

**BAYOU STEEL CORPORATION**  
**P.O. BOX 5000**  
**LA PLACE, LOUISIANA 70069-1156**

**EMISSION COMPLIANCE TESTS**

**BAGHOUSE STACK** (source ID 1-77)

**JULY 23, 2004**

**PERMIT NUMBER : 885 (M-2)**

Testing conducted by :

**E T S**

**EMISSION TESTING SERVICES, INC.**

**P.O. BOX 15075**

**BATON ROUGE, LOUISIANA 70895**

**(225) 925-8405**

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# EMISSION TEST REPORT CERTIFICATION

for

BAYOU STEEL CORPORATION

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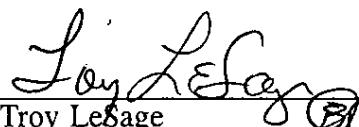
Emission Testing Services, Inc. is certified by the Louisiana Department of Environmental Quality (LDEQ) as a qualified environmental testing laboratory under the Louisiana Environmental Laboratory Accreditation Program (LELAP).

I certify that I have personally examined and am familiar with the information submitted herein, and based on my inquiries of those individuals immediately responsible for obtaining the information, I believe the submitted information is true, accurate, and complete.

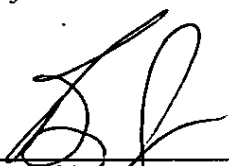
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Wendy Stehling  
Bayou Steel Corporation  
Plant Representative

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Troy LeSage  
Emission Testing Services, Inc.  
Project Leader

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Emission Testing Services, Inc.  
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# TABLE of CONTENTS

|      |                                                                       |        |
|------|-----------------------------------------------------------------------|--------|
| I.   | Introduction .....                                                    | 1.1    |
| II.  | Summary                                                               |        |
|      | Test Results Summary .....                                            | 2.1    |
|      | Test Method Modifications, Deviations, and Unusual Conditions .....   | 2.1    |
|      | Test Conclusions .....                                                | 2.1    |
|      | Process Description .....                                             | 2.3    |
| III. | Procedure .....                                                       | 3.1    |
| IV.  | Analytical Technique .....                                            | 4.1    |
| V.   | Quality Assurance/Quality Control .....                               | 5.1    |
|      | Chain of Custody .....                                                | 5.2    |
| VI.  | Test Data and Calculations .....                                      | 6.0.1  |
|      | <u>Baghouse Stack</u> .....                                           | 6.1.1  |
|      | Sample Point Location                                                 |        |
|      | EPA Methods 2, 4, and 29 .....                                        | 6.1.2  |
|      | EPA Method 3 .....                                                    | 6.1.3  |
|      | EPA Method 1, Verification of Absence of Cyclonic Flow .....          | 6.1.4  |
|      | EPA Methods 2, 3, and 4 (stack gas flow rate, mole wt., and moisture) |        |
|      | Test Data & Calculations, Runs 1-3 .....                              | 6.1.5  |
|      | EPA Method 29 (lead and mercury)                                      |        |
|      | Data Summary & Calculations, Runs 1-3 .....                           | 6.1.11 |
|      | Analyses of Samples .....                                             | 6.1.15 |
|      | Unit Operating Data .....                                             | 6.1.26 |
| VII. | Appendix .....                                                        | 7.0.1  |
|      | A. Resumes of Test Personnel .....                                    | 7.1.1  |
|      | B. Test Equipment Calibrations .....                                  | 7.2.1  |
|      | C. Correspondence, Bayou Steel and LDEQ .....                         | 7.3.1  |
|      | D. Permit Number 885 (M-2) Excerpts .....                             | 7.4.1  |

## LIST of TABLES

|    |                                                     |     |
|----|-----------------------------------------------------|-----|
| I. | Emission Test Results Summary, Baghouse Stack ..... | 2.2 |
|----|-----------------------------------------------------|-----|

## LIST of FIGURES

|      |                                                       |       |
|------|-------------------------------------------------------|-------|
| I.   | Schematic Drawing of Process .....                    | 2.4   |
| II.  | Sample Point Location, EPA Methods 2, 4, and 29 ..... | 6.1.2 |
| III. | Sample Point Location, EPA Method 3 .....             | 6.1.3 |

## LIST of STANDARD RESULT NOTATIONS

- $\leq$  or  $<$     None detected. Stated result is the minimum detection limit. Actual result may be less including the result 0.
- $\Delta$  or !    Stated result is the sum or average of multiple component results; or a result based on the sum of individual component results from a multi-part sampling train. At least one of the component results has a detectable quantity and at least one of the component results has a none detectable quantity; and the value of the minimum detection limit for the none detectable component(s) is significant in comparison with the value of the detectable component(s). The actual result may be less; however, not less than the result computed with the detectable component(s) only.

## I. INTRODUCTION

Emission Testing Services, Inc. (ETS) was contracted by Bayou Steel Corporation (Bayou Steel) to conduct emission testing at Bayou Steel's plant located near the town of LaPlace, Louisiana in St. James Parish, Louisiana. Emissions from the Baghouse Stack were tested to determine the emission rates of lead and mercury. Tests were conducted in order to demonstrate compliance with emission permit limits. The Baghouse Stack, source ID 1-77, operates under permit number 885 (M-2) issued by the Louisiana Department of Environmental Quality (LDEQ).

All tests were conducted using EPA test methods. The emission rates of lead and mercury were determined using EPA Method 29. EPA Methods 1 - 4 were used to determine the number and location of sample points, and the velocity, moisture, molecular weight, and volumetric flow rate of the stack gas.

The ETS test team consisted of Project Leader Troy LeSage and a test crew consisting of Ronald McCabe and Joel Richard. Wendy Stehling represented Bayou Steel and coordinated testing with plant operations. During the emission tests, the LDEQ was represented onsite by Jim Stone (SERO), Tim Bergeron (ECS-Technology) and Cedric Mellion (EED-TRI).

Emissions from the Baghouse Stack were tested on July 23, 2004. Three, 72-min duration tests were conducted.

## II. SUMMARY

### Test Results Summary

On July 23, 2004 emissions from the Baghouse Stack at Bayou Steel were tested to determine the emission rates of lead and mercury. Results of the tests are presented in Table I.

### Test Method Modifications, Deviations and Unusual Conditions

EPA methods were used to determine all pollutant and stack gas data. All modifications to and deviations from the standard test methods have been documented above. All unusual conditions have been noted above.

### Test Conclusions

Quality assurance procedures meeting EPA and LDEQ requirements were used during the emission tests. All quality indicators, with the exception of those noted above, were within the range of acceptable results. Test data are complete, accurate, and representative of source conditions. Overall, the quality of data gathered are acceptable to meet project objectives.

**TABLE I**  
**EMISSION TEST RESULTS SUMMARY**

BAYOU STEEL CORPORATION

BAGHOUSE STACK (source ID 1-77)

| <u>PARAMETER</u> | <u>Permit Limit<br/>Max./Avg.</u> | <u>RUN 1</u> | <u>RUN 2</u> | <u>RUN 3</u> | <u>AVERAGE</u> |
|------------------|-----------------------------------|--------------|--------------|--------------|----------------|
| DATE             |                                   | 7-23-04      | 7-23-04      | 7-23-04      |                |
| TIME             |                                   | 0934-1047    | 1158-1314    | 1605-1723    |                |
| MERCURY          |                                   |              |              |              |                |
| ug/dscf          |                                   | 0.0670       | 0.0696       | 0.1908       | 0.1091         |
| lb/hr            |                                   | 0.00133      | 0.00140      | 0.00403      | 0.00225        |
| LEAD             |                                   |              |              |              |                |
| ug/dscf          |                                   | 9.735        | 10.66        | 10.53        | 10.31          |
| lb/hr            |                                   | 0.1938       | 0.2151       | 0.2124       | 0.2071         |
| STACK GAS DATA   |                                   |              |              |              |                |
| Temperature, F   |                                   | 241          | 241          | 240          | 241            |
| Moisture, vol %  |                                   | 4.08         | 3.05         | 4.64         | 3.92           |
| Velocity, ft/sec |                                   | 66.33        | 66.43        | 67.52        | 66.76          |
| Flow Rate, acfm  |                                   | 208477       | 208786       | 212216       | 209826         |
| , dscfm          |                                   | 150510       | 152492       | 152533       | 151845         |

## **PROCESS DESCRIPTION**

Bayou Steel operates a steel mill, which includes two separate Electric Arc Furnaces (EAF) and a Ladle Metallurgical Facility (LMF). The EAF steel melting process consists of melting scrap steel, carbon sources, lime, flux, alloys, and other iron bearing material in a refractory lined vessel using three high voltage electrodes to produce a recovered steel product. Liquid steel is transferred either to the LMF for further refining or, to the continuous casting area where it is poured into the billet molds. The continuous strand is cooled and cut into various lengths. Billets are either sold as products or processed in the Rolling Mill by reheating followed by shaping using various rolling operations. Steel sections, angles, channels, and I-beams are cut or sheared to various lengths and transferred to the shipping warehouse for storage and loading.

### **ELECTRIC ARC FURNACE STEEL MILL**

The EAF steel melting process is a batch operation. Each batch is called a heat and requires approximately 60 minutes. A heat consists of the following steps:

**EAF Preparation** – In preparation for charging and melting the scrap steel, the furnace electrodes are aligned and the furnace is coated with a protective layer of gunnite at the slag zone.

**First Charge and Melt** – The furnace is loaded with the initial charge of scrap steel and other materials. The roof is placed on the furnace and electrical current is applied to the electrodes to melt the first charge of scrap material.

**Potential Intermediate Charges and Melts** – The furnace roof is removed and the intermediate charge of scrap material and additives are added to the furnace. The roof is lowered onto the furnace and current is applied to melt the second charge of material.

**Final Charge and Melt** – The furnace roof is removed and the final charge of scrap material and additives are added to the furnace. The roof is lowered onto the furnace and current is applied to melt the final charge of material.

**Oxidizing and Refining** – Oxygen is injected into the molten steel to oxidize impurities and carbon. Electrical current is applied to refine the molten steel to meet product specifications.

**Slagging and Tapping** – The EAF is tilted backward to empty slag into a slag pot. Slag is cooled and transferred to a material stockpile. Following slagging, the EAF is tilted forward to pour the molten steel into a teeming ladle.

Figure -1  
Bayou Steel  
Process Flow Diagram

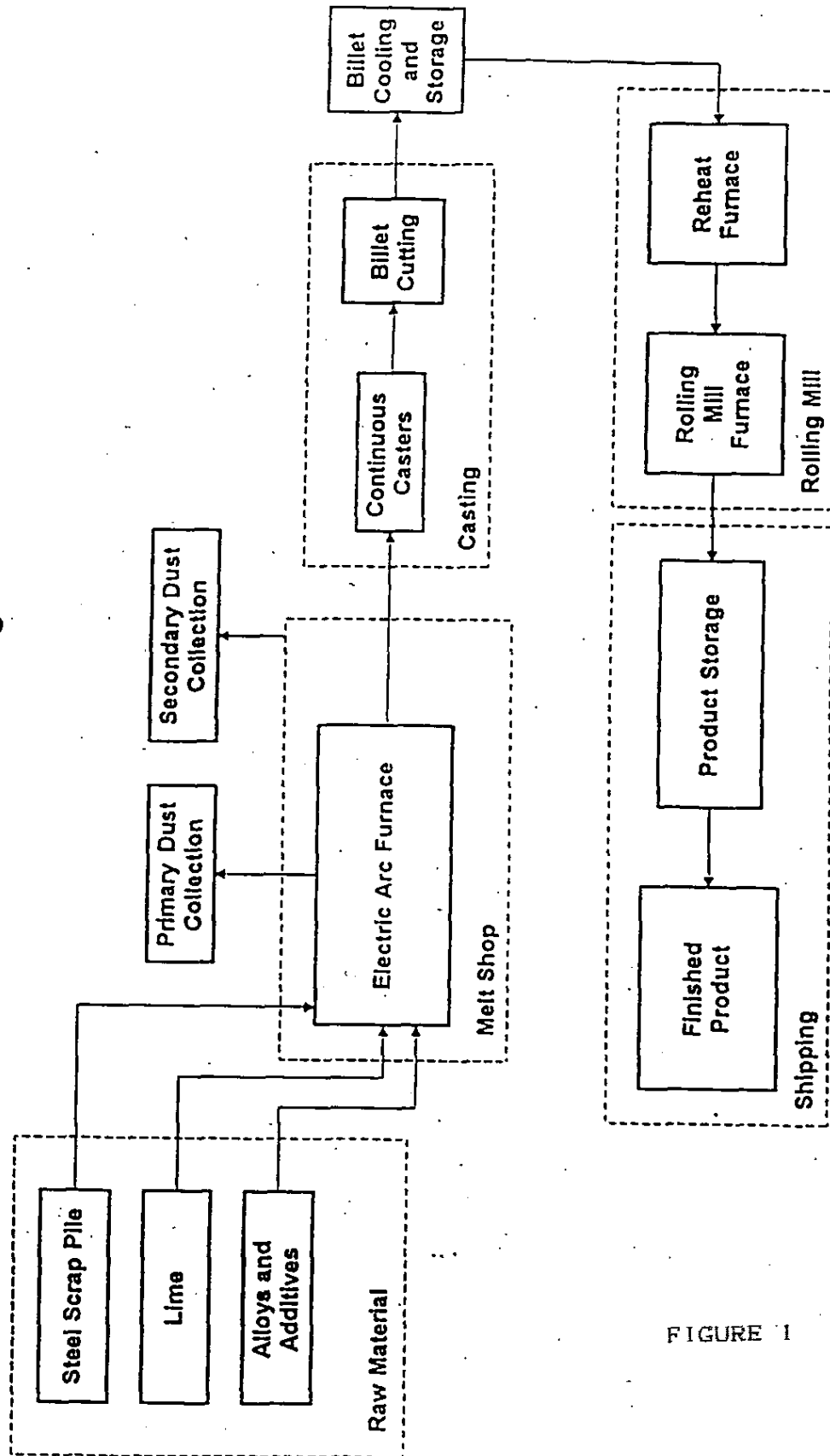


FIGURE 1

Bayou Steel Title V Draft 8/21/98 f:\users\kille5\bayout\5genfig.vsd

### **III. PROCEDURE**

Emissions were determined using EPA methods found in Appendix A, Part 60, Title 40 of the Code of Federal Regulations. A brief description of each method used follows.

#### **LOCATION of SAMPLE POINTS**

Stack gas flow rate, moisture, lead, and mercury determinations were conducted at test points selected per EPA Method 1.

Oxygen and carbon dioxide samples were collected from a point located at the center of the stack. This test point is in conformance with the applicable test methods.

#### **EPA METHOD 1:**

##### **SAMPLE and VELOCITY TRAVERSES for STATIONARY SOURCES**

Method 1 is applicable to stacks having a diameter greater than 12 in. The method recommends that sampling points be located 8 diameters downstream and 2 diameters upstream from the nearest flow disturbances; however, any distances greater than the minimum 2 diameters downstream and 0.5 diameters upstream are acceptable. These distances help insure the collection of a representative sample in the absence of cyclonic flow. Cyclonic flow is detected by measuring the stack gas flow Yaw angle at each test point. The average yaw angle is required to be less than 20 degrees.

The Baghouse Stack has a stack diameter of 98.0 in. The sampling point was located 6.73 stack diameters downstream and 7.96 stack diameters upstream from the nearest flow disturbances. During testing, 16 sample points were used, divided into 8 traverse points located across 2 perpendicular diameters of the stack with access to the points through 2 sampling ports. Cyclonic flow was not detected.

#### **EPA METHOD 2:**

##### **DETERMINATION of STACK GAS VELOCITY and VOLUMETRIC FLOW RATE ( Type S pitot tube )**

The average gas velocity in the stack was determined from the gas molecular weight, moisture content, and the average velocity head measured using a type S pitot tube. Volumetric flow rate was determined from the velocity and stack cross-sectional area.

### **EPA METHOD 3:**

#### **GAS ANALYSIS FOR CARBON DIOXIDE, OXYGEN, EXCESS AIR, and DRY MOLECULAR WEIGHT**

Molecular weight of the stack gas was calculated from the oxygen, carbon dioxide, moisture, and nitrogen concentration data. Oxygen concentration data were obtained using EPA Method 3A and moisture concentration data were obtained using EPA Method 4. Balance of the stack gas composition was assumed to be nitrogen.

#### **GRAB SAMPLE**

Carbon dioxide concentration data were obtained from an analysis of stack gas samples using an Orsat analyzer. A sample of the stack gas was continuously extracted from the stack and was transferred through a heated, Teflon sample line to a sample conditioning unit where particulate and moisture was removed. A portion of the conditioned sample was introduced to the Orsat for analysis.

### **EPA METHOD 4:**

#### **DETERMINATION of MOISTURE CONTENT in STACK GASES**

Moisture of the stack gas was determined by extracting a gas sample from the stack throughout the duration of the test while traversing the stack with the sample probe. Sample gas passed from the heated probe, through a heated sample line to a particulate filter and a series of four impingers immersed in an ice bath. The first two impingers initially contained known weights of water, the third was empty, and the fourth contained a known weight of silica gel. Water vapor in the gas sample was condensed and trapped in the impingers. Sample volume was measured using a dry gas meter located downstream of the impinger train.

### **EPA METHOD 29 :**

#### **DETERMINATION of METALS EMISSIONS from STATIONARY SOURCES**

A gas sample was extracted from the stack isokinetically using a heated glass probe fitted with a particulate filter. Sample gas passed from the probe, through a series of four impingers immersed in an ice bath. The first and second impingers contained a nitric acid solution, the third was empty, and the fourth impinger contained silica gel. Sample flow rate was established using a diaphragm pump and was controlled using a valve. A calibrated dry gas meter was used to determine the total gas sample volume.

After sampling, the filter was recovered from the filter holder. The front half of the filter holder and probe were washed and the washings were collected as the probe wash sample. The contents of the first, second, and third impingers were collected as a single impinger sample. The impingers and connecting glassware were washed with the washings added to the impinger sample. Sample containers were labeled and sealed for shipment to the laboratory for analyses.

## **IV. ANALYTICAL TECHNIQUE**

All sample analyses were conducted following EPA methodology. Presented below are brief descriptions of each method used.

### **EPA METHOD 3:**

#### **GAS ANALYSIS FOR CARBON DIOXIDE, OXYGEN, EXCESS AIR, and DRY MOLECULAR WEIGHT**

The concentration of carbon dioxide in the stack gas was determined using an Orsat analyzer. Analysis was based on the differential sample volume of the gas sample before and after passing the sample through an oxygen absorbing reagent.

Oxygen concentration was determined using EPA Method 3A.

### **EPA METHOD 4:**

#### **DETERMINATION of MOISTURE CONTENT in STACK GASES**

The mass of water vapor condensed from the sample gas was determined gravimetrically.

### **EPA METHOD 29 :**

#### **DETERMINATION of METALS EMISSIONS from STATIONARY SOURCES**

Prior to analysis, the filter was digested in nitric acid. The mass of metals collected in the various samples was analyzed using an atomic adsorption spectrometer (AA).

## **V. QUALITY ASSURANCE/ QUALITY CONTROL**

Test results have been validated by following rigorous quality assurance (QA) and quality control (QC) procedures documented in ETS' Standard Operating Procedures. These procedures meet and/or exceed EPA requirements and have approval by the LDEQ under the Louisiana Environmental Laboratory Accreditation Program (LELAP).

The QA/QC programs ensure that the test data are representative of the source conditions by verifying the completeness, accuracy, and precision of the test data. QA/QC functions cover all aspects of the test including field testing, sampling, and analysis, sample transport and laboratory analysis, and data processing and reporting.

Emission testing at Bayou Steel included a series of QA/QC functions. All QA/QC functions were completed satisfactorily within the required limits.

## CHAIN of CUSTODY

For those samples being transported to the laboratory for analysis, a Chain of Custody form was prepared during the sample recovery process. The sample ID, number of samples, liquid level when applicable, name of the sample recovery supervisor, name of the person responsible for sample recovery and the signature of the sample trustee were recorded on the custody form.

During all subsequent handing, the custody form accompanied the samples. As personnel relinquished responsibility for the samples, the receiving sample trustee verified the number and integrity of the samples and signed the custody form.

Upon receipt at the analytical laboratory, the lab sample trustee verified the number, type, and integrity of the samples. These data were recorded on the custody form along with the date of receipt and lab sample trustees signature.

At the time of analysis, the laboratory analyst recorded the analysis date and the laboratory supervisors name on the custody form. The analyst signed the custody form and attached it to the analytical results.

Chain of Custody forms for samples collected during testing follow on the next pages along with the analytical request forms.

CLIENT: BAYOU STEEL

SOURCE: BAGHOUSE STACK

| ETS SAMPLE ID   | LAB ID NUMBER | SAMPLE DESCRIPTION | COLLECTION DATE | SAMPLE MEDIA | PRESERVATIVE/ TYPE & AMOUNT | STORE ON ICE | VOLUME MARKED | SEALED |
|-----------------|---------------|--------------------|-----------------|--------------|-----------------------------|--------------|---------------|--------|
| PW-R1           | 14070973      | PROBE WASH         | 7/23/2004       | 0.1N HNO3    | N/A                         | Y            | Y             | Y      |
| PW-R2           | 14070974      | PROBE WASH         | 7/23/2004       | 0.1N HNO3    | N/A                         | Y            | Y             | Y      |
| PW-R3           | 14070975      | PROBE WASH         | 7/23/2004       | 0.1N HNO3    | N/A                         | Y            | Y             | Y      |
| IMP 1&2-R1      | 14070976      | IMPINGER CATCH     | 7/23/2004       | HNO3/H2O2    | N/A                         | Y            | Y             | Y      |
| IMP 1&2-R2      | 14070977      | IMPINGER CATCH     | 7/23/2004       | HNO3/H2O2    | N/A                         | Y            | Y             | Y      |
| IMP 1&2-R3      | 14070978      | IMPINGER CATCH     | 7/23/2004       | HNO3/H2O2    | N/A                         | Y            | Y             | Y      |
| IMP 3-R1        | 14070979      | IMPINGER CATCH     | 7/23/2004       | 0.1N HNO3    | N/A                         | Y            | Y             | Y      |
| IMP 3-R2        | 14070980      | IMPINGER CATCH     | 7/23/2004       | 0.1N HNO3    | N/A                         | Y            | Y             | Y      |
| IMP 3-R3        | 14070981      | IMPINGER CATCH     | 7/23/2004       | 0.1N HNO3    | N/A                         | Y            | Y             | Y      |
| BLANK 0.1N HNO3 | 14070982      | BLANK              | 7/23/2004       | 0.1N HNO3    | N/A                         | Y            | Y             | Y      |
| BLANK DI H2O    | 14070983      | BLANK              | 7/23/2004       | DI H2O       | N/A                         | Y            | Y             | Y      |
| BLANK HNO3/H2O2 | 14070984      | BLANK              | 7/23/2004       | HNO3/H2O2    | N/A                         | Y            | Y             | Y      |

TOTAL NUMBER of SAMPLES including BLANKS and SPIKES: 12  
 SAMPLES COLLECTED BY: Ron McCabe  
 FIELD SAMPLE RECOVERY SUPERVISOR: Ron McCabe  
 SAMPLE TRUSTEE FROM SAMPLE POINT: Joel Richard

| SAMPLES TRANSFERRED TO (LAB NAME) | TRANSFER DATE | TRANSFER METHOD | NUMBER OF SAMPLES | CONDITION OF SAMPLES | NOTES | RECEIVING SAMPLE TRUSTEE SIGNATURE |
|-----------------------------------|---------------|-----------------|-------------------|----------------------|-------|------------------------------------|
| CHATELUX                          | 07/25/04      | By hand         | 12                | Good                 |       | Ron McCabe                         |
|                                   |               |                 |                   |                      |       |                                    |
|                                   |               |                 |                   |                      |       |                                    |

ANALYSIS REQUIRED: LEAD AND MERCURY AS PER EPA METHOD 29

DATE of ANALYSIS: 07/29/04

ANALYST: HARRIS

REPORT DATE: 08/02/04

REPORT NUMBER: 14070973

NOTES

CLIENT: BAYOU STEEL SOURCE: BAGHOUSE STACK

| ETS SAMPLE ID  | LAB ID NUMBER | SAMPLE DESCRIPTION | COLLECTION DATE | SAMPLE MEDIA | PRESERVATIVE/TYPE & AMOUNT | STORE ON ICE | VOLUME MARKED | SEALED |
|----------------|---------------|--------------------|-----------------|--------------|----------------------------|--------------|---------------|--------|
| IMP 4&5-R1     | P4070985      | IMPINGER CATCH     | 7/23/2004       | KMnO4        | N/A                        | Y            | Y             | Y      |
| IMP 4&5-R2     | P4070986      | IMPINGER CATCH     | 7/23/2004       | KMnO4        | N/A                        | Y            | Y             | Y      |
| IMP 4&5-R3     | P4070987      | IMPINGER CATCH     | 7/23/2004       | KMnO4        | N/A                        | Y            | Y             | Y      |
| IMP 4&5-R1-HCL | P4070988      | IMPINGER CATCH     | 7/23/2004       | 8 N HCL      | N/A                        | Y            | Y             | Y      |
| IMP 4&5-R2-HCL | P4070989      | IMPINGER CATCH     | 7/23/2004       | 8 N HCL      | N/A                        | Y            | Y             | Y      |
| IMP 4&5-R3-HCL | P4070990      | IMPINGER CATCH     | 7/23/2004       | 8 N HCL      | N/A                        | Y            | Y             | Y      |
| BLANK KMnO4    | P4070991      | BLANK              | 7/23/2004       | KMnO4        | N/A                        | Y            | Y             | Y      |
| BLANK 8 N HCL  | P4070992      | BLANK              | 7/23/2004       | 8 N HCL      | N/A                        | Y            | Y             | Y      |
|                |               |                    |                 |              |                            |              |               |        |
|                |               |                    |                 |              |                            |              |               |        |
|                |               |                    |                 |              |                            |              |               |        |
|                |               |                    |                 |              |                            |              |               |        |

TOTAL NUMBER OF SAMPLES INCLUDING BLANKS AND SPIKES: 8 FIELD SAMPLE RECOVERY SUPERVISOR: Ron McCabe  
 SAMPLES COLLECTED BY: Ron McCabe SAMPLE TRUSTEE FROM SAMPLE POINT: Joel Richard

| SAMPLES TRANSFERRED TO (LAB NAME) | TRANSFER DATE | TRANSFER METHOD | NUMBER OF SAMPLES | CONDITION OF SAMPLES | NOTES | RECEIVING SAMPLE TRUSTEE SIGNATURE |
|-----------------------------------|---------------|-----------------|-------------------|----------------------|-------|------------------------------------|
| CHEMTEX                           | 07/25/04      | By hand         | 8                 | Good                 |       | Ker Speddy                         |
|                                   |               |                 |                   |                      |       |                                    |
|                                   |               |                 |                   |                      |       |                                    |

ANALYSIS REQUIRED: MERCURY AS PER EPA METHOD 29 DATE OF ANALYSIS: 07/29/04  
 ANALYST: HARUNA  
 REPORT DATE: 08/02/04  
 REPORT NUMBER: 06070985

NOTES

## CHAIN of CUSTODY and ANALYTICAL REQUIREMENTS

|                     |                        |
|---------------------|------------------------|
| CLIENT: BAYOU STEEL | SOURCE: BAGHOUSE STACK |
|---------------------|------------------------|

[illegible]

|                                                        |                                                |
|--------------------------------------------------------|------------------------------------------------|
| TOTAL NUMBER of SAMPLES including BLANKS and SPIKES: 4 | FIELD SAMPLE RECOVERY SUPERVISOR: Ron McCabe   |
| SAMPLES COLLECTED BY: Ron McCabe                       | SAMPLE TRUSTEE FROM SAMPLE POINT: Joel Richard |

| SAMPLES TRANSFERRED<br>TO<br>(LAB NAME) | TRANSFER<br>DATE | TRANSFER<br>METHOD | NUMBER<br>OF SAMPLES | CONDITION<br>OF SAMPLES | NOTES | RECEIVING SAMPLE TRUSTEE<br>SIGNATURE |
|-----------------------------------------|------------------|--------------------|----------------------|-------------------------|-------|---------------------------------------|
| CHEMTEX                                 | 07/25/04         | By hand            | 4                    | Good                    |       | KCPaddy                               |
|                                         |                  |                    |                      |                         |       |                                       |
|                                         |                  |                    |                      |                         |       |                                       |

|                                                                    |                   |
|--------------------------------------------------------------------|-------------------|
| ANALYSIS REQUIRED: MERCURY AND LEAD AS PER EPA REFERENCE METHOD 29 | DATE of ANALYSIS: |
|                                                                    | ANALYST:--        |
|                                                                    | REPORT DATE:      |
|                                                                    | REPORT NUMBER:    |

## NOTES

## VI. TEST DATA and CALCULATIONS

All emission test field data, unit operations data, and laboratory data are presented in this section along with the associated data reduction calculations.

Data from the field data forms were manually input into a computer for data processing and calculations. Integrity of data input is maintained by using a double entry system. The computer performed all calculations and produced the calculations and results summary pages. Input data accuracy were further verified by comparison of raw field data to the computer data printed on the summary pages. Computer program integrity and calculations verification are validated by processing a known set of data. Further controls on the computer program are conducted by comparison of manual spot calculations of the raw data input to computer calculations results.

## **EMISSION TESTS**

### **on the BAGHOUSE STACK**

Emission tests were conducted on the Baghouse Stack to determine the concentration of oxygen and carbon dioxide; and the concentration and mass emission rates of lead and mercury.

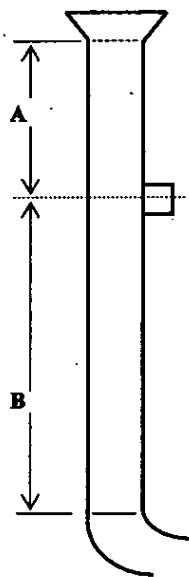
Flow rate, lead, and mercury emissions were determined following EPA Methods 2, 4, and 29 using a combined sampling train. Oxygen and carbon dioxide emissions were determined using EPA Method 3. Prior to the emission tests, the absence of cyclonic flow at the sampling point was determined using EPA Method 1.

Lead, mercury, stack gas velocity, and moisture samples and measurements were obtained at sample traverse points, Figure II, selected per EPA Method 1. Oxygen and carbon dioxide samples and measurements were obtained from a single sample point, Figure III, located near the center of the stack.

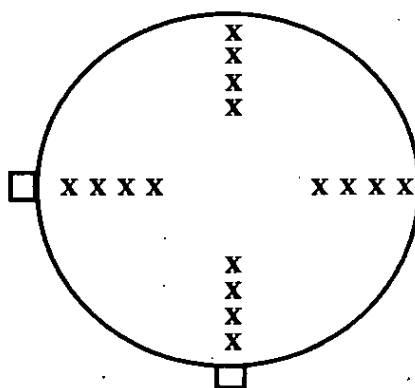
Test data and associated calculations are presented on the following pages.

