	14.87	98.84	0.002
3	5.52	56.28	0.096
4	2.88	19.09	0.084
5	1.65	2.22	0.038
6	1.10	0.69	0.004
7	0.89	0.31	0.001
8	0.63	0.00	0.001
9	0.52	0.00	0.000
10	0.44	0.00	0.000
final	<0.44	0.00	0.000
TOTAL			0.229

***** INPUT DATA *****

DATE OF TEST NOVEMBER 30, 1989
 TIME OF TEST 14:15-15:15
 LOCATION OF TEST BOEING PLANT NO. 2, BLDG. 2-10
 TEST NUMBER 1
 PART. DIAM. TYPE C (I=IMP AERO, C=CLAS AERO, P=PHYSICAL)
 TEST TYPE OUTLET
 RUN NUMBER 3-TANK 5 - FILE NAME: B:T1R3-TANK 5.OUT
 REMARKS:
 IMPACTOR TYPE MK5-78
 MARK 5 IMPACTOR WITH A 78 HOLE FINAL STAGE

WATER VAPOR 4.00%
 CARBON DIOXIDE 0.10%
 CARBON MONOXIDE 0.00%
 OXYGEN 20.90%
 SULFUR DIOXIDE 0.00%
 NITROGEN 79.00%
 PARTICLE DENSITY 1.00 GRAMS/CM³

GAS METER VOLUME 21.480 CUBIC FEET
 IMPACTOR DELTA P 1.00 INCHES HG
 ORIFICE DELTA P 0.43 INCHES H2O
 STACK PRESS. (BELOW ATMOS.) -0.02 INCHES H2O
 BAROMETRIC PRESS. 30.45 INCHES HG
 STACK TEMPERATURE 80.0 DEGREES F
 METER TEMPERATURE 92.3 DEGREES F
 IMPACTOR TEMPERATURE 80.0 DEGREES F
 SAMPLE TIME 60.00 MINUTES
 AV. VELOCITY OF STACK GAS 1868.80 FEET/MINUTE
 GAS METER PRESSURE 0.00 IN HG
 NOZZLE DIAMETER 0.19 INCHES
 MAXIMUM AERODYN. DIAMETER 60.00 MICRONS

MASS GAIN ON STAGE 1 0.46 MG
 MASS GAIN ON STAGE 2 0.09 MG
 MASS GAIN ON STAGE 3 0.31 MG
 MASS GAIN ON STAGE 4 0.32 MG
 MASS GAIN ON STAGE 5 0.26 MG
 MASS GAIN ON STAGE 6 0.14 MG
 MASS GAIN ON STAGE 7 0.10 MG
 MASS GAIN ON STAGE 8 0.14 MG
 MASS GAIN ON STAGE 9 0.06 MG
 MASS GAIN ON STAGE 10 0.05 MG
 MASS GAIN ON FINAL FILTER 1.04 MG

RESULTS

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DATE OF TEST NOVEMBER 30, 1989
 TIME OF TEST 14:15-15:15
 LOCATION OF TEST BOEING PLANT NO. 2, BLDG. 2-10
 TEST NUMBER 1 -
 RUN NUMBER 3-TANK 5
 ACTUAL FLOW RATE (STACK CONDITIONS) 0.365 CFM
 FLOW RATE (STANDARD CONDITIONS) 0.348 CFM
 PERCENT ISOKINETIC SAMPLING 101.21 %

VISCOSITY OF GAS STREAM

0.0001802 GRAMS/CM-SEC

STAGE	CCF	DP (CLAS AERO)	DP (IMP AERO)	CUM FRACTION
1	1.010	16.438	16.518	0.8451
2	1.011	14.870	14.949	0.8148
3	1.029	5.524	5.604	0.7104
4	1.055	2.879	2.958	0.6027
5	1.097	1.646	1.724	0.5152
6	1.145	1.103	1.180	0.4680
7	1.180	0.890	0.967	0.4343
8	1.256	0.631	0.708	0.3872
9	1.316	0.518	0.595	0.3670
10	1.385	0.436	0.513	0.3502

TOTAL MASS PER DRY NORMAL CUBIC METER 5.0209 MG/CUBIC METER

PART. DIAM. PARTICLE SIZE (MICRONS)	TYPE C CUMFR (STD. DEV.)	(I=IMP AERO, C=CLAS AERO, P=PHYSICAL) CUMFR (PER CENT)	CUM.MASS (MG/DRY N.CU.METER)	dM/dLOG D
0.20	-0.5795	28.1	1.412	0.977
0.25	-0.5236	30.0	1.508	1.007
0.40	-0.4059	34.2	1.719	1.064
0.50	-0.3487	36.4	1.826	1.125
0.75	-0.2300	40.9	2.054	1.596
1.00	-0.1177	45.3	2.275	1.838
1.50	0.0114	50.5	2.533	1.276
2.00	0.1027	54.1	2.716	1.683
2.50	0.1934	57.7	2.895	2.018
4.00	0.4290	66.6	3.344	2.065
5.00	0.5246	70.0	3.515	1.394
7.50	0.5958	72.4	3.637	0.343
10.00	0.6416	73.9	3.713	1.069
15.00	0.9054	81.7	4.104	3.446
20.00	1.3140	90.6	4.547	3.116
25.00	1.7271	95.8	4.810	2.309
40.00	4.1752	100.0	5.021	0.009
50.00	10.6763	100.0	5.021	0.000

**** RESULTS (CONTINUED) ****

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TIME OF TEST 14:15-15:15
 LOCATION OF TEST BOEING PLANT NO. 2, BLDG. 2-10
 TEST NUMBER 1
 RUN NUMBER 3-TANK 5

*** INHALABLE PARTICULATE MATTER ***

CUM. MASS LESS THAN 2.5 MICRON: 2.90 MG/DRY NORMAL CU.METER (57.7 %)
 CUM. MASS LESS THAN 5.0 MICRON: 3.51 MG/DRY NORMAL CU.METER (70.0 %)
 CUM. MASS LESS THAN 10.0 MICRON: 3.71 MG/DRY NORMAL CU.METER (73.9 %)
 CUM. MASS LESS THAN 15.0 MICRON: 4.10 MG/DRY NORMAL CU.METER (81.7 %)

NOTE: DIAMETERS FOR INHALABLE PARTICULATE ARE CLASSICAL AERODYNAMIC DIAMETERS.

LOG-NORMAL SIZE DISTRIBUTION PARAMETERS

LEAST SQUARES LINE : $Y = -0.11 + 0.88X$
 MASS GEOMETRIC MEAN DIAMETER 1.329
 GEOMETRIC STANDARD DEVIATION 13.741
 CORRELATION COEFFICIENT 0.996

AT

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TRAVERSE SAMPLING DATA

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922223

Client <u>B...</u> Date <u>11/30/82</u> Sample Location <u>Tub #31 Van...</u> Operators <u>K...</u> Sample Box # <u>A</u> Run# <u>3 - Particle Sizing</u> <u>10/27</u>	SCHEMATIC TRAVERSE LAYOUT Stack Diameter <u>45 d</u> Distance Upstream _____ Distance Downstream _____ Filter # <u>A</u> tare _____ mgs Final Initial Net Wt. Wt. Wt. #1 Bubbler <u>1267.3</u> <u>1259.1</u> - _____ #2 Impinger <u>619.7</u> <u>617.5</u> - _____ #3 Bubbler <u>495.8</u> - <u>493.9</u> - _____ #4 Silica Gel <u>725.2</u> - <u>718.8</u> - _____ TOTAL WATER VOLUME <u>18.7</u>	Start Time <u>14:15</u> Stop Time <u>15:15</u> Barometric Pressure "Hg <u>30.45</u> Static Pres "H ₂ O _____ Production Rate <u>Bath on</u> NOMOGRAPH SETUP % Moisture <u>2</u> Meter Temp. <u>95</u> Stack Temp. <u>75</u> ΔH _e <u>1.92</u> Y <u>1.015</u> Pitot # <u>4</u> Side # <u>4</u> Cp <u>1.82</u> Nozzle Diameter <u>.188</u> K Factor _____ Reference ΔP _____
EQUIPMENT CHECKS Initial/Final Leak Rate Cfm <u>0.01</u> / _____ Leak Test Vac <u>31"</u> / _____ Pitots, Pretest _____ Pitots, Posttest _____ Orsat Sampling System <u>N/A</u> Tedlar Bag <u>N/A</u> Thermocouple @ _____ °F		

Sample Point	Elap Time Min.	Dry Gas Meter Reading Cu. Ft.	Pitot Reading (ΔP), In. H ₂ O	Orifice Setting (ΔH), In H ₂ O		Gas Meter Temp °F		Pump Vacuum In. Hg Gauge	Filter Box Temp °F	Imp. Exit Temp °F	Stack Temp °F
				Ideal	Actual	In	Out				
Point 3	0	925.298	.30	.43	.43	63	64	9	N/A	45	80
"	5		.30	.43	.43	86	64	9		45	80
"	10		.30	.43	.43	105	64	9		45	80
"	15		.30	.43	.43	115	65	9		46	80
"	20		.30	.43	.43	121	66	9		46	80
"	25		.30	.43	.43	124	68	9		45	80
"	30		.30	.43	.43	127	69	9		46	80
"	35		.30	.43	.43	129	70	9		45	80
"	40		.30	.43	.43	130	71	9		45	80
"	45		.30	.43	.43	131	72				80
"	50		.30	.43	.43	132	73				80
"	55		.30	.43	.43	133	74				80
"	60	946.778									

430

92.3

80

Particle Sizing

11/30/89

Chromic Acid Bath 5

Temp. (Bath) 94°F Part Descrip. - Supports

Run 3 P.S.

TimeVoltsAmperes

Lath on

1415

2.0

200

1

1416

3.5

1200

1

1417

8.0

1800

53

1418

13.5

1800

1419

18.0

1800

1420

21.5

1421

21.8

1422

22.0

1423

22.0

1424

22.0

1425

22.0

1430

22.0

1435

22.0

1440

22.0

1445

22.0

1450

22.0

1455

22.0

1500

22.0

1505

22.0

1510

22.0

Bath off

1510

$$(200 + 1200 + 53 \times 1800)$$

1920 amp-hr/hr

20.8 volts

48

1800

SECTION 4
AMBIENT WORKROOM SAMPLE

Sample Type:	Ambient Workroom Sample 1
Sampling Date:	August 31, 1989
Sample Times:	10:22-16:52 (390 minutes)
Run Number:	1
Lab Numbers:	915740, 915741, 915743
Process Data	
Bath Status:	Bath On and Off During Test
Ambient Temperature:	80° F
Hexavalent Chromium	
Concentration:	0.295 mg/dscm
Concentration:	0.14 ppm
Total Chromium	
Concentration:	0.249 mg/dscm
Concentration:	0.12 ppm
Description of sampling set-up: Sampling site was 53 inches above ground, 7 feet from the north end on tank #5, 10 inches away from east edge of tank, adjacent to ventilation opening #56. The top edge of the tank is 43 inches above the ground. The acid liquid level was approximately 6 inches below the top of the tank.	

METHOD 1-5 - HEXAVALENT AND TOTAL CHROMIUM EMISSIONS
AM TEST, INC. - AIR QUALITY DIVISION

FILE NAME:	3BO#5WR1	LAB #:	915740
CLIENT:	BOEING PLANT #2	START TIME:	10:22 O'CLOCK
LOCATION:	SEATTLE, WASHINGTON	STOP TIME:	16:52 O'CLOCK
SAMPLE SITE:	BLDG 210/TANK #5	SAMPLE TIME:	390.0 MINUTES
SAMPLE DATE:	AUGUST 31, 1989	CONDITION:	BATH ON & OFF
RUN #:	1-CR+6		
OPERATORS:	S. MACKEY		
CONTACT:	P. SIEBENALER		

FINAL WT. OF H2O G.	INIT.WT. OF H2O G	NET WT. OF H2O G.	PITOT Cp:	
1274.9	1250.4	24.5	NOZZLE DIA INCHES:	NA
629.0	629.9	-0.9	NOZZLE AREA FT^2:	NA
475.3	473.4	1.9	STACK DIA. INCHES:	NA
817.4	783.8	33.6	STACK AREA FT^2:	NA
TOTAL H2O GAIN:		59.1	METER TEMP. DEG F:	147.1
TOTAL VOLUME (SCF)		2.79	BAROM. PRES. "HG:	30.20
PERCENT MOISTURE:		1.45	STATIC PRES. "H2O:	0.00
Bws:		0.0145	STACK PRES. "HG:	30.20
			ORIFICE PRES "H2O:	1.0
			METER PRES. "HG:	30.27

INIT. METER VOL.:	830.633	AVERAGE % CO2:	0.1
FINAL METER VOL.:	1045.964	AVERAGE % O2:	20.9
VOLUME SAMPLED:	215.331	AVERAGE % CO:	0
STD VOLUME (DSCF):	189.298	STACK GAS MW. DRY:	28.85
STD VOLUME (DSCM):	5.361	STACK GAS MW. WET:	28.69
Y FACTOR:	0.999		

HEXAVALENT CHROMIUM

HEXAVALENT CHROMIUM CONCENTRATION (ug):	1581.3
HEXAVALENT CHROMIUM CONCENTRATION (mg/dscm):	0.295
HEXAVALENT CHROMIUM IN SAMPLE (ppm):	0.14

TOTAL CHROMIUM

TOTAL CHROMIUM CONCENTRATION (ug):	1336.7
TOTAL CHROMIUM CONC. ON FILTER (ug):	< 0.30
TOTAL CHROMIUM CONCENTRATION (mg/dscm):	0.249
TOTAL CHROMIUM IN SAMPLE (ppm):	0.12

*Note: Slight differences in total chromium and hexavalent chromium concentrations are due to different methods of analysis.



TRAVERSE SAMPLING DATA

Page 1 of 1

3B045WR2
Client Boeing Plant 2
Date 8/31/87
Sample Location Workroom Air
NE of Bath #5
Operators KSM
Sample Box A
Run# 1 Workroom (Total Cr/Cr⁶ Sample Train)

SCHEMATIC TRAVERSE LAYOUT

Stack Diameter N/A
Distance Upstream _____
Distance Downstream _____

Start Time 10:22
Stop Time 16:52
Barometric _____
Pressure "Hg 30.20"
Static Pres "H₂O _____
Production Rate _____

EQUIPMENT CHECKS

Initial/Final
Leak Rate Cfm <.02 / .005
Leak Test Vac 15" / 11"
____ Pitots, Pretest
____ Pitots, Posttest
____ Orsat Sampling System
____ Tedlar Bag
____ Thermocouple @ _____ °F

NOMOGRAPH SETUP

% Moisture N/A
Meter Temp. _____
Stack Temp. _____
ΔH@ _____ Y _____
Pitot# _____ Side# _____
Cp _____
Nozzle Diameter _____
K Factor _____
Reference ΔP _____

Filter # Tellur tare _____ mgs
Final Initial Net
Wt. Wt. Wt.
#1 Bubbler 657.1 - 1250.4 = _____
#2 Impinger 629.0 - 629.9 = _____
#3 Bubbler 475.3 - 473.4 = _____
#4 Silica Gel 817.4 - 783.8 = _____
TOTAL WATER VOLUME _____

Sample Point	Elap Time Min.	Dry Gas Meter Reading Cu. Ft.	Pitot Reading (ΔP), In. H ₂ O	Orifice Setting (ΔH), In H ₂ O		Gas Meter Temp °F		Pump Vacuum In. Hg Gauge	Filter Box Temp °F	Imp. Exit Temp °F	Stack Temp °F
				Ideal	Actual	In	Out				
Start	0	830.633	N/A	7.00	1.00	106	72	7.5		65	77
15	15				1.0	155	78	7.4		64	77
30	30				1.0	170	86	7.3		60	77
45	45				1.0	178	94	7.0		60	77
1 Hour	60				1.0	183	100	7.0		60	77
75	75				1.0	183	103	7.0		61	78
90	90				1.0	183	107	7.0		61	78
105	105				1.0	187	103	7.0		61	79
2 Hours	120				1.0	190	109	7.0		61	79
135	135				1.0	190	110	7.0		63	79
150	150				1.0	192	111	7.0		61	81
165	165				1.0	192	113	7.0		60	82
3 Hours	180				1.0	193	113	7.0		58	81
195	195				1.0	194	114	7.0		58	80
210	210				1.0	194	114	7.0		58	80
225	225				1.0	194	114	7.0		58	81
4 Hours	240				1.0	194	115	7.0		57	81
255	255				1.0	195	115	7.0		57	82
270	270				1.0	195	116	7.0		57	81
285	285				1.0	195	116	7.0		58	81
5 Hours	300				1.0	195	116	7.0		59	80
315	315				1.0	195	116	7.0		59	80
330	330				1.0	195	116	7.0		61	81
345	345				1.0	196	116	7.0		61	81
6 Hours	360				1.0	196	116	7.0		63	81
					1.0	196	116	7.0		64	82

8/31/31 Boating Plant 2

Run 1 — Started with Parts into bath @ 10:26 AM
(Purified Sicg) Removed Parts 11:21 AM

Readings during Test:

10:45	23.0 Volts	1.830 Amps	94.5° Bath Temperature
10:55	23.0 Volts	1.830 Amps	
11:03	23.1 Amps	1.830 Amp	78°F ambient
11:11	23.2 Amps	1.820 Amp	
11:20	23.2 Volts	1.820 Amp	
11:22	0.5 V (Off Circuit)	0 Amps	

Velocity Measurements between Run 1 & 2:

Opening #	ft/min reading
1	2270
2	1810
3	1740
4	1640
5	1650
6	1220
7	730
8	1060
9	730
10	820
11	680
12	340
13	620

(Readings from 11:35 - 11:50)
(Empty Bath)

← Workroom Air Samples Here; Wet Surfaces Too

SECTION 5
VENTILATION SYSTEM EVALUATION

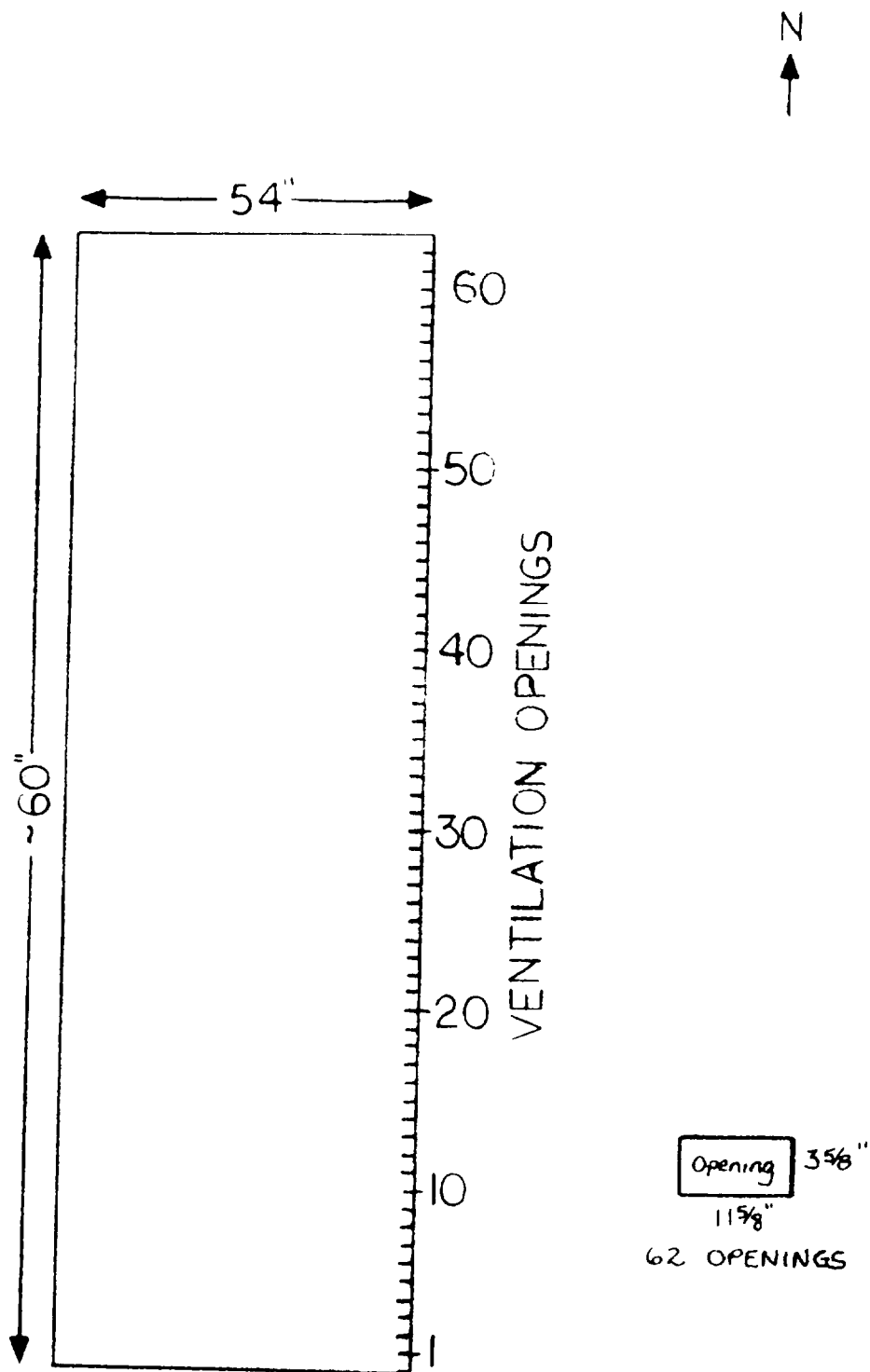


Figure 3. Diagram of the #5A chromic acid anodizing tank and ventilation system at Boeing Plant 2 in Seattle, Washington.

Sample Type:	Ventilation Opening Velocities
Sampling Dates:	August 22, August 31, November 30, 1989
Description of sampling procedure: A Kurz velometer with a digital readout in feet per minute was used to measure the velocity at each vent opening along the east side of the #5 chromic anodize aluminum tank. There are 62 openings along the east side. The measurement was taken at the centroid of each 3.375 by 11.625 inch opening. The velocity was lowest from openings 54-58, therefore, the ambient workroom sample was taken at that point.	

Velocity Traverse

Boeing - Plant 2 - #5A Chromic Anodize Aluminum Tank
 Date: August 22, 1989
 Time: 11:55-12:15

<u>Vent #</u>	<u>Velocity (ft/min)</u>	<u>Vent #</u>	<u>Velocity ft/min</u>
1	2050	32	1330
2		33	
3	2060	34	980
4		35	
5	2450	36	970
6		37	
7	1830	38	460
8		39	
9	1810	40	730
10		41	
11	1720	42	790
12		43	
13	1800	44	690
14		45	
15	1700	46	630
16		47	
17	1740	48	810
18		49	
19	1570	50	1090
20		51	
21	1560	52	1020
22		53	
23	1560	54	240
24		55	
25	930	56	340
26		57	
27	1110	58	620
28		59	
29	960	60	470
30		61	
31	810	62	

Ambient Temperature 74°F

Velocity Traverse

85

Boeing - Plant 2 - #5A Chromic Anodize Aluminum Tank
Date: August 22, 1989
Time: 16:55 - 17:15

<u>Vent #</u>	<u>Velocity (ft/min)</u>	<u>Vent #</u>	<u>Velocity ft/min</u>
1		32	1060
2	1780	33	
3		34	
4	1690	35	1090
5		36	1080
6	2140	37	
7		38	1130
8	1800	39	
9		40	830
10	1690	41	
11		42	860
12	1640	43	
13		44	780
14	1770	45	
15		46	820
16	1560	47	
17		48	730
18	1420	49	
19		50	690
20	1500	51	
21		52	690
22	1470	53	
23		54	700
24	1220	55	
25		56	320
26	1390	57	
27		58	620
28	1190	59	
29		60	550
30	990	61	
31		62	510

Ambient Temperature 83°F

Velocity Traverse

86

Boeing - Plant 2 - #5A Chromic Anodize Aluminum Tank

Date: August 31, 1989

Time: 11:35 - 11:50

<u>Vent #</u>	<u>Velocity (ft/min)</u>	<u>Vent #</u>	<u>Velocity ft/min</u>
1	2270	32	
2		33	
3		34	
4		35	
5		36	1060
6	1810	37	
7		38	
8		39	
9		40	
10		41	730
11		42	
12	1740	43	
13		44	
14		45	
15		46	820
16	1640	47	
17		48	
18		49	
19		50	
20		51	680
21	1650	52	
22		53	
23		54	
24		55	
25		56	340
26	1220	57	
27		58	
28		59	
29		60	
30		61	620
31	730	62	

Ambient Temperature 78°F

Velocity Traverse

87

Boeing - Plant 2 - #5A Chromic Anodize Aluminum Tank
Date: August 31, 1989
Time: 14:20-14:50

<u>Vent #</u>	<u>Velocity (ft/min)</u>	<u>Vent #</u>	<u>Velocity ft/min</u>
1	2380	32	
2		33	
3		34	
4		35	
5		36	1060
6	2230	37	
7		38	
8		39	
9		40	
10		41	820
11	1650	42	
12		43	
13		44	
14		45	
15		46	
16	1700	47	
17		48	
18		49	
19		50	
20		51	720
21	1610	52	
22		53	
23		54	
24		55	
25		56	280
26	1390	57	
27		58	
28		59	
29		60	
30		61	500
31	720	62	

Ambient Temperature 81°F

Velocity Traverse

88

Boeing - Plant 2 - #5A Chromic Anodize Aluminum Tank
Date: November 30, 1989
Time: 11:00 - 11:05

<u>Vent #</u>	<u>Velocity (ft/min)</u>	<u>Vent #</u>	<u>Velocity ft/min</u>
1		32	
2		33	
3		34	
4		35	970
5	2400	36	
6		37	
7		38	
8		39	
9		40	750
10	1790	41	
11		42	
12		43	
13		44	
14		45	950
15	1690	46	
16		47	
17		48	
18		49	
19		50	460
20	1560	51	
21		52	
22		53	
23		54	
24		55	260
25	960	56	
26		57	
27		58	
28		59	
29		60	600
30	1010	61	
31		62	

Ambient Temperature 76°F

SECTION 6
CHROMIC ACID SAMPLES
TAKEN FROM THE BATH

Sample Type:	Acid Sample
Sampling Date:	September 19, 1989
Lab Number:	917176
Hexavalent Chromium:	5,292,000 micrograms/sample 5.3 grams/sample
Total Chromium:	48,470,000 micrograms/sample 48.5 grams/sample

Sample Type:	Acid Sample
Sampling Date:	November 30, 1989
Lab Number:	922117
Hexavalent Chromium:	6,578,000 micrograms/sample 6.6 grams/sample
Total Chromium:	6,325,000 micrograms/sample 6.3 grams/sample

METHODOLOGY REFERENCES

Hexavalent chromium testing and analysis methods detailed in a paper titled "Method Development and Testing for Measurement of Source Levels of Hexavalent and Total Chromium" by Daniel G. Bivens and W.G. DeWees were utilized for this project. Sampling procedures specified in the July 1, 1988 Title 40 Code of Federal Regulations, Part 60 (40 CFR 60), Appendix A, Methods 1-5 were also used. Quality assurance procedures for source testing are outlined in the EPA's reference manual titled Quality Assurance Handbook for Air Pollution Measurement Systems, Volume 3, EPA-600/4-77-027b.

The specific sampling and analysis procedures utilized for the particle size distribution tests detailed in the operations manual for the Mark 3-5 impactor by Dr. Michael J. Pilat and the "Procedures for Cascade Impactor Calibration and Operation in Process Streams - Revised 1983 to Include PM₁₀ Source Sampling" prepared by Mr. D. Bruce Harris for the U.S. EPA, February 1984. Methodology and procedures specified in "Recommended Methodology for the Determination of Particle Size Distributions in Ducted Sources" prepared by the Southern Research Institute for the California Air Resources Board, ARB Contract A3-092-32, May 1986 were also referenced for sampling strategies.

SAMPLING AND ANALYSIS PROCEDURES

CHROMIUM SAMPLES

The sample train used for collecting chromium (Cr) and hexavalent chromium (Cr⁺⁶) samples was an EPA Method 5 design with modifications. A typical Method 5 sample train schematic is included as Figure 5 in Appendix B of this report. The sample train did not include a heated front-half filter. A quartz probe with an attached nozzle was inserted into the stack to draw a sample into the impingers. The probe was equipped with "S" type pitot tubes to measure velocity and a thermocouple sensor to measure the stack temperature at each sample point. The thermocouple probe was connected to a Fluke^R digital thermocouple indicator which is accurate to within ± 1 degree Fahrenheit. The condenser section of the sample train consisted of a modified Greenburg-Smith bubbler containing 100 milliliters (ml) of 0.1 N sodium hydroxide (NaOH) absorbing solution, a second impinger containing 100 ml of NaOH absorbing solution, a third impinger containing 100 ml of 0.1 N nitric acid (HNO₃), an empty bubbler, a back-half filter holder containing a Teflon^R filter, and a final bubbler containing indicating silica gel desiccant. The condenser section was maintained at a temperature below 68° F by adding ice to the condenser section throughout sampling.