## TRAVERSE POINT LAYOUT

METHODS-1-4 & 29



CLIENT: BAYOU STEEL  
 DATE: 7/22/2004  
 UNIT TESTED: BAGHOUSE STACK  
 LOCATION: LAPLACE, LA  
 UPSTREAM DIST. (A): (INCHES) 780 DIAMETERS: 7.96  
 DOWNSTREAM DIST. (B): (INCHES) 660 DIAMETERS: 6.73  
 INSIDE DIAMETER (INCHES): 98  
 COUPLING LENGTH (INCHES): 6  
 COUPLING TYPE: 4" SCREW ON



CROSS SECTIONAL LAYOUT

FIGURE 11

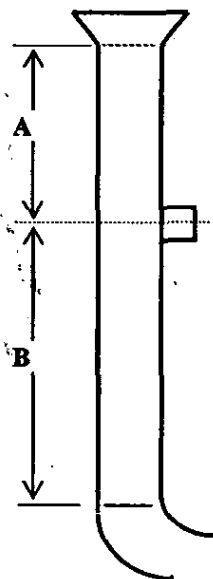
TOTAL TRAVERSE POINTS= 16

| TRAVERSE POINT | DISTANCE<br>% OF DIAMETER | STACK<br>DIAMETER | COUPLING<br>LENGTH | TRAVERSE<br>POINTS |
|----------------|---------------------------|-------------------|--------------------|--------------------|
| 1              | 3.2                       | 98                | 6                  | 9.14               |
| 2              | 10.5                      | 98                | 6                  | 16.29              |
| 3              | 19.4                      | 98                | 6                  | 25.01              |
| 4              | 32.3                      | 98                | 6                  | 37.65              |
| 5              | 67.7                      | 98                | 6                  | 72.35              |
| 6              | 80.6                      | 98                | 6                  | 84.99              |
| 7              | 89.5                      | 98                | 6                  | 93.71              |
| 8              | 96.8                      | 98                | 6                  | 100.86             |

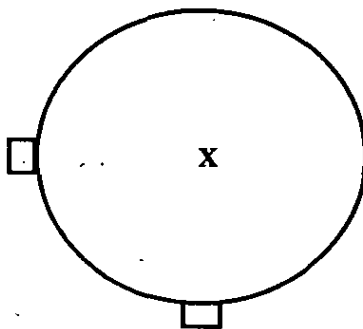
SIGNATURE: Zon McCabe

## TRAVERSE POINT LAYOUT

### METHODS 3



CLIENT: BAYOU STEEL  
 DATE: 07/22/04  
 UNIT TESTED: BAGHOUSE STACK  
 LOCATION: LAPLACE, LA  
 UPSTREAM DIST. (A): 780  
 DOWNSTREAM DIST. (B): 660  
 INSIDE DIAMETER (INCHES): 98  
 COUPLING LENGTH (INCHES): 6  
 COUPLING TYPE: 4" SCREW ON



CROSS SECTIONAL LAYOUT

FIGURE 111

TOTAL TRAVERSE POINTS=

1

| TRAVERSE POINT | DISTANCE<br>% OF DIAMETER | STACK<br>DIAMETER | COUPLING<br>LENGTH | TRAVERSE<br>POINTS |
|----------------|---------------------------|-------------------|--------------------|--------------------|
| 1              | 0.500                     | 98                | 6                  | 55.00              |

SIGNATURE:

Ronald M. Cate

## VERIFICATION OF ABSENCE of CYCLONIC FLOW

COMPANY: Bayou Steel

DATE: 7-23-04

SOURCE: Byghouse Stack

STACK DIAMETER 98"

LOCATION: Norco, La.

OPERATOR: Joel Richard

|    | REFERENCE<br>ANGLE |         | REFERENCE<br>ANGLE |
|----|--------------------|---------|--------------------|
| 1  | <u>0</u>           | 13      | <u>1</u>           |
| 2  | <u>1</u>           | 14      | <u>2</u>           |
| 3  | <u>2</u>           | 15      | <u>1</u>           |
| 4  | <u>1</u>           | 16      | <u>1</u>           |
| 5  | <u>2</u>           | 17      |                    |
| 6  | <u>0</u>           | 18      |                    |
| 7  | <u>1</u>           | 19      |                    |
| 8  | <u>2</u>           | 20      |                    |
| 9  | <u>1</u>           | 21      |                    |
| 10 | <u>2</u>           | 22      |                    |
| 11 | <u>0</u>           | 23      |                    |
| 12 | <u>1</u>           | 24      |                    |
|    |                    | AVERAGE | <u>1.125*</u>      |

\* THE AVERAGE IS THE ABSOLUTE VALUE OF EACH DEGREE POINT DIVIDED BY THE NUMBER OF POINTS.

REFERENCE ANGLE CANNOT EXCEED 20 DEGREES OF AVERAGE OVERALL VALUE.

FORMS:CYCLONIC

PLANT: Bayou Steel SAMPLE BOX NO.: 35 RM PITOT TUBE ID: P-10-5 STACK DIAMETER, in.: 98"  
 DATE: 7-23-04 METER BOX NO.: 3 PITOT TUBE FACTOR: 833 METER ΔH@: 1.8127  
 LOCATION: Norco, La. BAROMETRIC PRESSURE: 29.95 FILTER ID:  METER D.G.M.F.: 1.0309  
 STACK ID: Bay House Stack AMBIENT TEMP.: 81°F FILTER TYPE:  K-FACTOR: .6580  
 RUN NO.: 1 OPERATOR: Dee Richard NOZZLE DIAMETER, IN.: .170 T-FACTOR: 461.91

| Traverse Point Number | Sampling Time (0), min. | Static Pressure (in. H <sub>2</sub> O) | Stack Temp. (T <sub>s</sub> ), °F | Velocity Head |        | Pressure Differential Across Orifice Meter (ΔH) in. H <sub>2</sub> O |         | Dry Gas Meter Volume (V <sub>m</sub> ), ft <sup>3</sup> | Gas Sample Temperature at Dry Gas Meter |                                | Probe Temp. °F | Sample Box Temp. °F | Temp of Gas Leaving Last Impinger °F | Pump Vacuum in. Hg gauge |
|-----------------------|-------------------------|----------------------------------------|-----------------------------------|---------------|--------|----------------------------------------------------------------------|---------|---------------------------------------------------------|-----------------------------------------|--------------------------------|----------------|---------------------|--------------------------------------|--------------------------|
|                       |                         |                                        |                                   | (APs)         | (ΔAPs) | Actual                                                               | Desired |                                                         | Inlet (T <sub>in</sub> ), °F            | Outlet (T <sub>out</sub> ), °F |                |                     |                                      |                          |
| 1                     | 9:34                    | -.650                                  | 234                               | 1.20          | 1.095  | .800                                                                 | .798    | 879.203                                                 | 105                                     | 97                             | 252            | 248                 | 58                                   | 3.5                      |
| 2                     | 9:38.5                  |                                        | 246                               | 1.10          | 1.048  | .720                                                                 | .719    | 881.510                                                 | 108                                     | 97                             | 242            | 245                 | 57                                   | 3.5                      |
| 3                     | 9:43                    |                                        | 251                               | 1.00          | 1.000  | .650                                                                 | .649    | 883.810                                                 | 110                                     | 98                             | 241            | 244                 | 56                                   | 3.5                      |
| 4                     | 9:47.5                  |                                        | 253                               | .940          | .9695  | .610                                                                 | .608    | 885.810                                                 | 112                                     | 99                             | 245            | 240                 | 56                                   | 3.5                      |
| 5                     | 9:52                    |                                        | 258                               | .960          | .9797  | .620                                                                 | .617    | 887.825                                                 | 114                                     | 101                            | 242            | 247                 | 56                                   | 3.5                      |
| 6                     | 9:56.5                  |                                        | 248                               | 1.05          | 1.024  | .690                                                                 | .685    | 889.820                                                 | 116                                     | 104                            | 245            | 248                 | 57                                   | 3.5                      |
| 7                     | 10:01                   |                                        | 231                               | 1.20          | 1.095  | .800                                                                 | .802    | 892.050                                                 | 117                                     | 105                            | 247            | 251                 | 56                                   | 3.5                      |
| 8                     | 10:05.5                 |                                        | 230                               | 1.10          | 1.048  | .740                                                                 | .736    | 894.350                                                 | 118                                     | 104                            | 243            | 250                 | 56                                   | 3.5                      |
| 9                     | 10:10                   |                                        | 233                               | 1.10          | 1.048  | .730                                                                 | .733    | 896.553                                                 | 118                                     | 104                            | 242            | 248                 | 57                                   | 3.5                      |
| 10                    | 10:20.5                 |                                        | 238                               | 1.20          | 1.095  | .790                                                                 | .794    | 898.875                                                 | 121                                     | 110                            | 242            | 248                 | 57                                   | 3.5                      |
| 11                    | 10:25                   |                                        | 240                               | 1.20          | 1.095  | .790                                                                 | .790    | 901.210                                                 | 119                                     | 107                            | 242            | 249                 | 58                                   | 3.5                      |
| 12                    | 10:29.5                 |                                        | 236                               | 1.05          | 1.024  | .700                                                                 | .696    | 903.670                                                 | 121                                     | 111                            | 243            | 250                 | 58                                   | 3.5                      |
| 13                    | 10:34                   |                                        | 227                               | .900          | .948   | .600                                                                 | .596    | 905.515                                                 | 122                                     | 112                            | 242            | 253                 | 59                                   | 3.5                      |
| 14                    | 10:38.5                 |                                        | 245                               | .940          | .969   | .620                                                                 | .615    | 907.505                                                 | 119                                     | 109                            | 240            | 256                 | 60                                   | 3.5                      |
| 15                    | 10:43                   |                                        | 238                               | .960          | .979   | .640                                                                 | .635    | 909.520                                                 | 121                                     | 109                            | 242            | 255                 | 60                                   | 3.5                      |
| 16                    | 10:47.5                 |                                        | 240                               | .980          | .989   | .650                                                                 | .646    | 911.735                                                 | 120                                     | 109                            | 241            | 253                 | 60                                   | 3.5                      |
| 17                    | 10:52                   |                                        |                                   |               |        |                                                                      |         | 913.670                                                 |                                         |                                |                |                     |                                      |                          |
| 18                    | 10:56                   |                                        |                                   |               |        |                                                                      |         |                                                         |                                         |                                |                |                     |                                      |                          |
| AVERAGE               |                         |                                        | 241.125                           |               | 1.025  | .709                                                                 |         | 34.467                                                  |                                         | 110.53                         |                |                     |                                      |                          |

| LIQUID COLLECTED |  | IMPINGING WEIGHTS |   |   |      |
|------------------|--|-------------------|---|---|------|
|                  |  | 1                 | 2 | 3 | 4    |
| FINAL            |  |                   |   |   | 29.7 |
| INITIAL          |  |                   |   |   | 5    |
| TOTAL WEIGHT     |  |                   |   |   |      |

COMMENTS:  
 Pitot tube leak check, impact side good @ 3.5" H<sub>2</sub>O  
 Pitot tube leak check, static side good @ 4.0" H<sub>2</sub>O  
 Pre-leak Rate @ 10 in.Hg 0.001 ft<sup>3</sup>/min.  
 Post-leak Rate @ 10 in.Hg 0.002 ft<sup>3</sup>/min.

## DETERMINATION of STACK GAS MOISTURE, MOLECULAR WEIGHT, VELOCITY, and VOLUMETRIC FLOW RATE

|                   |                                                            |      |                                                   |                  |                                                     |
|-------------------|------------------------------------------------------------|------|---------------------------------------------------|------------------|-----------------------------------------------------|
| A                 | - Cross-sectional area of the stack, ft <sup>2</sup>       | Pbar | - Barometric pressure, in. Hg                     | Vi               | - Water vapor condensed, impinger 1, g              |
| Acf               | - Stack gas flow rate, actual, acfm                        | Pa   | - Stack gas static pressure, in. H <sub>2</sub> O | Vii              | - Water vapor condensed, impinger 2, g              |
| Bws               | - Stack gas moisture fraction, %/100                       | Ps   | - Stack gas absolute pressure, in. Hg             | Viii             | - Water vapor condensed, impinger 3, g              |
| Cp                | - Pitot tube coefficient                                   | Pstd | - Standard absolute pressure, 29.92 in. Hg        | Viv              | - Water vapor condensed, impinger 4, g              |
| dH                | - Meter orific pressure differential, in. H <sub>2</sub> O | Qsd  | - Stack gas volumetric flow rate, dry acfm        | Vm               | - Gas meter sample volume, dry ft <sup>3</sup>      |
| dP                | - Stack gas velocity head, in. H <sub>2</sub> O            | R    | - Ideal gas constant, 21.85                       | Vmstd            | - Gas meter sample volume, dry std. ft <sup>3</sup> |
| F1                | - Conversion factor, 13.6 in. H <sub>2</sub> O/ in. Hg     | Tm   | - Meter temperature, R                            | Vs               | - Stack gas velocity, ft/sec                        |
| Kp                | - Pitot tube constant, 85.49                               | Ts   | - Stack gas temperature, R                        | Vw               | - Total water vapor condensed, ft <sup>3</sup>      |
| MCO <sub>2</sub>  | - Molecular weight of CO <sub>2</sub> , 44.01 lb/ lb mole  | Tstd | - Standard temperature, 528 R                     | Y                | - Dry gas meter calibration factor                  |
| Md                | - Stack gas molecular weight, dry lb/lb mole               |      |                                                   | %CO <sub>2</sub> | - Stack gas CO concentration, %/100                 |
| MH <sub>2</sub> O | - Molecular weight of water, 18.02 lb/lb mole              |      |                                                   | %N <sub>2</sub>  | - Stack gas N <sub>2</sub> concentration, %/100     |
| MN <sub>2</sub>   | - Molecular weight of N <sub>2</sub> , 28.01 lb/lb mole    |      |                                                   | O <sub>2</sub>   | - Stack gas O <sub>2</sub> concentration, %/100     |
| MO <sub>2</sub>   | - Molecular weight of O <sub>2</sub> , 32.00 lb/lb mole    |      |                                                   |                  |                                                     |
| Ms                | - Stack gas molecular weight, wet lb/lb mole               |      |                                                   |                  |                                                     |

$$Vw = \left\{ \frac{(Vi + Vii + Viii + Viv) R Tstd}{(453.6 \text{ g/lb}) Pstd MH_2O} \right\} = \left\{ \frac{(23.9 + 1.1 + -2.9 + 7.6)(21.85)(528)}{(453.6)(29.92)(18.02)} \right\} = 1.40105$$

$$Vmstd = Vm Y \left\{ \frac{(Pb + dH/ F1) Tstd}{Pstd Tm} \right\} = (34.467)(1.0309) \left\{ \frac{(29.950 + .6969/13.6)(528)}{(29.92)(571)} \right\} = 32.97250$$

$$Bws = \left\{ \frac{Vw}{Vw + Vmstd} \right\} = \left\{ \frac{(1.40105)}{(1.40105 + 32.97250)} \right\} = .0408$$

$$Md = (MCO_2)(\%CO_2) + (MO_2)(\%O_2) + (MN_2)(\%N_2) \\ = (44.01)(.001) + (32.00)(.198) + (28.01)(.801) = 28.816$$

$$Ms = Md(1 - Bws) + (MH_2O Bws) = (28.816)(1 - .0408) + (18.02)(.0408) = 28.376$$

$$Vs = Kp Cp (dP)^{1/2} \left\{ \frac{Ts}{Ps Ms} \right\}^{1/2} = (85.49)(.8320)(1.0259) \left\{ \frac{(701)}{(29.902)(28.376)} \right\}^{1/2} = 66.3327$$

$$Acf = (60 \text{ sec/min})(Vs A) = (60)(66.3327)(52.3817) = 208476.9$$

$$Qsd = (3600 \text{ sec/hr})(1 - Bws)(Vs A) \left\{ \frac{Tstd Ps}{Ts Pstd} \right\} \\ = (3600)(1 - .0408)(66.3327)(52.3817) \left\{ \frac{(528)(29.902)}{(701)(29.92)} \right\} = \begin{matrix} 9030603.0 \text{ dscf/hr} \\ 150510.0 \text{ dscf/min} \end{matrix}$$

PLANT: Bryan Steel SAMPLE BOX NO.: 5 A1 PITOT TUBE ID.: P-10.5 STACK DIAMETER, in.: 98"  
 DATE: 1-23-04 METER BOX NO.: 3 PITOT TUBE FACTOR: .832 METER Δ H@: 1.8127  
 LOCATION: Norco Co. BAROMETRIC PRESSURE: 29.95 FILTER ID.: 1-0309 K-FACTOR: .6750  
 STACK ID: August Stack AMBIENT TEMP.: 91°F NOZZLE DIAMETER, IN.: .170 T-FACTOR: 473.27  
 RUN NO.: 3 OPERATOR: Joel Richard

| Traverse Point Number | Sampling Time (θ), min. | Static Pressure (in. H <sub>2</sub> O) | Stack Temp. (T <sub>s</sub> ), °F | Velocity Head |       | Pressure Differential Across Orifice Meter (ΔH) in. H <sub>2</sub> O | Dry Gas Meter Volume (V <sub>m</sub> ), ft <sup>3</sup> | Gas Sample Temperature at Dry Gas Meter |                                | Probe Temp. °F | Sample Box Temp. °F | Temp of Gas Leaving Last Impinger °F | Pump Vacuum in. Hg gauge |
|-----------------------|-------------------------|----------------------------------------|-----------------------------------|---------------|-------|----------------------------------------------------------------------|---------------------------------------------------------|-----------------------------------------|--------------------------------|----------------|---------------------|--------------------------------------|--------------------------|
|                       |                         |                                        |                                   | (ΔPs)         | (ΔPv) |                                                                      |                                                         | Inlet (T <sub>in</sub> ), °F            | Outlet (T <sub>out</sub> ), °F |                |                     |                                      |                          |
| 0001                  | 11:58                   | -640                                   | 233                               | 1.30          | 1.14  | .890                                                                 | 919.715                                                 | 111                                     | 104                            | 243            | 245                 | 55                                   | 3.0                      |
| 2                     | 12:02.5                 |                                        | 243                               | 1.05          | 1.02  | .710                                                                 | 921.950                                                 | 115                                     | 103                            | 240            | 248                 | 55                                   | 3.5                      |
| 3                     | 12:07                   |                                        | 240                               | .980          | .989  | .660                                                                 | 924.350                                                 | 117                                     | 105                            | 241            | 250                 | 55                                   | 3.5                      |
| 4                     | 12:10.5                 |                                        | 242                               | .960          | .979  | .650                                                                 | 926.430                                                 | 117                                     | 106                            | 245            | 251                 | 55                                   | 3.5                      |
| 5                     | 12:16                   |                                        | 246                               | 1.05          | 1.024 | .700                                                                 | 928.470                                                 | 116                                     | 106                            | 242            | 253                 | 56                                   | 3.5                      |
| 6                     | 12:20.5                 |                                        | 243                               | 1.00          | 1.000 | .670                                                                 | 930.680                                                 | 117                                     | 106                            | 242            | 252                 | 56                                   | 3.5                      |
| 7                     | 12:25                   |                                        | 242                               | .970          | .984  | .650                                                                 | 932.748                                                 | 117                                     | 107                            | 243            | 250                 | 56                                   | 3.0                      |
| 8                     | 12:29.5                 |                                        | 247                               | .990          | .994  | .660                                                                 | 934.875                                                 | 118                                     | 107                            | 244            | 249                 | 56                                   | 3.0                      |
| 0009                  | 12:34                   |                                        |                                   |               |       |                                                                      | 936.960                                                 |                                         |                                |                |                     |                                      |                          |
| 0010                  | 12:38                   |                                        | 241                               | 1.25          | 1.118 | .840                                                                 | 936.960                                                 | 118                                     | 107                            | 242            | 250                 | 57                                   | 3.0                      |
| 10                    | 12:42.5                 |                                        | 243                               | 1.20          | 1.095 | .810                                                                 | 939.330                                                 | 118                                     | 107                            | 240            | 247                 | 57                                   | 3.5                      |
| 11                    | 12:47                   |                                        | 231                               | 1.15          | 1.072 | .790                                                                 | 941.810                                                 | 121                                     | 109                            | 241            | 248                 | 57                                   | 3.5                      |
| 12                    | 12:51.5                 |                                        | 235                               | 1.10          | 1.048 | .750                                                                 | 944.020                                                 | 121                                     | 109                            | 243            | 252                 | 58                                   | 3.5                      |
| 13                    | 12:56                   |                                        | 242                               | 1.05          | 1.024 | .710                                                                 | 946.250                                                 | 122                                     | 110                            | 242            | 251                 | 58                                   | 3.5                      |
| 14                    | 13:00.5                 |                                        | 240                               | .980          | .989  | .660                                                                 | 948.460                                                 | 122                                     | 110                            | 240            | 250                 | 59                                   | 3.5                      |
| 15                    | 13:05                   |                                        | 239                               | .960          | 1.00  | .680                                                                 | 949.610                                                 | 123                                     | 111                            | 239            | 251                 | 59                                   | 3.0                      |
| 16                    | 13:09.5                 |                                        | 241                               | .990          | .994  | .670                                                                 | 952.680                                                 | 123                                     | 112                            | 240            | 252                 | 59                                   | 3.0                      |
| 0017                  | 13:14                   |                                        |                                   |               |       |                                                                      | 954.865                                                 |                                         |                                |                |                     |                                      |                          |
| AVERAGE               | 12 min                  | -640                                   | 240.5                             |               | 1.029 | .718                                                                 | 250.150                                                 |                                         | 112.916                        |                |                     |                                      |                          |

## IMPINGER WEIGHTS

| LIQUID COLLECTED | IMPINGER WEIGHTS |   |   |      |
|------------------|------------------|---|---|------|
|                  | 1                | 2 | 3 | 4    |
| FINAL            |                  |   |   | 22.3 |
| INITIAL          |                  |   |   |      |
| TOTAL WEIGHT     |                  |   |   |      |

## ORSAT MEASUREMENT

| ORSAT MEASUREMENT                                    |                |    |                |
|------------------------------------------------------|----------------|----|----------------|
| CO <sub>2</sub>                                      | O <sub>2</sub> | CO | N <sub>2</sub> |
| 0.2                                                  | 19.8           |    |                |
| Orsat leak check <input checked="" type="checkbox"/> |                |    |                |
| Method (3 or 3A) <u>3</u>                            |                |    |                |
| Barometer ID <u>1</u>                                |                |    |                |

## COMMENTS:

Pitot tube leak check, impact side good 4.0" H<sub>2</sub>O  
 Pitot tube leak check, static side good 3.5" H<sub>2</sub>O  
 Pre-leak Rate @ 10 in. Hg 0.00 ft<sup>3</sup>/min.  
 Post-leak Rate @ 10 in. Hg 0.00 ft<sup>3</sup>/min.

## DETERMINATION of STACK GAS MOISTURE, MOLECULAR WEIGHT, VELOCITY, and VOLUMETRIC FLOW RATE

|                   |                                                            |      |                                                   |                  |                                                     |
|-------------------|------------------------------------------------------------|------|---------------------------------------------------|------------------|-----------------------------------------------------|
| A                 | - Cross-sectional area of the stack, ft <sup>2</sup>       | Pbar | - Barometric pressure, in. Hg                     | Vi               | - Water vapor condensed, impinger 1, g              |
| Acf               | - Stack gas flow rate, actual, acfm                        | Pa   | - Stack gas static pressure, in. H <sub>2</sub> O | Vii              | - Water vapor condensed, impinger 2, g              |
| Bws               | - Stack gas moisture fraction, %/100                       | Ps   | - Stack gas absolute pressure, in. Hg             | Viii             | - Water vapor condensed, impinger 3, g              |
| Cp                | - Pitot tube coefficient                                   | Pstd | - Standard absolute pressure, 29.92 in. Hg        | Viv              | - Water vapor condensed, impinger 4, g              |
| dH                | - Meter orific pressure differential, in. H <sub>2</sub> O | Qsd  | - Stack gas volumetric flow rate, dry acfm        | Vm               | - Gas meter sample volume, dry ft <sup>3</sup>      |
| dP                | - Stack gas velocity head, in. H <sub>2</sub> O            | R    | - Ideal gas constant, 21.85                       | Vmstd            | - Gas meter sample volume, dry std. ft <sup>3</sup> |
| F1                | - Conversion factor, 13.6 in. H <sub>2</sub> O/ in. Hg     | Tm   | - Meter temperature, R                            | Vs               | - Stack gas velocity, ft/sec                        |
| Kp                | - Pitot tube constant, 85.49                               | Ts   | - Stack gas temperature, R                        | Vw               | - Total water vapor condensed, ft <sup>3</sup>      |
| MCO <sub>2</sub>  | - Molecular weight of CO <sub>2</sub> , 44.01 lb/ lb mole  | Tstd | - Standard temperature, 528 R                     | Y                | - Dry gas meter calibration factor                  |
| Md                | - Stack gas molecular weight, dry lb/lb mole               |      |                                                   | %CO <sub>2</sub> | - Stack gas CO concentration, %/100                 |
| MH <sub>2</sub> O | - Molecular weight of water, 18.02 lb/lb mole              |      |                                                   | %N <sub>2</sub>  | - Stack gas N <sub>2</sub> concentration, %/100     |
| MN <sub>2</sub>   | - Molecular weight of N <sub>2</sub> , 28.01 lb/lb mole    |      |                                                   | O <sub>2</sub>   | - Stack gas O <sub>2</sub> concentration, %/100     |
| MO <sub>2</sub>   | - Molecular weight of O <sub>2</sub> , 32.00 lb/lb mole    |      |                                                   |                  |                                                     |
| Ms                | - Stack gas molecular weight, wet lb/lb mole               |      |                                                   |                  |                                                     |

$$Vw = \left\{ \frac{(Vi + Vii + Viii + Viv) R Tstd}{(453.6 \text{ g/lb}) Pstd MH_2O} \right\} = \left\{ \frac{(19.4 + 1.9 + -3.7 + 4.7)(21.85)(528)}{(453.6)(29.92)(18.02)} \right\} = 1.05196$$

$$Vmstd = Vm Y \left\{ \frac{(Pb + dH/F1) Tstd}{Pstd Tm} \right\} = (35.150)(1.0309) \left\{ \frac{(29.950 + .7188/13.6)(528)}{(29.92)(573)} \right\} = 33.48461$$

$$Bws = \left\{ \frac{Vw}{Vw + Vmstd} \right\} = \left\{ \frac{(1.05196)}{(1.05196 + 33.48461)} \right\} = .0305$$

$$Md = (MCO_2)(\%CO_2) + (MO_2)(\%O_2) + (MN_2)(\%N_2) \\ = (44.01)(.002) + (32.00)(.198) + (28.01)(.800) = 28.832$$

$$Ms = Md(1 - Bws) + (MH_2O Bws) = (28.832)(1 - .0305) + (18.02)(.0305) = 28.503$$

$$Vs = Kp Cp (dP)^{1/2} \left\{ \frac{Ts}{Ps Ms} \right\}^{1/2} = (85.49)(.8320)(1.0302) \left\{ \frac{(701)}{(29.903)(28.503)} \right\}^{1/2} = 66.4312$$

$$Acf = (60 \text{ sec/min})(Vs A) = (60)(66.4312)(52.3817) = 208786.4$$

$$Qsd = (3600 \text{ sec/hr})(1 - Bws)(Vs A) \left\{ \frac{Tstd Ps}{Ts Pstd} \right\} \\ = (3600)(1 - .0305)(66.4312)(52.3817) \left\{ \frac{(528)(29.903)}{(701)(29.92)} \right\} = 9149506.0 \text{ dscf/hr} \\ = 152491.8 \text{ dscf/min}$$

# ETS<sup>®</sup> EMISSION TESTING SERVICES, INC., FIELD DATA, METHOD(S) 1-4 + 29

PLANT: Bayer Steel SAMPLE BOX NO.: 10-5 PITOT TUBE ID.: P-10-5 STACK DIAMETER, in.: 98"  
 DATE: 7-23-64 METER BOX NO.: 3 PITOT TUBE FACTOR: 832 METER Δ H@: 1.8127  
 LOCATION: Norco, La. BAROMETRIC PRESSURE: 29.95 FILTER ID.: 1.0309  
 STACK ID.: Bayhouse Stack AMBIENT TEMP.: 90°F FILTER TYPE: 6750  
 RUN NO.: 3 OPERATOR: Joe L. Richard NOZZLE DIAMETER, IN.: 1.70 T-FACTOR: 473.27

| Traverse Point Number | Sampling Time (0), min. | Static Pressure (in. H <sub>2</sub> O) | Stack Temp. (T <sub>s</sub> ), °F | Velocity Head      |                    | Pressure Differential Across Orifice Meter (ΔH) in. H <sub>2</sub> O |         | Dry Gas Meter Volume (V <sub>m</sub> ), ft <sup>3</sup> | Gas Sample Temperature at Dry Gas Meter |                                | Probe Temp. °F | Sample Box Temp. °F | Temp of Gas Leaving Last Impinger °F | Pump Vacuum in. Hg gauge |
|-----------------------|-------------------------|----------------------------------------|-----------------------------------|--------------------|--------------------|----------------------------------------------------------------------|---------|---------------------------------------------------------|-----------------------------------------|--------------------------------|----------------|---------------------|--------------------------------------|--------------------------|
|                       |                         |                                        |                                   | Δ(P <sub>s</sub> ) | (ΔP <sub>s</sub> ) | Actual                                                               | Desired |                                                         | Inlet (T <sub>in</sub> ), °F            | Outlet (T <sub>out</sub> ), °F |                |                     |                                      |                          |
| 1                     | 16:05                   | -650                                   | 240                               | 1.18               | 1.18               | 950                                                                  | 946     | 973.448                                                 | 97                                      | 88                             | 243            | 253                 | 53                                   | 3.0                      |
| 2                     | 16:08.5                 |                                        | 238                               | 1.30               | 1.14               | 880                                                                  | 881     | 975.890                                                 | 100                                     | 88                             | 242            | 252                 | 53                                   | 3.5                      |
| 3                     | 16:14                   |                                        | 235                               | 1.10               | 1.04               | 750                                                                  | 749     | 978.285                                                 | 102                                     | 88                             | 240            | 251                 | 54                                   | 3.0                      |
| 4                     | 16:18.5                 |                                        | 238                               | 1.05               | 1.02               | 710                                                                  | 711     | 980.600                                                 | 102                                     | 88                             | 245            | 250                 | 54                                   | 3.5                      |
| 5                     | 16:23                   |                                        | 240                               | 1.10               | 1.04               | 740                                                                  | 743     | 982.785                                                 | 102                                     | 90                             | 247            | 249                 | 54                                   | 3.5                      |
| 6                     | 16:27.5                 |                                        | 241                               | 1.10               | 1.04               | 740                                                                  | 743     | 984.915                                                 | 104                                     | 90                             | 242            | 250                 | 55                                   | 3.0                      |
| 7                     | 16:32                   |                                        | 240                               | 1.00               | 1.00               | 680                                                                  | 676     | 987.150                                                 | 107                                     | 92                             | 241            | 252                 | 55                                   | 3.0                      |
| 8                     | 16:36.5                 |                                        | 237                               | 1.05               | 1.02               | 710                                                                  | 712     | 989.350                                                 | 108                                     | 92                             | 240            | 257                 | 56                                   | 3.0                      |
| 9                     | 16:41                   |                                        |                                   |                    |                    |                                                                      |         | 991.476                                                 |                                         |                                |                |                     |                                      |                          |
| 10                    | 16:47                   |                                        | 238                               | 1.20               | 1.09               | 810                                                                  | 813     | 991.476                                                 | 99                                      | 91                             | 239            | 256                 | 56                                   | 3.0                      |
| 11                    | 16:51.5                 |                                        | 240                               | 1.10               | 1.04               | 740                                                                  | 743     | 993.770                                                 | 103                                     | 93                             | 240            | 253                 | 57                                   | 3.5                      |
| 12                    | 16:56                   |                                        | 242                               | 1.10               | 1.04               | 740                                                                  | 743     | 996.000                                                 | 104                                     | 92                             | 242            | 254                 | 57                                   | 3.0                      |
| 13                    | 17:00.5                 |                                        | 241                               | 1.00               | 1.00               | 680                                                                  | 675     | 998.240                                                 | 106                                     | 92                             | 241            | 252                 | 58                                   | 3.0                      |
| 14                    | 17:05                   |                                        | 247                               | 1.05               | 1.02               | 760                                                                  | 762     | 1000.330                                                | 106                                     | 93                             | 243            | 251                 | 59                                   | 3.0                      |
| 15                    | 17:09.5                 |                                        | 243                               | 1.00               | 1.00               | 670                                                                  | 673     | 1002.490                                                | 108                                     | 93                             | 242            | 250                 | 60                                   | 3.0                      |
| 16                    | 17:14                   |                                        | 240                               | 970                | 984                | 660                                                                  | 655     | 1004.610                                                | 110                                     | 93                             | 241            | 250                 | 60                                   | 3.0                      |
| 17                    | 17:18.5                 |                                        | 241                               | 960                | 979                | 650                                                                  | 648     | 1006.565                                                | 110                                     | 94                             | 240            | 252                 | 60                                   | 3.0                      |
| 18                    | 17:23                   |                                        |                                   |                    |                    |                                                                      |         | 1008.673                                                |                                         |                                |                |                     |                                      |                          |
| AVERAGE               | 17 min                  | -650                                   | 240.06                            |                    | 1.039              | 738                                                                  |         | 35.225                                                  |                                         | 92.03                          |                |                     |                                      |                          |

| IMPINGER WEIGHTS |   |   |   |   |
|------------------|---|---|---|---|
| LIQUID COLLECTED | 1 | 2 | 3 | 4 |
| FINAL            |   |   |   |   |
| INITIAL          |   |   |   |   |
| TOTAL WEIGHT     |   |   |   |   |

| ORSAT MEASUREMENT |                |    |                |
|-------------------|----------------|----|----------------|
| CO <sub>2</sub>   | O <sub>2</sub> | CO | N <sub>2</sub> |
| 0.2               | 19.2           |    |                |
| Orsat leak check  |                |    |                |
| Method (3 or 3A)  |                |    |                |
| Barometer ID      |                |    |                |

COMMENTS:

Pitot tube leak check, impact side: good @ 40" H<sub>2</sub>O  
 Pitot tube leak check, static side: good @ 4.5" H<sub>2</sub>O  
 Pre-leak Rate @ 10 in. Hg: 0.003 ft<sup>3</sup>/min.  
 Post-leak Rate @ 10 in. Hg: 0.001 ft<sup>3</sup>/min.