The sample train was connected to a control box by means of an umbilical cord which contains a vacuum hose, pitot lines, thermocouple wires and a 4-wire electrical cord. The control box (meter box) was used to monitor stack conditions and to facilitate isokinetic sampling. The control box consists of a diaphragm pump which is used to pull the stack gas through the sample train, fine and coarse metering valves to control the sampling rate, a vacuum gauge which measures the pressure drop from the sampling nozzle to the metering valves, and a calibrated

dry gas meter. At the outlet of the dry gas meter is a calibrated orifice which is used to isokinetically control the flow of gas through the metering system. The pressure drop across the orifice was monitored with both low and high range magnehelic gauges. The pitot tubes utilized to measure stack gas velocity are connected to the control box via the umbilical cord. The control box contains low and high range magnehelic gauges which are used for the velocity measurement.

The chrome anodizing tank ventilation system exhausts to a 48 inch diameter circular stack with two (2) sampling ports available 90 degrees apart. The sampling ports are located 2 feet upstream and 6 feet downstream from the nearest flow disturbance. Two (2) traverses of six (6) points each were performed during each chromium test. Figure 4 located in Appendix B of this report is a schematic of the stack and the point locations selected. The sample probe was marked with felt pen to indicate the proper point location.

Stack condition measurements were made prior to collecting a sample. The appropriate sample nozzle was selected and isokinetic operating parameters were established utilizing a Hewlett-Packard programmable calculator. The sampling nozzle, probe and condenser section glassware were all cleaned and rinsed with dilute nitric acid and deionized water prior to assembling the sample train. The sample train was assembled and leak tested following the procedures outlined in Method 5. Before each test, a final check was made to assure that the process was operating at the desired production rate and the desired operating parameters (e.g. whether parts were in the bath or not). Ice was added to the condenser section. The sample nozzle was positioned in the stack at the first sample point. The sample pump was then turned on and the gas sampling rate was adjusted for isokinetic sampling. Sampling proceeded isokinetically at each of the 6 traverse

points. The pump was then turned off and the sample train was carefully moved to the second port. The nozzle was then positioned at the first point of the second traverse, the pump was again turned on and isokinetic sampling was performed at the 6 traverse points. Upon completion of the second traverse the sample probe was removed from the stack and a post-test leak check was performed according to Method 5 procedures.

Following sample collection, the samples were transferred to a temporary laboratory area for clean up. The back-half filters were transferred to glass petri dishes labeled with the sample date, client name and run number. These filters, along with an unused filter to be analyzed as a blank, were submitted to the Am Test laboratory for washing and chromium analysis.

The contents of the nozzle, probe liner and connective glassware were quantitatively transferred to a glass storage container using 0.1 N NaOH. An iodine flask with a female ball joint end was attached to the male ball joint end of the probe to assure that no material collected inside the glassware was lost during the rinsing and brushing of the probe. The contents of the iodine flask were quantitatively transferred to the storage container labeled with sample date, client name, and run number. A portion of the reagent was placed in a glass storage container and submitted with the samples to the Am Test laboratory for analysis for chromium.

The bubblers and impingers utilized for the condenser section of the sample train were weighed with a readability of ± 0.1 grams before and after sampling on a Mettler PE3000 electronic top loading balance. The difference between the initial and final weights of the condenser section constitute the amount of moisture gain

during the run. The contents of the first two (2) impingers containing sodium hydroxide absorbing solution were then transferred to a 1000 ml glass graduated cylinder. The bubblers and impingers were rinsed with 0.1 N NaOH reagent into the graduated cylinder, and the liquid level was recorded. The liquid was then transferred to the corresponding sample container for each run which contained the probe wash. For some samples, the solutions from the probe rinse, 1st impinger and 2nd impinger were analyzed separately to evaluate collection efficiency for this method. The liquid in the 3rd and 4th impingers containing HNO₃ were transferred to a 1000 ml glass graduated cylinder. The bubblers and impingers were rinsed with 0.1 N HNO₃ reagent into the graduated cylinder, and the liquid level was recorded. The sample was then transferred to a labeled sample container. The samples were then transferred to the Am Test, Inc. laboratory for chromium analysis. The sodium hydroxide solutions were analyzed for both hexavalent chromium and total chromium. The nitric acid solutions and the teflon filter were analyzed for total chromium only. Hexavalent chromium (Cr⁺⁶) analysis was performed using EPA Method 7176, which is a diphenylcarbazide colorimetric method. The hexavalent chromium analyses were completed within 48 hours after collecting the samples. Total chromium (Cr) analysis was performed using EPA Method 200.7, which utilizes inductively coupled plasma (ICP) spectroscopy. The laboratory results were presented in units of micrograms per sample. Those units were converted to concentrations in air.

PARTICLE SIZE DISTRIBUTION SAMPLES

Cascade impactors separate the sampled aerosol particles into size increments by inertial impaction of the particles onto a collection surface, in this case ultrapure microfiber quartz filter paper. This occurs at successive stages through the impactor, hence the name "Cascade". The resulting index of the measured particle

size is traditionally separated by the particle diameter collected with 50% collection efficiency by each jet stage, and this diameter is usually called the "cut diameter" and is characterized by the symbol " D_{50} ". The aerodynamic cut diameter is the diameter of a unit density sphere which will be collected with 50% efficiency by the specific impactor jet stage.

For these tests Am Test used straight nozzles at the inlet to a Pilat (U of W) Mark 5 source test Cascade impactor. A photograph of the Mark 5 impactor with a straight nozzle is illustrated in Figure 6 in Appendix B of this report. A complete Cascade impactor sampling train is illustrated in Figure 7 in Appendix B of this report. The Mark 5 impactors were assembled using the jet stages listed for configuration #78, which has a 78 hole final stage. In this configuration, the Mark 5 impactor provided eleven (11) aerodynamic particle size cut diameters, of sizes between 0.25 and 20 microns in diameter.

Whatman QM-A ultra-pure quartz microfiber filter substrates which were mounted on stainless steel inserts and baked at 500° F for 2 hours, desiccated for 24 hours and weighed to a constant weight on a Mettler AE163 electronic balance (set to a time integrating mode with a readability of 0.01 milligrams) were used to line each collection plate. Following the impactor run, the substrates were desiccated for 24 hours and weighed again.

The impactor probe was connected to a condenser section identical to the chromium samples. The sample train was connected to a control box as described for the chromium samples. The impingers were weighed before and after each test for calculating the percent moisture in the gas stream. The condenser section was leak-checked prior to starting a test. The flow rate through the impactor was pre-

set to the rate necessary for isokinetic sampling at the specific velocity point. The particle size distribution samples were collected at a point of average velocity in the stack. The impactor was positioned in the stack at the sample point with the nozzle facing away from the gas stream and was allowed to come to stack temperature for approximately one-half (1/2) hour. Ice was added to the condenser section of the particle size sample train. The nozzle was then turned to face the flow and the sample pump was turned on and the sampling rate was maintained at the pre-set rate necessary for isokinetic sampling.

After a sample had been collected the pump was then turned off and the impactor was removed from the stack, taking care that the nozzle tip did not touch the port nipple. The impactor was detached from the probe and carefully transferred to Am Test's temporary laboratory. The impactor was allowed to cool and was carefully disassembled and inspected. Each stage was inspected for proper particulate matter deposition. All interior impactor surfaces were checked for wall loss. The stainless steel inserts, onto which the substrates are mounted, were transferred to individual petri dishes and placed into a Labconco^R desiccator. Two (2) substrate blanks for each sample set were kept with the sample to audit desiccation and weighing techniques. To obtain final weights, the substrates were desiccated for 24 hours and weighed. The weights were recorded on the data sheet and in a bound laboratory notebook. The total weight of each substrate and stainless steel insert is approximately 1 gram. The low tare weight and simple donut-like shape of the Pilat (U of W) Mark 5 Cascade impactor insert-substrate combination allows for a great degree of weighing accuracy.

Once final weights were obtained for the substrates, each filter which lines the substrates was placed in a separate glass jar for submittal to the laboratory for

chromium analysis. The substrates were collectively rinsed into a separate jar. The appropriate blank filters and reagents were submitted along with the samples.

QUALITY ASSURANCE

A strict quality assurance program was followed throughout preparation, sampling, analysis, data reduction, and report preparation. This program includes recent equipment calibrations, careful chain-of-custody procedures, the use of ACS quality or better reagents, analysis of control samples, and "by-hand" calculation checks of computerized results.

The sample nozzles used to collect isokinetic samples were calibrated on-site before sampling using inside calipers readable to 0.001 inches. The dry gas meters used to accurately measure sample volumes have been recently calibrated using a spirometer at the Washington State Department of Ecology (DOE) laboratory in Redmond, Washington. The "S" type pitot tubes used for velocity measurement have also been recently calibrated utilizing a wind tunnel and a standard "P" type pitot tube and are inspected regularly for proper alignment. The digital Fluke thermocouple indicators used to obtain temperature measurements are accurate to ± 1 degree Fahrenheit. Each thermocouple probe used to monitor temperatures is checked quarterly at 3 different temperature settings.

In addition to quantitative clean-up and analysis procedures, filter and reagent blanks, as well as standard solutions were carried throughout the analysis procedures. The samples were weighed to constant weights of ± 0.05 milligrams following desiccation in a Labconco "Autodry Cabinet" desiccator. This desiccator is an electronic dehumidifier which automatically maintains the humidity inside the desiccator. The dehumidifier automatically recharges the internal desiccant every 5.5 hours with a small heater and fan inside the chamber. An Airguide humidity indicator accurate to $\pm 1\%$ is used to check the humidity inside the

desiccator when obtaining tare and final weights. Indicating silica gel desiccant is added to the chamber as necessary to maintain the humidity at the desired level. The Mettler AE163 electronic balance used to obtain weights was set to a time integrating mode (100,000 readings per minute) with a readability of 0.01 milligrams. The balance was calibrated prior to every use. The calibration of Am Test's Mettler balances is checked by the manufacturer on a yearly basis.

Each stage of the Mark 5 cascade impactor has been calibrated using a polydispersed aerosol and optical size analyzer at a range of temperatures and flow rates to determine the inertial impaction parameter for that particular stage. This parameter is intrinsic for each stage being controlled by the physical configuration of the stage and other pertinent aerodynamic values. The stages are periodically examined for wear and corrosion and are replaced as necessary.

Additional information with respect to Am Test, Inc.'s laboratory quality assurance and quality control protocol programs is included in the Appendix of this report.

CALCULATION OF RESULTS

The velocity, airflow, molecular weight, and moisture results were calculated using EPA 40 CFR 60 Method 1-5 criteria. Copies of pertinent equations are included in the Appendix of this report. Final results calculations were performed using spreadsheet programs run on a Hewlett-Packard Vectra computer system. Sample "by-hand" calculations of results were completed using a Hewlett-Packard calculator, and may be found in the Appendix of this report.

The particle size distribution results were computer generated in the Am Test Air Quality Division office utilizing a Cascade impactor data reduction program. This computer program is considered as "state-of-the-art" by particle sizing experts throughout the United States. Computer printouts of the particle size distribution results are included in Appendix A. To plot the particle size distribution, the column titled "aerodynamic diameter" (in micrometers) was plotted against the column titled "percent less than" on semi-log versus probability graph paper to illustrate the particle size distribution for each Mark 5 run.

APPENDIX A

ANALYSIS REPORT

CLIENT: Am Test, Inc. - Air Quality Division

DATE RECEIVED: 8/23/89

REPORT TO: Kris Hansen

DATE REPORTED: 9/11/89

BOEING PLANT #2

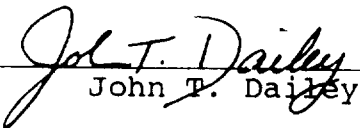
Laboratory Sample Numbers	Client Identification	Total Chromium (ug)	Hexavalent Chromium (ug)	Volume (ml)
915088	Blank (0.1N NaOH)	<0.60	0.036	100.
915089	Run 1 Probe	1,040.	1,670. 1,650.] 1060	215.
915090	Run 1 First Impinger	78.6	94.	130.
915091	Run 2 Probe & First Impinger	1,030.	1,970.	285.
915092	Run 3 Probe & First Impinger	283.	321.	329.
915093	Run 1 Second Impinger	102.	120.	130.
915094	Run 2 Second Impinger	113.	122. 123.] 122.5	139.
915095	Run 3 Second Impinger	2.2	11.5	144.
DETECTION LIMIT*		0.006	0.025	-
EPA Method used		200.7	7176	-

< = less than

*Values reported in mg/l.

JTD/pb

REPORTED BY


John T. Dailey

ANALYSIS REPORTCLIENT: Am Test, Inc. - Air Quality
Division

DATE RECEIVED: 8/23/89

REPORT TO: Kris Hansen

DATE REPORTED: 8/31/89

BOEING PLANT #2

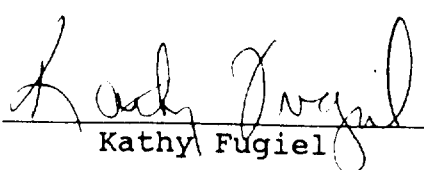
Laboratory Sample Nos.	Client Identification	Total Chromium	Volume (ml)
915096	Blank Filter	<0.15*	-
915097	Run 1 Filter	<0.15*	-
915098	Run 2 Filter	<0.18*	-
915099	Run 3 Filter	<0.15*	-
915100	Run 1 HNO ₃ Solution	<1.00**	166.
915101	Run 2 HNO ₃ Solution	<1.02**	170.
915102	Run 3 HNO ₃ Solution	<0.894**	149.
915103	Blank Solution (0.1 N HNO ₃)	<0.600**	100.
DETECTION LIMIT		0.006	-
EPA Method used		200.7 (ICP)	-

*Reported in ug/filter.

**Reported in ug.

KF/pb

REPORTED BY


Kathy Fugiel

ANALYSIS REPORT

CLIENT: Air Quality Division

DATE RECEIVED: 8/30/89

REPORT TO: Kris Hansen

DATE REPORTED: 9/7/89

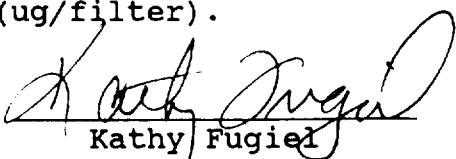
BOEING PLANT 2

Laboratory Sample No.	Client Identification	Total Chromium (ug) *	Hexavalent Chromium (ug)
915486	Run 1 1st Impinger & Probe	297.	324.
915487	Run 1 2nd Impinger	4.16	7.49
915488	0.1 N NaOH Blank	0.70	2.2
915489	Run 1 HNO ₃ 3rd & 4th Imp	<1.06	-
915490	0.1 N HNO ₃ Blank	<0.60	-
915491	Run 1 Teflon Filter*	2.0	-
915492	Teflon Filter Blank*	<0.30	-
EPA Method		200.7	7196

*Filter samples reported as (ug/filter).