## DETERMINATION of STACK GAS MOISTURE, MOLECULAR WEIGHT, VELOCITY, and VOLUMETRIC FLOW RATE

|                   |                                                             |      |                                                   |                  |                                                     |
|-------------------|-------------------------------------------------------------|------|---------------------------------------------------|------------------|-----------------------------------------------------|
| A                 | - Cross-sectional area of the stack, ft <sup>2</sup>        | Pbar | - Barometric pressure, in. Hg                     | Vi               | - Water vapor condensed, impinger 1, g              |
| Acf               | - Stack gas flow rate, actual, acfm                         | Pa   | - Stack gas static pressure, in. H <sub>2</sub> O | Vii              | - Water vapor condensed, impinger 2, g              |
| Bws               | - Stack gas moisture fraction, %/100                        | Ps   | - Stack gas absolute pressure, in. Hg             | Viii             | - Water vapor condensed, impinger 3, g              |
| Cp                | - Pitot tube coefficient                                    | Pstd | - Standard absolute pressure, 29.92 in. Hg        | Viv              | - Water vapor condensed, impinger 4, g              |
| dH                | - Meter orifice pressure differential, in. H <sub>2</sub> O | Qsd  | - Stack gas volumetric flow rate, dry scfm        | Vm               | - Gas meter sample volume, dry ft <sup>3</sup>      |
| dP                | - Stack gas velocity head, in. H <sub>2</sub> O             | R    | - Ideal gas constant, 21.85                       | Vmstd            | - Gas meter sample volume, dry std. ft <sup>3</sup> |
| F1                | - Conversion factor, 13.6 in. H <sub>2</sub> O/ in. Hg      | Tm   | - Meter temperature, R                            | Vs               | - Stack gas velocity, ft/sec                        |
| Kp                | - Pitot tube constant, 85.49                                | Ts   | - Stack gas temperature, R                        | Vw               | - Total water vapor condensed, ft <sup>3</sup>      |
| MCO <sub>2</sub>  | - Molecular weight of CO <sub>2</sub> , 44.01 lb/ lb mole   | Tstd | - Standard temperature, 528 R                     | Y                | - Dry gas meter calibration factor                  |
| Md                | - Stack gas molecular weight, dry lb/lb mole                |      |                                                   | %CO <sub>2</sub> | - Stack gas CO concentration, %/100                 |
| MH <sub>2</sub> O | - Molecular weight of water, 18.02 lb/lb mole               |      |                                                   | %N <sub>2</sub>  | - Stack gas N <sub>2</sub> concentration, %/100     |
| MN <sub>2</sub>   | - Molecular weight of N <sub>2</sub> , 28.01 lb/lb mole     |      |                                                   | O <sub>2</sub>   | - Stack gas O <sub>2</sub> concentration, %/100     |
| MO <sub>2</sub>   | - Molecular weight of O <sub>2</sub> , 32.00 lb/lb mole     |      |                                                   |                  |                                                     |
| Ms                | - Stack gas molecular weight, wet lb/lb mole                |      |                                                   |                  |                                                     |

$$Vw = \left\{ \frac{(Vi + Vii + Viii + Viv) R Tstd}{(453.6 \text{ g/lb}) Pstd MH_2O} \right\} = \left\{ \frac{(31.1 + .8 + .0 + 3.7)(21.85)(528)}{(453.6)(29.92)(18.02)} \right\} = 1.67937$$

$$Vmstd = Vm Y \left\{ \frac{(Pb + dH/F1) Tstd}{Pstd Tm} \right\} = (35.225)(1.0309) \left\{ \frac{(29.950 + .7381/13.6)(528)}{(29.92)(558)} \right\} = 34.47911$$

$$Bws = \left\{ \frac{Vw}{Vw + Vmstd} \right\} = \left\{ \frac{(1.67937)}{(1.67937 + 34.47911)} \right\} = .0464$$

$$Md = (MCO_2)(\%CO_2) + (MO_2)(\%O_2) + (MN_2)(\%N_2) \\ = (44.01)(.002) + (32.00)(.192) + (28.01)(.806) = 28.808$$

$$Ms = Md(1 - Bws) + (MH_2O Bws) = (28.808)(1 - .0464) + (18.02)(.0464) = 28.307$$

$$Vs = Kp Cp (dP)^{1/2} \left\{ \frac{Ts}{Ps Ms} \right\}^{1/2} = (85.49)(.8320)(1.0439) \left\{ \frac{(700)}{(29.902)(28.307)} \right\}^{1/2} = 67.5224$$

$$Acf = (60 \text{ sec/min})(Vs A) = (60)(67.5224)(52.3817) = 212216.0$$

$$Qsd = (3600 \text{ sec/hr})(1 - Bws)(Vs A) \left\{ \frac{Tstd Ps}{Ts Pstd} \right\} \\ = (3600)(1 - .0464)(67.5224)(52.3817) \left\{ \frac{(528)(29.902)}{(700)(29.92)} \right\} = 9151957.0 \text{ dscf/hr} \\ 152532.6 \text{ dscf/min}$$

## **METALS EMISSIONS per EPA METHOD 29**

During emission tests for the metals, lead and mercury samples were collected in sampling train combined with the moisture and flow rate sample train. Sample volume, etc. are recorded on test data sheets presented beginning on page 6.1.5.

A summary of the metals sample collection data and the emission concentration and emission rate calculations are presented on the following pages.

## METALS EMISSIONS per EPA METHOD 29

|      |                                                           |       |                                                           |
|------|-----------------------------------------------------------|-------|-----------------------------------------------------------|
| An   | - Cross-sectional area of sampler nozzle, ft <sup>2</sup> | St    | - Total sampling time, min                                |
| Bws  | - Stack gas moisture fraction, %/100                      | Tm    | - Average dry gas meter temperature, deg R                |
| Csi  | - Conc. of metals emissions, ug/dscf                      | Ts    | - Stack gas temperature, deg R                            |
| dH   | - Dry gas meter orifice press. diff., in-H <sub>2</sub> O | Tstd  | - Std. absolute temp, EPA, 528 R                          |
| Eri  | - Emission rate of metals emissions, lb/hr                | Vm    | - Volume of gas sample, actual dry ft <sup>3</sup>        |
| F1   | - Conversion factor, 2.2046 X 10 <sup>-9</sup> lb/ug      | Vmstd | - Sample vol, dry, std ft <sup>3</sup> , 68F, 29.92 in.Hg |
| I    | - Percent isokinetic, % of ideal sampling rate            |       |                                                           |
| Msi  | - Mass of metal detected in sample, ug                    |       |                                                           |
| Pbar | - Barometric press. at sampling site, in. Hg              | Vs    | - Stack gas velocity, ft/sec                              |
| Ps   | - Stack gas pressure, absolute, in. Hg                    | Y     | - Dry gas meter calibration factor                        |
| Pstd | - Standard absolute press., 29.92 in. Hg                  |       |                                                           |
| Qsd  | - Stack gas volumetric flow rate, dry ft <sup>3</sup> /hr |       |                                                           |

$$Vmstd = Vm Y \left\{ \frac{(Tstd)(Pbar + dH/13.6)}{(Tm)(Pstd)} \right\} = (34.467)(1.0309) \left\{ \frac{(528)(29.950 + .6969/13.6)}{(571)(29.92)} \right\} = 32.97250$$

$$I = \left\{ \frac{Ts Vmstd Pstd (100)}{Tstd Vs An St Ps (60)(1-Bws)} \right\} = \left\{ \frac{(701)(32.97250)(29.92)(100)}{(528)(66.3327)(.00015762)(72.00)(29.902) 60 (1 - .0408)} \right\} = 101.11$$

### ----- LEAD -----

$$Csi = (Msi / Vmstd) = (321.00 / 32.97250) = 9.7354$$

$$Eri = (Msi F1 Qsd) / (Vmstd) = [(321.00)(2.2046 \times 10^{-9})(9030603.0)] / (32.97250) = 1.19382$$

### ----- MERCURY -----

$$Csi = (Msi / Vmstd) = (2.21 / 32.97250) = 0.0670$$

$$Eri = (Msi F1 Qsd) / (Vmstd) = [(2.21)(2.2046 \times 10^{-9})(9030603.0)] / (32.97250) = 0.00133$$

## METALS EMISSIONS per EPA METHOD 29

|      |                                                           |       |                                                           |
|------|-----------------------------------------------------------|-------|-----------------------------------------------------------|
| An   | - Cross-sectional area of sampler nozzle, ft <sup>2</sup> | St    | - Total sampling time, min                                |
| Bws  | - Stack gas moisture fraction, %/100                      | Tm    | - Average dry gas meter temperature, deg R                |
| Csi  | - Conc. of metals emissions, ug/dscf                      | Is    | - Stack gas temperature, deg R                            |
| dH   | - Dry gas meter orifice press. diff., in-H <sub>2</sub> O | Tstd  | - Std. absolute temp, EPA, 528 R                          |
| Eri  | - Emission rate of metals emissions, lb/hr                | Vm    | - Volume of gas sample, actual dry ft <sup>3</sup>        |
| F1   | - Conversion factor, 2.2046 X 10 <sup>-9</sup> lb/ug      | Vmstd | - Sample vol, dry, std ft <sup>3</sup> , 68F, 29.92 in.Hg |
| I    | - Percent isokinetic, % of ideal sampling rate            |       |                                                           |
| Msi  | - Mass of metal detected in sample, ug                    | Vs    | - Stack gas velocity, ft/sec                              |
| Pbar | - Barometric press. at sampling site, in. Hg              | Y     | - Dry gas meter calibration factor                        |
| Ps   | - Stack gas pressure, absolute, in. Hg                    |       |                                                           |
| Pstd | - Standard absolute press., 29.92 in. Hg                  |       |                                                           |
| Qsd  | - Stack gas volumetric flow rate, dry ft <sup>3</sup> /hr |       |                                                           |

$$Vmstd = Vm Y \left\{ \frac{(Tstd)(Pbar + dH/13.6)}{(Tm)(Pstd)} \right\} = (35.150)(1.0309) \left\{ \frac{(528)(29.950 + .7188/13.6)}{(573)(29.92)} \right\} = 33.48462$$

$$I = \left\{ \frac{Ts Vmstd Pstd (100)}{Tstd Vs An St Ps (60)(1-Bws)} \right\} = \left\{ \frac{(701)(33.48462)(29.92)(100)}{(528)(66.4312)(.00015762)(72.00)(29.903)60(1-.0305)} \right\} = 101.35$$

### ----- LEAD -----

$$Csi = (Msi / Vmstd) = (357.00 / 33.48462) = 10.6616$$

$$Eri = (Msi F1 Qsd) / (Vmstd) = [(357.00)(2.2046 \times 10^{-9})(9149506.0)] / (33.48462) = 2.21506$$

### ----- MERCURY -----

$$Csi = (Msi / Vmstd) = (2.33 / 33.48462) = 0.0696$$

$$Eri = (Msi F1 Qsd) / (Vmstd) = [(2.33)(2.2046 \times 10^{-9})(9149506.0)] / (33.48462) = 0.00140$$

## METALS EMISSIONS per EPA METHOD 29

|      |                                                           |       |                                                           |
|------|-----------------------------------------------------------|-------|-----------------------------------------------------------|
| An   | - Cross-sectional area of sampler nozzle, ft <sup>2</sup> | St    | - Total sampling time, min                                |
| Bws  | - Stack gas moisture fraction, %/100                      | Tm    | - Average dry gas meter temperature, deg R                |
| Csi  | - Conc. of metals emissions, ug/dscf                      | Ts    | - Stack gas temperature, deg R                            |
| dH   | - Dry gas meter orifice press. diff., in-H <sub>2</sub> O | Tstd  | - Std. absolute temp, EPA, 528 R                          |
| Eri  | - Emission rate of metals emissions, lb/hr                | Vm    | - Volume of gas sample, actual dry ft <sup>3</sup>        |
| F1   | - Conversion factor, 2.2046 X 10 <sup>-9</sup> lb/ug      | Vmstd | - Sample vol, dry, std ft <sup>3</sup> , 68F, 29.92 in.Hg |
| I    | - Percent isokinetic, % of ideal sampling rate            |       |                                                           |
| Msi  | - Mass of metal detected in sample, ug                    | Vs    | - Stack gas velocity, ft/sec                              |
| Pbar | - Barometric press. at sampling site, in. Hg              | Y     | - Dry gas meter calibration factor                        |
| Ps   | - Stack gas pressure, absolute, in. Hg                    |       |                                                           |
| Pstd | - Standard absolute press., 29.92 in. Hg                  |       |                                                           |
| Qsd  | - Stack gas volumetric flow rate, dry ft <sup>3</sup> /hr |       |                                                           |

$$Vmstd = Vm Y \left\{ \frac{(Tstd)(Pbar + dH/13.6)}{(Tm)(Pstd)} \right\} = (35.225)(1.0309) \left\{ \frac{(528)(29.950 + .7381/13.6)}{(558)(29.92)} \right\} = 34.47912$$

$$I = \left\{ \frac{Ts Vmstd Pstd (100)}{Tstd Vs An St Ps (60)(1-Bws)} \right\} = \left\{ \frac{(700)(34.47912)(29.92)(100)}{(528)(67.5224)(.00015762)(72.00)(29.902) 60 (1 - .0464)} \right\} = 104.33$$

### ----- LEAD -----

$$Csi = (Msi / Vmstd) = (363.00 / 34.47912) = 10.5281$$

$$Eri = (Msi F1 Qsd) / (Vmstd) = [(363.00)(2.2046 \times 10^{-9})(9151957.0)] / (34.47912) = .21242$$

### ----- MERCURY -----

$$Csi = (Msi / Vmstd) = (6.58 / 34.47912) = .1908$$

$$Eri = (Msi F1 Qsd) / (Vmstd) = [(6.58)(2.2046 \times 10^{-9})(9151957.0)] / (32.97250) = .00403$$

## LABORATORY ANALYSES of METALS SAMPLES

During the emission tests, metals samples were collected in the probe wash, filter, and impinger samples. These samples were transported to Chemtex Environmental and Industrial Hygiene Services located in Port Arthur, Texas for analyses. A summary of analytical results are presented on the following page followed by the complete analytical report.

Chemtex Environmental and Industrial Hygiene Services is certified by the Louisiana Department of Environmental Quality (LDEQ) as a qualified environmental testing laboratory under the Louisiana Environmental Laboratory Accreditation Program (LELAP).

## Metals Analysis per EPA Method 29

Analytical Laboratory : Chemtex Environmental & Industrial Hygiene Services

Client Name : Bayou Steel  
Source Name : Baghouse Stack  
Run No. : 1

| HNO3 PROBE WASH                              |              |                     |              |                     |                                        | IMPINGERS 1 & 2, HNO3/H2O2 |                     |                    |                     |                                        |
|----------------------------------------------|--------------|---------------------|--------------|---------------------|----------------------------------------|----------------------------|---------------------|--------------------|---------------------|----------------------------------------|
| SAMPLE ID                                    | SAMPLE       |                     | BLANK        |                     | SAMPLE<br>Blank Corrected<br>ug/sample | SAMPLE                     |                     | BLANK              |                     | SAMPLE<br>Blank Corrected<br>ug/sample |
|                                              | VOLUME<br>ml | RESULT<br>mg/sample | VOLUME<br>ml | RESULT<br>mg/sample |                                        | VOLUME<br>ml               | RESULT<br>mg/sample | VOLUME<br>ml       | RESULT<br>mg/sample |                                        |
| Lead                                         | 170.00       | 0.172000            | 210.000      | < 0.011000          | 172.000                                | 274.00                     | < 0.014000          | 102.000            | < 0.005000          | < 14.000                               |
| Mercury                                      | 170.00       | 0.000187            | 210.000      | < 0.000210          | 0.187                                  | 274.00                     | < 0.000270          | 102.000            | < 0.000100          | < 0.270                                |
| IMPINGER 3, HNO3                             |              |                     |              |                     |                                        | IMPINGERS 4 & 5, KMnO4     |                     |                    |                     |                                        |
| SAMPLE ID                                    | SAMPLE       |                     | BLANK        |                     | SAMPLE<br>Blank Corrected<br>ug/sample | SAMPLE                     |                     | BLANK              |                     | SAMPLE<br>Blank Corrected<br>ug/sample |
|                                              | VOLUME<br>ml | RESULT<br>mg/sample | VOLUME<br>ml | RESULT<br>mg/sample |                                        | VOLUME<br>ml               | RESULT<br>mg/sample | VOLUME<br>ml       | RESULT<br>mg/sample |                                        |
| Lead                                         | 90.00        | < 0.005000          | 210.000      | < 0.011000          | < 5.000                                | 430.00                     | 0.022000            | 60.000             | < 0.005000          | 22.000                                 |
| Mercury                                      | 90.00        | < 0.000090          | 210.000      | < 0.000210          | < 0.090                                | 430.00                     | < 0.000430          | 60.000             | < 0.000060          | < 0.430                                |
| IMPINGERS 4 & 5, HCl RINSE                   |              |                     |              |                     |                                        | FILTERS                    |                     |                    |                     |                                        |
| SAMPLE ID                                    | SAMPLE       |                     | BLANK        |                     | SAMPLE<br>Blank Corrected<br>ug/sample | SAMPLE                     |                     | BLANK              |                     | SAMPLE<br>Blank Corrected<br>ug/sample |
|                                              | VOLUME<br>ml | RESULT<br>mg/sample | VOLUME<br>ml | RESULT<br>mg/sample |                                        | RESULT<br>ug/sample        |                     | CONC.<br>ug/sample |                     |                                        |
| Lead                                         | 234.00       | < 0.012000          | 105.000      | < 0.005000          | < 12.000                               | 96.00                      |                     | < 3.00             |                     | 96.00                                  |
| Mercury                                      | 234.00       | < 0.000230          | 105.000      | < 0.000110          | < 0.230                                | < 1.00                     |                     | < 1.00             |                     | < 1.00                                 |
| TOTAL SAMPLE<br>Blank Corrected<br>ug/sample |              |                     |              |                     |                                        |                            |                     |                    |                     |                                        |
| Lead                                         |              |                     |              |                     | 1321.00                                |                            |                     |                    |                     |                                        |
| Mercury                                      |              |                     |              |                     | 12.21                                  |                            |                     |                    |                     |                                        |

## Metals Analysis per EPA Method 29

Analytical Laboratory : Chemtex Environmental & Industrial Hygiene Services

Client Name : Bayou Steel  
Source Name : Baghouse Stack  
Run No. : 2

| SAMPLE ID | HNO3 PROBE WASH            |                     |              |                     |                                              | IMPINGERS 1 & 2, HNO3/H2O2 |                     |                    |                     |                                        |
|-----------|----------------------------|---------------------|--------------|---------------------|----------------------------------------------|----------------------------|---------------------|--------------------|---------------------|----------------------------------------|
|           | SAMPLE                     |                     | BLANK        |                     | SAMPLE<br>Blank Corrected<br>ug/sample       | SAMPLE                     |                     | BLANK              |                     | SAMPLE<br>Blank Corrected<br>ug/sample |
|           | VOLUME<br>ml               | RESULT<br>mg/sample | VOLUME<br>ml | RESULT<br>mg/sample |                                              | VOLUME<br>ml               | RESULT<br>mg/sample | VOLUME<br>ml       | RESULT<br>mg/sample |                                        |
| Lead      | 260.00                     | 0.213000            | 210.000      | < 0.011000          | 213.000                                      | 294.00                     | < 0.015000          | 102.000            | < 0.005000          | < 15.000                               |
| Mercury   | 260.00                     | 0.000290            | 210.000      | < 0.000210          | 0.290                                        | 294.00                     | < 0.000290          | 102.000            | < 0.000100          | < 0.290                                |
| SAMPLE ID | IMPINGER 3, HNO3           |                     |              |                     |                                              | IMPINGERS 4 & 5, KMnO4     |                     |                    |                     |                                        |
|           | SAMPLE                     |                     | BLANK        |                     | SAMPLE<br>Blank Corrected<br>ug/sample       | SAMPLE                     |                     | BLANK              |                     | SAMPLE<br>Blank Corrected<br>ug/sample |
|           | VOLUME<br>ml               | RESULT<br>mg/sample | VOLUME<br>ml | RESULT<br>mg/sample |                                              | VOLUME<br>ml               | RESULT<br>mg/sample | VOLUME<br>ml       | RESULT<br>mg/sample |                                        |
| Lead      | 90.00                      | < 0.005000          | 210.000      | < 0.011000          | < 5.000                                      | 430.00                     | 0.039000            | 60.000             | < 0.005000          | 39.000                                 |
| Mercury   | 90.00                      | < 0.000090          | 210.000      | < 0.000210          | < 0.090                                      | 430.00                     | < 0.000430          | 60.000             | < 0.000060          | < 0.430                                |
| SAMPLE ID | IMPINGERS 4 & 5, HCl RINSE |                     |              |                     |                                              | FILTERS                    |                     |                    |                     |                                        |
|           | SAMPLE                     |                     | BLANK        |                     | SAMPLE<br>Blank Corrected<br>ug/sample       | SAMPLE                     |                     | BLANK              |                     | SAMPLE<br>Blank Corrected<br>ug/sample |
|           | VOLUME<br>ml               | RESULT<br>mg/sample | VOLUME<br>ml | RESULT<br>mg/sample |                                              | RESULT<br>ug/sample        |                     | CONC.<br>ug/sample |                     |                                        |
| Lead      | 234.00                     | < 0.012000          | 105.000      | < 0.005000          | < 12.000                                     | 73.00                      |                     | < 3.00             |                     | 73.00                                  |
| Mercury   | 234.00                     | < 0.000230          | 105.000      | < 0.000110          | < 0.230                                      | < 1.00                     |                     | < 1.00             |                     | < 1.00                                 |
|           |                            |                     |              |                     | TOTAL SAMPLE<br>Blank Corrected<br>ug/sample |                            |                     |                    |                     |                                        |
| SAMPLE ID |                            |                     |              |                     |                                              |                            |                     |                    |                     |                                        |
| Lead      |                            |                     |              |                     | 1357.00                                      |                            |                     |                    |                     |                                        |
| Mercury   |                            |                     |              |                     | 12.33                                        |                            |                     |                    |                     |                                        |

## Metals Analysis per EPA Method 29

Analytical Laboratory : Chemtex Environmental & Industrial Hygiene Services

Client Name : Bayou Steel  
Source Name : Baghouse Stack  
Run No. : 3

| HNO3 PROBE WASH                              |              |                     |              |                     |                                        | IMPINGERS 1 & 2, HNO3/H2O2 |                     |                    |                     |                                        |
|----------------------------------------------|--------------|---------------------|--------------|---------------------|----------------------------------------|----------------------------|---------------------|--------------------|---------------------|----------------------------------------|
| SAMPLE ID                                    | SAMPLE       |                     | BLANK        |                     | SAMPLE<br>Blank Corrected<br>ug/sample | SAMPLE                     |                     | BLANK              |                     | SAMPLE<br>Blank Corrected<br>ug/sample |
|                                              | VOLUME<br>ml | RESULT<br>mg/sample | VOLUME<br>ml | RESULT<br>mg/sample |                                        | VOLUME<br>ml               | RESULT<br>mg/sample | VOLUME<br>ml       | RESULT<br>mg/sample |                                        |
| Lead                                         | 234.00       | 0.171000            | 210.000      | < 0.011000          | 171.000                                | 314.00                     | < 0.016000          | 102.000            | < 0.005000          | < 16.000                               |
| Mercury                                      | 234.00       | 0.004450            | 210.000      | < 0.000210          | 4.450                                  | 314.00                     | < 0.000310          | 102.000            | < 0.000100          | < 0.310                                |
| IMPINGER 3, HNO3                             |              |                     |              |                     |                                        | IMPINGERS 4 & 5, KMnO4     |                     |                    |                     |                                        |
| SAMPLE ID                                    | SAMPLE       |                     | BLANK        |                     | SAMPLE<br>Blank Corrected<br>ug/sample | SAMPLE                     |                     | BLANK              |                     | SAMPLE<br>Blank Corrected<br>ug/sample |
|                                              | VOLUME<br>ml | RESULT<br>mg/sample | VOLUME<br>ml | RESULT<br>mg/sample |                                        | VOLUME<br>ml               | RESULT<br>mg/sample | VOLUME<br>ml       | RESULT<br>mg/sample |                                        |
| Lead                                         | 105.00       | < 0.005000          | 210.000      | < 0.011000          | < 5.000                                | 470.00                     | 0.028000            | 60.000             | < 0.005000          | 28.000                                 |
| Mercury                                      | 105.00       | < 0.000110          | 210.000      | < 0.000210          | < 0.110                                | 470.00                     | < 0.000470          | 60.000             | < 0.000060          | < 0.470                                |
| IMPINGERS 4 & 5, HCl RINSE                   |              |                     |              |                     |                                        | FILTERS                    |                     |                    |                     |                                        |
| SAMPLE ID                                    | SAMPLE       |                     | BLANK        |                     | SAMPLE<br>Blank Corrected<br>ug/sample | SAMPLE                     |                     | BLANK              |                     | SAMPLE<br>Blank Corrected<br>ug/sample |
|                                              | VOLUME<br>ml | RESULT<br>mg/sample | VOLUME<br>ml | RESULT<br>mg/sample |                                        | RESULT<br>ug/sample        |                     | CONC.<br>ug/sample |                     |                                        |
| Lead                                         | 240.00       | < 0.012000          | 105.000      | < 0.005000          | < 12.000                               | 131.00                     |                     | < 3.00             |                     | 131.00                                 |
| Mercury                                      | 240.00       | < 0.000240          | 105.000      | < 0.000110          | < 0.240                                | < 1.00                     |                     | < 1.00             |                     | < 1.00                                 |
| TOTAL SAMPLE<br>Blank Corrected<br>ug/sample |              |                     |              |                     |                                        |                            |                     |                    |                     |                                        |
| Lead                                         |              |                     |              |                     | 1363.00                                |                            |                     |                    |                     |                                        |
| Mercury                                      |              |                     |              |                     | 16.58                                  |                            |                     |                    |                     |                                        |



Environmental & Industrial Hygiene Services

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138 S. Cities Service Hwy., Sulphur, Louisiana 70663 • (337) 626-2121 FAX (337) 626-0405

Client: **E T S**  
10461 Mammoth Dr.  
Baton Rouge, LA 70814

Report Date: 08/02/04  
Sample Matrix: Liquid  
Date Collected: 07/23/04  
Collected By: Ron McCabe  
Date Received: 07/25/04  
CHEMTEX FILE #: P4070973

Phone: (225) 925-8405; Fax (225) 925-2343

**AIHA** Laboratory # 101478

**NVLAP** Lab Code 200635-0

**nelap** certificate # 02077

RESULTS OF ANALYSIS  
CLIENT: Bayou Steel  
SOURCE: Baghouse Stack

| CHEMTEX<br># | Sample          | Parameter | Sampling         |           | Results |           | MDL  |  |
|--------------|-----------------|-----------|------------------|-----------|---------|-----------|------|--|
|              | Identification  |           | Volume<br>(mg/l) | mg/Sample | mg/l    | mg/Sample | mg/l |  |
| P4070973     | PW-R1           | Lead      | 170              | 0.172     | 1.01    | 0.009     | 0.05 |  |
| P4070974     | PW-R2           | Lead      | 260              | 0.213     | 0.82    | 0.013     | 0.05 |  |
| P4070975     | PW-R3           | Lead      | 234              | 0.171     | 0.73    | 0.012     | 0.05 |  |
| P4070976     | IMP 1&2-R1      | Lead      | 274              | < 0.014   | < 0.05  | 0.014     | 0.05 |  |
| P4070977     | IMP 1&2-R2      | Lead      | 294              | < 0.015   | < 0.05  | 0.015     | 0.05 |  |
| P4070978     | IMP 1&2-R3      | Lead      | 314              | < 0.016   | < 0.05  | 0.016     | 0.05 |  |
| P4070979     | IMP 3-R1        | Lead      | 90               | < 0.005   | < 0.05  | 0.005     | 0.05 |  |
| P4070980     | IMP 3-R2        | Lead      | 90               | < 0.005   | < 0.05  | 0.005     | 0.05 |  |
| P4070981     | IMP 3-R3        | Lead      | 105              | < 0.005   | < 0.05  | 0.005     | 0.05 |  |
| P4070982     | BLANK 0.1N HNO3 | Lead      | 210              | < 0.011   | < 0.05  | 0.011     | 0.05 |  |
| P4070983     | BLANK DI H2O    | Lead      | 184              | < 0.009   | < 0.05  | 0.009     | 0.05 |  |
| P4070984     | BLANK HNO3/H2O2 | Lead      | 102              | < 0.005   | < 0.05  | 0.005     | 0.05 |  |
| Method Blank | DI Water        | Lead      | ---              |           | < 0.05  | ---       | 0.05 |  |

MDL: Method Detection Limit

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138 S. Cities Service Hwy., Sulphur, Louisiana 70663 • (337) 626-2121 FAX (337) 626-0405

Client: **E T S**  
10461 Mammoth Dr.  
Baton Rouge, LA 70814

Report Date: 08/02/04  
Sample Matrix: Liquid  
Date Collected: 07/23/04  
Collected By: Ron McCabe  
Date Received: 07/25/04  
CHEMTEX FILE #: P4070973

Phone: (225) 925-8405; Fax (225) 925-2343

**AIHA** Laboratory # 101478

**NVLAP** Lab Code 200635-0

**nelap** certificate # 02077

RESULTS OF ANALYSIS  
CLIENT: Bayou Steel  
SOURCE: Baghouse Stack

| CHEMTEX<br># | Sample<br>Identification | Parameter | Sampling         | Results   |       | MDL       |      |
|--------------|--------------------------|-----------|------------------|-----------|-------|-----------|------|
|              |                          |           | Volume<br>(mg/l) | ug/Sample | ug/l  | ug/Sample | ug/l |
| P4070973     | PW-R1                    | Mercury   | 170              | 0.19      | 1.1   | 0.17      | 1.0  |
| P4070974     | PW-R2                    | Mercury   | 260              | 0.29      | 1.1   | 0.26      | 1.0  |
| P4070975     | PW-R3                    | Mercury   | 234              | 4.45      | 19.0  | 0.23      | 1.0  |
| P4070976     | IMP 1&2-R1               | Mercury   | 274              | < 0.27    | < 1.0 | 0.27      | 1.0  |
| P4070977     | IMP 1&2-R2               | Mercury   | 294              | < 0.29    | < 1.0 | 0.29      | 1.0  |
| P4070978     | IMP 1&2-R3               | Mercury   | 314              | < 0.31    | < 1.0 | 0.31      | 1.0  |
| P4070979     | IMP 3-R1                 | Mercury   | 90               | < 0.09    | < 1.0 | 0.09      | 1.0  |
| P4070980     | IMP 3-R2                 | Mercury   | 90               | < 0.09    | < 1.0 | 0.09      | 1.0  |
| P4070981     | IMP 3-R3                 | Mercury   | 105              | < 0.11    | < 1.0 | 0.11      | 1.0  |
| P4070982     | BLANK 0.1N HNO3          | Mercury   | 210              | < 0.21    | < 1.0 | 0.21      | 1.0  |
| P4070983     | BLANK DI H2O             | Mercury   | 184              | < 0.18    | < 1.0 | 0.18      | 1.0  |
| P4070984     | BLANK HNO3/H2O2          | Mercury   | 102              | < 0.10    | < 1.0 | 0.10      | 1.0  |
| Method Blank | DI Water                 | Mercury   | ---              | < 1.0     | ---   | ---       | 1.0  |

MDL: Method Detection Limit

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Client: **E T S**  
10461 Mammoth Dr.  
Baton Rouge, LA 70814

Report Date: 08/02/04

Phone: (225) 925-8405; Fax (225) 925-2343

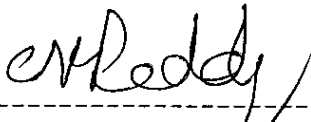
CHEMTEX FILE #: P4070973

LABORATORY QUALITY ASSURANCE/QUALITY CONTROL DATA

| <u>Parameter</u> | <u>Units</u> | <u>True Value</u> | <u>Obtained Value</u> | <u>% Recovery</u> |
|------------------|--------------|-------------------|-----------------------|-------------------|
| Total Lead       | mg/l         | 0.250             | 0.268/0.299*          | 105               |
| Total Mercury    | ug/l         | 5.0               | 4.8/4.8*              | 100               |

| <u>Parameter</u> | <u>Method Reference</u> | <u>Date Analyzed/Analysts</u> |
|------------------|-------------------------|-------------------------------|
| Total Lead       | EPA Method 29           | 07/29/04 MHVR/NR              |
| Total Mercury    | EPA Method 29           | 07/29/04 MHVR/NR              |

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-----  
**Dr. C. N. Reddy, Ph.D, CIH, ASP**  
**Director**

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Client: **E T S**  
10461 Mammoth Dr.  
Baton Rouge, LA 70814

Report Date: 08/02/04  
Sample Matrix: Liquid  
Date Collected: 07/23/04  
Collected By: Ron McCabe  
Date Received: 07/25/04  
CHEMTEX FILE #: P4070985

Phone: (225) 925-8405; Fax (225) 925-2343

**AIHA** Laboratory # 101478

**NVLAP** Lab Code 200635-0

**nelap** certificate # 02077

RESULTS OF ANALYSIS

CLIENT: Bayou Steel

SOURCE: Baghouse Stack

| CHEMTEX<br># | Sample                                | Parameter | Sampling<br>Volume |           | Results |           | MDL  |  |
|--------------|---------------------------------------|-----------|--------------------|-----------|---------|-----------|------|--|
|              | Identification                        |           | (mg/l)             | mg/Sample | mg/l    | mg/Sample | mg/l |  |
| P4070985     | IMP 4&5-R1                            | Lead      | 430                | < 0.022   | < 0.05  | 0.022     | 0.05 |  |
| P4070986     | IMP 4&5- <del>R1</del> <b>R2</b>      | Lead      | 430                | 0.039     | 0.09    | 0.022     | 0.05 |  |
| P4070987     | IMP 4&5- <del>R1</del> <b>R3</b>      | Lead      | 470                | 0.028     | 0.06    | 0.024     | 0.05 |  |
| P4070988     | IMP 4&5-R1-HCL                        | Lead      | 234                | < 0.012   | < 0.05  | 0.012     | 0.05 |  |
| P4070989     | IMP 4&5- <del>R1</del> <b>R2</b> -HCL | Lead      | 234                | < 0.012   | < 0.05  | 0.012     | 0.05 |  |
| P4070990     | IMP 4&5- <del>R1</del> <b>R3</b> -HCL | Lead      | 240                | < 0.012   | < 0.05  | 0.012     | 0.05 |  |
| P4070991     | BLANK KmnO4                           | Lead      | 60                 | 0.005     | 0.08    | 0.003     | 0.05 |  |
| P4070992     | BLANK 8 N HCL                         | Lead      | 105                | < 0.005   | < 0.05  | 0.005     | 0.05 |  |
| Method Blank | DI Water                              | Lead      | ---                | < 0.05    | ---     | ---       | 0.05 |  |

MDL: Method Detection Limit

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Client: **E T S**  
10461 Mammoth Dr.  
Baton Rouge, LA 70814

Report Date: 08/02/04  
Sample Matrix: Liquid  
Date Collected: 07/23/04  
Collected By: Ron McCabe  
Date Received: 07/25/04  
CHEMTEX FILE #: P4070985

Phone: (225) 925-8405; Fax (225) 925-2343

**AIHA** Laboratory # 101478

**NVLAP** Lab Code 200635-0

**nelap** certificate # 02077

RESULTS OF ANALYSIS

CLIENT: Bayou Steel

SOURCE: Baghouse Stack

| CHEMTEX<br># | Sample<br>Identification  | Parameter | Sampling<br>Volume<br>(mg/l) | Results   |       | MDL       |      |
|--------------|---------------------------|-----------|------------------------------|-----------|-------|-----------|------|
|              |                           |           |                              | ug/Sample | ug/l  | ug/Sample | ug/l |
| P4070985     | IMP 4&5-R1                | Mercury   | 430                          | < 0.43    | < 1.0 | 0.43      | 1.0  |
| P4070986     | IMP 4&5-R1 <b>R2</b>      | Mercury   | 430                          | < 0.43    | < 1.0 | 0.43      | 1.0  |
| P4070987     | IMP 4&5-R1 <b>R3</b>      | Mercury   | 470                          | < 0.47    | < 1.0 | 0.47      | 1.0  |
| P4070988     | IMP 4&5-R1-HCL            | Mercury   | 234                          | < 0.23    | < 1.0 | 0.23      | 1.0  |
| P4070989     | IMP 4&5-R1 <b>R2</b> -HCL | Mercury   | 234                          | < 0.23    | < 1.0 | 0.23      | 1.0  |
| P4070990     | IMP 4&5-R1 <b>R3</b> -HCL | Mercury   | 240                          | < 0.24    | < 1.0 | 0.24      | 1.0  |
| P4070991     | BLANK KmnO4               | Mercury   | 60                           | < 0.06    | < 1.0 | 0.06      | 1.0  |
| P4070992     | BLANK 8 N HCL             | Mercury   | 105                          | < 0.11    | < 1.0 | 0.11      | 1.0  |
| Method Blank | DI Water                  | Mercury   | Blank                        | < 1.0     | ---   | ---       | 1.0  |

MDL: Method Detection Limit

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138 S. Cities Service Hwy., Sulphur, Louisiana 70663 • (337) 626-2121 FAX (337) 626-0405

Client: **E T S**  
10461 Mammoth Dr.  
Baton Rouge, LA 70814

Report Date: 08/02/04

Phone: (225) 925-8405; Fax (225) 925-2343

CHEMTEX FILE #: P4070985

LABORATORY QUALITY ASSURANCE/QUALITY CONTROL DATA

| <u>Parameter</u> | <u>Units</u> | <u>True Value</u> | <u>Obtained Value</u> | <u>% Recovery</u> |
|------------------|--------------|-------------------|-----------------------|-------------------|
| Total Lead       | mg/l         | 0.250             | 0.268/0.299*          | 105               |
| Total Mercury    | ug/l         | 5.0               | 4.8/4.8*              | 100               |

| <u>Parameter</u> | <u>Method Reference</u> | <u>Date Analyzed/Analysts</u> |
|------------------|-------------------------|-------------------------------|
| Total Lead       | EPA Method 29           | 07/29/04 MHVR/NR              |
| Total Mercury    | EPA Method 29           | 07/29/04 MHVR/NR              |

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138 S. Cities Service Hwy., Sulphur, Louisiana 70663 • (337) 626-2121 FAX (337) 626-0405

Client: **E T S**  
10461 Mammoth Dr.  
Baton Rouge, LA 70814

Report Date: 07/30/04  
Sample Matrix: Quartz  
Date Collected: 07/23/04  
Collected By: Ron McCabe  
Date Received: 07/25/04  
CHEMTEX FILE #: P4070993

Phone: (225) 925-8405; Fax (225) 925-2343

**AIHA** Laboratory # 101478

**NVLAP** Lab Code 200635-0

**nelap** certificate # 02077

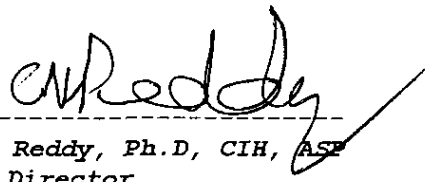
RESULTS OF ANALYSIS  
CLIENT: Bayou Steel  
SOURCE: Baghouse Stack

| CHEMTEX #    | Sample ID.   | Parameter     | Result (ug/sample) | MDL (ug/sample) |
|--------------|--------------|---------------|--------------------|-----------------|
| P4070993     | Filter-R1    | Total Lead    | 96.0               | 3.0             |
|              |              | Total Mercury | < 1.0              | 1.0             |
| P4070994     | Filter-R2    | Total Lead    | 73.0               | 3.0             |
|              |              | Total Mercury | < 1.0              | 1.0             |
| P4070995     | Filter-R3    | Total Lead    | 131.0              | 3.0             |
|              |              | Total Mercury | < 1.0              | 1.0             |
| P4070996     | Blank Filter | Total Lead    | < 3.0              | 3.0             |
|              |              | Total Mercury | < 1.0              | 1.0             |
| Method Blank | Blank Filter | Total Lead    | < 3.0              | 3.0             |
|              |              | Total Mercury | < 1.0              | 1.0             |

LABORATORY QUALITY ASSURANCE/QUALITY CONTROL DATA

| Parameter     | Units | True Value | Obtained Value |
|---------------|-------|------------|----------------|
| Total Lead    | ug/l  | 250        | 268/302*       |
| Total Mercury | ug/l  | 5.0        | 4.8/4.8*       |

| Parameter     | Method Reference | Date Analyzed/Analysts |
|---------------|------------------|------------------------|
| Total Lead    | EPA Method 29    | 07/29/04 MHVR/NR       |
| Total Mercury | EPA Method 29    | 07/29/04 MHVR/NR       |

  
Dr. C. N. Reddy, Ph.D, CIH, ASE  
Director

bmb/CNR

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## UNIT OPERATING DATA

During the emission tests, unit operating data were recorded by Bayou Steel. These data are presented on the following pages.



# Bayou Steel Corporation

## Scrap Blend Procedure

Blend #65 3-Buckets

Heat# 27245

Date 7-22-04

Turn C

Oper Cowdy

Foreman Deck

| Header |               | Alm  | Sub  | Weights |        |             |
|--------|---------------|------|------|---------|--------|-------------|
| Layer  | Description   | Code | Code | Alm     | Actual | Deviation % |
| 1      | Bushling      | 16   |      | 0       |        | 0%          |
| 2      | Home Plt      | 12   |      | 7000    | 8      | 9%          |
| 3      | #2 Bundles    | 5    |      | 5000    | 5      | 6%          |
| 4      | Turnings      | 1    |      | 12000   | 16     | 16%         |
|        | Barge / Plate | 1    |      | 17000   | 13     | 22%         |
|        | #1 Heavy      | 7    |      | 13000   | 15     | 17%         |
|        | Mixed 1&2     | 11   |      | 8000    | 20     | 10%         |
|        |               |      |      |         |        | 0%          |
| 6      | Shredded      | 10   |      | 15000   | 20     | 19%         |
| Total  |               |      |      | 77000   | 99     |             |

| First BackChg |               | Alm  | Sub  | Weights |        |             |
|---------------|---------------|------|------|---------|--------|-------------|
| Layer         | Description   | Code | Code | Alm     | Actual | Deviation % |
| 1             | Bushling      | 16   |      | 2000    |        | 3%          |
| 2             | Turnings      |      |      | 10000   | 8      | 15%         |
| 3             | Barge / Plate | 1    |      | 14000   | 5      | 22%         |
|               | #1 Heavy      | 1    |      | 16000   | 17     | 25%         |
|               | Mixed 1&2     | 7    |      | 8000    | 13     | 12%         |
|               |               |      |      |         |        | 0%          |
|               |               |      |      |         |        | 0%          |
| 5             | Shredded      | 10   |      | 15000   | 14     | 23%         |
| Total         |               |      |      | 65000   | 86     |             |

| Second BackChg |             | Alm  | Sub  | Weights |        |             |
|----------------|-------------|------|------|---------|--------|-------------|
| Layer          | Description | Code | Code | Alm     | Actual | Deviation % |
| 1              | Mixed 1&2   | 7    |      | 14000   | 15     | 42%         |
|                | Turnings    | 11   |      | 8000    |        | 9%          |
|                | Mill Crop   | 15   |      | 3000    | 5      | 12%         |
|                | #1 Heavy    | 1    |      | 4000    | 10     | 24%         |
|                | Shredded    |      |      | 4000    | 5      |             |
| Total          |             |      |      | 33000   | 35     |             |

150



# Bayou Steel Corporation

## Heat Record

Crew: C  
Date: 7/23/04  
Grade: A36 F60

Melter: Duck  
1st Helper: Wayne  
Ladleman: Tebe

Heat #: 27246

Pulse Counter  
1st Charge 7/26 096  
Last Charge 7/29 187

Tap To Tap Time 64

Lost Time EQUALS Lost \$MONEY\$ !!!!!!!!!!!

| Electrodes |     |     |
|------------|-----|-----|
| Ad         | Slp | Brk |
| A          |     |     |
| B          |     |     |
| C          |     |     |

| Previous Heat Tap                |       |                   |
|----------------------------------|-------|-------------------|
| PON                              | POFF  | kWh/ton           |
| Headr                            | 9:05  | 916 (220)         |
| 1 Back                           | 9:18  | 926 (220)         |
| 2 Back                           | 9:28  |                   |
| 3 Back                           |       |                   |
| Tap Start: 9:52 Tap Finish: 9:55 |       |                   |
| Power On                         | 37.7  | LMF               |
| kWh                              | 29810 | kWh               |
| kWh/Ton                          | 321   | kWh/Ton           |
| Plan                             | (360) | Plan (25)         |
| Ladle Data                       |       |                   |
| Ladle No.                        | 10    | # Hits Pig 5      |
| Heats                            | 6     | Sur OK            |
| Temp                             |       |                   |
| Temperature Data                 |       |                   |
| Time                             | kWh   | Temp Carbon O2ppm |
| 1                                |       | 2989 12           |
| 2                                |       |                   |
| 3                                |       |                   |
| 4                                |       |                   |
| Ldl                              |       |                   |

| EAF Additions   |          | Ladle Additions |         |
|-----------------|----------|-----------------|---------|
| Pas             |          | Tap             | Trim    |
| Lime            | 5000     | SiMn            | 1675    |
| MgO             | 1500     | FeSi            | 325     |
| Chg C           |          | FeMn            |         |
| Foamy           | 2667     | Coke            |         |
| Oxgyn           | 996      | BPI             |         |
| N Gas           | 207      | Lime            | 800     |
|                 |          | De-Sul          |         |
|                 |          | FeV             |         |
|                 |          | FeAl            |         |
|                 |          | CaC             | 50      |
|                 |          | SIC             | 100     |
|                 |          | CAI             | 200     |
| Sampling Data   |          |                 |         |
| Material        | Location |                 |         |
| Amount          |          |                 |         |
| Scan Compliance |          |                 |         |
| Charge          | Header   | 1st Bck         | 2nd Bck |
| Deviation       |          |                 |         |
|                 |          |                 | TOTAL   |

Never Be Satisfied Always a Better Way

| Process Weights |          |           |
|-----------------|----------|-----------|
| Charge lbs      | Tap Tons | Cast Tons |
| 190,000         | 84       |           |

| Ladle Sent To |         |
|---------------|---------|
| To LMF        | St to C |
| ✓             |         |

| Chemistries |       |       |    |    |       |    |    |    |    |    |   |
|-------------|-------|-------|----|----|-------|----|----|----|----|----|---|
|             | C     | Mn    | P  | S  | Si    | Cu | Ni | Cr | Mo | Sn | V |
| Alm         | 13/10 | 74/55 | 40 | 50 | 18/26 | 59 |    |    |    |    |   |
| P/n         |       |       |    |    |       |    |    |    |    |    |   |

### Procedure Compliance Summary

|                   | Gol | Act | Dev | Reason         | (Use Delay Code & Description) |
|-------------------|-----|-----|-----|----------------|--------------------------------|
| Tap               | 3   | 3   |     |                |                                |
| Turn Around       | 2   | 4   | 2   | A1-8           |                                |
| Power On          | 11  | 11  |     |                |                                |
| First BackCharge  | 2   | 2   |     |                |                                |
| Power On          | 8   | 8   |     |                |                                |
| Second BackCharge | 2   |     |     |                |                                |
| Power On          | 6   |     |     |                |                                |
| Third Back Charge | 0   |     |     | A1-2 9:50-9:52 |                                |
| Power On          | 0   |     |     |                |                                |
| Refine            | 11  |     |     |                |                                |
| Total             | 45  |     |     |                |                                |

Action Items:

Maintenance Barriers:

9434 1st Test (6.5.00)

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# Bayou Steel Corporation

## Scrap Blend Procedure

nd #65 3-Buckets

Mat# 37246

Date 7-22

Turn C

per Sanborn

Foreman Dick

| Header |               | Aim  |  | Sub  |       | Weights |             |
|--------|---------------|------|--|------|-------|---------|-------------|
| Layer  | Description   | Code |  | Code | Aim   | Actual  | Deviation % |
| 1      | Bushling      | 16   |  |      | 0     |         | 0%          |
| 2      | Home Pit      | 12   |  |      | 7000  |         | 9%          |
| 3      | #2 Bundles    | 5    |  |      | 5000  | 5       | 6%          |
| 4      | Turnings      | 1    |  |      | 12000 | 15      | 16%         |
|        | Barge / Plate | 1    |  |      | 17000 | 20      | 22%         |
|        | #1 Heavy      | 7    |  |      | 13000 | 20      | 17%         |
|        | Mixed 1&2     | 11   |  |      | 8000  | 20      | 10%         |
|        |               |      |  |      |       |         | 0%          |
| 6      | Shredded      | 10   |  |      | 15000 | 20      | 19%         |
| Total  |               |      |  |      | 77000 | 90      |             |

| First BackChg |               | Aim  |  | Sub  |       | Weights |             |
|---------------|---------------|------|--|------|-------|---------|-------------|
| Layer         | Description   | Code |  | Code | Aim   | Actual  | Deviation % |
| 1             | Bushling      | 16   |  |      | 2000  |         | 3%          |
| 2             | Turnings      |      |  |      | 10000 |         | 15%         |
| 3             | Barge / Plate | 1    |  |      | 14000 | 10      | 22%         |
|               | #1 Heavy      | 1    |  |      | 16000 | 20      | 25%         |
|               | Mixed 1&2     | 7    |  |      | 8000  | 10      | 12%         |
|               |               |      |  |      |       |         | 0%          |
|               |               |      |  |      |       |         | 0%          |
| 5             | Shredded      | 10   |  |      | 15000 | 20      | 23%         |
| Total         |               |      |  |      | 65000 | 60      |             |

| Second BackChg |             | Aim  |  | Sub  |       | Weights |             |
|----------------|-------------|------|--|------|-------|---------|-------------|
| Layer          | Description | Code |  | Code | Aim   | Actual  | Deviation % |
| 1              | Mixed 1&2   | 7    |  |      | 14000 | 20      | 42%         |
|                | Turnings    | 11   |  |      | 8000  | 10      | 9%          |
|                | Mill Crop   | 15   |  |      | 3000  |         | 12%         |
|                | #1 Heavy    | 1    |  |      | 4000  | 5       | 24%         |
|                | Shredded    |      |  |      | 4000  | 5       |             |
| Total          |             |      |  |      | 33000 | 40      |             |

190



# Bayou Steel Corporation

## Heat Record

Crew: C  
Date: 7/23/04  
Grade: A3644w

Melter: Duck  
1st Helper: Wayne  
Ladleman: T46

Heat #: 27247

Pulse Counter  
1st Charge 7129187  
Last Charge 7132630

Tap To Tap Time 54

Lost Time EQUALS Lost \$MONEY\$ !!!!!!!!!!!

| Electrodes |  |  |
|------------|--|--|
| Ad-Slp Brk |  |  |
| A          |  |  |
| B          |  |  |
| C          |  |  |

|                                                |              |                       |
|------------------------------------------------|--------------|-----------------------|
| Previous Heat Tap <u>9:52</u>                  |              |                       |
|                                                | PON          | POFF kWh/ton          |
| Headr                                          | <u>10:00</u> | <u>10:11</u> (220)    |
| 1 Back                                         | <u>10:13</u> | <u>10:22</u> (220)    |
| 2 Back                                         | <u>10:24</u> |                       |
| 3 Back                                         |              |                       |
| Tap Start <u>10:46</u> Tap Finish <u>10:49</u> |              |                       |
| Power On                                       | <u>40.2</u>  | LME                   |
| kWh                                            | <u>32100</u> | kWh                   |
| kWh/Ton                                        | <u>345</u>   | kWh/Ton               |
| Plan                                           | <u>(360)</u> | Plan <u>(25)</u>      |
| Ladle Data                                     |              |                       |
| Ladle No                                       | <u>8</u>     | # Hts Plg <u>1</u>    |
| Heats                                          | <u>45</u>    | Str OK                |
| Temp                                           |              |                       |
| Temperature Data (250) (1000-140)              |              |                       |
| Time                                           | kWh          | Temp Carbon O2ppm     |
| 1                                              |              | <u>3026</u> <u>11</u> |
| 2                                              |              | <u>3100</u>           |
| 3                                              |              |                       |
| 4                                              |              |                       |
| Ldl                                            |              |                       |

|                  |             |                 |                       |
|------------------|-------------|-----------------|-----------------------|
| FAR Addition     |             | Ladle Additions |                       |
|                  | Tap         | Tap             | Trim                  |
| Lime             | <u>5000</u> | SiMn            | <u>1675</u>           |
| MgO              | <u>1800</u> | FeSi            | <u>330</u>            |
| Chg C            |             | FeMn            |                       |
| Foamy            | <u>3057</u> | Coke            | <u>50</u>             |
| Oxygen           | <u>1067</u> | BPI             |                       |
| N Gas            | <u>215</u>  | Lime            | <u>800</u>            |
|                  |             | De-Sul          |                       |
|                  |             | FeV             |                       |
|                  |             | FeAl            |                       |
|                  |             | CaC             | <u>50</u>             |
|                  |             | SiC             | <u>100</u>            |
|                  |             | QAL             | <u>200</u>            |
| Gonning Data     |             |                 |                       |
| Material         | Location    |                 |                       |
| Amount           |             |                 |                       |
| Scrap Compliance |             |                 |                       |
| Charge           | Header      | 1st Bck         | 2nd Bck 3rd Bck TOTAL |
| Deviation        |             |                 |                       |

Never Be Satisfied Always a Better Way

|                 |           |           |
|-----------------|-----------|-----------|
| Process Weights |           |           |
| Charge lbs      | Tap Tons  | Cast Tons |
| <u>190,000</u>  | <u>83</u> |           |

|                                     |         |
|-------------------------------------|---------|
| Ladle Sent To                       |         |
| To LMF                              | St to C |
| <input checked="" type="checkbox"/> |         |

| Chemistries |              |              |           |           |              |           |    |    |    |    |   |
|-------------|--------------|--------------|-----------|-----------|--------------|-----------|----|----|----|----|---|
|             | C            | Mn           | P         | S         | Si           | Cu        | Ni | Cr | Mo | Sn | V |
| Arm Pin     | <u>13/18</u> | <u>70/85</u> | <u>40</u> | <u>50</u> | <u>18/26</u> | <u>59</u> |    |    |    |    |   |

### Procedure Compliance Summary

|                   | Go! | Act | Dev | Reason (Use Delay Code & Description) |
|-------------------|-----|-----|-----|---------------------------------------|
| Tap               | 3   | 9   |     |                                       |
| Turn Around       | 2   | 5   | 3   | <u>A1-3</u>                           |
| Power On          | 11  | 11  |     |                                       |
| First BackCharge  | 2   | 2   |     |                                       |
| Power On          | 8   | 9   | 1   | <u>A4-6</u>                           |
| Second BackCharge | 2   | 2   |     |                                       |
| Power On          | 6   |     |     |                                       |
| Third Back Charge | 0   |     |     |                                       |
| Power On          | 0   |     |     |                                       |
| Refine            | 11  |     |     |                                       |
| Total             | 45  |     |     |                                       |

Action Items:

Maintenance Barriers:

Record  
247

# Bayou Steel Corporation Scrap Blend Procedure

Blend #65 3-Bunkate

Heat# 27247

Date 7-22

Turn C

Oper Cowb

Foreman ARK

## Header

| Layer | Description   | Aim Code | Sub Code | Aim   | Actual | Deviation | %   |
|-------|---------------|----------|----------|-------|--------|-----------|-----|
| 1     | Bushling      | 16       |          | 0     |        |           | 0%  |
| 2     | Home Pit      | 12       |          | 7000  |        |           | 9%  |
| 3     | #2 Bundles    | 5        |          | 5000  |        |           | 6%  |
| 4     | Turnings      | 1        |          | 12000 | 5      |           | 16% |
|       | Barge / Plate | 1        |          | 17000 | 20     |           | 22% |
|       | #1 Heavy      | 7        |          | 13000 | 20     |           | 17% |
|       | Mixed 1&2     | 11       |          | 8000  | 20     |           | 10% |
|       |               |          |          |       |        |           | 0%  |
| 6     | Shredded      | 10       |          | 15000 | 20     |           | 19% |
| Total |               |          |          | 77000 | 95     |           |     |

## First BackChg

| Layer | Description   | Aim Code | Sub Code | Aim   | Actual | Deviation | %   |
|-------|---------------|----------|----------|-------|--------|-----------|-----|
| 1     | Bushling      | 16       |          | 2000  |        |           | 3%  |
| 2     | Turnings      |          |          | 10000 | 10     |           | 15% |
| 3     | Barge / Plate | 1        |          | 14000 | 10     |           | 22% |
|       | #1 Heavy      | 1        |          | 16000 | 10     |           | 25% |
|       | Mixed 1&2     | 7        |          | 8000  | 10     |           | 12% |
|       |               |          |          |       |        |           | 0%  |
|       |               |          |          |       |        |           | 0%  |
| 5     | Shredded      | 10       |          | 15000 | 14     |           | 23% |
| Total |               |          |          | 65000 | 54     |           |     |

## Second BackChg

| Layer | Description | Aim Code | Sub Code | Aim   | Actual | Deviation | %   |
|-------|-------------|----------|----------|-------|--------|-----------|-----|
| 1     | Mixed 1&2   | 7        |          | 14000 | 20     |           | 42% |
|       | Turnings    | 11       |          | 8000  | 10     |           | 9%  |
|       | Mill Crop   | 15       |          | 3000  |        |           | 12% |
|       | #1 Heavy    | 1        |          | 4000  | 5      |           | 24% |
|       | Shredded    |          |          | 4000  | 5      |           |     |
| Total |             |          |          | 33000 | 41     |           |     |

190



# Bayou Steel Corporation

## Heat Record

Crew: CMelter: DuckDate: 7-23-041st Helper: WSGrade: A36-44WLadleman: JBHeat #: 27248**Pulse Counter**1st Charge 7/29/07Last Charge 7/30/07Tap To Tap Time 53

Lost Time EQUALS Lost \$MONEY\$ !!!!!!!!!!!