KF/ja

REPORTED BY:


Kathy Fugiel

ANALYSIS REPORT

CLIENT: Am Test, Inc. - Air Quality Division

DATE RECEIVED: 9/1/89

REPORT TO: Kris Hansen

DATE REPORTED: 9/12/89

BOEING PLANT #2 - BUILDING 210

Laboratory Sample Numbers	Client Identification	Hexavalent Chromium	Total Chromium	Volume (ml)
<u>Blank</u>				
915737	0.1N NaOH	<2.5	<0.60	100.
915738	0.1N HNO ₃	-	<0.60	100.
915739	Teflon Filter	-	<0.30	-
<u>R1 Workroom (Bath #5)</u>				
915740	NaOH Imp #1	1,553.	1,311.	187.
915741	NaOH Imp #2	28.3	25.7	133.
915742	NHO ₃ Imp #3 & #4	-	<0.87	145.
915743	Filter	-	<0.30	-
<u>R1-PS</u>				
915744	Impactor Rinse NaOH	156.	162.	183.
915745	Probe Rinse	1.16	4.45	89.
915746	Imp #1	<3.7	<0.90	150.
915747	Imp #2	<3.3	<0.79	132.
915748	Imp #3 & #4	-	<0.83	138.
915749	Filter	-	<0.30	-
<u>R2</u>				
915750	Probe Rinse	620.	603.	178.
915751	Imp #1	26.1	32.0	130.
915752	Imp #2	43.2	42.3	137.
915753	Imp #3 & #4	-	1.09	121.
915754	Filter	-	<0.30	-

-2-

CLIENT: Am Test, Inc. - Air Quality Division

DATE RECEIVED: 9/1/89

REPORT TO: Kris Hansen

DATE REPORTED: 9/12/89

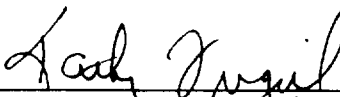
BOEING PLANT #2 - BUILDING 210

Laboratory Sample Numbers	Client Identification	Hexavalent Chromium	Total Chromium	Volume (ml)
<u>R3</u>				
915755	Probe	654.	596.	143.
915756	Imp #1	35.3	34.0	141.
915757	Imp #2	44.2	42.2	141.
915758	Imp #3 & #4	-	<0.96	160.
915759	Filter	-	<0.30	-

Liquid Solutions are reported in units of ug.
Filter Samples are reported in units of ug/filter.
Volumes are reported in units of ml.

KF/pb

REPORTED BY


Kathy Fugiel

ANALYSIS REPORTCLIENT: Am Test, Inc. - Air Quality
Division

DATE RECEIVED: 9/6/89

REPORT TO: Kris Hansen

DATE REPORTED: 9/18/89

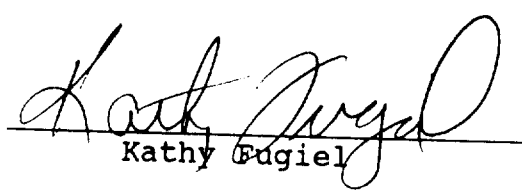
BOEING PLANT #2

Laboratory Sample Nos.	Client Identification	Total Chromium	Volume (ml)
915962	Rinse of Substrates	0.75 ug	50.
915963	Blank Solution	<0.60 ug	100.
915965	Blank Filters	0.65*	-
915966	1	4.75*	-
915967	2	3.47*	-
915968	3	62.7*	-
915969	4	55.7*	-
915970	5	12.*	-
915971	6	3.3*	-
915972	7	0.67*	-
915973	8	0.42*	-
915974	9	0.45*	-
915975	10	0.40*	-
915976	12	6.7*	-
Filter Reagent Blank		0.20 ug	-
EPA Method No.		200.7 (ICP)	-

*Reported in ug/filter.

KF/pb

REPORTED BY


Kathy Eugiel

ANALYSIS REPORT

CLIENT: Air Quality Division

DATE RECEIVED: 9/20/89

REPORT TO: Kris Hansen

DATE REPORTED: 9/29/89

BOEING PLANT 2

Laboratory Sample No.	Client Identification	Chromic Acid Bath #5 Total Chromium	Hexavalent Chromium
917067	Run 1 Imp 1 & 2 (.1N NaOH)	24.5	<6.25
917068	Run 1 Imp 3 & 4 (0.1 HNO ₃)	1.33	-
917069	Run 1 Teflon Filter	0.175	-
917070	Run 2 Imp 1 & 2 (0.1 NaOH)	268.	247. 246.]
917071	Run 2 Imp 3 & 4 (0.1 HNO ₃)	1.64	-
917072	Run 2 Teflon Filter	0.275	-
917073	Blank Solution (0.1 NaOH)	<1.00	<2.5
917074	Blank Solution (0.1 NHCO ₃)	1.2	-
917075	Blank Teflon Filter	0.175	-
917076	Bath #5 Sample 48,470,000.	5,292,000.	131
917077	Run 1 Probe (0.1 N NaOH)	28.8	23.1
917078	Run 2 Probe (0.1 N NaOH)	1,141.	1,212.
Detection Limit (ug/ml)		0.006	0.025
EPA Method		200.7 (ICP)	7196

Solutions reported in ug, filter reported as ug/filter.

KF/ja

REPORTED BY:

Kathy Fugiel

ANALYSIS REPORT

CLIENT: AM TEST, INC. - AIR QUALITY
DIVISION

DATE RECEIVED: 12/4/89
DATE REPORTED: 12/11/89
DATE REVISED: 1/30/90

REPORT TO: Kris Hansen

BOEING PLANT #2

Laboratory Sample Nos.	Client Identification	Chromium (ug/filter)	Volume (ml)
922208	Stage RB-1	1.72	-
922209	Stage RB-2	1.20	-
922210	Stage RB-3	33.5	-
922211	Stage RB-4	49.8	-
922212	Stage RB-5	24.0	-
922213	Stage RB-6	3.60	-
922214	Stage RB-7	0.58	-
922215	Stage RB-8	0.32	-
922216	Stage RB-9	0.35	-
922217	Stage RB-10	<0.15	-
922218	Stage RB-12	9.0	-
922219	Rinse of RB Substrates	1.62*	116.
922220	Rinse of H Substrates	<0.6*	100.
922221	Blank Sol.	<0.6*	130.
922222	Blank Filters**	<0.15	-
922223	Stage H-1	0.45	-
922224	Stage H-2	1.12	-
922225	Stage H-3	57.8	-

*Results are in ug.

**4 Mark 5 filters.

Filters were brought to 25 mls. total volume.

-2-

CLIENT: AM TEST, INC. - AIR QUALITY
DIVISION

DATE RECEIVED: 12/4/89
DATE REPORTED: 12/11/89
DATE REVISED: 1/30/90

REPORT TO: Kris Hansen

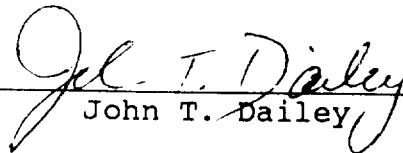
BOEING PLANT #2

Laboratory Sample Nos.	Client Identification	Chromium (ug/filter)	Volume (ml)
922226	Stage H-4	50.5	-
922227	Stage H-5	22.9	-
922228	Stage H-6	2.08	-
922229	Stage H-7	0.52	-
922230	Stage H-8	0.42	-
922231	Stage H-9	<0.15	-
922232	Stage H-10	<0.15	-
922233	Stage H-12	<0.15	-
BLANK 1		<0.15	-
BLANK 2		<0.15	-

Filters were brought to 25 mls. total volume.

JTD/pb

REPORTED BY


John T. Dailey

ANALYSIS REPORTCLIENT: AM TEST, INC. - AIR QUALITY
DIVISIONDATE RECEIVED: 11/30/89
DATE REPORTED: 12/1/89
DATE REVISED: 1/30/90

REPORT TO: Kris Hansen

BOEING PLANT #2

Laboratory Sample Numbers	Client Identification	Chromium (ug)	Hexavalent Chromium (ug)	Volume (ml)
922090	Blank 0.1 N NaOH	<0.6	<25.	100.
922091	Blank 0.1 N HNO ₃	<0.6	-	100.
922092	Blank Teflon Filter	<0.15*	-	-
922093	Run 1 Teflon Filter	<0.15*	-	-
922094	Run 1 NaOH Imp 1 & 2	470.	438.	395.
922095	Run 1 HNO ₃ Imp 3 & 4	<1.1	-	177.
922096	R2-PS Teflon Filter	<0.15*	-	-
922097	R2-PS NaOH Imp 1 & 2	6.08	<70.	380.
922098	R2-PS HNO ₃ Imp 3 & 4	<0.8	-	133.
922099	R2 Impactor Stages Rinse	24.2	<53.	212.

*Results are in ug/filter.

Filters were brought to 25 mls. total volume.

-2-

CLIENT: AM TEST, INC. - AIR QUALITY
DIVISIONDATE RECEIVED: 11/30/89
DATE REPORTED: 12/1/89
DATE REVISED: 1/30/90

REPORT TO: Kris Hansen

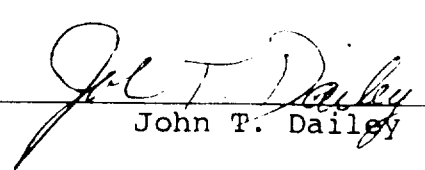
BOEING PLANT #2

Laboratory Sample Numbers	Client Identification	Chromium (ug)	Hexavalent Chromium (ug)	Volume (ml)
922100	R2 Straight Nozzle Rinse	86.6	68.4	38.
922101	R3-PS Teflon Filter	-	-	-
922102	R3-PS NaOH Imp 1 & 2	<2.16	<90.	360.
922103	R3-PS HNO ₃ Imp 3 & 4	1.34	-	168.
922104	R3-PS Impactor Rinse	26.1	<32.	128.
922105	R3-PS Nozzle Rinse	30.2	22.6	20.
922106	R4 Teflon Filter	<0.15*	-	-
922107	R4 NaOH Imp 1 & 2	6.90	679.	350.
922108	R4 HNO ₃ Imp 3 & 4	<0.9	-	157.

*Results are in ug/filter.
Filters were brought to 25 mls. total volume.

JTD/pb

REPORTED BY


John T. Dailey

ANALYSIS REPORTCLIENT: AM TEST, INC. - AIR QUALITY
DIVISIONDATE RECEIVED: 12/1/89
DATE REPORTED: 12/11/89
DATE REVISED: 1/30/90

REPORT TO: Kris Hansen

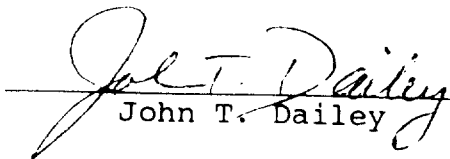
BOEING PLANT #2

Laboratory Sample Nos.	Client Identification	Chromium (ug)	Hexavalent Chromium (ug)	Volume (ml)
922111	Blank 0.1 N NaOH	<0.6	25.	100.
922112	Blank 0.1 N HNO ₃	<0.6	-	100.
922113	Blank Teflon Filter	<0.15*	-	-
922114	Run 5 NaOH Imp 1 & 2	458.	442.	409.
922115	Run 5 HNO ₃ Imp 3 & 4	1.20	-	171.
922116	Run 5 Teflon Filter	<0.15*	-	-
922117	Chromic Acid Bath #5	6,325,000.	6,578,000.	253.

*Results are in ug/filter.
Filters were brought to 25 mls. total volume.

JTD/pb

REPORTED BY


John T. Dailey

APPENDIX B

SAMPLE CALCULATION SHEET METHODS 1-5

CLIENT: BOEING PLANT #2

DATE OF TEST: 8-22-89

LOCATION: Seattle, Wash.

RUN #: 1 B0#5CR1

Lab # 915090

Particulate Matter Emission Concentration - Equation 5-1
1- Bath On

$$V_{m_{std}} = 17.647^{\circ}R / "Hg * 54.27 \text{ ft}^3 * .993 * (30.04 "Hg + (1.278 "H_2O / 13.6)) / (460 + 75.0^{\circ}F)$$

$$= 53.570 \text{ dscf}$$

$$dscm = 53.570 \text{ dscf} / 35.31 \text{ ft}^3/\text{m}^3$$

$$= 1.517 \text{ dscm}$$

Substitution of Equation 5-4 into 5-5

$$W_a = \text{mg} * \text{ml} / \text{ml}$$

$$= \text{mg}$$

$$M_n = (\text{net weight filter catch}) + (\text{net weight "B" section}) - W_a + \text{Back-half}$$

$$= \text{mg} = \text{mg} + \text{mg} - \text{mg} + \text{mg}$$

$$C_s = (0.001 \text{ g/mg}) * (15.43 \text{ grains/gram}) * \text{mg} / \text{dscf}$$

$$= \text{gr/dscf} \quad (\text{Equation 5-6})$$

$$\text{gr/dscf @ 7\% O}_2 = \text{gr/dscf} * (20.9\% - 7\% \text{O}_2) / (20.9\% - \text{\%O}_2)$$

$$= \text{gr/dscf @ 7\% O}_2$$

$$\text{gr/dscf @ 12\% CO}_2 = \text{gr/dscf} * 12\% / \text{\%CO}_2$$

$$= \text{gr/dscf @ 12\% CO}_2$$

$$\text{mg/dscm} = \text{mg} / \text{dscm}$$

$$= \text{mg/dscm}$$

Particulate Matter Emission Rate

$$\text{pounds/hour} = \text{gr/dscf} * \text{dscf/min} * 60 \text{ min/hr} * 1 \text{ lb/7000 grains}$$

$$= \text{lb/hr}$$

Moisture - Equation 5-2 and 5-3

$$V_{w_{std}} = 0.04715 \text{ ft}^3/\text{g} * 16.7 \text{ grams of H}_2\text{O collected in impingers}$$

$$= 0.787 \text{ scf}$$

SAMPLE CALCULATION SHEET (continued)
METHODS 1-5

$$B_{ws} = (.787 \text{ scf}) / (.787 \text{ scf} + 53.570 \text{ dscf})$$

$$= 0.0145$$

$$\% \text{Moisture} = 0.0145 * 100$$

$$= 1.45 \%$$

Molecular weight - Equation 3-2

$$M_d = 0.440 * (0.1 \% \text{CO}_2) + 0.320 * (20.9 \% \text{O}_2) + 0.280 * (79.0 \% \text{CO} + \% \text{N}_2)$$

$$M_d = 28.85 \text{ g/g-mole (dry)}$$

$$M_s = 28.85 \text{ g/g-mole} * (1 - 0.0145) + 18.0 \text{ g/g-mole} * 0.0145$$

$$M_s = 28.69 \text{ g/g-mole (wet)}$$

Stack gas velocity and volumetric flow rate - Equation 2-9 and 2-10

$$V_s = 85.49 * .84 * .4987 * \sqrt{538.5^\circ \text{R} / 28.69 \text{ g/g-mole} / 30.04 \text{ "Hg}}$$

$$V_s = 28.30 \text{ ft/sec (std)}$$

$$Q_{sd} = 3600 * (1 - 0.0145) * 28.30 \text{ ft/sec} * 12.566 \text{ ft}^2 * (528^\circ \text{R} / 538.5^\circ \text{R}) * (30.04 \text{ "Hg} / 29.92 \text{ "Hg})$$

$$= 1242.2498 \text{ dscf/hr} / 60 \text{ min/hr}$$

$$= 20704.1 \text{ dscf/min (dry standard cubic feet per minute)}$$

$$\text{acfm} = 28.30 \text{ ft/sec} * 12.566 \text{ ft}^2 * 60 \text{ sec/min}$$

$$= 21340.7 \text{ acfm (actual cubic feet per minute)}$$

Isokinetic variation - Equation 5-8

$$I = 0.09450 * 53.570 \text{ dscf} * 538.5^\circ \text{R} / (30.04 \text{ "Hg} * 28.30 \text{ ft/sec} * 60 \text{ min} * 0.005343 \text{ ft}^2 * (1 - 0.0145))$$

$$I = 10.1 \%$$

All of the above numbered equations are from the 40 CFR 60 and assume English units.

Example Calculations for Chromium
Boeing Plant 2, #5A Chrome Anodizing Tank
August 22, 1989, Run 1 with Bath On
Lab #'s 915089, 915090, 915093, 915097, 915100

Sample	$\mu\text{g Cr}$	$\mu\text{g Cr}^{+6}$
Probe	1040	1660
1st Impinger	78.6	94.
2nd Impinger	102	120
3rd Impinger	<1.00	—
Filter	<0.15	—
TOTAL	1220.6	1874.0

Hexavalent Chromium (Cr^{+6})

$$\frac{1874 \mu\text{g in sample} * \frac{1 \text{ mg}}{1000 \mu\text{g}}}{1.517 \text{ dscm of gas sampled}} = \boxed{1.235 \text{ mg/dscm}}$$

$$1.235 \text{ mg/dscm} * \frac{22.414 \text{ ml/m-mole}}{51.996 \text{ mg/m-mole}} * \frac{293.15^\circ\text{K}}{273.15^\circ\text{K}} * \frac{1 \text{ m}^3}{10^6 \text{ ml}} = 10^6 \text{ ppm}$$

$$= \boxed{0.57 \text{ ppm}}$$

$$1.235 \text{ mg/dscm} * 60 \text{ mg/hr} * \frac{1 \text{ m}^3}{35.32 \text{ ft}^3} * 20704.1 \text{ dscf/min} = \boxed{43,456.5 \frac{\text{mg}}{\text{hr}}}$$

$$43456.5 \text{ mg/hr} / 1825 \text{ amp-hr} = \boxed{23.8 \text{ mg/amp-hr}}$$

Total Chromium

$$\frac{1220.6 \mu\text{g}}{1.517 \text{ dscm}} * \frac{1 \text{ mg}}{1000 \mu\text{g}} = \boxed{0.805 \text{ mg/dscm}}$$

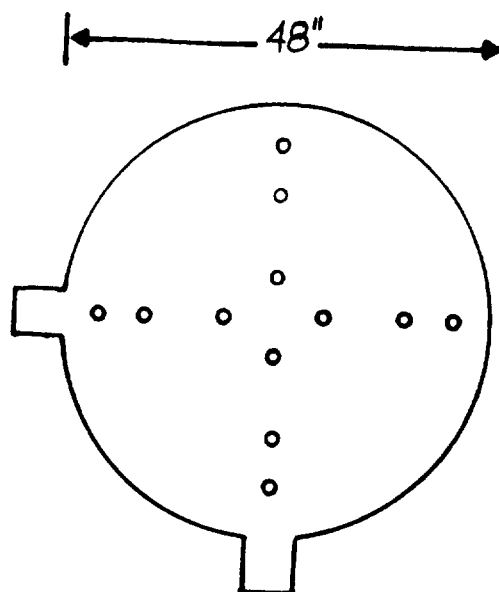
$$0.805 \text{ mg/dscm} * \frac{22.414 \text{ ml/m-mole}}{51.996 \text{ mg/m-mole}} * \frac{293.15^\circ\text{K}}{273.15^\circ\text{K}} * \frac{1 \text{ m}^3}{10^6 \text{ ml}} * 10^6 \text{ ppm} = \boxed{0.37 \text{ ppm}}$$

$$0.805 \text{ mg/dscm} * 60 \text{ mg/hr} * \frac{1 \text{ m}^3}{35.32 \text{ ft}^3} * 20704.1 \text{ dscf/min} = \boxed{28304.7 \text{ mg/hr}}$$

$$\frac{28304.7 \text{ mg/hr}}{1825 \text{ amp-hr/hr}} = \boxed{15.5 \text{ mg/amp-hr}}$$

CROSS SECTIONAL AREA

Traverse Point	Distance (inches)
1	2.11
2	7.01
3	14.21
4	33.79
5	40.99
6	45.89

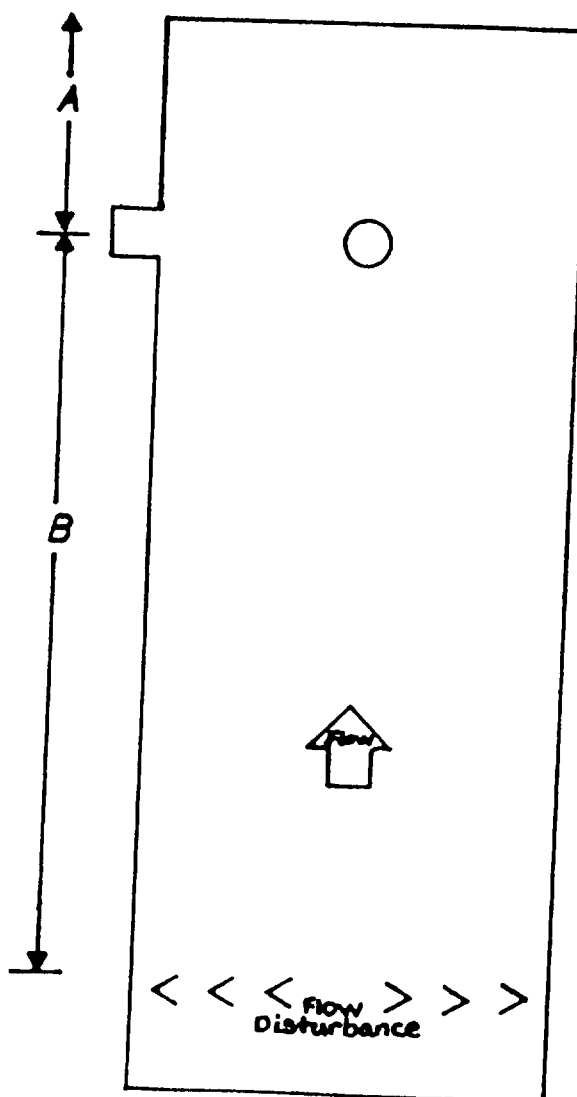
**STACK DIMENSIONS**

48 inch diameter circular stack

2 ports

A = 2 feet

B = 6 feet

**Figure 4. Location of sampling ports and traverse points.**

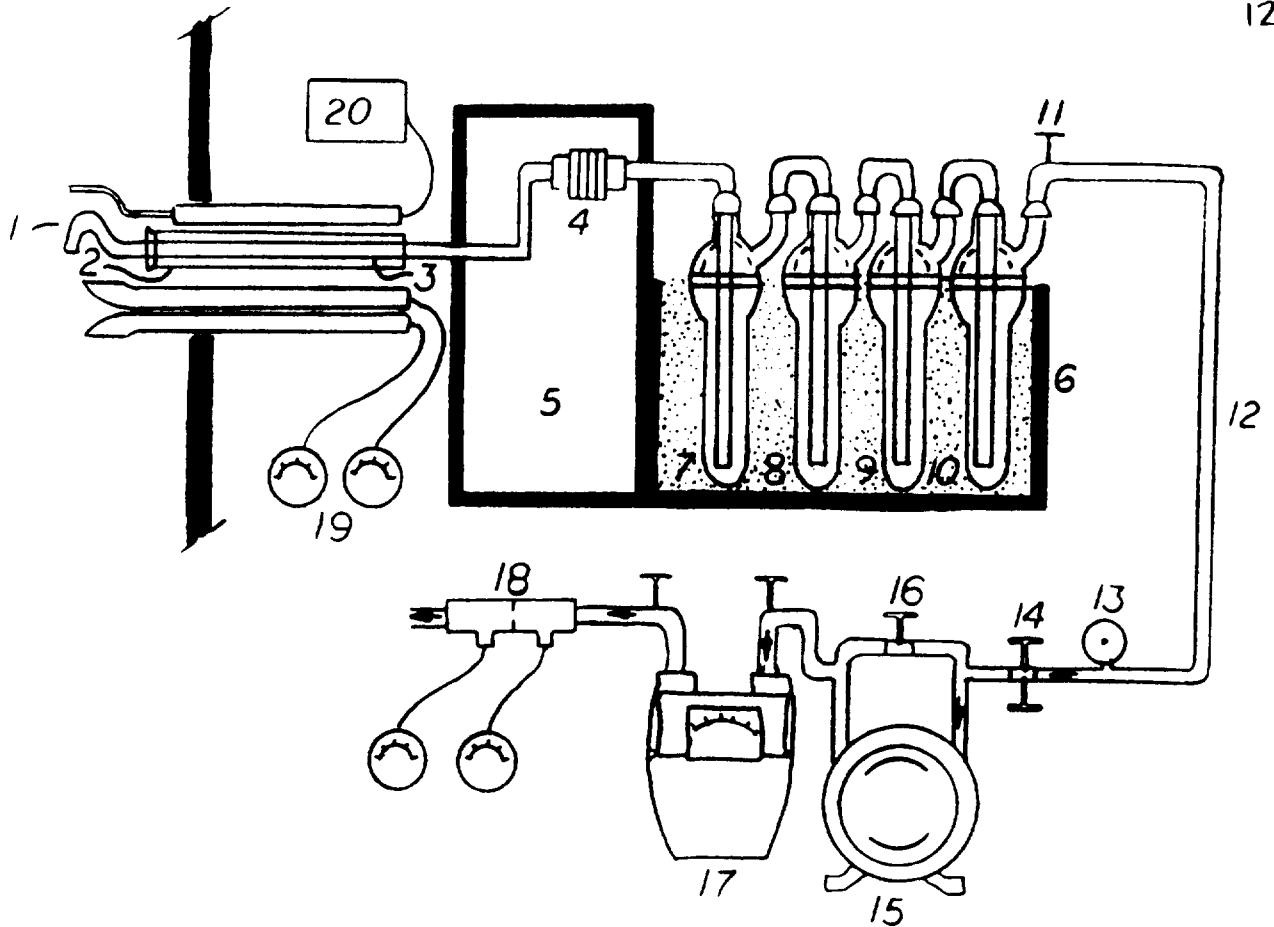
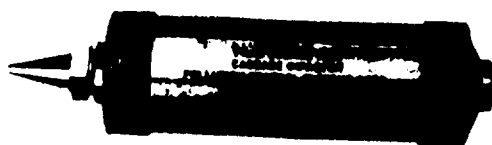


Figure 5. Method 5 Sample Train.

1. Sampling nozzle
2. Sampling probe sheath
3. Heated sample probe liner
4. Out of stack filter assembly
5. Heated filter compartment maintained at $248^{\circ}\text{F} \pm 25^{\circ}\text{F}$
(or temperature specified in 40 CFR subpart)
6. Impinger case - contains ice during sampling
7. First impinger containing 100 ml H_2O
8. Modified Greenburg-Smith impinger containing 100 ml H_2O
9. Third impinger - empty
10. Fourth impinger containing indicating silica gel desiccant
11. Impinger exit gas temperature sensor
12. Umbilical cord - vacuum line
13. Vacuum gauge
14. Fine and coarse adjustment valves
15. Leak free pump
16. By-pass valve
17. Dry gas meter with inlet and outlet temperature sensors
18. Orifice meter with magnehelic gauges
19. S-type pitot tube with magnehelic gauges
20. Fluke multi-channel digital thermocouple indicator



Mark 5 with sampling nozzle



PCSC Precutter with Nozzle on Mark 3

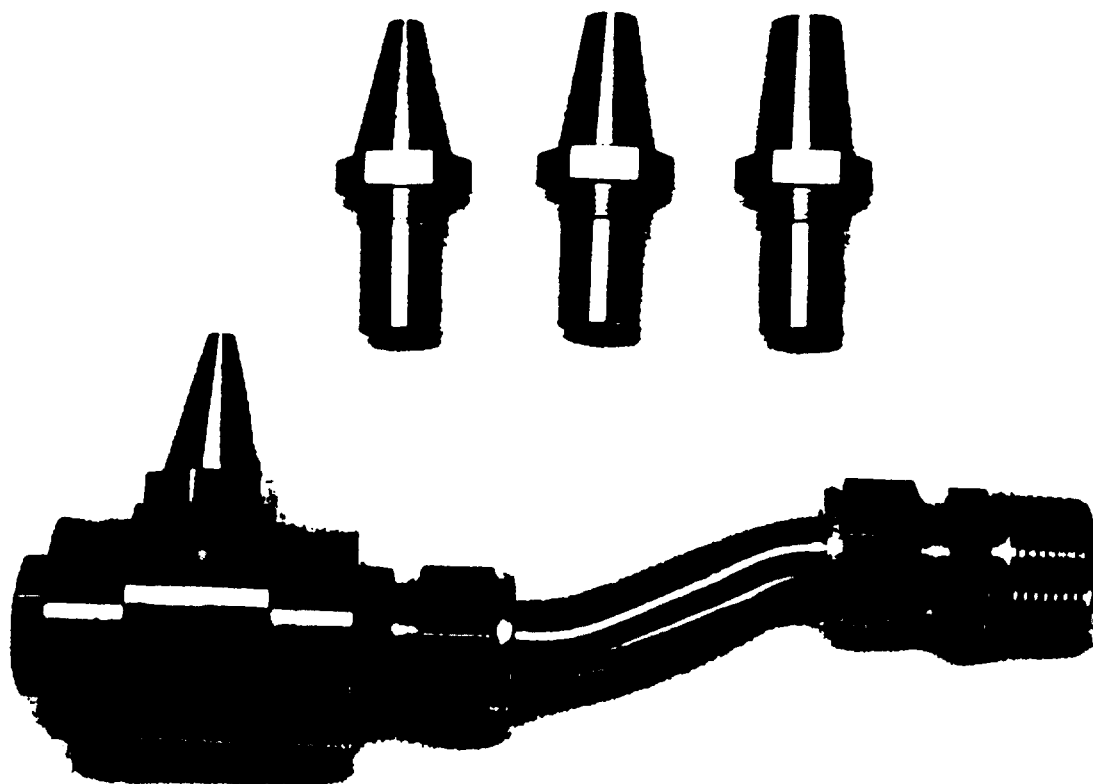


Figure 6. Illustration of Pilat (U of W) Mark 5 Cascade impactor, Mark 3 impactor equipped with a PCSC precutter attachment, and an enlargement of the PCSC precutter attachment.