Electrodes

Ad Slp Brk

|   |  |  |
|---|--|--|
| A |  |  |
| B |  |  |
| C |  |  |

Previous Heat Tap 10:46

|        | PON          | POFF         | kWh/ton |
|--------|--------------|--------------|---------|
| Headr  | <u>10:53</u> | <u>11:04</u> | (220)   |
| 1 Back | <u>11:08</u> | <u>11:15</u> | (220)   |
| 2 Back | <u>11:11</u> |              |         |
| 3 Back |              |              |         |

Tap Start 11:39 Tap Finish 11:42Power On 37.2 LMFkWh 29040 kWhkWh/Ton 310 kWh/TonPlan (360) Plan (25)Ladle Data 7 Stir InfoLadle No 7 # Hts Plg 42Heats 89 Stir OK

Temp

Temperature Data (2900) (1000-110)

|     | Time | kWh | Temp        | Carbon    | O2ppm |
|-----|------|-----|-------------|-----------|-------|
| 1   |      |     | <u>3200</u> | <u>12</u> |       |
| 2   |      |     |             |           |       |
| 3   |      |     |             |           |       |
| 4   |      |     |             |           |       |
| Ldl |      |     |             |           |       |

| FAR Additions |             | Ladle Additions |             |
|---------------|-------------|-----------------|-------------|
| Fls           | Tap         | Trim            |             |
| Lime          | <u>5000</u> | SiMn            | <u>1678</u> |
| MgO           | <u>1300</u> | FeSi            | <u>325</u>  |
| Chg C         |             | FeMn            |             |
| Foamy         | <u>2618</u> | Coke            | <u>50</u>   |
| Oxygen        | <u>971</u>  | BPI             |             |
| N Gas         | <u>308</u>  | Lime            | <u>800</u>  |
|               |             | De-Sul          |             |
|               |             | FeV             |             |
|               |             | FeAl            |             |
|               |             | CaC             | <u>50</u>   |
|               |             | SiC             | <u>100</u>  |
|               |             | GAH             | <u>200</u>  |

| Ginning Data |          |
|--------------|----------|
| Material     | Location |
| Amount       |          |

| Scrap Compliance |        |         |         |         |
|------------------|--------|---------|---------|---------|
| Charge           | Header | 1st Bck | 2nd Bck | 3rd Bck |
| Deviation        |        |         |         |         |

Never Be Satisfied Always a Better Way

| Process Weights |            |           |
|-----------------|------------|-----------|
| Charge lbs      | Tap Tons   | Cast Tons |
| <u>185,000</u>  | <u>8.6</u> |           |

| Ladle Sent To                       |         |
|-------------------------------------|---------|
| To LMF                              | St to C |
| <input checked="" type="checkbox"/> |         |

**Chemistries**

|         | C            | Mn           | P         | S         | Si           | Cu        | Ni | Cr | Mo | Sn | V |
|---------|--------------|--------------|-----------|-----------|--------------|-----------|----|----|----|----|---|
| Alm Pin | <u>13/17</u> | <u>70/85</u> | <u>40</u> | <u>60</u> | <u>12/26</u> | <u>59</u> |    |    |    |    |   |

**Procedure Compliance Summary**

|                   | Gol | Act | Dev | Reason | (Use Delay Code & Description) |
|-------------------|-----|-----|-----|--------|--------------------------------|
| Tap               | 3   | 3   |     |        |                                |
| Turn Around       | 2   | 4   | 2   | A1-B   |                                |
| Power On          | 11  | 11  |     |        |                                |
| First BackCharge  | 2   | 4   | 2   | A4-L   |                                |
| Power On          | 8   | 7   |     |        |                                |
| Second BackCharge | 2   | 2   |     |        |                                |
| Power On          | 6   |     |     |        |                                |
| Third Back Charge | 0   |     |     |        |                                |
| Power On          | 0   |     |     |        |                                |
| Refine            | 11  |     |     |        |                                |
| Total             | 45  |     |     |        |                                |

Action Items:

Maintenance Barriers:

# Bayou Steel Corporation

## Scrap Blend Procedure

Blend #65 3-Buckets

Heat# 27248

Date 7-22-08

Turn C

Oper Low So

Foreman Pink

### Header

| Layer | Description   | Alm Code | Sub Code | Weights |        |           |     |
|-------|---------------|----------|----------|---------|--------|-----------|-----|
|       |               |          |          | Alm     | Actual | Deviation | %   |
| 1     | Bushling      | 16       |          | 0       |        |           | 0%  |
| 2     | Home Pit      | 12       |          | 7000    |        |           | 9%  |
| 3     | #2 Bundles    | 5        |          | 5000    | 5      |           | 6%  |
| 4     | Turnings      | 1        |          | 12000   | 11     |           | 16% |
|       | Barge / Plate | 1        |          | 17000   | 13     |           | 22% |
|       | #1 Heavy      | 7        |          | 13000   | 15     |           | 17% |
|       | Mixed 1&2     | 11       |          | 8000    | 20     |           | 10% |
|       |               |          |          |         |        |           | 0%  |
| 6     | Shredded      | 10       |          | 15000   | 20     |           | 19% |
| Total |               |          |          | 77000   | 86     |           |     |

### First BackChg

| Layer | Description   | Alm Code | Sub Code | Weights |        |           |     |
|-------|---------------|----------|----------|---------|--------|-----------|-----|
|       |               |          |          | Alm     | Actual | Deviation | %   |
| 1     | Bushling      | 16       |          | 2000    |        |           | 3%  |
| 2     | Turnings      |          |          | 10000   | 15     |           | 15% |
| 3     | Barge / Plate | 1        |          | 14000   | 8      |           | 22% |
|       | #1 Heavy      | 1        |          | 16000   | 15     |           | 25% |
|       | Mixed 1&2     | 7        |          | 8000    | 15     |           | 12% |
|       |               |          |          |         |        |           | 0%  |
|       |               |          |          |         |        |           | 0%  |
| 5     | Shredded      | 10       |          | 15000   | 20     |           | 23% |
| Total |               |          |          | 65000   | 73     |           |     |

### Second BackChg

| Layer | Description | Alm Code | Sub Code | Weights |        |           |     |
|-------|-------------|----------|----------|---------|--------|-----------|-----|
|       |             |          |          | Alm     | Actual | Deviation | %   |
| 1     | Mixed 1&2   | 7        |          | 14000   | 20     |           | 42% |
|       | Turnings    | 11       |          | 8000    | 8      |           | 8%  |
|       | Mill Crop   | 15       |          | 3000    |        |           | 12% |
|       | #1 Heavy    | 1        |          | 4000    |        |           | 24% |
|       | Shredded    |          |          | 4000    |        |           |     |
| Total |             |          |          | 33000   | 26     |           |     |



# Bayou Steel Corporation

## Heat Record

Crew: CDate: 7-23-04Grade: A36Melter: Auek1st Helper: WSLadleman: JBHeat #: 27249**Pulse Counter**1st Charge 7135551Last Charge 7138666Tap To Tap Time 55

Lost Time EQUALS Lost \$MONEY\$ !!!!!!!!!!!

| Electrodes |     |     |
|------------|-----|-----|
| Ad         | Slp | Brk |
| A          |     |     |
| B          |     |     |
| C          |     |     |

| Previous Heat Tap <u>11:39</u> |              |                    |
|--------------------------------|--------------|--------------------|
|                                | PON          | POFF kWh/ton       |
| Headr                          | <u>11:50</u> | <u>12:01</u> (220) |
| 1 Back                         | <u>12:03</u> | <u>12:13</u> (220) |
| 2 Back                         | <u>12:15</u> |                    |
| 3 Back                         |              |                    |

|           |              |            |              |
|-----------|--------------|------------|--------------|
| Tap Start | <u>12:39</u> | Tap Finish | <u>12:32</u> |
| Power On  | <u>38.4</u>  | LME        |              |
| kWh       | <u>29670</u> | kWh        |              |
| kWh/Ton   | <u>316</u>   | kWh/Ton    |              |
| Plan      | (360)        | Plan       | (25)         |

| Ladle Data |           | Stir Info  |           |
|------------|-----------|------------|-----------|
| Ladle No   | <u>5</u>  | # Hits Pig | <u>10</u> |
| Heats      | <u>10</u> | Stir OK    |           |
| Temp       |           |            |           |

| Temperature Data (2950) (0.02-0.10) |     |             |              |
|-------------------------------------|-----|-------------|--------------|
| Time                                | kWh | Temp        | Carbon O2ppm |
| 1                                   |     | <u>3040</u> | <u>12</u>    |
| 2                                   |     |             |              |
| 3                                   |     |             |              |
| 4                                   |     |             |              |
| Ldl                                 |     |             |              |

| FAB Additions |              | Ladle Additions |             |
|---------------|--------------|-----------------|-------------|
|               | Pas          | Tap             | Trim        |
| Lime          | <u>5000</u>  | SiMn            | <u>1665</u> |
| MgO           | <u>1300</u>  | FeSi            | <u>330</u>  |
| Chg C         |              | FeMn            |             |
| Foamy         | <u>26.97</u> | Coke            |             |
| Oxygn         | <u>1010</u>  | BPI             |             |
| N Gas         | <u>208</u>   | Lime            | <u>800</u>  |
|               |              | De-Sul          |             |
|               |              | FeV             |             |
|               |              | FeAl            |             |
|               |              | CaC             | <u>50</u>   |
|               |              | SiC             | <u>100</u>  |
|               |              | GA1             | <u>200</u>  |

| Gunning Data     |        |          |         |         |
|------------------|--------|----------|---------|---------|
| Material         |        | Location |         |         |
| Amount           |        |          |         |         |
| Scrap Compliance |        |          |         |         |
| Charge           | Header | 1st Bck  | 2nd Bck | 3rd Bck |
| Deviation        |        |          |         |         |

Never Be Satisfied Always a Better Way

| Process Weights |           |           |
|-----------------|-----------|-----------|
| Charge lbs      | Tap Tons  | Cast Tons |
| <u>180,000</u>  | <u>81</u> |           |

| Ladle Sent To                       |         |
|-------------------------------------|---------|
| To LMF                              | St to C |
| <input checked="" type="checkbox"/> |         |

| Chemistries |             |              |           |           |              |           |    |    |    |    |   |
|-------------|-------------|--------------|-----------|-----------|--------------|-----------|----|----|----|----|---|
|             | C           | Mn           | P         | S         | Si           | Cu        | Ni | Cr | Mo | Sn | V |
| Alm Pin     | <u>8/13</u> | <u>70/85</u> | <u>40</u> | <u>50</u> | <u>18/26</u> | <u>80</u> |    |    |    |    |   |

**Procedure Compliance Summary**

|                   | Gol | Act | Dev | Reason         | (Use Delay Code & Description) |
|-------------------|-----|-----|-----|----------------|--------------------------------|
| Tap               | 3   | 3   |     |                |                                |
| Turn Around       | 2   | 8   | 6   | <u>AR-3(4)</u> | <u>A4-1(2)</u>                 |
| Power On          | 11  | 11  |     |                |                                |
| First BackCharge  | 2   | 2   |     |                |                                |
| Power On          | 8   | 10  | 2   | <u>A4-6</u>    |                                |
| Second BackCharge | 2   | 2   |     |                |                                |
| Power On          | 6   |     |     |                |                                |
| Third Back Charge | 0   |     |     |                |                                |
| Power On          | 0   |     |     |                |                                |
| Refine            | 11  |     |     |                |                                |
| Total             | 45  |     |     |                |                                |

**Action Items:**Test #2 11:58 :OB min into Header**Maintenance Barriers:**

# Bayou Steel Corporation

## Scrap Blend Procedure

Blend #65 3-Buckets

Heat# 27288

Date 7/22

Turn C

Oper Carbo

Foreman Dick

| Header |               | Alm  | Sub  | Weights |        |           |     |
|--------|---------------|------|------|---------|--------|-----------|-----|
| Layer  | Description   | Code | Code | Alm     | Actual | Deviation | %   |
| 1      | Bushling      | 16   |      | 0       |        |           | 0%  |
| 2      | Home Plt      | 12   |      | 7000    |        |           | 9%  |
| 3      | #2 Bundles    | 5    |      | 5000    | 3      |           | 6%  |
| 4      | Turnings      | 1    |      | 12000   | 10     |           | 16% |
|        | Barge / Plate | 1    |      | 17000   | 20     |           | 22% |
|        | #1 Heavy      | 7    |      | 13000   | 25     |           | 17% |
|        | Mixed 1&2     | 11   |      | 8000    | 25     |           | 10% |
|        |               |      |      |         |        |           | 0%  |
| 6      | Shredded      | 10   |      | 15000   | 20     |           | 19% |
| Total  |               |      |      | 77000   | 103    |           |     |

| First BackChg |               | Alm  | Sub  | Weights |        |           |     |
|---------------|---------------|------|------|---------|--------|-----------|-----|
| Layer         | Description   | Code | Code | Alm     | Actual | Deviation | %   |
| 1             | Bushling      | 16   |      | 2000    |        |           | 3%  |
| 2             | Turnings      |      |      | 10000   |        |           | 15% |
| 3             | Barge / Plate | 1    |      | 14000   | 14     |           | 22% |
|               | #1 Heavy      | 1    |      | 16000   | 18     |           | 25% |
|               | Mixed 1&2     | 7    |      | 8000    | 12     |           | 12% |
|               |               |      |      |         |        |           | 0%  |
|               |               |      |      |         |        |           | 0%  |
| 5             | Shredded      | 10   |      | 15000   | 6      |           | 23% |
| Total         |               |      |      | 65000   | 55     |           |     |

| Second BackChg |             | Alm  | Sub  | Weights |        |           |     |
|----------------|-------------|------|------|---------|--------|-----------|-----|
| Layer          | Description | Code | Code | Alm     | Actual | Deviation | %   |
| 1              | Mixed 1&2   | 7    |      | 14000   | 15     |           | 42% |
|                | Turnings    | 11   |      | 8000    | 7      |           | 9%  |
|                | Mill Crop   | 15   |      | 3000    |        |           | 12% |
|                | #1 Heavy    | 1    |      | 4000    |        |           | 24% |
|                | Shredded    |      |      | 4000    |        |           |     |
| Total          |             |      |      | 33000   | 22     |           |     |

180



# Bayou Steel Corporation

# Heat Record

Crew: CMelter: DuckHeat #: 27250Date: 7-23-091st Helper: WCSGrade: #36Ladleman: JB**Pulse Counter**1st Charge 7438656Last Charge 7441332

Tap To Tap Time

2:38 = 158min.

Lost Time EQUALS Lost \$MONEY\$ !!!!!!!!!!!

Electrodes  
Add Slip Brk

|   |  |  |
|---|--|--|
| A |  |  |
| B |  |  |
| C |  |  |

Previous Heat Tap 12:34

|        | PON        | POFF        | kWh/ton |
|--------|------------|-------------|---------|
| Headr  | <u>111</u> | <u>1:24</u> | (220)   |
| 1 Back |            |             | (220)   |
| 2 Back |            |             |         |
| 3 Back |            |             |         |

|           |              |            |             |
|-----------|--------------|------------|-------------|
| Tap Start | <u>3:12</u>  | Tap Finish |             |
| Power On  | <u>36.0</u>  | LME        |             |
| kWh       | <u>27430</u> | kWh        |             |
| kWh/Ton   | <u>310</u>   | kWh/Ton    |             |
| Plan      | <u>(360)</u> | Plan       | <u>(25)</u> |

|            |           |           |          |
|------------|-----------|-----------|----------|
| Ladle Data |           | Stir Info |          |
| Ladle No.  | <u>8</u>  | # Hts Pig | <u>2</u> |
| Heats      | <u>96</u> | Stir OK   |          |
| Temp       |           |           |          |

**Temperature Data**

|     | Time | kWh | Temp        | Carbon   | O2ppm |
|-----|------|-----|-------------|----------|-------|
| 1   |      |     | <u>2977</u> | <u>9</u> |       |
| 2   |      |     | <u>3150</u> |          |       |
| 3   |      |     |             |          |       |
| 4   |      |     |             |          |       |
| Edi |      |     |             |          |       |

**EAF Additions**

|       | Flux        |
|-------|-------------|
| Lime  | <u>5000</u> |
| MgO   | <u>1800</u> |
| Chg C |             |
| Foamy | <u>2619</u> |
| Oxgyn | <u>141</u>  |
| N Gas | <u>128</u>  |

**Ladle Additions**

|        | Tap        | Trim |
|--------|------------|------|
| SiMn   | <u>960</u> |      |
| FeSi   | <u>175</u> |      |
| FeMn   |            |      |
| Coke   |            |      |
| BPI    |            |      |
| Lime   | <u>800</u> |      |
| De-Sul |            |      |
| FeV    |            |      |
| FeAl   |            |      |
| CaC    | <u>50</u>  |      |
| SiC    | <u>100</u> |      |
| GA1    | <u>200</u> |      |

**Conforming Data**

|                  |                                      |
|------------------|--------------------------------------|
| Material         | Location                             |
| Amount           |                                      |
| Scrap Compliance |                                      |
| Charge           | Header 1st Bck 2nd Bck 3rd Bck TOTAL |
| Deviation        |                                      |

Never Be Satisfied Always a Better Way

**Process Weights**

| Charge lbs    | Tap Tons  | Cast Tons |
|---------------|-----------|-----------|
| <u>27,000</u> | <u>01</u> |           |

**Ladle Sent To**

| To LMF   | St to C |
|----------|---------|
| <u>✓</u> |         |

**Chemistries**

|     | C           | Mn           | P         | S         | Si           | Cu        | Ni | Cr | Mo | Sn | V |
|-----|-------------|--------------|-----------|-----------|--------------|-----------|----|----|----|----|---|
| Aim | <u>8/13</u> | <u>70/85</u> | <u>40</u> | <u>50</u> | <u>10/26</u> | <u>50</u> |    |    |    |    |   |
| Pin |             |              |           |           |              |           |    |    |    |    |   |

**Procedure Compliance Summary**

|                   | Got | Act | Dev | Reason (Use Delay Code & Description)     |
|-------------------|-----|-----|-----|-------------------------------------------|
| Tap               | 3   | 4   |     |                                           |
| Turn Around       | 2   | 33  | 31  | <u>Add 1 slip Bt 1 of Clean slow line</u> |
| Power On          | 11  | 13  | 2   | <u>A4-6</u>                               |
| First BackCharge  | 2   |     |     |                                           |
| Power On          | 8   |     |     |                                           |
| Second BackCharge | 2   |     |     |                                           |
| Power On          | 6   |     |     | <u>A1-2 3:09</u>                          |
| Third Back Charge | 0   |     |     |                                           |
| Power On          | 0   |     |     |                                           |
| Refine            | 11  |     |     |                                           |
| Total             | 45  |     |     |                                           |

**Action Items:**

Maintenance Barriers:

Test # 3 2700

# Bayou Steel Corporation

## Scrap Blend Procedure

Blend #65 3-Buckets

Heat# 27250

Date 7-22

Turn C

Oper C. C. C.

Foreman D. K.

| Header |               | Alm. Code |           | Sub. Code   |               | Weights   |     |
|--------|---------------|-----------|-----------|-------------|---------------|-----------|-----|
| Layer  | Description   | Alm. Code | Sub. Code | Alm. Weight | Actual Weight | Deviation | %   |
| 1      | Bushling      | 16        |           | 0           |               |           | 0%  |
| 2      | Home Pit      | 12        |           | 7000        |               |           | 9%  |
| 3      | #2 Bundles    | 5         |           | 5000        |               |           | 6%  |
| 4      | Turnings      | 1         |           | 12000       |               |           | 16% |
|        | Barge / Plate | 1         |           | 17000       | 13            |           | 22% |
|        | #1 Heavy      | 7         |           | 13000       | 25            |           | 17% |
|        | Mixed 1&2     | 11        |           | 8000        | 17            |           | 10% |
|        |               |           |           |             |               |           | 0%  |
| 6      | Shredded      | 10        |           | 15000       | 15            |           | 19% |
| Total  |               |           |           | 77000       | 60            |           |     |

| First BackChg |               | Alm. Code |           | Sub. Code   |               | Weights   |     |
|---------------|---------------|-----------|-----------|-------------|---------------|-----------|-----|
| Layer         | Description   | Alm. Code | Sub. Code | Alm. Weight | Actual Weight | Deviation | %   |
| 1             | Bushling      | 16        |           | 2000        | 2             |           | 3%  |
| 2             | Turnings      |           |           | 10000       |               |           | 15% |
| 3             | Barge / Plate | 1         |           | 14000       | 19            |           | 22% |
|               | #1 Heavy      | 1         |           | 16000       | 26            |           | 25% |
|               | Mixed 1&2     | 7         |           | 8000        | 8             |           | 12% |
|               |               |           |           |             |               |           | 0%  |
|               |               |           |           |             |               |           | 0%  |
| 5             | Shredded      | 10        |           | 15000       | 15            |           | 23% |
| Total         |               |           |           | 65000       | 65            |           |     |

| Second BackChg |             | Alm. Code |           | Sub. Code   |               | Weights   |     |
|----------------|-------------|-----------|-----------|-------------|---------------|-----------|-----|
| Layer          | Description | Alm. Code | Sub. Code | Alm. Weight | Actual Weight | Deviation | %   |
| 1              | Mixed 1&2   | 7         |           | 14000       | 20            |           | 42% |
|                | Turnings    | 11        |           | 8000        |               |           | 9%  |
|                | Mill Crop   | 15        |           | 3000        |               |           | 12% |
|                | #1 Heavy    | 1         |           | 4000        |               |           | 24% |
|                | Shredded    |           |           | 4000        | 5             |           |     |
| Total          |             |           |           | 33000       | 25            |           |     |

180



# Bayou Steel Corporation

# Heat Record

Crew: CMelter: DuekHeat #: 27251Date: 7-23-091st Helper: WSGrade: 436Ladleman: JBElectrodes  
Ad Slp Brk

|   |  |  |  |
|---|--|--|--|
| A |  |  |  |
| B |  |  |  |
| C |  |  |  |

Pulse Counter

1st Charge 7141532Last Charge 7142634Tap To Tap Time 245

Lost Time EQUALS Lost \$MONEY\$ !!!!!!!!!!!!!

Previous Heat Tap 3:12

|        | PON | POFF | kWh/ton |
|--------|-----|------|---------|
| Headr  |     |      | (220)   |
| 1 Back |     |      | (220)   |
| 2 Back |     |      |         |
| 3 Back |     |      |         |

Tap Start 3:57 Tap Finish 3:59

|          |              |         |
|----------|--------------|---------|
| Power On | <u>12.7</u>  | LMF     |
| kWh      | <u>10630</u> | kWh     |
| kWh/Ton  |              | kWh/Ton |
| Plan     | (360)        | Plan    |
|          | (25)         |         |

|                    |           |
|--------------------|-----------|
| Ladle Data         | Sur Info  |
| Ladle No. <u>8</u> | # Hts Pig |
| Heats <u>44</u>    | Sur OK    |
| Temp               |           |

Temperature Data (2350) (10.05-10)

|     | Time | kWh | Temp        | Carbon    | O2ppm |
|-----|------|-----|-------------|-----------|-------|
| 1   |      |     | <u>3069</u> | <u>10</u> |       |
| 2   |      |     | <u>3150</u> |           |       |
| 3   |      |     |             |           |       |
| 4   |      |     |             |           |       |
| Ldl |      |     |             |           |       |

| FAR Additions |             | Ladle Additions |      |
|---------------|-------------|-----------------|------|
|               | Pma         | Tap             | Trim |
| Lime          | <u>5000</u> | SiMn <u>575</u> |      |
| MgO           | <u>1800</u> | FeSi <u>175</u> |      |
| Chg C         |             | FeMn            |      |
| Foamy         | <u>1026</u> | Coke            |      |
| Oxgyn         | <u>352</u>  | BPI             |      |
| N Gas         | <u>105</u>  | Lime <u>800</u> |      |
|               |             | De-Sul          |      |
|               |             | FeV             |      |
|               |             | FeAl            |      |
|               |             | CaC <u>50</u>   |      |
|               |             | SiC <u>100</u>  |      |
|               |             | GA1 <u>200</u>  |      |

Ginning Data

|          |          |
|----------|----------|
| Material | Location |
| Amount   |          |

Scrap Compliance

| Charge    | Header | 1st bck | 2nd Bck | 3rd Bck | TOTAL |
|-----------|--------|---------|---------|---------|-------|
| Deviation |        |         |         |         |       |

Never Be Satisfied Always a Better Way

| Process Weights |           |           |
|-----------------|-----------|-----------|
| Charge lbs      | Tap Tons  | Cast Tons |
| <u>27,000</u>   | <u>85</u> |           |

| Ladle Sent To                       |         |
|-------------------------------------|---------|
| To LMF                              | St to C |
| <input checked="" type="checkbox"/> |         |

Chemistries

|     | C           | Mn           | P         | S         | Si           | Cu        | Ni | Cr | Mo | Sn | V |
|-----|-------------|--------------|-----------|-----------|--------------|-----------|----|----|----|----|---|
| Aim | <u>8/13</u> | <u>70/85</u> | <u>40</u> | <u>50</u> | <u>18/26</u> | <u>50</u> |    |    |    |    |   |
| Pin |             |              |           |           |              |           |    |    |    |    |   |

## Procedure Compliance Summary

|                   | Go! | Act | Dev | Reason | (Use Delay Code & Description) |
|-------------------|-----|-----|-----|--------|--------------------------------|
| Tap               | 3   |     |     |        |                                |
| Turn Around       | 2   |     |     |        |                                |
| Power On          | 11  |     |     |        |                                |
| First BackCharge  | 2   |     |     |        |                                |
| Power On          | 8   |     |     |        |                                |
| Second BackCharge | 2   |     |     |        |                                |
| Power On          | 6   |     |     |        |                                |
| Third Back Charge | 0   |     |     |        |                                |
| Power On          | 0   |     |     |        |                                |
| Refine            | 11  |     |     |        |                                |
| Total             | 45  |     |     |        |                                |

Action Items:

Maintenance Barriers:

# Bayou Steel Corporation

## Scrap Blend Procedure

Blend #65 3-Buckets

Heat# 27257

Date 7-22

Turn C

Oper Eric S

Foreman DUCK

| Header |               |          |          | Weights |        |           |     |
|--------|---------------|----------|----------|---------|--------|-----------|-----|
| Layer  | Description   | Aim Code | Sub Code | Aim     | Actual | Deviation | %   |
| 1      | Bushling      | 16       |          | 0       |        |           | 0%  |
| 2      | Home Pit      | 12       |          | 7000    | 5      |           | 9%  |
| 3      | #2 Bundles    | 5        |          | 5000    |        |           | 6%  |
| 4      | Turnings      | 1        |          | 12000   | 15     |           | 16% |
|        | Barge / Plate | 1        |          | 17000   | 20     |           | 22% |
|        | #1 Heavy      | 7        |          | 13000   | 20     |           | 17% |
|        | Mixed 1&2     | 11       |          | 8000    | 20     |           | 10% |
|        |               |          |          |         |        |           | 0%  |
| 6      | Shredded      | 10       |          | 15000   | 16     |           | 19% |
| Total  |               |          |          | 77000   | 86     |           |     |

| First BackChg |               |          |          | Weights |        |           |     |
|---------------|---------------|----------|----------|---------|--------|-----------|-----|
| Layer         | Description   | Aim Code | Sub Code | Aim     | Actual | Deviation | %   |
| 1             | Bushling      | 16       |          | 2000    | 3      |           | 3%  |
| 2             | Turnings      |          |          | 10000   | 7      |           | 15% |
| 3             | Barge / Plate | 1        |          | 14000   | 7      |           | 22% |
|               | #1 Heavy      | 1        |          | 16000   | 15     |           | 25% |
|               | Mixed 1&2     | 7        |          | 8000    | 15     |           | 12% |
|               |               |          |          |         |        |           | 0%  |
|               |               |          |          |         |        |           | 0%  |
| 5             | Shredded      | 10       |          | 15000   | 12     |           | 23% |
| Total         |               |          |          | 65000   | 57     |           |     |

| Second BackChg |             |          |          | Weights |        |           |     |
|----------------|-------------|----------|----------|---------|--------|-----------|-----|
| Layer          | Description | Aim Code | Sub Code | Aim     | Actual | Deviation | %   |
| 1              | Mixed 1&2   | 7        |          | 14000   | 14     |           | 42% |
|                | Turnings    | 11       |          | 8000    |        |           | 9%  |
|                | Mill Crop   | 15       |          | 3000    | 6      |           | 12% |
|                | #1 Heavy    | 1        |          | 4000    | 4      |           | 24% |
|                | Shredded    |          |          | 4000    | 3      |           |     |
| Total          |             |          |          | 33000   | 27     |           |     |

180



# Bayou Steel Corporation

## Heat Record

Crew: C  
Date: 7-23-04  
Grade: A3652950

Melter: Duck  
1st Helper: WS  
Ladleman: JB

Heat #: 27252

Pulse Counter  
1st Charge 7142634  
Last Charge 7149603

Tap To Tap Time 135

Lost Time EQUALS Lost \$MONEY\$ !!!!!!!!!!!!!

| Electrodes |                                     |                          |
|------------|-------------------------------------|--------------------------|
| Ad         | Sip                                 | Brk                      |
| A          | <input checked="" type="checkbox"/> | <input type="checkbox"/> |
| B          | <input type="checkbox"/>            | <input type="checkbox"/> |
| C          | <input type="checkbox"/>            | <input type="checkbox"/> |

|                   |              |             |              |
|-------------------|--------------|-------------|--------------|
| Previous Heat Tap | <u>3167</u>  |             |              |
| PON               | POFF         | kWh/ton     |              |
| Headr             | <u>4:03</u>  | (220)       |              |
| 1 Back            |              | (220)       |              |
| 2 Back            |              |             |              |
| 3 Back            |              |             |              |
| Tap Start         | <u>4:32</u>  | Tap Finish  |              |
| Power On          | <u>22.6</u>  | LMF         |              |
| kWh               | <u>12840</u> | kWh         |              |
| kWh/Ton           |              | kWh/Ton     |              |
| Plan              | (360)        | Plan        | (25)         |
| Ladle Data        |              | Str Info    |              |
| Ladle No.         | <u>4</u>     | # Hts Plg   | <u>39</u>    |
| Heats             | <u>87</u>    | Str OK      |              |
| Temp              |              |             |              |
| Temperature Data  | (2350)       | (2000-10)   |              |
| Time              | kWh          | Temp        | Carbon O2ppm |
| 1                 | <u>429</u>   | <u>3050</u> | <u>7</u>     |
| 2                 |              |             |              |
| 3                 |              | <u>3020</u> | <u>10</u>    |
| 4                 |              |             |              |
| Ldl               |              |             |              |

|                  |             |                 |             |         |       |
|------------------|-------------|-----------------|-------------|---------|-------|
| EAF Additions    |             | Ladle Additions |             |         |       |
| Tap              |             | Tap             | Trim        |         |       |
| Lime             | <u>5000</u> | SiMn            | <u>1060</u> |         |       |
| MgO              | <u>1300</u> | FeSi            | <u>320</u>  |         |       |
| Chg C            | <u>—</u>    | FeMn            |             |         |       |
| Foamy            | <u>928</u>  | Coke            |             |         |       |
| Oxgyn            | <u>322</u>  | BPI             |             |         |       |
| N Gas            | <u>95</u>   | Lime            | <u>800</u>  |         |       |
|                  |             | De-Sul          |             |         |       |
|                  |             | FeV             |             |         |       |
|                  |             | FeAl            |             |         |       |
|                  |             | CaC             | <u>50</u>   |         |       |
|                  |             | SiC             | <u>100</u>  |         |       |
|                  |             | Al              | <u>200</u>  |         |       |
| Ginning Data     |             |                 |             |         |       |
| Material         |             | Location        |             |         |       |
| Amount           |             |                 |             |         |       |
| Scrap Compliance |             |                 |             |         |       |
| Charge           | Header      | 1st Bck         | 2nd Bck     | 3rd Bck | TOTAL |
| Deviation        |             |                 |             |         |       |

Never Be Satisfied Always a Better Way

|                 |           |           |
|-----------------|-----------|-----------|
| Process Weights |           |           |
| Charge lbs      | Tap Tons  | Cast Tons |
| <u>96000</u>    | <u>74</u> |           |

|                                     |         |
|-------------------------------------|---------|
| Ladle Sent To                       |         |
| To LMF                              | St to C |
| <input checked="" type="checkbox"/> |         |

| Chemistries |            |              |           |           |              |           |    |    |    |    |              |
|-------------|------------|--------------|-----------|-----------|--------------|-----------|----|----|----|----|--------------|
|             | C          | Mn           | P         | S         | Si           | Cu        | Ni | Cr | Mo | Sn | V            |
| Aim         | <u>213</u> | <u>80/40</u> | <u>30</u> | <u>50</u> | <u>20/27</u> | <u>50</u> |    |    |    |    | <u>30/40</u> |
| Rin         |            |              |           |           |              |           |    |    |    |    |              |

### Procedure Compliance Summary

|                    | Got | Act       | Dev | Reason      | (Use Delay Code & Description) |
|--------------------|-----|-----------|-----|-------------|--------------------------------|
| Tap                | 3   | 3         |     |             |                                |
| Turn Around        | 2   | 3         |     |             |                                |
| Power On           | 11  |           |     | <u>A3-2</u> |                                |
| First Back Charge  | 2   |           |     |             |                                |
| Power On           | 8   |           |     |             |                                |
| Second Back Charge | 2   |           |     |             |                                |
| Power On           | 6   |           |     |             |                                |
| Third Back Charge  | 0   |           |     |             |                                |
| Power On           | 0   |           |     |             |                                |
| Refine             | 11  |           |     |             |                                |
| Total              | 45  | <u>35</u> |     |             |                                |

### Action Items:

Maintenance Barriers:

4<sup>th</sup> Test 4:04 p.m. (D.E.Q.)

# Bayou Steel Corporation

## Scrap Blend Procedure

Blend #65 3-Buckets

Heat# 27252

Date 7-23-04

Turn C

Oper Cowboy

Foreman Quik

### Header

| Layer | Description   | Alm Code | Sub Code | Weights |        |           |     |
|-------|---------------|----------|----------|---------|--------|-----------|-----|
|       |               |          |          | Alm     | Actual | Deviation | %   |
| 1     | Bushling      | 16       |          | 0       |        |           | 0%  |
| 2     | Home Pit      | 12       |          | 7000    | 6      |           | 9%  |
| 3     | #2 Bundles    | 5        |          | 5000    |        |           | 6%  |
| 4     | Turnings      | 1        |          | 12000   | 10     |           | 16% |
|       | Barge / Plate | 1        |          | 17000   | 20     |           | 22% |
|       | #1 Heavy      | 7        |          | 13000   | 20     |           | 17% |
|       | Mixed 1&2     | 11       |          | 8000    | 20     |           | 10% |
|       |               |          |          |         |        |           | 0%  |
| 6     | Shredded      | 10       |          | 15000   | 30     |           | 19% |
| Total |               |          |          | 77000   | 96     |           |     |

### First BackChg

See Heat # 257  
1st  
2nd

| Layer | Description   | Alm Code | Sub Code | Weights |        |           |     |
|-------|---------------|----------|----------|---------|--------|-----------|-----|
|       |               |          |          | Alm     | Actual | Deviation | %   |
| 1     | Bushling      | 16       |          | 2000    |        |           | 3%  |
| 2     | Turnings      |          |          | 10000   |        |           | 15% |
| 3     | Barge / Plate | 1        |          | 14000   |        |           | 22% |
|       | #1 Heavy      | 1        |          | 16000   |        |           | 25% |
|       | Mixed 1&2     | 7        |          | 8000    |        |           | 12% |
|       |               |          |          |         |        |           | 0%  |
|       |               |          |          |         |        |           | 0%  |
| 5     | Shredded      | 10       |          | 15000   |        |           | 23% |
| Total |               |          |          | 65000   | 57     |           |     |

### Second BackChg

| Layer | Description | Alm Code | Sub Code | Weights |        |           |     |
|-------|-------------|----------|----------|---------|--------|-----------|-----|
|       |             |          |          | Alm     | Actual | Deviation | %   |
| 1     | Mixed 1&2   | 7        |          | 14000   |        |           | 42% |
|       | Turnings    | 11       |          | 8000    |        |           | 9%  |
|       | Mill Crop   | 15       |          | 3000    |        |           | 12% |
|       | #1 Heavy    | 1        |          | 4000    |        |           | 24% |
|       | Shredded    |          |          | 4000    |        |           |     |
| Total |             |          |          | 33000   | 27     |           |     |

# Bayou Steel Corporation

## Heat Record

**Crew:**

Date:

**Grade:**

**Melter:**

**1st Helper:**

**Ladleman:**

Heat #: 27253

| Electrodes |    |     |     |
|------------|----|-----|-----|
|            | Ad | Slp | Brk |
| A          |    |     |     |
| B          |    |     |     |
| C          |    |     |     |

**Pulse Counter:**  
1st Charge 7144603  
Last Charge 7144595

## Tap To Tap Time

158

**Lost Time EQUALS Lost \$MONEY\$ !!!!!!!!!!!!!**

| Previous Heat Tap: 432 |     |      |           |
|------------------------|-----|------|-----------|
|                        | PON | POFF | kWh/ton   |
| Headr                  | 442 | 454  | (220) 175 |
| 1 Back                 | 456 | 504  | (220) 213 |
| 2 Back                 | 508 |      |           |
| 3 Back                 |     |      |           |

|           |       |            |      |
|-----------|-------|------------|------|
| Tap Start | 532   | Tap Finish |      |
| Power On  | 2860  | LMF        |      |
| kWh       | 319   | kWh        |      |
| kWh/Ton   |       | kWh/Ton    |      |
| Plan      | (360) | Plan       | (25) |

|                    |                     |
|--------------------|---------------------|
| <b>Ladle Data</b>  | <b>Surf Info</b>    |
| Ladle No. <u>5</u> | # Hts Plg <u>11</u> |
| Heats <u>11</u>    | Surf OK <u>11</u>   |
| Temp <u>1986</u>   |                     |

| Temperature Data (250 - 300 °C) |      |     |      |              |
|---------------------------------|------|-----|------|--------------|
|                                 | Time | kWh | Temp | Carbon O2ppm |
| 1                               | 523  | 319 | 304  | 12           |
| 2                               |      |     |      |              |
| 3                               |      |     | 3010 |              |
| 4                               |      |     |      |              |

| FAB Additions |      | Ladle Additions |      |
|---------------|------|-----------------|------|
| Plas          |      | Tap             | Trim |
| Lime          | 5000 | SiMn            | 1965 |
| MgO           | 1000 | FeSi            | 260  |
| Chg C         |      | FeMn            |      |
| Foamy         | 725  | Coke            |      |
| Oxgyn         | 508  | BPI             |      |
| N Gas         | 173  | Lime            | 800  |
|               |      | De-Sul          |      |
|               |      | FeV             |      |
|               |      | FeAl            |      |
|               |      | CaC             | 50   |
|               |      | SiC             | 100  |
|               |      | Al              | 200  |

|                  |          |         |         |         |       |
|------------------|----------|---------|---------|---------|-------|
| Grinding Data    |          |         |         |         |       |
| Material         | Location |         |         |         |       |
| Amount           |          |         |         |         |       |
| Scrap Compliance |          |         |         |         |       |
| Charge           | Header   | 1st Bck | 2nd Bck | 3rd Bck | TOTAL |
| Deviation        | 96       | 57      | 27      |         | 180   |

| Process Weights |          |           |
|-----------------|----------|-----------|
| Charge lbs      | Tap Tons | Cast Tons |
| 180             | 87       |           |

|               |         |
|---------------|---------|
| Ladle Sent To |         |
| To LMF        | St to C |
| ✓             |         |

**Never Be Satisfied Always a Better Way**

| Chemistries |     |     |    |    |      |    |    |    |    |    |       |
|-------------|-----|-----|----|----|------|----|----|----|----|----|-------|
|             | C   | Mn  | P  | S  | Si   | Cu | Ni | Cr | Mo | Sn | V     |
| Aim Pin     | 873 | 890 | 30 | 50 | 2027 | 50 |    |    |    |    | 30-40 |

## Procedure Compliance Summary

|                   | Gol | Act | Dev | Reason (Use Delay Code & Description) |
|-------------------|-----|-----|-----|---------------------------------------|
| Tap               | 3   | 3   | -   |                                       |
| Turn Around       | 2   | 7   | 5   | A 1-3 Robin's                         |
| Power On          | 11  | 12  | 1   | A 4-6                                 |
| First BackCharge  | 2   | 2   | -   |                                       |
| Power On          | 8   | 10  | 2   | A 4-6 Run                             |
| Second BackCharge | 2   | 2   | -   |                                       |
| Power On          | 6   |     |     |                                       |
| Third Back Charge | 0   |     | 5   | A 6-6 heavy load                      |
| Power On          | 0   |     |     |                                       |
| Refine            | 11  |     |     |                                       |
| Total             | 45  | 58  | 13  |                                       |

**Action Items:**

456

### **Maintenance Barriers:**

# Bayou Steel Corporation

## Scrap Blend Procedure

Blend #65 3-Buckets

Heat# 27253

Date 7-23

Turn C

Oper Carey

Foreman Ark

### Header

| Layer | Description   | Alm  |     | Sub  |     | Weights |        | Deviation | % Dev |
|-------|---------------|------|-----|------|-----|---------|--------|-----------|-------|
|       |               | Code | Val | Code | Val | Alm     | Actual |           |       |
| 1     | Bushling      | 16   |     |      |     | 0       |        |           | 0%    |
| 2     | Home Pit      | 12   |     |      |     | 7000    |        |           | 9%    |
| 3     | #2 Bundles    | 5    |     |      |     | 5000    |        |           | 6%    |
| 4     | Turnings      | 1    |     |      |     | 12000   | 10     |           | 16%   |
|       | Barge / Plate | 1    |     |      |     | 17000   | 20     |           | 22%   |
|       | #1 Heavy      | 7    |     |      |     | 13000   | 20     |           | 17%   |
|       | Mixed 1&2     | 11   |     |      |     | 8000    | 20     |           | 10%   |
|       |               |      |     |      |     |         |        |           | 0%    |
| 6     | Shredded      | 10   |     |      |     | 15000   | 20     |           | 19%   |
| Total |               |      |     |      |     | 77000   | 90     |           |       |

### First BackChg

| Layer | Description   | Alm  |     | Sub  |     | Weights |        | Deviation | % Dev |
|-------|---------------|------|-----|------|-----|---------|--------|-----------|-------|
|       |               | Code | Val | Code | Val | Alm     | Actual |           |       |
| 1     | Bushling      | 16   |     |      |     | 2000    |        |           | 3%    |
| 2     | Turnings      |      |     |      |     | 10000   |        |           | 15%   |
| 3     | Barge / Plate | 1    |     |      |     | 14000   | 16     |           | 22%   |
|       | #1 Heavy      | 1    |     |      |     | 16000   | 8      |           | 25%   |
|       | Mixed 1&2     | 7    |     |      |     | 8000    | 21     |           | 12%   |
|       |               |      |     |      |     |         |        |           | 0%    |
|       |               |      |     |      |     |         |        |           | 0%    |
| 5     | Shredded      | 10   |     |      |     | 15000   | 17     |           | 23%   |
| Total |               |      |     |      |     | 65000   | 60     |           |       |

### Second BackChg

| Layer | Description | Alm  |     | Sub  |     | Weights |        | Deviation | % Dev |
|-------|-------------|------|-----|------|-----|---------|--------|-----------|-------|
|       |             | Code | Val | Code | Val | Alm     | Actual |           |       |
| 1     | Mixed 1&2   | 7    |     |      |     | 14000   | 17     |           | 42%   |
|       | Turnings    | 11   |     |      |     | 8000    |        |           | 9%    |
|       | Mill Crop   | 15   |     |      |     | 3000    | 10     |           | 12%   |
|       | #1 Heavy    | 1    |     |      |     | 4000    | 6      |           | 24%   |
|       | Shredded    |      |     |      |     | 4000    | 8      |           |       |
| Total |             |      |     |      |     | 33000   | 41     |           |       |

191,000

EVR0001  
07/28/04

BAYOU STEEL CORPORATION  
FURNACE #1 & #2 TOTAL FLOW (SCFM) - EVERY 15 MIN

1  
08:11

| END<br>DATE<br>---- | END<br>TIME<br>---- | AVG<br>--- | MAX<br>--- | MIN<br>--- |
|---------------------|---------------------|------------|------------|------------|
| 07/23/04            | 00:00:57            | 113,799.76 | 116,068.38 | 111,843.71 |
| 07/23/04            | 00:02:27            | 113,540.63 | 117,435.90 | 109,841.27 |
| 07/23/04            | 00:03:58            | 115,219.65 | 117,216.12 | 113,137.98 |
| 07/23/04            | 00:05:28            | 113,433.19 | 117,118.44 | 111,037.85 |
| 07/23/04            | 00:06:59            | 111,420.43 | 114,847.38 | 108,498.17 |
| 07/23/04            | 00:08:29            | 111,034.32 | 114,822.95 | 109,499.39 |
| 07/23/04            | 00:09:59            | 109,752.81 | 112,771.67 | 107,350.43 |
| 07/23/04            | 00:11:29            | 107,390.31 | 110,964.59 | 105,372.41 |
| 07/23/04            | 00:12:58            | 108,607.79 | 110,622.71 | 105,372.41 |
| 07/23/04            | 00:14:28            | 106,911.68 | 111,697.20 | 101,929.18 |
| 07/23/04            | 00:16:00            | 105,303.22 | 119,389.50 | 101,245.42 |
| 07/23/04            | 00:17:29            | 108,828.38 | 118,901.10 | 91,746.03  |
| 07/23/04            | 00:18:99            | 105,455.98 | 109,548.23 | 96,166.05  |
| 07/23/04            | 00:20:30            | 110,128.34 | 112,527.47 | 107,936.51 |
| 07/23/04            | 00:22:00            | 116,280.83 | 125,909.65 | 111,599.51 |
| 07/23/04            | 00:23:30            | 121,566.68 | 125,909.65 | 113,137.98 |
| 07/23/04            | 00:25:00            | 127,663.55 | 138,901.09 | 108,595.85 |
| 07/23/04            | 00:26:29            | 122,307.96 | 135,213.67 | 118,412.70 |
| 07/23/04            | 00:28:01            | 124,499.25 | 130,280.83 | 118,412.70 |
| 07/23/04            | 00:29:30            | 121,444.04 | 126,666.66 | 116,410.26 |
| 07/23/04            | 00:31:00            | 116,694.62 | 120,903.54 | 113,992.67 |
| 07/23/04            | 00:32:31            | 114,827.30 | 118,241.76 | 112,600.73 |
| 07/23/04            | 00:34:01            | 116,739.38 | 119,023.20 | 114,334.55 |
| 07/23/04            | 00:35:31            | 113,813.32 | 116,752.14 | 111,257.63 |
| 07/23/04            | 00:37:01            | 112,672.63 | 116,434.68 | 109,865.69 |
| 07/23/04            | 00:38:30            | 111,369.15 | 117,509.16 | 109,157.51 |
| 07/23/04            | 00:40:02            | 109,806.81 | 111,306.47 | 107,643.47 |
| 07/23/04            | 00:41:31            | 103,418.26 | 112,478.63 | 90,744.81  |
| 07/23/04            | 00:43:01            | 110,545.92 | 124,957.27 | 79,096.46  |
| 07/23/04            | 00:44:32            | 114,684.30 | 123,980.46 | 109,890.11 |
| 07/23/04            | 00:46:02            | 110,379.87 | 115,238.09 | 107,448.11 |
| 07/23/04            | 00:47:32            | 108,935.83 | 112,258.85 | 106,031.74 |
| 07/23/04            | 00:49:02            | 108,861.21 | 110,476.19 | 105,811.97 |
| 07/23/04            | 00:50:33            | 110,736.95 | 113,479.85 | 105,543.34 |
| 07/23/04            | 00:52:03            | 109,708.31 | 113,382.17 | 107,081.80 |
| 07/23/04            | 00:53:32            | 99,998.10  | 112,429.79 | 89,035.41  |
| 07/23/04            | 00:55:02            | 111,537.65 | 126,080.59 | 82,319.90  |
| 07/23/04            | 00:56:33            | 111,760.95 | 115,286.94 | 109,499.39 |
| 07/23/04            | 00:58:03            | 115,833.67 | 120,952.38 | 110,598.29 |
| 07/23/04            | 00:59:33            | 111,517.02 | 113,504.27 | 109,304.03 |
| 07/23/04            | 01:01:02            | 108,835.71 | 113,626.38 | 105,641.02 |
| 07/23/04            | 01:02:33            | 108,997.15 | 112,136.75 | 104,664.23 |
| 07/23/04            | 01:04:03            | 112,094.97 | 114,114.77 | 109,059.83 |
| 07/23/04            | 01:05:34            | 109,267.95 | 111,477.41 | 107,032.97 |
| 07/23/04            | 01:07:04            | 109,026.45 | 114,578.76 | 107,032.97 |
| 07/23/04            | 01:08:34            | 106,242.03 | 115,286.94 | 100,634.92 |
| 07/23/04            | 01:10:04            | 109,588.39 | 116,337.00 | 101,050.06 |
| 07/23/04            | 01:11:33            | 110,203.77 | 119,951.16 | 102,222.22 |
| 07/23/04            | 01:13:03            | 107,521.64 | 113,089.13 | 95,042.73  |
| 07/23/04            | 01:14:34            | 102,347.58 | 109,084.25 | 91,086.69  |
| 07/23/04            | 01:16:04            | 108,452.59 | 112,576.31 | 104,786.33 |
| 07/23/04            | 01:17:35            | 114,318.00 | 123,858.37 | 103,785.10 |
| 07/23/04            | 01:19:05            | 122,761.63 | 125,396.83 | 115,457.88 |

EVR0001  
07/28/04

BAYOU STEEL CORPORATION  
FURNACE #1 & #2 TOTAL FLOW (SCFM) - EVERY 15 MIN

2  
08:11

| END<br>DATE | END<br>TIME | AVG        | MAX        | MIN        |
|-------------|-------------|------------|------------|------------|
| 07/23/04    | 01:20:35    | 125,521.09 | 137,753.36 | 105,006.10 |
| 07/23/04    | 01:22:05    | 126,494.91 | 133,455.44 | 122,197.80 |
| 07/23/04    | 01:23:34    | 119,804.09 | 123,467.64 | 115,628.81 |
| 07/23/04    | 01:25:06    | 115,115.45 | 117,704.52 | 112,039.07 |
| 07/23/04    | 01:26:35    | 118,042.05 | 122,783.88 | 114,188.03 |
| 07/23/04    | 01:28:05    | 116,005.97 | 118,998.78 | 113,308.91 |
| 07/23/04    | 01:29:36    | 116,844.39 | 119,780.22 | 114,310.13 |
| 07/23/04    | 01:31:06    | 115,585.40 | 119,560.44 | 111,965.81 |
| 07/23/04    | 01:32:36    | 117,140.14 | 120,048.84 | 114,285.71 |
| 07/23/04    | 01:34:06    | 113,241.89 | 120,317.46 | 103,418.80 |
| 07/23/04    | 01:35:37    | 116,621.90 | 132,674.00 | 100,244.20 |
| 07/23/04    | 01:37:07    | 128,470.22 | 134,139.19 | 122,442.00 |
| 07/23/04    | 01:38:36    | 119,835.57 | 127,032.97 | 114,871.80 |
| 07/23/04    | 01:40:06    | 116,649.03 | 120,952.38 | 114,896.22 |
| 07/23/04    | 01:41:37    | 116,735.59 | 120,952.38 | 111,819.29 |
| 07/23/04    | 01:43:07    | 116,562.74 | 122,026.86 | 114,236.88 |
| 07/23/04    | 01:44:37    | 115,189.52 | 117,338.22 | 113,431.02 |
| 07/23/04    | 01:46:07    | 107,330.08 | 119,169.72 | 93,919.41  |
| 07/23/04    | 01:47:38    | 112,600.19 | 127,374.84 | 98,144.08  |
| 07/23/04    | 01:49:08    | 118,873.70 | 124,737.48 | 114,114.77 |
| 07/23/04    | 01:50:37    | 115,863.52 | 119,316.24 | 112,136.75 |
| 07/23/04    | 01:52:07    | 115,333.60 | 119,218.56 | 111,941.39 |
| 07/23/04    | 01:53:38    | 115,762.85 | 118,559.22 | 113,137.98 |
| 07/23/04    | 01:55:08    | 115,648.08 | 118,021.98 | 110,622.71 |
| 07/23/04    | 01:56:38    | 116,897.30 | 118,852.26 | 113,211.23 |
| 07/23/04    | 01:58:08    | 114,200.52 | 118,779.00 | 110,549.45 |
| 07/23/04    | 01:59:39    | 113,815.22 | 117,020.76 | 108,937.73 |
| 07/23/04    | 02:01:09    | 113,255.73 | 116,288.16 | 109,719.17 |
| 07/23/04    | 02:02:38    | 112,691.36 | 116,874.23 | 109,865.69 |
| 07/23/04    | 02:04:08    | 117,175.15 | 120,830.28 | 113,015.88 |
| 07/23/04    | 02:05:39    | 121,146.66 | 125,689.87 | 116,385.84 |
| 07/23/04    | 02:07:09    | 119,957.40 | 124,371.19 | 114,554.34 |
| 07/23/04    | 02:08:38    | 114,070.27 | 120,366.30 | 106,666.66 |
| 07/23/04    | 02:10:08    | 119,374.84 | 126,837.61 | 115,360.20 |
| 07/23/04    | 02:11:40    | 115,308.91 | 121,416.36 | 107,277.16 |
| 07/23/04    | 02:13:10    | 117,237.28 | 120,781.44 | 111,452.99 |
| 07/23/04    | 02:14:39    | 105,604.94 | 118,632.48 | 95,848.59  |
| 07/23/04    | 02:16:09    | 113,497.22 | 117,509.16 | 110,989.01 |
| 07/23/04    | 02:17:40    | 119,636.41 | 130,085.47 | 108,034.19 |
| 07/23/04    | 02:19:10    | 125,164.29 | 129,279.61 | 118,827.84 |
| 07/23/04    | 02:20:39    | 129,477.41 | 141,953.61 | 103,003.66 |
| 07/23/04    | 02:22:11    | 127,739.25 | 134,798.53 | 121,660.56 |
| 07/23/04    | 02:23:41    | 120,086.55 | 125,299.15 | 116,776.55 |
| 07/23/04    | 02:25:11    | 118,068.10 | 126,178.27 | 116,190.48 |
| 07/23/04    | 02:26:40    | 118,913.85 | 126,178.27 | 115,018.31 |
| 07/23/04    | 02:28:10    | 117,956.86 | 119,926.74 | 114,676.44 |
| 07/23/04    | 02:29:41    | 115,074.21 | 120,537.24 | 112,722.84 |
| 07/23/04    | 02:31:11    | 112,335.64 | 118,852.26 | 109,987.79 |
| 07/23/04    | 02:32:40    | 103,516.48 | 116,263.73 | 92,039.07  |
| 07/23/04    | 02:34:12    | 107,429.66 | 120,610.50 | 94,261.30  |
| 07/23/04    | 02:35:42    | 125,435.90 | 137,680.09 | 107,741.15 |
| 07/23/04    | 02:37:12    | 117,657.58 | 124,224.66 | 114,969.48 |
| 07/23/04    | 02:38:41    | 113,782.12 | 117,777.78 | 111,623.93 |

EVR0001  
07/28/04

BAYOU STEEL CORPORATION  
FURNACE #1 & #2 TOTAL FLOW (SCFM) - EVERY 15 MIN

3  
08:11

| END<br>DATE | END<br>TIME | AVG        | MAX        | MIN        |
|-------------|-------------|------------|------------|------------|
| ----        | ----        | ---        | ---        | ---        |
| 07/23/04    | 02:40:11    | 114,029.30 | 116,996.34 | 111,062.27 |
| 07/23/04    | 02:41:42    | 112,124.00 | 114,505.49 | 108,766.79 |
| 07/23/04    | 02:43:12    | 102,842.77 | 114,505.49 | 92,551.89  |
| 07/23/04    | 02:44:41    | 107,334.96 | 110,891.33 | 103,614.16 |
| 07/23/04    | 02:46:13    | 114,513.09 | 128,083.03 | 105,152.63 |
| 07/23/04    | 02:47:42    | 121,482.84 | 123,394.38 | 115,213.67 |
| 07/23/04    | 02:49:13    | 120,795.28 | 126,080.59 | 117,411.48 |
| 07/23/04    | 02:50:43    | 122,256.14 | 128,742.37 | 118,192.92 |
| 07/23/04    | 02:52:12    | 123,604.66 | 127,008.55 | 120,146.52 |
| 07/23/04    | 02:53:43    | 118,111.79 | 121,221.00 | 114,749.70 |
| 07/23/04    | 02:55:13    | 115,936.23 | 117,948.72 | 114,090.35 |
| 07/23/04    | 02:56:44    | 114,987.66 | 117,240.54 | 110,964.59 |
| 07/23/04    | 02:58:14    | 115,524.63 | 121,758.24 | 112,087.91 |
| 07/23/04    | 02:59:43    | 116,120.47 | 121,758.24 | 112,210.02 |
| 07/23/04    | 03:01:13    | 113,608.20 | 116,361.41 | 110,549.45 |
| 07/23/04    | 03:02:44    | 112,603.45 | 117,362.64 | 110,354.09 |
| 07/23/04    | 03:04:14    | 110,460.45 | 117,362.64 | 104,102.56 |
| 07/23/04    | 03:05:44    | 110,706.01 | 120,683.76 | 97,313.80  |
| 07/23/04    | 03:07:14    | 110,806.95 | 115,824.18 | 106,910.87 |
| 07/23/04    | 03:08:45    | 117,554.20 | 123,125.77 | 112,478.63 |
| 07/23/04    | 03:10:15    | 122,218.15 | 131,819.30 | 111,721.61 |
| 07/23/04    | 03:11:44    | 124,764.62 | 129,792.43 | 119,755.80 |
| 07/23/04    | 03:13:14    | 129,368.61 | 141,465.20 | 109,181.93 |
| 07/23/04    | 03:14:45    | 127,805.73 | 133,357.75 | 124,981.69 |
| 07/23/04    | 03:16:15    | 124,209.20 | 129,157.51 | 120,439.56 |
| 07/23/04    | 03:17:45    | 119,557.18 | 124,420.02 | 116,459.09 |
| 07/23/04    | 03:19:15    | 118,425.72 | 122,612.95 | 115,579.98 |
| 07/23/04    | 03:20:46    | 121,082.08 | 123,492.06 | 117,631.26 |
| 07/23/04    | 03:22:16    | 121,606.84 | 126,617.83 | 118,266.18 |
| 07/23/04    | 03:23:45    | 121,071.50 | 124,078.14 | 117,753.36 |
| 07/23/04    | 03:25:15    | 118,800.16 | 120,879.12 | 115,677.66 |
| 07/23/04    | 03:26:46    | 110,345.41 | 119,072.04 | 98,852.26  |
| 07/23/04    | 03:28:16    | 115,062.54 | 119,682.54 | 109,865.69 |
| 07/23/04    | 03:29:47    | 123,608.47 | 137,118.44 | 104,664.23 |
| 07/23/04    | 03:31:17    | 120,651.74 | 125,641.02 | 118,779.00 |
| 07/23/04    | 03:32:47    | 128,875.32 | 137,655.67 | 119,511.60 |
| 07/23/04    | 03:34:17    | 123,997.55 | 129,768.01 | 118,925.52 |
| 07/23/04    | 03:35:46    | 119,812.23 | 121,587.30 | 117,826.62 |
| 07/23/04    | 03:37:18    | 121,281.51 | 123,956.05 | 117,216.12 |
| 07/23/04    | 03:38:47    | 124,694.62 | 126,446.88 | 121,514.04 |
| 07/23/04    | 03:40:17    | 118,707.91 | 123,467.64 | 112,380.95 |
| 07/23/04    | 03:41:48    | 109,639.67 | 118,754.58 | 99,462.76  |
| 07/23/04    | 03:43:18    | 118,132.41 | 129,059.83 | 99,316.24  |
| 07/23/04    | 03:44:48    | 125,266.86 | 131,062.27 | 120,170.94 |
| 07/23/04    | 03:46:18    | 118,773.03 | 121,904.77 | 116,483.52 |
| 07/23/04    | 03:47:49    | 117,366.71 | 120,952.38 | 109,328.45 |
| 07/23/04    | 03:49:19    | 119,162.94 | 123,223.45 | 114,358.98 |
| 07/23/04    | 03:50:48    | 115,132.00 | 117,558.00 | 110,134.31 |
| 07/23/04    | 03:52:18    | 115,501.29 | 118,974.36 | 110,647.13 |
| 07/23/04    | 03:53:49    | 117,460.05 | 123,052.50 | 114,920.63 |
| 07/23/04    | 03:55:19    | 114,487.86 | 118,412.70 | 112,673.99 |
| 07/23/04    | 03:56:49    | 113,637.50 | 115,433.45 | 112,283.27 |
| 07/23/04    | 03:58:19    | 113,780.22 | 117,069.59 | 112,234.43 |