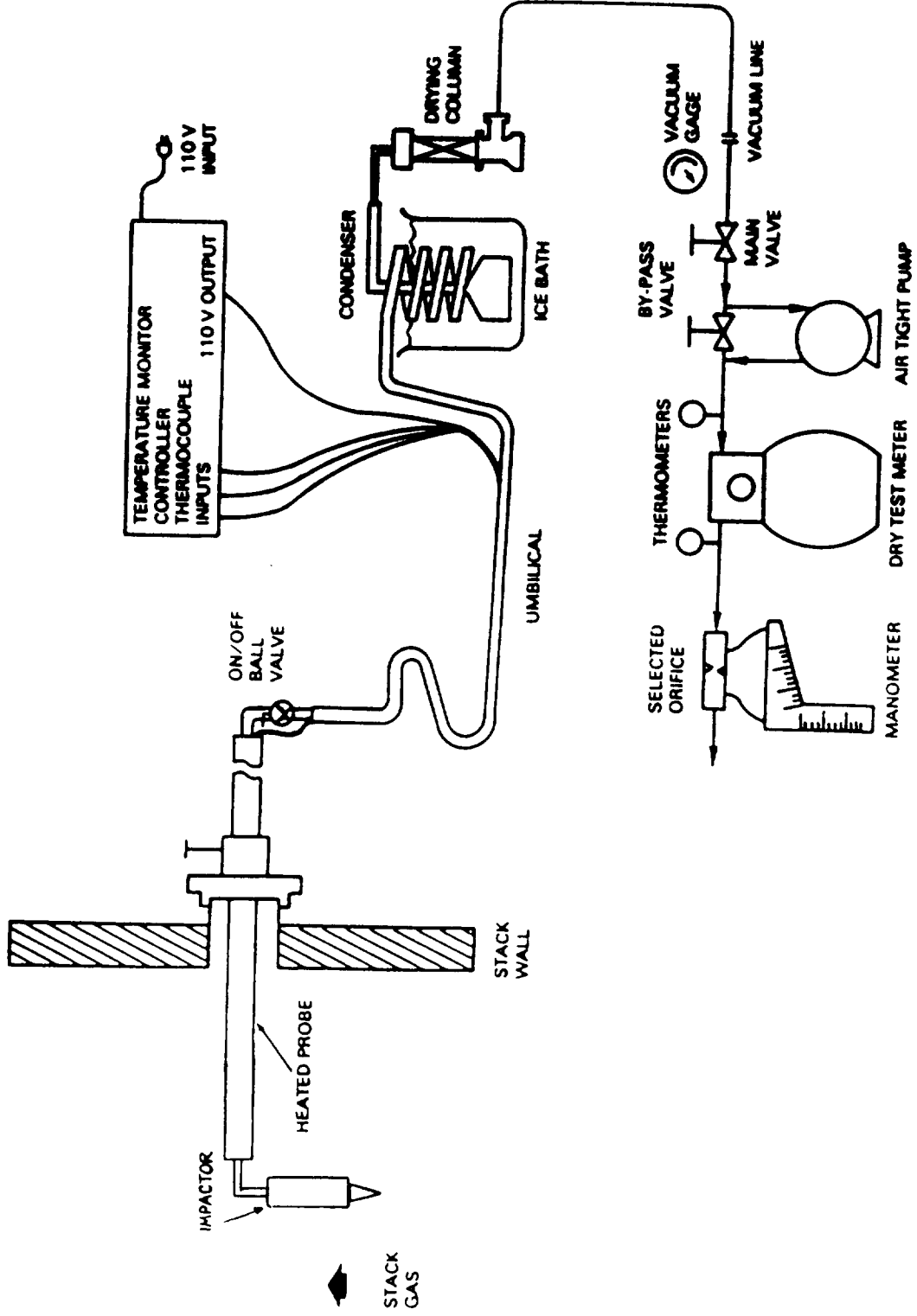


Figure 7. Cascade impactor particulate sampling train.

METHOD 1 - LOCATION OF TRAVERSE POINTS

Circular Stacks

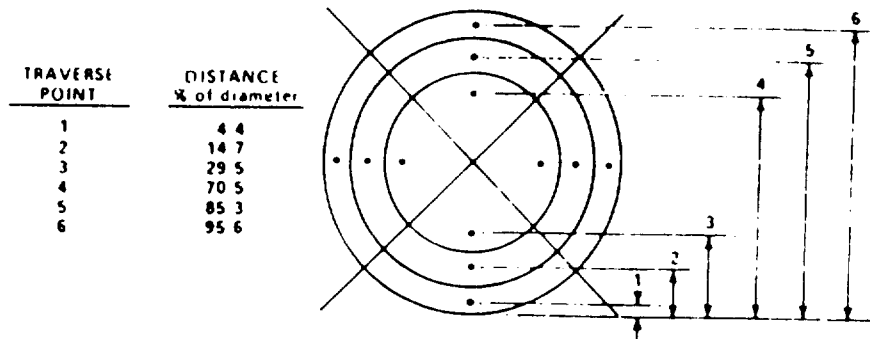


Figure 1.3. Example showing circular stack cross section divided into 12 equal areas, with location of traverse points indicated.

TABLE 1-2. LOCATION OF TRAVERSE POINTS IN CIRCULAR STACKS

(Percent of stack diameter from inside wall to traverse point)

Traverse point number on a diameter	Number of traverse points on a diameter—											
	2	4	6	8	10	12	14	16	18	20	22	24
1	14.6	6.7	4.4	3.2	2.6	2.1	1.8	1.6	1.4	1.3	1.1	1.1
2	85.4	25.0	14.6	10.5	8.2	6.7	5.7	4.9	4.4	3.9	3.5	3.2
3		75.0	29.6	19.4	14.6	11.8	9.9	8.5	7.5	6.7	6.0	5.5
4			93.3	70.4	32.3	22.6	17.7	14.6	12.5	10.9	9.7	8.7
5				85.4	67.7	34.2	25.0	20.1	16.9	14.6	12.9	11.6
6					95.6	80.6	65.8	55.6	48.0	41.8	36.5	32.2
7						89.5	77.4	64.4	54.3	46.5	40.2	35.8
8							96.8	85.4	75.0	63.4	55.0	48.4
9								91.8	82.3	73.1	62.5	55.0
10									97.4	88.2	79.9	71.7
11										93.3	85.4	78.0
12											97.9	90.1
13												94.3
14												
15												
16												
17												
18												

Rectangular Stacks

For a rectangular cross section, an equivalent diameter (D_e) shall be calculated from the following equation, to determine the upstream and downstream distances:

$$D_e = \frac{2LW}{(L+W)}$$

where L = length and W = width.

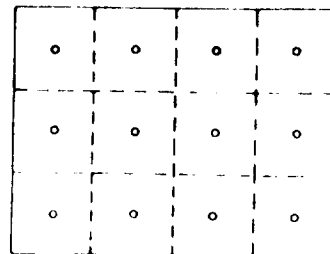
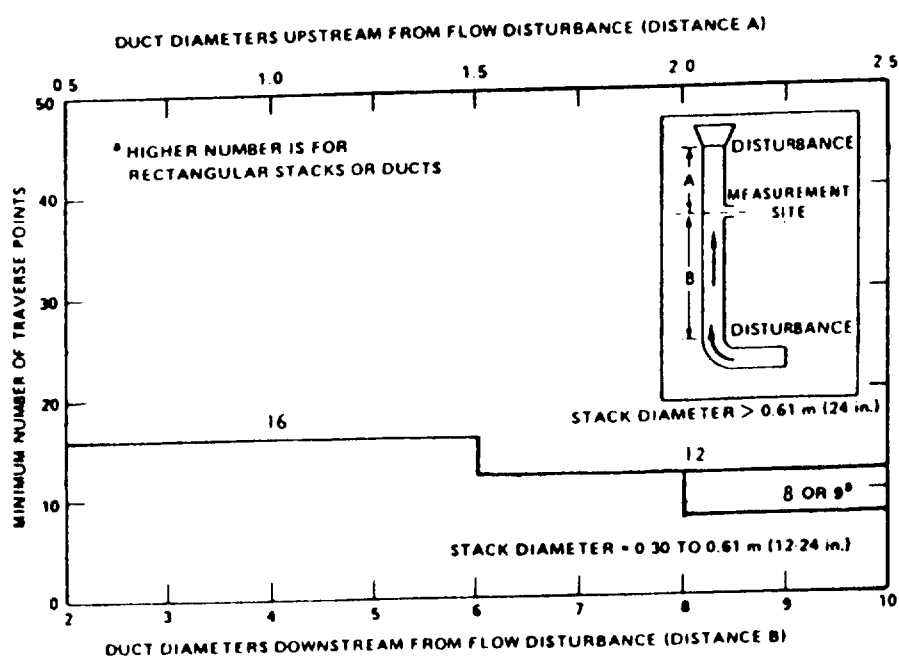
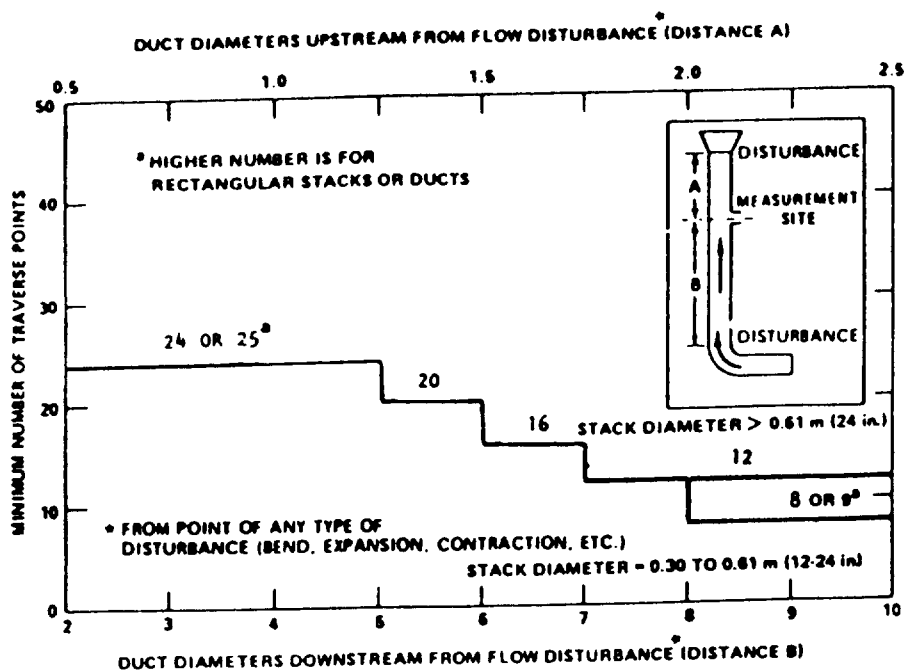


Figure 1.4. Example showing rectangular stack cross section divided into 12 equal areas, with a traverse point at centroid of each area.

METHOD 1 - MINIMUM NUMBER OF TRAVERSE POINTS



METHOD 2 - STACK GAS VELOCITY AND VOLUMETRIC FLOW CALCULATIONS

5.1 Nomenclature.

A = Cross-sectional area of stack, m^2 (ft²).
 B_w = Water vapor in the gas stream (from Method 5 or Reference Method 4), proportion by volume.
 C_p = Pitot tube coefficient, dimensionless.
 K_p = Pitot tube constant.

$$34.97 \frac{m}{sec} \left[\frac{(g/g\text{-mole})(mm\ Hg)}{(^{\circ}K)(mm\ H_2O)} \right]^{1/2}$$

for the metric system and

$$85.49 \frac{ft}{sec} \left[\frac{(lb/lb\text{-mole})(in. Hg)}{(^{\circ}R)(in. H_2O)} \right]^{1/2}$$

for the English system.

M_d = Molecular weight of stack gas, dry basis (see Section 3.6) g/g-mole (lb/lb-mole).
 M_w = Molecular weight of stack gas, wet basis, g/g-mole (lb/lb-mole).
 $= M_d(1 - B_w) + 18.0 B_w$

Eq. 2-5

P_{bar} = Barometric pressure at measurement site, mm Hg (in. Hg).

P_s = Stack static pressure, mm Hg (in. Hg).

P_t = Absolute stack gas pressure, mm Hg (in. Hg).

$= P_{bar} + P_s$

Eq. 2-6

Eq. 2-6

P_{std} = Standard absolute pressure, 760 mm Hg (29.92 in. Hg).

Q_{std} = Dry volumetric stack gas flow rate corrected to standard conditions, dscm/hr (dscf/hr).

L = Stack temperature, $^{\circ}C$ ($^{\circ}F$).

T_s = Absolute stack temperature, $^{\circ}K$, ($^{\circ}R$).
 $= 273 + L$ for metric.

Eq. 2-7

$= 460 + L$ for English.

Eq. 2-8

T_{std} = Standard absolute temperature, 293 $^{\circ}K$ (528 $^{\circ}R$).

v_s = Average stack gas velocity, m/sec (ft/sec).

Δp = Velocity head of stack gas, mm H₂O (in. H₂O).

3,600 = Conversion factor, sec/hr.

18.0 = Molecular weight of water, g/g-mole (lb/lb-mole).

5.2 Average Stack Gas Velocity.

$$v_s = K_p C_p (\sqrt{\Delta p})_{avg} \sqrt{\frac{T_{std}}{P_s M_s}}$$

Equation 2-9

5.3 Average Stack Gas Dry Volumetric Flow Rate.

$$Q_{std} = 3,600(1 - B_w) v_s A \left(\frac{T_{std}}{T_s} \right) \left(\frac{P_s}{P_{std}} \right)$$

Eq. 2-10

METHOD 3 - MOLECULAR WEIGHT AND EXCESS AIR CALCULATIONS

6.1 Nomenclature.

M_d = Dry molecular weight, g/g-mole (lb/lb-mole).

%EA = Percent excess air.

%CO₂ = Percent CO₂ by volume (dry basis).

%O₂ = Percent O₂ by volume (dry basis).

%CO = Percent CO by volume (dry basis).

%N₂ = Percent N₂ by volume (dry basis).

0.264 = Ratio of O₂ to N₂ in air, v/v.

0.280 = Molecular weight of N₂ or CO, divided by 100.

0.320 = Molecular weight of O₂, divided by 100.

0.440 = Molecular weight of CO, divided by 100.

6.2 Percent Excess Air. Calculate the percent excess air (if applicable), by substituting the appropriate values of percent O₂, CO, and N₂ (obtained from Section 4.1.3 or 4.2.4) into Equation 3-1.

% EA =

$$\frac{\%O_2 - 0.5\% CO}{0.264\% N_2 (\%O_2 - 0.5\% CO)} \times 100$$

Eq. 3-1

NOTE: The equation above assumes that ambient air is used as the source of O₂, and that the fuel does not contain appreciable amounts of N₂ (as do coke oven or blast furnace gases). For those cases when appreciable amounts of N₂ are present (coal, oil, and natural gas do not contain appreciable amounts of N₂) or when oxygen enrichment is used, alternate methods, subject to approval of the Administrator, are required.

6.3 Dry Molecular Weight. Use Equation 3-2 to calculate the dry molecular weight of the stack gas

$$M_d = 0.440(\%CO_2) + 0.320(\%O_2) + 0.280(\%N_2 + \%CO)$$

Eq. 3-2

METHOD 4 - STACK GAS MOISTURE CALCULATIONS

2.3.1 Nomenclature.

- B_w = Proportion of water vapor, by volume, in the gas stream.
- M_w = Molecular weight of water, 18.0 g/g-mole (18.0 lb/lb-mole).
- P_m = Absolute pressure (for this method, same as barometric pressure) at the dry gas meter, mm Hg (in. Hg).
- P_{std} = Standard absolute pressure, 760 mm Hg (29.92 in. Hg).
- R = Ideal gas constant, 0.06236 (mm Hg) (m³)/(g-mole) (°K) for metric units and 21.85 (in. Hg) (ft³)/(lb-mole) (°R) for English units.
- T_m = Absolute temperature at meter, °K (°R).
- T_{std} = Standard absolute temperature, 293° K (528°R).
- V_m = Dry gas volume measured by dry gas meter, dcm (dcf).
- ΔV_m = Incremental dry gas volume measured by dry gas meter at each traverse point, dcm (dcf).
- $V_{m(wid)}$ = Dry gas volume measured by the dry gas meter, corrected to standard conditions, dscm (dscf).
- $V_{w(wid)}$ = Volume of water vapor condensed corrected to standard conditions, scm (scf).
- $V_{w(wid)}$ = Volume of water vapor collected in silica gel corrected to standard conditions, scm (scf).
- V_f = Final volume of condenser water, ml.
- V_i = Initial volume, if any, of condenser water, ml.
- W_f = Final weight of silica gel or silica gel plus impinger, g.
- W_i = Initial weight of silica gel or silica gel plus impinger, g.
- Y = Dry gas meter calibration factor.
- ρ_w = Density of water, 0.9982 g/ml (0.002201 lb/ml).

2.3.2 Volume of Water Vapor Condensed.

$$V_{w(wid)} = \frac{(V_f - V_i) \rho_w R T_{std}}{P_{std} M_w}$$

$$= K_1 (V_f - V_i)$$

Eq. 4-1

$$K_1 = 0.001333 \text{ m}^3/\text{ml} \text{ for metric units}$$

$$= 0.04707 \text{ ft}^3/\text{ml} \text{ for English units}$$

2.3.3 Volume of Water Vapor Collected in Silica Gel

$$V_{w(wid)} = \frac{(W_f - W_i) R T_{std}}{P_{std} M_w}$$

$$= K_2 (W_f - W_i)$$

Eq. 4-2

Where:

$$K_2 = 0.001335 \text{ m}^3/\text{g} \text{ for metric units}$$

$$= 0.04715 \text{ ft}^3/\text{g} \text{ for English units}$$

2.3.4 Sample Gas Volume.

$$V_{m(wid)} = V_m Y \frac{(P_m)(T_{std})}{(P_{std})(T_m)}$$

$$= K_3 Y \frac{V_m P_m}{T_m}$$

Eq. 4-3

Where:

$$K_3 = 0.3858 \text{ °K/mm Hg for metric units}$$

$$= 17.64 \text{ °R/in. Hg for English units}$$

NOTE: If the post-test leak rate (Section 2.2.6) exceeds the allowable rate, correct the value of V_m in Equation 4-3, as described in Section 6.3 of Method 5.

2.3.5 Moisture Content.

$$B_w = \frac{V_{w(wid)} + V_{w(wid)}}{V_{w(wid)} + V_{w(wid)} + V_{m(wid)}}$$

Eq. 4-4

NOTE: In saturated or moisture droplet-laden gas streams, two calculations of the moisture content of the stack gas shall be made, one using a value based upon the saturated conditions (see Section 1.2), and another based upon the results of the impinger analysis. The lower of these two values of B_w shall be considered correct.

METHOD 5 - PARTICULATE EMISSION CALCULATIONS - (1)

6.1 Nomenclature.

A_n = Cross-sectional area of nozzle, m^2 (ft^2).
 B_w = Water vapor in the gas stream, proportion by volume.
 C_a = Acetone blank residue concentration, mg/g .
 C_p = Concentration of particulate matter in stack gas, dry basis, corrected to standard conditions, $g/dscm$ ($g/dscf$).
 I = Percent of isokinetic sampling.
 L_m = Maximum acceptable leakage rate for either a pretest leak check or for a leak check following a component change; equal to $0.0057 m^3/min$ ($0.02 cfm$) or 4 percent of the average sampling rate, whichever is less.
 L_n = Individual leakage rate observed during the leak check conducted prior to the " n^{th} " component change ($n=1, 2, 3, \dots, n$), m^3/min (cfm).
 L_p = Leakage rate observed during the post-test leak check, m^3/min (cfm).
 m_a = Mass of residue of acetone after evaporation, mg .
 m_p = Total amount of particulate matter collected, mg .
 M_w = Molecular weight of water, $18.0 g/g\text{-mole}$ ($18.0 lb/lb\text{-mole}$).
 P_{bar} = Barometric pressure at the sampling site, $mm\ Hg$ ($in.\ Hg$).
 P_s = Absolute stack gas pressure, $mm\ Hg$ ($in.\ Hg$).
 P_{std} = Standard absolute pressure, $760\ mm\ Hg$ ($29.92\ in.\ Hg$).
 R = Ideal gas constant, $0.06236\ mm\ Hg\cdot m^3/K\cdot g\text{-mole}$ ($21.85\ in.\ Hg\cdot ft^3/R\cdot lb\text{-mole}$).
 T_m = Absolute average dry gas meter temperature (see Figure 5-2), $^{\circ}K$ ($^{\circ}R$).
 T_s = Absolute average stack gas temperature (see Figure 5-2), $^{\circ}K$ ($^{\circ}R$).
 T_{std} = Standard absolute temperature, $293^{\circ}\ K$ ($528^{\circ}\ R$).
 V_a = Volume of acetone blank, ml .
 V_{aw} = Volume of acetone used in wash, ml .
 V_l = Total volume of liquid collected in impingers and silica gel (see Figure 5-3), ml .
 V_m = Volume of gas sample as measured by dry gas meter, dcm ($dscf$).
 V_{mstd} = Volume of gas sample measured by the dry gas meter, corrected to standard conditions, $dscm$ ($dscf$).
 V_{wstd} = Volume of water vapor in the gas sample, corrected to standard conditions, scm (scf).
 v_s = Stack gas velocity, calculated by Method 2, Equation 2-9, using data obtained from Method 5, m/sec (ft/sec).
 W_a = Weight of residue in acetone wash, mg .
 Y = Dry gas meter calibration factor.
 ΔH = Average pressure differential across the orifice meter (see Figure 5-2), $mm\ H_2O$ ($in.\ H_2O$).
 ρ_a = Density of acetone, mg/ml (see label on bottle).

ρ_w = Density of water, $0.9982\ g/ml$ ($0.002201\ lb/ml$).

θ = Total sampling time, min .

θ_1 = Sampling time interval, from the beginning of a run until the first component change, min .

θ_2 = Sampling time interval, between two successive component changes, beginning with the interval between the first and second changes, min .

θ_n = Sampling time interval, from the final (n^{th}) component change until the end of the sampling run, min .

13.6 = Specific gravity of mercury.

60 = Sec/min .

100 = Conversion to percent.

6.2 Average Dry Gas Meter Temperature and Average Orifice Pressure Drop. See data sheet (Figure 5-2).

6.3 Dry Gas Volume. Correct the sample volume measured by the dry gas meter to standard conditions ($20^{\circ}\ C$, $760\ mm\ Hg$ or $68^{\circ}\ F$, $29.92\ in.\ Hg$) by using Equation 5-1.

$$V_{mstd} = V_m Y \left(\frac{T_{std}}{T_m} \right) \left[\frac{P_{bar} + \frac{\Delta H}{13.6}}{P_{std}} \right]$$

$$= K_1 V_m Y \frac{P_{bar} + (\Delta H/13.6)}{T_m}$$

Equation 5-1

Where:

$K_1 = 0.3858\ ^{\circ}K/mm\ Hg$ for metric units

$= 17.64\ ^{\circ}R/in.\ Hg$ for English units

NOTE: Equation 5-1 can be used as written unless the leakage rate observed during any of the mandatory leak checks (i.e., the post-test leak check or leak checks conducted prior to component changes) exceeds L_m . If L_p or L_n exceeds L_m , Equation 5-1 must be modified as follows:

(a) Case I. No component changes made during sampling run. In this case, replace V_m in Equation 5-1 with the expression:

$$[V_m - (L_p - L_m)\theta]$$

(b) Case II. One or more component changes made during the sampling run. In this case, replace V_m in Equation 5-1 by the expression:

$$\left[V_m - (L_1 - L_m)\theta_1 - \sum_{i=2}^n (L_i - L_m)\theta_i - (L_n - L_m)\theta_n \right]$$

and substitute only for those leakage rates (L_i or L_n) which exceed L_m .

6.4 Volume of Water Vapor.

METHOD 5 - PARTICULATE EMISSION CALCULATIONS - (2)

$$V_{m(s,d)} = V_{1r} \left(\frac{P_{1r}}{P_{s,d}} \right) \left(\frac{RT_{s,d}}{P_{s,d}} \right) = K_1 V_{1r} \quad \text{Equation 5-2}$$

Where:

$K_1 = 0.001333 \text{ m}^3/\text{ml}$ for metric units
 $= 0.04707 \text{ ft}^3/\text{ml}$ for English units.

6.5 Moisture Content.

$$B_{w1} = \frac{V_{w(s,d)}}{V_{m(s,d)} + V_{w(s,d)}}$$

Eq. 5-3

NOTE: In saturated or water droplet-laden gas streams, two calculations of the moisture content of the stack gas shall be made, one from the impinger analysis (Equation 5-3), and a second from the assumption of saturated conditions. The lower of the two values of B_w shall be considered correct. The procedure for determining the moisture content based upon assumption of saturated conditions is given in the Note of Section 1.2 of Method 4. For the purposes of this method, the average stack gas temperature from Figure 5-2 may be used to make this determination, provided that the accuracy of the in-stack temperature sensor is $\pm 1^\circ \text{C}$ (2°F).

6.6 Acetone Blank Concentration.

$$C_a = \frac{m_a}{V_a P_a} \quad \text{Eq. 5-4}$$

6.7 Acetone Wash Blank.

$$W_a = C_a V_{aw} P_a \quad \text{Eq. 5-5}$$

6.8 Total Particulate Weight. Determine the total particulate catch from the sum of the weights obtained from Containers 1 and 2 less the acetone blank (see Figure 5-3).

NOTE: Refer to Section 4.1.5 to assist in calculation of results involving two or more filter assemblies or two or more sampling trains.

6.9 Particulate Concentration.

$$C_p = (0.001 \text{ g/mg}) (m_p / V_{m(s,d)})$$

Eq. 5-6

6.10 Conversion Factors:

From	To	Multiply by
acv	m ³	0.02832
g/h ¹	g/h ¹	15.43
g/h ¹	lb/h ¹	2.205 × 10 ⁻³
g/h ¹	g/m ³	35.31

6.11 Isokinetic Variation.

6.11.1 Calculation From Raw Data

I =

$$100 T_s (K_1 V_{1r} + (P_{1r}/T_{1r})(P_{w,s} + \Delta H/13.6)) / 60 \theta v_s P_s A_s$$

Eq. 5-7

Where:

$K_1 = 0.003454 \text{ mm Hg} \cdot \text{m}^3/\text{ml} \cdot ^\circ \text{K}$ for metric units.
 $= 0.002669 \text{ in. Hg} \cdot \text{ft}^3/\text{ml} \cdot ^\circ \text{R}$ for English units.

6.11.2 Calculation From Intermediate Values.

$$I = \frac{T_s V_{m(s,d)} P_{s,d} 100}{T_{s,d} v_s \theta A_s P_s 60 (1 - B_{w,s})}$$

$$= K_1 \frac{T_s V_{m(s,d)}}{P_s V_s A_s \theta (1 - B_{w,s})}$$

Equation 5-8

where:

$K_1 = 4.320$ for metric units
 $= 0.09450$ for English units.

6.12 Acceptable Results. If 90 percent $< I < 110$ percent, the results are acceptable. If the particulate results are low in comparison to the standard, and I is over 110 percent or less than 90 percent, the Administrator may accept the results.