EVR0001  
07/28/04

BAYOU STEEL CORPORATION  
FURNACE #1 & #2 TOTAL FLOW (SCFM) - EVERY 15 MIN

4  
08:11

| END<br>DATE | END<br>TIME | AVG        | MAX        | MIN        |
|-------------|-------------|------------|------------|------------|
| 07/23/04    | 03:59:50    | 113,397.91 | 115,311.35 | 108,693.53 |
| 07/23/04    | 04:01:19    | 103,785.65 | 108,693.53 | 96,581.20  |
| 07/23/04    | 04:02:50    | 109,491.79 | 115,238.09 | 106,959.70 |
| 07/23/04    | 04:04:20    | 117,574.28 | 131,282.05 | 109,890.11 |
| 07/23/04    | 04:05:50    | 122,492.20 | 125,592.19 | 115,604.40 |
| 07/23/04    | 04:07:20    | 126,603.99 | 133,064.72 | 121,343.10 |
| 07/23/04    | 04:08:49    | 129,477.41 | 133,431.02 | 124,053.73 |
| 07/23/04    | 04:10:19    | 128,084.38 | 131,746.03 | 123,223.45 |
| 07/23/04    | 04:11:50    | 133,962.56 | 136,581.20 | 129,670.33 |
| 07/23/04    | 04:13:20    | 133,937.33 | 137,191.70 | 131,135.53 |
| 07/23/04    | 04:14:51    | 134,768.69 | 139,194.14 | 132,503.05 |
| 07/23/04    | 04:16:21    | 135,828.78 | 138,901.09 | 131,550.67 |
| 07/23/04    | 04:17:51    | 135,926.47 | 138,949.94 | 132,576.31 |
| 07/23/04    | 04:19:21    | 137,007.19 | 138,779.00 | 135,360.20 |
| 07/23/04    | 04:20:50    | 135,910.73 | 140,390.72 | 132,796.09 |
| 07/23/04    | 04:22:20    | 136,193.45 | 141,050.06 | 130,451.77 |
| 07/23/04    | 04:23:51    | 136,063.77 | 139,633.70 | 132,991.45 |
| 07/23/04    | 04:25:21    | 136,757.56 | 143,174.61 | 133,601.95 |
| 07/23/04    | 04:26:52    | 138,527.20 | 150,280.83 | 119,633.70 |
| 07/23/04    | 04:28:22    | 139,115.19 | 148,669.11 | 133,089.14 |
| 07/23/04    | 04:29:52    | 130,961.34 | 134,822.95 | 127,301.59 |
| 07/23/04    | 04:31:22    | 126,419.21 | 130,256.41 | 121,880.34 |
| 07/23/04    | 04:32:51    | 124,495.45 | 126,788.77 | 122,271.06 |
| 07/23/04    | 04:34:23    | 127,247.32 | 130,378.51 | 125,250.30 |
| 07/23/04    | 04:35:52    | 122,821.60 | 125,860.80 | 120,341.88 |
| 07/23/04    | 04:37:22    | 121,609.01 | 126,105.01 | 119,072.04 |
| 07/23/04    | 04:38:53    | 113,595.71 | 121,245.42 | 99,194.14  |
| 07/23/04    | 04:40:23    | 115,921.59 | 121,709.40 | 110,769.23 |
| 07/23/04    | 04:41:53    | 122,726.36 | 137,777.78 | 117,118.44 |
| 07/23/04    | 04:43:23    | 132,191.30 | 144,786.33 | 107,887.66 |
| 07/23/04    | 04:44:52    | 125,062.54 | 129,841.27 | 121,978.02 |
| 07/23/04    | 04:46:24    | 121,745.49 | 124,493.28 | 120,317.46 |
| 07/23/04    | 04:47:53    | 123,188.98 | 126,275.95 | 117,924.30 |
| 07/23/04    | 04:49:23    | 122,789.85 | 126,349.20 | 118,656.90 |
| 07/23/04    | 04:50:54    | 116,648.76 | 120,268.62 | 112,551.89 |
| 07/23/04    | 04:52:24    | 111,313.80 | 120,317.46 | 96,043.95  |
| 07/23/04    | 04:53:54    | 107,668.98 | 115,042.73 | 92,893.77  |
| 07/23/04    | 04:55:24    | 122,594.22 | 130,989.01 | 92,893.77  |
| 07/23/04    | 04:56:53    | 118,329.40 | 121,123.32 | 114,529.91 |
| 07/23/04    | 04:58:25    | 116,601.82 | 120,366.30 | 112,307.70 |
| 07/23/04    | 04:59:54    | 116,614.84 | 119,145.30 | 113,455.43 |
| 07/23/04    | 05:01:24    | 115,254.10 | 119,194.14 | 111,452.99 |
| 07/23/04    | 05:02:55    | 112,373.63 | 116,849.82 | 109,914.53 |
| 07/23/04    | 05:04:25    | 112,185.32 | 115,482.30 | 109,694.75 |
| 07/23/04    | 05:05:54    | 112,016.55 | 115,482.30 | 109,426.13 |
| 07/23/04    | 05:07:25    | 113,930.54 | 116,849.82 | 112,161.17 |
| 07/23/04    | 05:08:56    | 109,194.68 | 115,384.62 | 105,421.24 |
| 07/23/04    | 05:10:26    | 111,262.52 | 118,510.38 | 106,959.70 |
| 07/23/04    | 05:11:55    | 104,779.81 | 111,819.29 | 98,485.96  |
| 07/23/04    | 05:13:25    | 102,627.05 | 112,112.34 | 85,225.88  |
| 07/23/04    | 05:14:56    | 113,902.86 | 118,437.12 | 103,882.78 |
| 07/23/04    | 05:16:26    | 112,200.52 | 117,191.70 | 102,808.30 |
| 07/23/04    | 05:17:55    | 112,662.05 | 116,459.09 | 109,157.51 |

EVR0001  
07/28/04

BAYOU STEEL CORPORATION  
FURNACE #1 & #2 TOTAL FLOW (SCFM) - EVERY 15 MIN

5  
08:11

| END<br>DATE | END<br>TIME | AVG        | MAX        | MIN        |
|-------------|-------------|------------|------------|------------|
| 07/23/04    | 05:19:25    | 116,338.35 | 121,172.16 | 111,501.83 |
| 07/23/04    | 05:20:57    | 124,637.09 | 131,404.16 | 114,798.53 |
| 07/23/04    | 05:22:27    | 125,795.96 | 128,595.85 | 121,587.30 |
| 07/23/04    | 05:23:56    | 127,941.39 | 141,001.22 | 123,492.06 |
| 07/23/04    | 05:25:26    | 131,479.31 | 143,003.66 | 105,689.87 |
| 07/23/04    | 05:26:57    | 126,696.24 | 133,260.08 | 122,490.84 |
| 07/23/04    | 05:28:27    | 119,833.67 | 123,907.20 | 117,020.76 |
| 07/23/04    | 05:29:56    | 120,957.80 | 123,931.63 | 118,388.28 |
| 07/23/04    | 05:31:26    | 122,754.58 | 128,034.19 | 117,631.26 |
| 07/23/04    | 05:32:58    | 121,644.28 | 126,031.74 | 119,413.92 |
| 07/23/04    | 05:34:28    | 116,209.20 | 120,000.00 | 113,040.30 |
| 07/23/04    | 05:35:57    | 108,928.77 | 118,437.12 | 96,825.40  |
| 07/23/04    | 05:37:27    | 115,045.72 | 120,293.04 | 109,304.03 |
| 07/23/04    | 05:38:58    | 119,555.55 | 124,932.84 | 114,065.94 |
| 07/23/04    | 05:40:28    | 128,306.88 | 137,680.09 | 109,523.81 |
| 07/23/04    | 05:41:57    | 128,254.78 | 133,382.17 | 124,542.13 |
| 07/23/04    | 05:43:27    | 122,107.99 | 126,715.51 | 118,608.06 |
| 07/23/04    | 05:44:58    | 121,359.38 | 125,763.13 | 117,899.88 |
| 07/23/04    | 05:46:29    | 121,842.09 | 125,152.63 | 119,316.24 |
| 07/23/04    | 05:47:58    | 118,023.06 | 124,688.65 | 113,772.89 |
| 07/23/04    | 05:49:28    | 116,163.07 | 119,877.90 | 98,290.60  |
| 07/23/04    | 05:50:59    | 107,594.36 | 114,139.20 | 98,266.18  |
| 07/23/04    | 05:52:29    | 112,798.80 | 117,704.52 | 103,931.63 |
| 07/23/04    | 05:53:58    | 118,792.30 | 122,393.16 | 113,748.48 |
| 07/23/04    | 05:55:30    | 122,115.86 | 135,824.17 | 106,813.19 |
| 07/23/04    | 05:57:00    | 131,442.14 | 141,050.06 | 124,029.30 |
| 07/23/04    | 05:58:30    | 122,860.40 | 127,203.91 | 117,289.38 |
| 07/23/04    | 05:59:59    | 122,309.59 | 126,349.20 | 116,166.05 |
| 07/23/04    | 06:01:30    | 122,949.66 | 126,788.77 | 120,610.50 |
| 07/23/04    | 06:03:00    | 120,799.62 | 124,981.69 | 117,484.73 |
| 07/23/04    | 06:04:30    | 116,792.56 | 119,072.04 | 114,505.49 |
| 07/23/04    | 06:06:00    | 115,095.10 | 116,703.30 | 112,527.47 |
| 07/23/04    | 06:07:31    | 113,915.07 | 115,677.66 | 111,330.89 |
| 07/23/04    | 06:09:01    | 112,256.14 | 115,091.58 | 107,155.07 |
| 07/23/04    | 06:10:30    | 110,850.36 | 114,505.49 | 107,155.07 |
| 07/23/04    | 06:12:00    | 111,699.63 | 113,431.02 | 108,937.73 |
| 07/23/04    | 06:13:31    | 112,302.80 | 115,311.35 | 110,061.05 |
| 07/23/04    | 06:15:01    | 109,930.81 | 112,063.49 | 106,642.25 |
| 07/23/04    | 06:16:31    | 102,446.62 | 107,301.59 | 94,017.09  |
| 07/23/04    | 06:18:01    | 104,700.59 | 107,838.83 | 99,438.34  |
| 07/23/04    | 06:19:32    | 110,501.97 | 116,776.55 | 103,369.96 |
| 07/23/04    | 06:21:02    | 116,377.42 | 119,926.74 | 112,576.31 |
| 07/23/04    | 06:22:31    | 119,053.32 | 124,151.41 | 114,920.63 |
| 07/23/04    | 06:24:01    | 121,437.52 | 124,957.27 | 117,264.96 |
| 07/23/04    | 06:25:32    | 126,727.45 | 146,788.77 | 103,809.52 |
| 07/23/04    | 06:27:02    | 129,346.36 | 134,285.72 | 123,247.86 |
| 07/23/04    | 06:28:32    | 128,137.30 | 132,503.05 | 123,980.46 |
| 07/23/04    | 06:30:03    | 122,983.86 | 126,568.98 | 118,192.92 |
| 07/23/04    | 06:31:33    | 119,580.79 | 121,636.14 | 117,655.68 |
| 07/23/04    | 06:33:03    | 118,641.70 | 122,173.38 | 116,361.41 |
| 07/23/04    | 06:34:32    | 119,060.38 | 122,173.38 | 116,727.72 |
| 07/23/04    | 06:36:02    | 117,685.52 | 122,466.42 | 114,358.98 |
| 07/23/04    | 06:37:33    | 116,027.95 | 119,780.22 | 113,235.66 |

EVR0001  
07/28/04

BAYOU STEEL CORPORATION  
FURNACE #1 & #2 TOTAL FLOW (SCFM) - EVERY 15 MIN

6  
08:11

| END<br>DATE | END<br>TIME | AVG        | MAX        | MIN        |
|-------------|-------------|------------|------------|------------|
| ----        | ----        | ---        | ---        | ---        |
| 07/23/04    | 06:39:03    | 113,168.36 | 116,141.63 | 109,621.49 |
| 07/23/04    | 06:40:33    | 103,337.95 | 114,432.23 | 95,091.58  |
| 07/23/04    | 06:42:04    | 112,558.41 | 126,886.45 | 96,239.31  |
| 07/23/04    | 06:43:34    | 116,668.30 | 121,611.72 | 111,282.05 |
| 07/23/04    | 06:45:04    | 113,954.15 | 116,996.34 | 108,913.31 |
| 07/23/04    | 06:46:33    | 113,741.42 | 115,457.88 | 111,697.20 |
| 07/23/04    | 06:48:03    | 115,058.20 | 118,119.66 | 111,575.09 |
| 07/23/04    | 06:49:34    | 116,249.09 | 118,070.82 | 114,627.59 |
| 07/23/04    | 06:51:04    | 113,222.09 | 118,534.80 | 109,474.97 |
| 07/23/04    | 06:52:34    | 102,605.34 | 110,183.15 | 91,159.95  |
| 07/23/04    | 06:54:05    | 112,049.38 | 128,327.23 | 95,555.55  |
| 07/23/04    | 06:55:35    | 117,648.35 | 122,930.41 | 114,481.08 |
| 07/23/04    | 06:57:05    | 111,670.05 | 114,481.08 | 108,424.91 |
| 07/23/04    | 06:58:34    | 116,317.73 | 119,658.12 | 112,625.16 |
| 07/23/04    | 07:00:05    | 115,629.09 | 118,803.42 | 112,600.73 |
| 07/23/04    | 07:01:35    | 112,051.28 | 114,969.48 | 109,450.55 |
| 07/23/04    | 07:03:05    | 110,574.41 | 113,846.16 | 106,910.87 |
| 07/23/04    | 07:04:34    | 108,220.05 | 111,159.95 | 105,909.65 |
| 07/23/04    | 07:06:06    | 110,206.48 | 112,796.09 | 106,446.88 |
| 07/23/04    | 07:07:35    | 107,519.20 | 110,769.23 | 105,128.20 |
| 07/23/04    | 07:09:05    | 107,140.69 | 111,819.29 | 103,809.52 |
| 07/23/04    | 07:10:36    | 97,324.11  | 105,909.65 | 89,328.45  |
| 07/23/04    | 07:12:06    | 98,616.74  | 107,985.35 | 89,328.45  |
| 07/23/04    | 07:13:36    | 105,886.85 | 112,625.16 | 100,512.82 |
| 07/23/04    | 07:15:06    | 113,240.80 | 120,781.44 | 107,301.59 |
| 07/23/04    | 07:16:37    | 116,539.14 | 127,301.59 | 112,063.49 |
| 07/23/04    | 07:18:07    | 124,595.58 | 133,528.69 | 86,739.93  |
| 07/23/04    | 07:19:36    | 121,367.25 | 128,107.45 | 116,581.20 |
| 07/23/04    | 07:21:06    | 115,913.98 | 118,119.66 | 113,162.39 |
| 07/23/04    | 07:22:37    | 114,758.65 | 118,827.84 | 112,503.05 |
| 07/23/04    | 07:24:07    | 113,874.91 | 119,365.08 | 109,206.35 |
| 07/23/04    | 07:25:37    | 113,205.80 | 117,631.26 | 109,133.09 |
| 07/23/04    | 07:27:07    | 113,395.20 | 118,144.08 | 109,499.39 |
| 07/23/04    | 07:28:38    | 114,295.21 | 117,387.05 | 111,184.38 |
| 07/23/04    | 07:30:08    | 114,439.56 | 119,877.90 | 110,964.59 |
| 07/23/04    | 07:31:37    | 108,165.78 | 115,482.30 | 96,630.04  |
| 07/23/04    | 07:33:07    | 112,335.37 | 116,971.91 | 108,009.77 |
| 07/23/04    | 07:34:38    | 113,587.30 | 118,656.90 | 109,670.33 |
| 07/23/04    | 07:36:08    | 119,418.80 | 122,051.28 | 116,605.62 |
| 07/23/04    | 07:37:38    | 125,200.38 | 143,174.61 | 108,058.61 |
| 07/23/04    | 07:39:08    | 129,942.75 | 143,174.61 | 122,979.24 |
| 07/23/04    | 07:40:39    | 120,599.65 | 125,470.09 | 117,704.52 |
| 07/23/04    | 07:42:09    | 118,339.71 | 122,832.73 | 114,822.95 |
| 07/23/04    | 07:43:38    | 119,320.58 | 123,833.95 | 115,995.12 |
| 07/23/04    | 07:45:08    | 118,421.38 | 122,832.73 | 115,360.20 |
| 07/23/04    | 07:46:39    | 114,745.90 | 116,947.50 | 112,380.95 |
| 07/23/04    | 07:48:09    | 108,437.12 | 115,921.86 | 92,087.91  |
| 07/23/04    | 07:49:39    | 104,813.19 | 116,849.82 | 89,768.01  |
| 07/23/04    | 07:51:10    | 119,514.86 | 123,565.32 | 111,575.09 |
| 07/23/04    | 07:52:40    | 113,758.24 | 118,046.40 | 112,063.49 |
| 07/23/04    | 07:54:10    | 112,538.87 | 117,875.46 | 108,009.77 |
| 07/23/04    | 07:55:39    | 115,720.26 | 118,876.68 | 111,379.73 |
| 07/23/04    | 07:57:09    | 112,066.20 | 118,632.48 | 108,498.17 |

EVR0001  
07/28/04

BAYOU STEEL CORPORATION  
FURNACE #1 & #2 TOTAL FLOW (SCFM) - EVERY 15 MIN

7  
08:11

| END<br>DATE | END<br>TIME | AVG        | MAX        | MIN        |
|-------------|-------------|------------|------------|------------|
| 07/23/04    | 07:58:40    | 111,698.82 | 115,409.04 | 108,766.79 |
| 07/23/04    | 08:00:10    | 108,213.00 | 112,503.05 | 104,664.23 |
| 07/23/04    | 08:01:39    | 109,128.20 | 112,967.03 | 105,030.52 |
| 07/23/04    | 08:03:11    | 108,121.83 | 110,085.47 | 106,202.69 |
| 07/23/04    | 08:04:41    | 103,032.97 | 109,719.17 | 98,876.68  |
| 07/23/04    | 08:06:11    | 101,964.45 | 105,836.38 | 99,511.60  |
| 07/23/04    | 08:07:40    | 106,322.62 | 111,868.13 | 101,831.50 |
| 07/23/04    | 08:09:10    | 97,921.86  | 104,908.42 | 93,504.27  |
| 07/23/04    | 08:10:41    | 100,797.45 | 107,765.57 | 96,947.50  |
| 07/23/04    | 08:12:11    | 107,000.13 | 109,133.09 | 104,420.02 |
| 07/23/04    | 08:13:40    | 110,661.51 | 122,612.95 | 91,990.23  |
| 07/23/04    | 08:15:12    | 122,735.59 | 133,724.05 | 81,416.36  |
| 07/23/04    | 08:16:41    | 117,785.38 | 124,200.24 | 114,652.02 |
| 07/23/04    | 08:18:12    | 114,354.63 | 117,826.62 | 107,203.91 |
| 07/23/04    | 08:19:41    | 108,720.12 | 114,700.85 | 102,148.96 |
| 07/23/04    | 08:21:11    | 110,897.57 | 116,166.05 | 104,981.69 |
| 07/23/04    | 08:22:42    | 112,626.78 | 116,678.88 | 109,328.45 |
| 07/23/04    | 08:24:12    | 108,273.51 | 111,282.05 | 104,713.06 |
| 07/23/04    | 08:25:41    | 108,065.12 | 110,109.89 | 105,909.65 |
| 07/23/04    | 08:27:13    | 100,245.55 | 108,205.13 | 89,255.19  |
| 07/23/04    | 08:28:42    | 103,292.63 | 118,779.00 | 83,858.37  |
| 07/23/04    | 08:30:13    | 108,862.02 | 116,825.40 | 99,609.28  |
| 07/23/04    | 08:31:44    | 109,329.27 | 113,333.34 | 100,683.76 |
| 07/23/04    | 08:33:15    | 106,704.66 | 112,796.09 | 99,658.12  |
| 07/23/04    | 08:34:45    | 107,605.48 | 111,965.81 | 99,169.72  |
| 07/23/04    | 08:36:15    | 109,801.93 | 112,405.38 | 107,350.43 |
| 07/23/04    | 08:37:44    | 96,913.58  | 110,427.35 | 85,885.23  |
| 07/23/04    | 08:39:14    | 108,495.45 | 118,363.86 | 82,222.22  |
| 07/23/04    | 08:40:45    | 115,126.85 | 117,167.27 | 112,234.43 |
| 07/23/04    | 08:42:15    | 110,062.41 | 114,456.66 | 108,498.17 |
| 07/23/04    | 08:43:46    | 110,648.48 | 114,529.91 | 107,374.84 |
| 07/23/04    | 08:45:16    | 107,231.04 | 109,523.81 | 104,786.33 |
| 07/23/04    | 08:46:46    | 106,837.61 | 109,670.33 | 103,760.69 |
| 07/23/04    | 08:48:16    | 106,005.97 | 109,890.11 | 103,101.34 |
| 07/23/04    | 08:49:45    | 101,265.77 | 105,665.45 | 96,239.31  |
| 07/23/04    | 08:51:17    | 105,438.88 | 111,990.23 | 96,019.54  |
| 07/23/04    | 08:52:46    | 103,950.62 | 106,813.19 | 101,025.64 |
| 07/23/04    | 08:54:16    | 102,862.57 | 107,326.01 | 98,461.54  |
| 07/23/04    | 08:55:47    | 104,375.26 | 110,354.09 | 95,262.52  |
| 07/23/04    | 08:57:17    | 97,711.30  | 107,106.23 | 90,671.55  |
| 07/23/04    | 08:58:47    | 102,041.79 | 116,190.48 | 80,903.54  |
| 07/23/04    | 09:00:16    | 108,582.28 | 115,335.77 | 101,123.32 |
| 07/23/04    | 09:01:47    | 96,357.34  | 105,689.87 | 81,611.72  |
| 07/23/04    | 09:03:18    | 101,543.89 | 109,963.37 | 86,691.09  |
| 07/23/04    | 09:04:48    | 109,563.16 | 115,213.67 | 105,030.52 |
| 07/23/04    | 09:06:17    | 111,918.33 | 124,273.51 | 97,313.80  |
| 07/23/04    | 09:07:48    | 120,888.62 | 130,622.71 | 93,284.49  |
| 07/23/04    | 09:09:18    | 119,507.53 | 124,468.87 | 116,874.23 |
| 07/23/04    | 09:10:47    | 114,287.07 | 119,487.18 | 110,915.75 |
| 07/23/04    | 09:12:17    | 113,743.05 | 117,020.76 | 111,037.85 |
| 07/23/04    | 09:13:48    | 110,061.05 | 112,429.79 | 106,666.66 |
| 07/23/04    | 09:15:18    | 109,957.95 | 113,162.39 | 102,783.88 |
| 07/23/04    | 09:16:49    | 111,183.02 | 117,704.52 | 106,544.57 |

EVR0001  
07/28/04

BAYOU STEEL CORPORATION  
FURNACE #1 & #2 TOTAL FLOW (SCFM) - EVERY 15 MIN

8  
08:11

| END<br>DATE | END<br>TIME | AVG        | MAX        | MIN        |
|-------------|-------------|------------|------------|------------|
| 07/23/04    | 09:18:18    | 105,410.39 | 109,694.75 | 88,669.11  |
| 07/23/04    | 09:19:49    | 99,342.02  | 102,954.82 | 91,208.79  |
| 07/23/04    | 09:21:19    | 110,014.92 | 115,897.44 | 84,884.01  |
| 07/23/04    | 09:22:48    | 111,999.73 | 114,603.17 | 110,500.61 |
| 07/23/04    | 09:24:18    | 109,461.41 | 112,234.43 | 104,957.27 |
| 07/23/04    | 09:25:49    | 105,882.52 | 111,379.73 | 101,294.26 |
| 07/23/04    | 09:27:19    | 112,606.16 | 120,170.94 | 107,399.27 |
| 07/23/04    | 09:28:50    | 107,841.54 | 116,630.04 | 93,357.75  |
| 07/23/04    | 09:30:20    | 107,286.66 | 121,245.42 | 94,163.62  |
| 07/23/04    | 09:31:50    | 119,618.77 | 125,738.70 | 113,089.13 |
| 07/23/04    | 09:33:20    | 115,504.00 | 119,169.72 | 110,647.13 |
| 07/23/04    | 09:34:49    | 110,291.69 | 113,333.34 | 107,155.07 |
| 07/23/04    | 09:36:19    | 109,160.22 | 112,112.34 | 104,688.65 |
| 07/23/04    | 09:37:50    | 107,054.67 | 112,722.84 | 99,780.22  |
| 07/23/04    | 09:39:20    | 104,396.96 | 109,865.69 | 97,728.94  |
| 07/23/04    | 09:40:51    | 107,855.11 | 110,061.05 | 105,543.34 |
| 07/23/04    | 09:42:21    | 104,661.51 | 110,451.77 | 94,554.34  |
| 07/23/04    | 09:43:51    | 101,014.79 | 108,278.39 | 96,556.77  |
| 07/23/04    | 09:45:21    | 105,691.22 | 108,840.05 | 101,489.63 |
| 07/23/04    | 09:46:50    | 104,376.61 | 107,936.51 | 99,658.12  |
| 07/23/04    | 09:48:20    | 104,592.32 | 109,670.33 | 101,001.22 |
| 07/23/04    | 09:49:51    | 102,737.76 | 107,252.75 | 94,822.95  |
| 07/23/04    | 09:51:21    | 97,983.99  | 102,979.24 | 94,725.27  |
| 07/23/04    | 09:52:52    | 92,553.25  | 106,031.74 | 77,558.00  |
| 07/23/04    | 09:54:22    | 94,566.55  | 105,836.38 | 67,448.11  |
| 07/23/04    | 09:55:52    | 102,448.79 | 112,893.77 | 90,573.87  |
| 07/23/04    | 09:57:22    | 108,038.26 | 115,604.40 | 102,564.10 |
| 07/23/04    | 09:58:51    | 109,325.73 | 114,945.05 | 104,664.23 |
| 07/23/04    | 10:00:21    | 117,286.66 | 121,880.34 | 109,523.81 |
| 07/23/04    | 10:01:52    | 115,757.70 | 128,766.79 | 93,333.34  |
| 07/23/04    | 10:03:22    | 127,363.99 | 134,529.92 | 111,452.99 |
| 07/23/04    | 10:04:53    | 118,521.23 | 122,954.82 | 113,455.43 |
| 07/23/04    | 10:06:23    | 117,171.34 | 121,001.22 | 113,821.73 |
| 07/23/04    | 10:07:52    | 112,307.70 | 115,506.72 | 109,084.25 |
| 07/23/04    | 10:09:23    | 110,123.45 | 115,653.23 | 101,294.26 |
| 07/23/04    | 10:10:52    | 112,383.66 | 118,876.68 | 105,763.13 |
| 07/23/04    | 10:12:22    | 109,918.60 | 111,990.23 | 105,177.05 |
| 07/23/04    | 10:13:53    | 103,880.07 | 111,721.61 | 94,407.81  |
| 07/23/04    | 10:15:23    | 100,009.50 | 102,002.45 | 94,725.27  |
| 07/23/04    | 10:16:54    | 96,058.88  | 118,412.70 | 46,837.61  |
| 07/23/04    | 10:18:24    | 114,074.07 | 119,389.50 | 109,426.13 |
| 07/23/04    | 10:19:53    | 109,023.20 | 113,894.99 | 102,661.78 |
| 07/23/04    | 10:21:24    | 113,808.16 | 116,727.72 | 108,888.89 |
| 07/23/04    | 10:22:54    | 112,010.58 | 116,923.08 | 106,739.93 |
| 07/23/04    | 10:24:25    | 109,959.30 | 117,460.32 | 105,470.09 |
| 07/23/04    | 10:25:54    | 100,127.52 | 109,670.33 | 93,601.95  |
| 07/23/04    | 10:27:24    | 108,134.58 | 116,971.91 | 90,109.89  |
| 07/23/04    | 10:28:55    | 113,021.03 | 114,896.22 | 109,816.85 |
| 07/23/04    | 10:30:25    | 112,719.58 | 115,702.08 | 107,838.83 |
| 07/23/04    | 10:31:56    | 109,467.64 | 113,113.55 | 106,666.66 |
| 07/23/04    | 10:33:26    | 110,204.31 | 112,820.52 | 107,765.57 |
| 07/23/04    | 10:34:56    | 110,859.86 | 114,749.70 | 108,400.49 |
| 07/23/04    | 10:36:26    | 108,195.36 | 111,452.99 | 105,909.65 |

EVR0001  
07/28/04

BAYOU STEEL CORPORATION  
FURNACE #1 & #2 TOTAL FLOW (SCFM) - EVERY 15 MIN

9  
08:11

| END<br>DATE | END<br>TIME | AVG        | MAX        | MIN        |
|-------------|-------------|------------|------------|------------|
| 07/23/04    | 10:37:55    | 106,339.44 | 109,108.67 | 102,930.41 |
| 07/23/04    | 10:39:25    | 105,823.63 | 108,693.53 | 102,124.54 |
| 07/23/04    | 10:40:56    | 105,244.34 | 110,061.05 | 99,853.48  |
| 07/23/04    | 10:42:26    | 102,211.37 | 107,960.93 | 94,920.63  |
| 07/23/04    | 10:43:57    | 101,326.82 | 104,639.80 | 95,995.12  |
| 07/23/04    | 10:45:27    | 102,278.66 | 105,860.80 | 97,948.72  |
| 07/23/04    | 10:46:57    | 103,480.13 | 109,279.61 | 97,191.70  |
| 07/23/04    | 10:48:27    | 103,148.55 | 110,573.87 | 94,188.03  |
| 07/23/04    | 10:49:56    | 98,348.94  | 102,759.46 | 90,866.91  |
| 07/23/04    | 10:51:28    | 97,853.75  | 103,614.16 | 88,693.53  |
| 07/23/04    | 10:52:57    | 108,947.77 | 116,923.08 | 98,705.74  |
| 07/23/04    | 10:54:27    | 112,530.73 | 124,200.24 | 105,543.34 |
| 07/23/04    | 10:55:58    | 118,811.02 | 130,818.07 | 93,431.02  |
| 07/23/04    | 10:57:28    | 113,422.60 | 123,540.91 | 97,362.64  |
| 07/23/04    | 10:58:58    | 112,289.52 | 117,387.05 | 99,145.30  |
| 07/23/04    | 11:00:27    | 111,766.11 | 115,115.99 | 107,277.16 |
| 07/23/04    | 11:01:58    | 109,178.40 | 113,040.30 | 105,128.20 |
| 07/23/04    | 11:03:28    | 108,397.23 | 112,283.27 | 103,003.66 |
| 07/23/04    | 11:04:59    | 103,261.70 | 107,277.16 | 99,096.46  |
| 07/23/04    | 11:06:29    | 103,969.88 | 111,746.03 | 96,141.63  |
| 07/23/04    | 11:07:59    | 95,055.76  | 106,398.05 | 76,971.91  |
| 07/23/04    | 11:09:29    | 107,305.38 | 117,411.48 | 100,366.30 |
| 07/23/04    | 11:11:01    | 113,014.79 | 125,616.61 | 91,306.47  |
| 07/23/04    | 11:12:30    | 110,752.95 | 115,286.94 | 106,251.52 |
| 07/23/04    | 11:14:00    | 105,558.00 | 113,382.17 | 98,217.34  |
| 07/23/04    | 11:15:31    | 107,406.32 | 110,402.93 | 102,442.00 |
| 07/23/04    | 11:17:01    | 109,349.07 | 113,846.16 | 105,738.70 |
| 07/23/04    | 11:18:30    | 96,989.55  | 109,304.03 | 81,538.46  |
| 07/23/04    | 11:20:01    | 97,898.52  | 114,822.95 | 81,440.78  |
| 07/23/04    | 11:21:31    | 106,878.04 | 112,869.35 | 98,339.44  |
| 07/23/04    | 11:23:02    | 108,009.77 | 112,918.20 | 104,004.88 |
| 07/23/04    | 11:24:31    | 105,566.41 | 111,575.09 | 98,998.78  |
| 07/23/04    | 11:26:01    | 106,792.56 | 115,238.09 | 101,978.02 |
| 07/23/04    | 11:27:32    | 106,790.66 | 110,427.35 | 104,371.19 |
| 07/23/04    | 11:29:02    | 106,808.84 | 108,937.73 | 103,272.28 |
| 07/23/04    | 11:30:31    | 103,779.68 | 108,522.59 | 100,146.52 |
| 07/23/04    | 11:32:01    | 101,603.04 | 103,882.78 | 98,827.84  |
| 07/23/04    | 11:33:32    | 103,349.07 | 106,935.29 | 99,047.62  |
| 07/23/04    | 11:35:03    | 99,651.06  | 102,319.90 | 95,409.04  |
| 07/23/04    | 11:36:32    | 101,769.09 | 107,985.35 | 96,068.38  |
| 07/23/04    | 11:38:02    | 101,152.90 | 103,980.46 | 99,023.20  |
| 07/23/04    | 11:39:33    | 98,361.15  | 102,637.36 | 91,452.99  |
| 07/23/04    | 11:41:03    | 95,039.48  | 101,587.30 | 87,326.01  |
| 07/23/04    | 11:42:32    | 97,791.34  | 105,787.55 | 88,449.33  |
| 07/23/04    | 11:44:02    | 106,493.55 | 113,992.67 | 100,586.08 |
| 07/23/04    | 11:45:33    | 107,849.41 | 114,212.45 | 103,052.50 |
| 07/23/04    | 11:47:04    | 111,359.92 | 118,388.28 | 105,250.30 |
| 07/23/04    | 11:48:33    | 117,484.47 | 124,053.73 | 109,450.55 |
| 07/23/04    | 11:50:03    | 118,073.53 | 126,398.05 | 111,599.51 |
| 07/23/04    | 11:51:34    | 115,049.52 | 132,551.89 | 104,688.65 |
| 07/23/04    | 11:53:04    | 131,892.83 | 142,319.91 | 120,854.70 |
| 07/23/04    | 11:54:33    | 120,384.48 | 123,663.00 | 113,284.49 |
| 07/23/04    | 11:56:03    | 112,704.38 | 114,017.09 | 111,111.11 |