NOMENCLATURE METHOD 5 CALCULATIONS

- $V_{m_{std}}$ = Volume of gas sample measured by the dry gas meter, corrected to standard conditions, dscm (dscf).
- Y = Dry gas meter calibration factor
- P_b = Barometric pressure at the sampling site, mm Hg (in. Hg)
- H = Average pressure differential across the orifice meter, mm H_2O (in. H_2O)
- T_m = Absolute average dry gas meter temperature, ° K (° R)
- dscm = Dry standard cubic meters
- dscf = Dry standard cubic feet
- W_a = Weight of residue in acetone wash
- M_a = Mass of residue of acetone after evaporation, mg
- C_a = Acetone blank residue concentration, mg/g
- V_a = Volume of acetone blank
- V_{aw} = Volume of acetone used in wash, ml
- M_n = Total amount of particulate matter collected, mg
- C_s = Concentration of particulate matter in stack gas, dry basis, corrected to standard conditions, mg/dscm (gr/dscf)
- gr/dscf = grains per dry standard cubic foot
- $V_{w_{std}}$ = Volume of water vapor in the gas sample, corrected to standard conditions, scm (scf)
- B_{ws} = Water vapor in the gas stream, proportion by volume
- M_d = Molecular weight of stack gas, g/g-mole on dry basis
- M_w = Molecular weight of stack gas, g/g-mole on wet basis
- V_s = Stack gas velocity, calculated by Method 2, Equation 2-9, using data obtained from Method 5, m/sec (ft/sec)
- C_p = Pitot tube coefficient, dimensionless
- Δ_p = Velocity head of stack gas, mm H_2O (in. H_2O)
- P_s = Absolute stack gas pressure, mm Hg (in. Hg)

NOMENCLATURE (continued)
METHOD 5 CALCULATIONS

- Q_{std} = Dry volumetric stack gas flow rate corrected to standard conditions, dscm/hr (dscf/hr)
- dscf/min = dry standard cubic feet per minute (also identified as dcfm or scfm)
- acfm = actual cubic feet per minute
- I = Percent of isokinetic sampling
- A_n = Cross-sectional area of nozzle, m^2 (ft^2)



am test inc.

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SOURCE

EMISSION

EVALUATION

NOVEMBER 23, 1988

Prepared For:

BOEING COMPANY
#5 CHROMIC ACID ANODIZING TANK VENT
SEATTLE, WASHINGTON
NOVEMBER 1, 1988

Submitted by:

KRIS A. HANSEN
DIRECTOR, AIR QUALITY DIVISION

JAMES A. GUENTHOER
PROJECT ENGINEER

AM TEST, INC.
REDMOND, WASHINGTON

We certify that the information contained herein is accurate and complete to the best of our knowledge.

METHOD 1-5 - PARTICULATE EMISSION CONCENTRATION RESULTS
AM TEST, INC. - AIR QUALITY DIVISION

FILE NAME: BOECR683
CLIENT: BOEING PLANT #2
LOCATION: SEATTLE, WASH
SAMPLE SITE: CHRONIC ACID BATH #5
SAMPLE DATE: NOVEMBER 1, 1988
RUN #: 3-CR-6
OPERATORS: GUENTHER/WIDMEYER
CONTACT: TERRY LORDS

LAB #: 822263
START TIME: 14:00 O'CLOCK
STOP TIME: 15:01 O'CLOCK
SAMPLE TIME: 60.0 MINUTES
CONDITION: BATH ON

HEXAVALENT CHROMIUM
MILLILITERS OF SOLUTION: 452
HEXAVALENT CHROMIUM CONCENTRATION (UG/ML): 4.8
HEXAVALENT CHROMIUM CONCENTRATION (MG/DSCF): 1.44
TOTAL HEXAVALENT CHROMIUM IN SAMPLE (PPM): 0.67
HEXAVALENT CHROMIUM EMISSION RATE (LBS/HR): 0.117

PITOT Cp: 0.85
NOZZLE DIA INCHES: 0.313
NOZZLE AREA FT^2: 0.0005
STACK DIA. INCHES: 48.00
STACK AREA FT^2: 12.566
METER TEMP. DEG F: 71.5
BAROM. PRES. "HG: 29.84
STATIC PRES. "H2O: -0.09
STACK PRES. "HG: 29.83
ORIFICE PRES "H2O: 1.435
METER PRES. "HG: 29.95

FINAL WT. INIT. WT. NET WT.
OF H2O G. OF H2O G. OF H2O G.
626.5 615.7 10.8
601.6 600.5 1.1
488.4 487.8 0.6
797.2 785.9 11.3
TOTAL H2O GAIN: 23.8
TOTAL VOLUME (SCF) 1.12
PERCENT MOISTURE: 2.07
BWS: 0.0207

INIT. METER VOL.: 101.307
FINAL METER VOL.: 155.848
VOLUME SAMPLED: 54.541
STD VOLUME (DSCF): 53.143
STD VOLUME (DSCM): 1.505
Y FACTOR: 0.98
AVERAGE % CO2: 0.0
AVERAGE % O2: 20.9
AVERAGE DPM CO: 0
STACK GAS MW. DRY: 28.84
STACK GAS MW. WET: 28.61

SAMPLE POINT	VELOCITY " OF H2O	TEMPERATURE DEGREES F.	SAMPLE POINT	VELOCITY " OF H2O	TEMPERATURE DEGREES F.
NW 1	0.22	79	NE 1	0.28	78
2	0.27	79	2	0.31	78
3	0.30	79	3	0.32	78
4	0.30	78	4	0.29	79
5	0.28	79	5	0.25	79
6	0.22	79	6	0.22	78

PERCENT ISOXINETICS: 96 %
STACK TEMPERATURE: 78.6 DEG. F. 538.6 DEG. R.
AVERAGE VELOCITY HEAD: 0.271 " OF H2O 30.02 FT/SEC.
STACK GAS VELOCITY: 22636.1 ACF/MIN. 21669.8 DSCF/MIN.
STACK GAS AIR FLOW:

METHOD 1-5 - PARTICULATE EMISSION CONCENTRATION RESULTS AM TEST, INC. - AIR QUALITY DIVISION

HEXAVALENT CHROMIUM

MILLILITERS OF SOLUTION: 450
HEXAVALENT CHROMIUM CONCENTRATION (UG/ML): 0.15
HEXAVALENT CHROMIUM CONCENTRATION (MG/DSCF): 0.022
TOTAL HEXAVALENT CHROMIUM IN SAMPLE (PPM): 0.010
HEXAVALENT CHROMIUM EMISSION RATE (LBS/HR): 0.002

LAB #: 822262
START TIME: 11:08 O'CLOCK
STOP TIME: 13:09 O'CLOCK
SAMPLE TIME: 120.0 MINUTES
CONDITION: BATH OFF

FILE NAME: BOEING PLANT #2
CLIENT: BOEING PLANT #2
LOCATION: SEATTLE, WASH
SAMPLE SITE: CHROMIC ACID BATH #5
SAMPLE DATE: NOVEMBER 1, 1968
RUN #: 2-CR+6
OPERATORS: GUENTHER/VIDMEYER
CONTACT: TERRY LORDS

FINAL WT. INIT. WT. MET WT.
OF H2O G. OF H2O G. OF H2O G.
609.7 590.9 18.8
592.1 588.0 4.1
471.1 469.6 1.5
834.8 816.0 18.8
TOTAL H2O GAIN: 43.2
TOTAL VOLUME (SCF) 2.03
PERCENT MOISTURE: 1.88
BWS: 0.0188

INIT. METER VOL.: 990.700
FINAL METER VOL.: 1099.623
VOLUME SAMPLED: 108.923
STD VOLUME (DSCF): 106.268
STD VOLUME (USCF): 3.010
Y FACTOR: 0.98

SAMPLE POINT	VELOCITY " OF H2O	TEMPERATURE DEGREES F.	SAMPLE POINT	VELOCITY " OF H2O	TEMPERATURE DEGREES F.
NE 1	0.28	75	NW 1	0.22	76
2	0.31	76	2	0.27	76
3	0.32	75	3	0.30	76
4	0.29	75	4	0.30	76
5	0.25	76	5	0.28	77
6	0.22	76	6	0.22	76

PERCENT ISOKINETICS: 96 %
STACK TEMPERATURE: 75.8 DEG. F. 535.8 DEG. R.
AVERAGE VELOCITY HEAD: 0.271 " OF H2O 29.95 FT/SEC.
STACK GAS VELOCITY: 22585.3 ACF/MIN. 21744.5 DSCF/MIN.
STACK GAS AIR FLOW:

METHOD 1-5 - PARTICULATE EMISSION CONCENTRATION RESULTS
AM TEST, INC. - AIR QUALITY DIVISION

FILE NAME: BOECR6R1
CLIENT: BOEING PLANT #2
LOCATION: SEATTLE, WASH
SAMPLE SITE: CHROMIC ACID BATH #5
SAMPLE DATE: NOVEMBER 1, 1968
RUN #: 1-CR-6
OPERATORS: GUENTHER/MIDMEYER
CONTACT: TERRY LORDS

LAB #: 822261
START TIME: 09:42 O'CLOCK
STOP TIME: 10:43 O'CLOCK
SAMPLE TIME: 60.0 MINUTES
CONDITION: BATH ON

HEXAVALENT CHROMIUM
MILLILITERS OF SOLUTION: 452
HEXAVALENT CHROMIUM CONCENTRATION (UG/ML): 5.4
HEXAVALENT CHROMIUM CONCENTRATION (MG/DSCM): 1.64
TOTAL HEXAVALENT CHROMIUM IN SAMPLE (PPM): 0.76
HEXAVALENT CHROMIUM EMISSION RATE (LBS/HR): 0.134

FINAL WT. INIT. WT. NET WT.
OF H2O G. OF H2O G. OF H2O G.

589.4 581.4 8.0
594.4 591.9 2.5
485.5 484.7 0.8
771.8 762.7 9.1

TOTAL H2O GAIN: 20.4
TOTAL VOLUME (SCF) 0.96
PERCENT MOISTURE: 1.79
BWS: 0.0179

PITOT Cp: 0.85
NOZZLE DIA INCHES: 0.313
NOZZLE AREA FT^2: 0.0005
STACK DIA. INCHES: 48.00
STACK AREA FT^2: 12.566
METER TEMP. DEG F: 65.4
BAROM. PRES. "HG: 29.80
STATIC PRES. "H2O: -0.09
STACK PRES. "HG: 29.79
ORIFICE PRES "H2O: 1.399
METER PRES. "HG: 29.90

INIT. METER VOL.: 937.063
FINAL METER VOL.: 990.517
VOLUME SAMPLED: 53.454
STD VOLUME (DSCF): 52.614
STD VOLUME (DSCM): 1.490
Y FACTOR: 0.98

AVERAGE % CO2: 0.0
AVERAGE % O2: 20.9
AVERAGE PPM CO: 0
STACK GAS MW. DRY: 28.84
STACK GAS MW. WET: 28.64

SAMPLE POINT	VELOCITY " OF H2O	TEMPERATURE DEGREES F.	SAMPLE POINT	VELOCITY " OF H2O	TEMPERATURE DEGREES F.
NV 1	0.22	76	NE 1	0.28	74
2	0.27	75	2	0.31	75
3	0.30	75	3	0.32	75
4	0.30	74	4	0.29	76
5	0.28	74	5	0.25	75
6	0.22	74	6	0.22	75

PERCENT ISOINETICS: 95 %
STACK TEMPERATURE: 74.8 DEG. F.
AVERAGE VELOCITY HEAD: 0.271 " OF H2O
STACK GAS VELOCITY: 29.92 FT/SEC.
STACK GAS AIR FLOW: 22560.6 ACF/MIN. 21780.2 DSCF/MIN.

SUMMARY OF RESULTS

The results of the three (3) tests for determining hexavalent chromium (Cr^{+6}) emissions, collected at the #5 chromic acid bath exhaust on November 1, 1988 are summarized in Table 1 below:

Table 1. Summary of Cr^{+6} emissions tests performed November 1, 1988 at Boeing's Plant No. 2.

SAMPLE RUN #	AM TEST LAB #	Cr^{+6} EMISSION CONC. mg/dscm	Cr^{+6} EMISSION CONC. ppm	Cr^{+6} EMISSION RATE lb/hr	AIR FLOW dscf/min
1	822261	1.64	0.76	0.134	21780
*2	822262	0.22	0.01	0.002	21745
3	822263	1.44	0.67	0.117	21670

* Run 2 occurred over a 2-hr period while no parts were in the bath.

The hexavalent chromium emission concentration is presented in units of milligrams per dry standard cubic meter (mg/dscm) and in parts per million (ppm). The Cr^{+6} emission rate is presented in units of pounds per hour (lb/hr). Airflow is also presented in units of dry standard cubic feet per minute (dscf/min). An acceptable leak check of less than 0.02 cfm at the highest vacuum rate (or greater) used during the test preceded and followed each run. The average percentage isokinetics for each run were within the acceptable limits of $100 \pm 10\%$. Computer printouts which detail the complete results may be found on the following pages.

analysis, data reduction, and final report preparation was performed by Mr. Kris A. Hansen, Ms. Angela F. Blaisdell, and Ms. Jan M. Widmeyer of Am Test. Am Test, Inc.'s Trace Metals Division performed the hexavalent chromium analysis using a diphenylcarbazide colorimetric method. Ms. Terry Lords and Mr. Chuck Strand represented the Boeing Company.

INTRODUCTION

The purpose of this testing program performed at the Boeing Company's Plant No. 2 in Seattle, Washington was to quantify the hexavalent chromium (Cr^{+6}) emissions exhausted from the #5 chromic acid anodizing tank which is one of the tanks in the 80 anodic tank line located in the 210 Building. The fumes which result from the plating process are controlled by blowing air horizontally across the top of the tank and sucking the fumes through ductwork with an axial fan to the exhaust stack. The plating cycle takes 55 minutes during which the vat is heated to a temperature of 95° C. Three (3) samples for determining hexavalent chromium were collected at this source on November 1, 1988. Two (2) of the samples were collected over one-hour periods during 2 anodizing cycles (run 1 and 3). One (1) sample was collected over a two-hour period while no parts were in the bath (run 2).

The sample method used is similar to EPA Method 5, which is detailed in the Title 40 Code of Federal Regulations, Part 60 (40 CFR 60), Appendix A. The sample train was modified to exclude the front-half filter and utilized 0.1 N sodium hydroxide (NaOH) solution in the impingers. A final back-half Teflon^R filter was connected in series to collect any Cr^{+6} which might break through the absorbing liquid. EPA Methods 1-4 were also performed during this testing project. Methods 1 and 2 were performed to determine the stack gas velocity and volumetric flow rate, Method 3 was performed to determine the molecular weight of the stack gas, and Method 4 was performed to determine the moisture content of the stack gas.

Mr. James A. Guenthoer, and Ms. Jan M. Widmeyer of Am Test, Inc.'s Air Quality Division based in Redmond, Washington performed the field sampling. Laboratory