EVR0001  
07/28/04

BAYOU STEEL CORPORATION  
FURNACE #1 & #2 TOTAL FLOW (SCFM) - EVERY 15 MIN

10  
08:11

| END<br>DATE | END<br>TIME | AVG        | MAX        | MIN        |
|-------------|-------------|------------|------------|------------|
| ----        | ----        | ----       | ----       | ----       |
| 07/23/04    | 11:57:34    | 110,716.87 | 113,821.73 | 106,129.43 |
| 07/23/04    | 11:59:05    | 111,226.97 | 113,724.05 | 106,129.43 |
| 07/23/04    | 12:00:35    | 113,238.09 | 116,459.09 | 108,229.55 |
| 07/23/04    | 12:02:05    | 110,153.58 | 114,261.30 | 105,250.30 |
| 07/23/04    | 12:03:35    | 103,684.16 | 111,941.39 | 86,227.11  |
| 07/23/04    | 12:05:05    | 97,268.48  | 100,366.30 | 92,454.21  |
| 07/23/04    | 12:06:34    | 106,751.59 | 119,365.08 | 50,940.17  |
| 07/23/04    | 12:08:04    | 114,004.61 | 118,461.54 | 107,228.33 |
| 07/23/04    | 12:09:35    | 110,729.07 | 113,772.89 | 106,471.30 |
| 07/23/04    | 12:11:05    | 105,660.84 | 108,595.85 | 98,803.42  |
| 07/23/04    | 12:12:36    | 105,310.54 | 110,427.35 | 99,755.80  |
| 07/23/04    | 12:14:06    | 105,612.80 | 108,498.17 | 103,272.28 |
| 07/23/04    | 12:15:36    | 98,183.15  | 108,302.80 | 88,424.91  |
| 07/23/04    | 12:17:06    | 108,221.95 | 117,387.05 | 88,131.87  |
| 07/23/04    | 12:18:35    | 112,482.70 | 116,727.72 | 105,323.56 |
| 07/23/04    | 12:20:05    | 107,568.30 | 114,212.45 | 103,443.23 |
| 07/23/04    | 12:21:36    | 108,036.90 | 111,501.83 | 103,565.32 |
| 07/23/04    | 12:23:06    | 108,751.59 | 112,918.20 | 104,688.65 |
| 07/23/04    | 12:24:37    | 105,897.71 | 110,842.49 | 101,514.04 |
| 07/23/04    | 12:26:07    | 107,267.95 | 112,576.31 | 100,830.28 |
| 07/23/04    | 12:27:37    | 105,227.52 | 112,576.31 | 99,975.58  |
| 07/23/04    | 12:29:07    | 103,620.67 | 109,426.13 | 97,484.73  |
| 07/23/04    | 12:30:36    | 102,500.88 | 109,450.55 | 98,388.28  |
| 07/23/04    | 12:32:06    | 103,540.91 | 108,205.13 | 99,047.62  |
| 07/23/04    | 12:33:37    | 105,361.55 | 108,009.77 | 102,686.20 |
| 07/23/04    | 12:35:07    | 101,825.53 | 105,152.63 | 97,777.78  |
| 07/23/04    | 12:36:38    | 102,316.10 | 108,131.87 | 95,164.84  |
| 07/23/04    | 12:38:08    | 101,067.97 | 104,004.88 | 99,072.04  |
| 07/23/04    | 12:39:38    | 101,645.64 | 109,670.33 | 91,233.21  |
| 07/23/04    | 12:41:08    | 110,024.42 | 117,680.10 | 94,529.91  |
| 07/23/04    | 12:42:37    | 115,562.34 | 119,438.34 | 110,402.93 |
| 07/23/04    | 12:44:07    | 120,172.02 | 127,081.80 | 113,846.16 |
| 07/23/04    | 12:45:38    | 115,677.93 | 119,609.28 | 111,819.29 |
| 07/23/04    | 12:47:08    | 118,437.39 | 123,199.02 | 114,383.39 |
| 07/23/04    | 12:48:39    | 120,405.10 | 123,638.59 | 112,136.75 |
| 07/23/04    | 12:50:09    | 123,791.62 | 128,131.87 | 118,583.64 |
| 07/23/04    | 12:51:39    | 121,747.66 | 127,423.69 | 116,581.20 |
| 07/23/04    | 12:53:09    | 128,772.48 | 134,358.97 | 119,731.38 |
| 07/23/04    | 12:54:38    | 128,722.02 | 131,916.97 | 122,246.64 |
| 07/23/04    | 12:56:08    | 130,843.30 | 133,968.25 | 128,302.80 |
| 07/23/04    | 12:57:39    | 130,350.29 | 136,947.50 | 126,471.30 |
| 07/23/04    | 12:59:09    | 131,676.58 | 137,094.02 | 127,863.25 |
| 07/23/04    | 13:00:40    | 130,524.48 | 136,703.30 | 119,853.48 |
| 07/23/04    | 13:02:10    | 128,301.45 | 138,681.31 | 120,293.04 |
| 07/23/04    | 13:03:39    | 136,471.58 | 142,832.72 | 132,063.48 |
| 07/23/04    | 13:05:09    | 136,498.72 | 142,393.16 | 130,231.99 |
| 07/23/04    | 13:06:40    | 136,221.41 | 139,487.17 | 131,623.94 |
| 07/23/04    | 13:08:10    | 141,083.44 | 145,518.92 | 137,973.14 |
| 07/23/04    | 13:09:41    | 141,400.08 | 144,810.75 | 139,120.88 |
| 07/23/04    | 13:11:11    | 142,623.25 | 145,958.48 | 140,024.42 |
| 07/23/04    | 13:12:41    | 139,660.02 | 152,771.67 | 129,084.25 |
| 07/23/04    | 13:14:11    | 143,266.58 | 154,505.50 | 132,918.19 |
| 07/23/04    | 13:15:40    | 134,204.05 | 136,385.84 | 131,746.03 |

EVR0001  
07/28/04

BAYOU STEEL CORPORATION  
FURNACE #1 & #2 TOTAL FLOW (SCFM) - EVERY 15 MIN

11  
08:11

| END<br>DATE | END<br>TIME | AVG        | MAX        | MIN        |
|-------------|-------------|------------|------------|------------|
| 07/23/04    | 13:17:10    | 133,255.45 | 135,775.33 | 129,450.55 |
| 07/23/04    | 13:18:41    | 133,100.80 | 139,560.44 | 127,032.97 |
| 07/23/04    | 13:20:11    | 131,181.66 | 136,630.03 | 125,738.70 |
| 07/23/04    | 13:21:42    | 126,507.39 | 129,719.17 | 122,148.96 |
| 07/23/04    | 13:23:12    | 123,121.96 | 125,811.97 | 119,291.82 |
| 07/23/04    | 13:24:42    | 119,783.48 | 122,271.06 | 118,217.34 |
| 07/23/04    | 13:26:12    | 114,265.37 | 119,755.80 | 99,926.74  |
| 07/23/04    | 13:27:41    | 110,150.59 | 124,566.55 | 103,076.92 |
| 07/23/04    | 13:29:11    | 115,090.76 | 124,566.55 | 102,442.00 |
| 07/23/04    | 13:30:42    | 123,626.91 | 126,495.73 | 120,561.66 |
| 07/23/04    | 13:32:12    | 123,370.51 | 126,520.15 | 121,172.16 |
| 07/23/04    | 13:33:43    | 127,247.32 | 130,891.33 | 123,418.80 |
| 07/23/04    | 13:35:13    | 131,054.13 | 135,750.92 | 128,107.45 |
| 07/23/04    | 13:36:43    | 134,021.44 | 136,923.08 | 131,916.97 |
| 07/23/04    | 13:38:13    | 136,160.09 | 138,412.70 | 134,065.94 |
| 07/23/04    | 13:39:42    | 138,440.64 | 141,587.30 | 134,285.72 |
| 07/23/04    | 13:41:12    | 140,377.70 | 144,615.39 | 136,752.14 |
| 07/23/04    | 13:42:43    | 140,718.77 | 151,062.27 | 128,376.07 |
| 07/23/04    | 13:44:13    | 141,343.92 | 144,737.48 | 138,779.00 |
| 07/23/04    | 13:45:44    | 142,282.19 | 145,616.61 | 140,586.08 |
| 07/23/04    | 13:47:14    | 140,736.67 | 144,200.25 | 138,339.44 |
| 07/23/04    | 13:48:44    | 141,613.89 | 145,567.77 | 138,779.00 |
| 07/23/04    | 13:50:14    | 143,302.13 | 145,934.06 | 141,636.14 |
| 07/23/04    | 13:51:43    | 144,249.89 | 145,738.70 | 142,222.22 |
| 07/23/04    | 13:53:13    | 144,588.25 | 147,081.81 | 142,637.36 |
| 07/23/04    | 13:54:44    | 147,832.59 | 149,768.02 | 144,395.61 |
| 07/23/04    | 13:56:14    | 146,837.88 | 150,402.94 | 144,493.28 |
| 07/23/04    | 13:57:45    | 147,072.31 | 149,645.91 | 144,297.92 |
| 07/23/04    | 13:59:15    | 147,657.84 | 151,892.55 | 143,028.08 |
| 07/23/04    | 14:00:44    | 148,827.03 | 158,730.16 | 137,802.20 |
| 07/23/04    | 14:02:14    | 148,043.69 | 151,941.39 | 146,031.75 |
| 07/23/04    | 14:03:45    | 148,425.72 | 153,455.44 | 145,934.06 |
| 07/23/04    | 14:05:15    | 149,205.81 | 152,136.75 | 145,641.03 |
| 07/23/04    | 14:06:45    | 150,364.94 | 153,479.86 | 147,032.97 |
| 07/23/04    | 14:08:15    | 150,163.08 | 153,943.83 | 146,739.92 |
| 07/23/04    | 14:09:46    | 151,674.94 | 156,190.47 | 149,206.34 |
| 07/23/04    | 14:11:16    | 149,459.50 | 152,576.31 | 146,813.19 |
| 07/23/04    | 14:12:45    | 149,805.72 | 152,356.53 | 147,057.39 |
| 07/23/04    | 14:14:15    | 151,610.64 | 155,189.25 | 149,279.61 |
| 07/23/04    | 14:15:46    | 152,813.19 | 154,676.44 | 148,595.84 |
| 07/23/04    | 14:17:16    | 151,414.19 | 155,726.50 | 148,595.84 |
| 07/23/04    | 14:18:47    | 151,616.33 | 153,992.67 | 148,864.47 |
| 07/23/04    | 14:20:16    | 152,254.52 | 155,457.88 | 148,913.31 |
| 07/23/04    | 14:21:47    | 151,413.64 | 154,627.59 | 148,327.23 |
| 07/23/04    | 14:23:17    | 152,711.17 | 155,116.00 | 150,989.02 |
| 07/23/04    | 14:24:46    | 153,920.23 | 155,970.70 | 151,379.73 |
| 07/23/04    | 14:26:16    | 151,868.13 | 154,065.94 | 149,328.45 |
| 07/23/04    | 14:27:47    | 151,677.11 | 153,357.75 | 150,085.47 |
| 07/23/04    | 14:29:17    | 153,300.23 | 155,286.94 | 150,989.02 |
| 07/23/04    | 14:30:48    | 153,487.17 | 156,117.22 | 151,282.05 |
| 07/23/04    | 14:32:17    | 153,286.66 | 156,605.61 | 151,135.53 |
| 07/23/04    | 14:33:48    | 154,145.98 | 157,802.20 | 151,868.13 |
| 07/23/04    | 14:35:18    | 154,532.36 | 156,825.39 | 152,527.47 |

EVR0001  
07/28/04

BAYOU STEEL CORPORATION  
FURNACE #1 & #2 TOTAL FLOW (SCFM) - EVERY 15 MIN

12  
08:11

| END<br>DATE<br>---- | END<br>TIME<br>---- | AVG<br>--- | MAX<br>--- | MIN<br>--- |
|---------------------|---------------------|------------|------------|------------|
| 07/23/04            | 14:36:47            | 154,751.05 | 157,973.14 | 152,649.58 |
| 07/23/04            | 14:38:17            | 153,358.03 | 156,776.56 | 150,256.41 |
| 07/23/04            | 14:39:48            | 154,388.00 | 157,826.63 | 150,354.09 |
| 07/23/04            | 14:41:18            | 153,768.83 | 156,410.25 | 151,233.22 |
| 07/23/04            | 14:42:49            | 152,787.69 | 156,483.52 | 150,109.89 |
| 07/23/04            | 14:44:19            | 154,730.97 | 157,045.17 | 152,576.31 |
| 07/23/04            | 14:45:49            | 154,849.81 | 165,738.70 | 145,470.08 |
| 07/23/04            | 14:47:19            | 156,090.89 | 159,706.95 | 154,285.72 |
| 07/23/04            | 14:48:48            | 153,973.95 | 155,848.59 | 151,062.27 |
| 07/23/04            | 14:50:18            | 152,856.33 | 155,116.00 | 150,842.48 |
| 07/23/04            | 14:51:49            | 151,428.58 | 155,116.00 | 149,743.59 |
| 07/23/04            | 14:53:19            | 151,548.77 | 158,095.23 | 143,833.94 |
| 07/23/04            | 14:54:50            | 141,555.56 | 147,887.67 | 136,190.47 |
| 07/23/04            | 14:56:20            | 136,456.92 | 140,586.08 | 134,578.75 |
| 07/23/04            | 14:57:50            | 131,737.63 | 134,822.95 | 128,644.69 |
| 07/23/04            | 14:59:20            | 130,350.56 | 132,503.05 | 127,252.75 |
| 07/23/04            | 15:00:49            | 124,790.40 | 130,598.29 | 121,611.72 |
| 07/23/04            | 15:02:19            | 124,240.40 | 127,228.33 | 120,830.28 |
| 07/23/04            | 15:03:50            | 121,990.50 | 126,495.73 | 118,730.16 |
| 07/23/04            | 15:05:20            | 121,674.40 | 123,956.05 | 118,827.84 |
| 07/23/04            | 15:06:51            | 117,336.86 | 121,562.88 | 112,405.38 |
| 07/23/04            | 15:08:21            | 122,536.97 | 126,056.16 | 114,993.90 |
| 07/23/04            | 15:09:51            | 118,428.16 | 122,393.16 | 112,576.31 |
| 07/23/04            | 15:11:21            | 111,984.27 | 115,042.73 | 107,203.91 |
| 07/23/04            | 15:12:50            | 115,315.16 | 119,316.24 | 111,013.43 |
| 07/23/04            | 15:14:20            | 119,524.08 | 122,881.56 | 112,551.89 |
| 07/23/04            | 15:15:51            | 121,318.41 | 125,543.34 | 112,551.89 |
| 07/23/04            | 15:17:21            | 126,217.07 | 129,548.23 | 123,101.34 |
| 07/23/04            | 15:18:52            | 129,078.01 | 133,235.66 | 125,567.77 |
| 07/23/04            | 15:20:22            | 132,934.20 | 135,360.20 | 129,987.79 |
| 07/23/04            | 15:21:52            | 136,189.39 | 144,713.06 | 129,548.23 |
| 07/23/04            | 15:23:22            | 138,544.56 | 149,768.02 | 126,300.37 |
| 07/23/04            | 15:24:51            | 137,873.56 | 139,584.86 | 136,239.31 |
| 07/23/04            | 15:26:21            | 137,337.95 | 139,804.64 | 135,506.72 |
| 07/23/04            | 15:27:52            | 135,463.58 | 137,362.64 | 133,626.38 |
| 07/23/04            | 15:29:22            | 136,269.16 | 139,438.34 | 132,478.63 |
| 07/23/04            | 15:30:53            | 136,292.77 | 140,317.45 | 134,505.50 |
| 07/23/04            | 15:32:23            | 136,348.39 | 138,705.73 | 135,042.73 |
| 07/23/04            | 15:33:52            | 138,115.59 | 140,927.95 | 136,385.84 |
| 07/23/04            | 15:35:23            | 139,928.64 | 142,246.64 | 137,582.42 |
| 07/23/04            | 15:36:53            | 142,388.83 | 145,689.86 | 139,194.14 |
| 07/23/04            | 15:38:22            | 142,689.73 | 145,641.03 | 139,120.88 |
| 07/23/04            | 15:39:53            | 145,081.81 | 149,816.84 | 138,339.44 |
| 07/23/04            | 15:41:23            | 138,758.38 | 142,295.48 | 133,357.75 |
| 07/23/04            | 15:42:54            | 137,747.11 | 144,615.39 | 131,843.72 |
| 07/23/04            | 15:44:24            | 134,174.47 | 141,098.91 | 128,131.87 |
| 07/23/04            | 15:45:53            | 125,848.87 | 129,352.87 | 121,318.68 |
| 07/23/04            | 15:47:23            | 118,695.43 | 123,345.55 | 113,382.17 |
| 07/23/04            | 15:48:54            | 122,526.93 | 127,374.84 | 118,534.80 |
| 07/23/04            | 15:50:24            | 126,167.14 | 129,230.77 | 121,807.08 |
| 07/23/04            | 15:51:54            | 131,042.20 | 133,235.66 | 128,351.65 |
| 07/23/04            | 15:53:24            | 135,925.66 | 141,221.00 | 129,255.19 |
| 07/23/04            | 15:54:55            | 129,950.08 | 135,579.97 | 125,396.83 |

EVR0001  
07/28/04

BAYOU STEEL CORPORATION  
FURNACE #1 & #2 TOTAL FLOW (SCFM) - EVERY 15 MIN

13  
08:11

| END<br>DATE | END<br>TIME | AVG        | MAX        | MIN        |
|-------------|-------------|------------|------------|------------|
| 07/23/04    | 15:56:25    | 121,907.20 | 127,960.93 | 118,266.18 |
| 07/23/04    | 15:57:54    | 127,539.27 | 130,744.81 | 121,514.04 |
| 07/23/04    | 15:59:24    | 117,326.01 | 128,205.13 | 107,472.53 |
| 07/23/04    | 16:00:55    | 119,497.76 | 124,346.77 | 115,775.34 |
| 07/23/04    | 16:02:25    | 126,458.01 | 130,940.17 | 122,417.59 |
| 07/23/04    | 16:03:56    | 134,399.67 | 141,904.77 | 128,888.89 |
| 07/23/04    | 16:05:26    | 135,618.50 | 151,892.55 | 112,600.73 |
| 07/23/04    | 16:06:56    | 136,427.63 | 141,416.36 | 132,478.63 |
| 07/23/04    | 16:08:26    | 128,400.76 | 133,650.80 | 122,124.54 |
| 07/23/04    | 16:09:55    | 122,803.96 | 125,396.83 | 120,268.62 |
| 07/23/04    | 16:11:25    | 121,838.83 | 124,175.82 | 119,096.46 |
| 07/23/04    | 16:12:56    | 120,435.22 | 125,299.15 | 116,337.00 |
| 07/23/04    | 16:14:26    | 118,682.13 | 121,636.14 | 113,968.26 |
| 07/23/04    | 16:15:57    | 119,540.36 | 122,222.22 | 115,726.49 |
| 07/23/04    | 16:17:27    | 120,338.08 | 124,395.60 | 117,509.16 |
| 07/23/04    | 16:18:57    | 123,530.32 | 127,521.37 | 116,752.14 |
| 07/23/04    | 16:20:27    | 120,783.34 | 122,735.04 | 118,388.28 |
| 07/23/04    | 16:21:56    | 119,123.05 | 122,124.54 | 114,456.66 |
| 07/23/04    | 16:23:26    | 117,695.02 | 121,050.06 | 115,457.88 |
| 07/23/04    | 16:24:57    | 116,407.00 | 118,705.74 | 113,992.67 |
| 07/23/04    | 16:26:27    | 115,879.80 | 117,582.41 | 113,333.34 |
| 07/23/04    | 16:27:58    | 114,771.67 | 118,168.50 | 112,210.02 |
| 07/23/04    | 16:29:28    | 109,121.15 | 115,775.34 | 101,196.58 |
| 07/23/04    | 16:30:58    | 112,083.03 | 116,605.62 | 109,230.77 |
| 07/23/04    | 16:32:28    | 118,421.11 | 120,024.42 | 116,605.62 |
| 07/23/04    | 16:33:57    | 118,881.02 | 122,686.20 | 111,672.77 |
| 07/23/04    | 16:35:27    | 122,376.34 | 127,228.33 | 117,948.72 |
| 07/23/04    | 16:36:58    | 126,204.59 | 128,742.37 | 120,854.70 |
| 07/23/04    | 16:38:28    | 128,431.70 | 141,562.88 | 114,749.70 |
| 07/23/04    | 16:39:59    | 132,401.30 | 135,677.66 | 129,841.27 |
| 07/23/04    | 16:41:29    | 134,301.72 | 138,705.73 | 131,477.41 |
| 07/23/04    | 16:42:59    | 132,775.75 | 138,681.31 | 126,471.30 |
| 07/23/04    | 16:44:30    | 138,412.70 | 154,993.89 | 113,797.31 |
| 07/23/04    | 16:46:00    | 133,043.83 | 140,830.28 | 128,253.97 |
| 07/23/04    | 16:47:30    | 123,939.77 | 128,400.49 | 119,536.02 |
| 07/23/04    | 16:49:00    | 119,963.64 | 124,297.92 | 118,070.82 |
| 07/23/04    | 16:50:29    | 119,014.79 | 122,222.22 | 117,460.32 |
| 07/23/04    | 16:51:59    | 117,983.18 | 122,393.16 | 113,724.05 |
| 07/23/04    | 16:53:30    | 115,225.34 | 120,317.46 | 112,356.53 |
| 07/23/04    | 16:55:00    | 113,436.17 | 117,484.73 | 107,741.15 |
| 07/23/04    | 16:56:31    | 109,501.02 | 115,506.72 | 99,242.98  |
| 07/23/04    | 16:58:01    | 108,279.48 | 128,913.31 | 94,261.30  |
| 07/23/04    | 16:59:31    | 119,325.20 | 125,054.95 | 113,943.84 |
| 07/23/04    | 17:01:01    | 114,440.10 | 117,094.02 | 109,255.19 |
| 07/23/04    | 17:02:31    | 112,034.19 | 117,924.30 | 107,936.51 |
| 07/23/04    | 17:04:00    | 114,238.77 | 116,971.91 | 111,770.45 |
| 07/23/04    | 17:05:31    | 114,230.36 | 118,070.82 | 110,085.47 |
| 07/23/04    | 17:07:01    | 110,676.44 | 114,774.12 | 103,516.48 |
| 07/23/04    | 17:08:32    | 98,175.55  | 109,304.03 | 84,151.41  |
| 07/23/04    | 17:10:02    | 113,614.16 | 124,664.23 | 98,681.32  |
| 07/23/04    | 17:11:31    | 113,303.48 | 117,875.46 | 110,573.87 |
| 07/23/04    | 17:13:01    | 111,851.85 | 117,753.36 | 107,277.16 |
| 07/23/04    | 17:14:32    | 116,320.17 | 120,073.26 | 108,791.21 |

EVR0001  
07/28/04

BAYOU STEEL CORPORATION  
FURNACE #1 & #2 TOTAL FLOW (SCFM) - EVERY 15 MIN

14  
08:11

| END<br>DATE | END<br>TIME | AVG        | MAX        | MIN        |
|-------------|-------------|------------|------------|------------|
| 07/23/04    | 17:16:02    | 116,794.73 | 119,584.86 | 114,456.66 |
| 07/23/04    | 17:17:32    | 112,733.69 | 115,457.88 | 110,549.45 |
| 07/23/04    | 17:19:02    | 109,785.10 | 112,112.34 | 106,715.51 |
| 07/23/04    | 17:20:33    | 109,452.18 | 111,892.55 | 105,958.48 |
| 07/23/04    | 17:22:03    | 109,854.56 | 111,013.43 | 108,034.19 |
| 07/23/04    | 17:23:32    | 105,654.87 | 110,134.31 | 102,832.73 |
| 07/23/04    | 17:25:02    | 100,882.11 | 106,666.66 | 96,288.16  |
| 07/23/04    | 17:26:33    | 101,687.70 | 104,029.30 | 98,974.36  |
| 07/23/04    | 17:28:03    | 104,982.50 | 123,467.64 | 99,731.38  |
| 07/23/04    | 17:29:33    | 110,297.92 | 116,166.05 | 100,708.18 |
| 07/23/04    | 17:31:03    | 114,514.18 | 117,704.52 | 109,719.17 |
| 07/23/04    | 17:32:34    | 115,674.13 | 119,853.48 | 110,378.51 |
| 07/23/04    | 17:34:04    | 120,828.11 | 126,227.11 | 116,874.23 |
| 07/23/04    | 17:35:33    | 123,315.16 | 127,423.69 | 117,606.84 |
| 07/23/04    | 17:37:03    | 124,858.50 | 140,708.19 | 105,958.48 |
| 07/23/04    | 17:38:34    | 127,643.20 | 132,747.25 | 122,051.28 |
| 07/23/04    | 17:40:04    | 134,703.30 | 148,791.20 | 104,737.48 |
| 07/23/04    | 17:41:35    | 124,318.00 | 129,206.35 | 118,461.54 |
| 07/23/04    | 17:43:04    | 118,973.00 | 120,879.12 | 115,848.59 |
| 07/23/04    | 17:44:35    | 115,924.02 | 119,780.22 | 112,942.61 |
| 07/23/04    | 17:46:05    | 114,907.07 | 119,780.22 | 111,037.85 |
| 07/23/04    | 17:47:34    | 114,446.07 | 117,118.44 | 111,965.81 |
| 07/23/04    | 17:49:04    | 113,784.29 | 116,800.98 | 111,746.03 |
| 07/23/04    | 17:50:35    | 104,249.36 | 112,551.89 | 95,506.72  |
| 07/23/04    | 17:52:06    | 106,455.02 | 110,964.59 | 100,537.24 |
| 07/23/04    | 17:53:36    | 116,948.85 | 126,202.69 | 83,760.69  |
| 07/23/04    | 17:55:05    | 116,797.18 | 121,440.78 | 114,456.66 |
| 07/23/04    | 17:56:36    | 110,828.92 | 114,529.91 | 107,814.41 |
| 07/23/04    | 17:58:06    | 107,986.98 | 112,332.11 | 103,980.46 |
| 07/23/04    | 17:59:35    | 111,916.43 | 113,040.30 | 110,451.77 |
| 07/23/04    | 18:01:05    | 108,444.72 | 112,332.11 | 105,787.55 |
| 07/23/04    | 18:02:36    | 101,752.55 | 110,842.49 | 88,278.39  |
| 07/23/04    | 18:04:06    | 100,187.77 | 113,821.73 | 82,881.56  |
| 07/23/04    | 18:05:37    | 114,361.96 | 120,439.56 | 109,841.27 |
| 07/23/04    | 18:07:07    | 110,591.78 | 114,407.81 | 108,595.85 |
| 07/23/04    | 18:08:37    | 110,113.41 | 113,137.98 | 106,984.13 |
| 07/23/04    | 18:10:07    | 110,627.05 | 112,722.84 | 106,324.79 |
| 07/23/04    | 18:11:36    | 106,220.32 | 109,279.61 | 102,808.30 |
| 07/23/04    | 18:13:06    | 107,906.66 | 109,914.53 | 105,323.56 |
| 07/23/04    | 18:14:37    | 103,794.88 | 105,787.55 | 100,854.70 |
| 07/23/04    | 18:16:07    | 106,727.72 | 111,355.31 | 100,854.70 |
| 07/23/04    | 18:17:38    | 106,996.88 | 109,865.69 | 104,957.27 |
| 07/23/04    | 18:19:08    | 106,260.48 | 108,498.17 | 102,808.30 |
| 07/23/04    | 18:20:38    | 98,668.30  | 103,565.32 | 93,015.88  |
| 07/23/04    | 18:22:08    | 107,813.05 | 119,291.82 | 95,555.55  |
| 07/23/04    | 18:23:37    | 108,116.13 | 119,145.30 | 98,949.94  |
| 07/23/04    | 18:25:07    | 102,784.42 | 108,791.21 | 96,971.91  |
| 07/23/04    | 18:26:38    | 111,506.98 | 119,145.30 | 100,415.14 |
| 07/23/04    | 18:28:08    | 112,983.31 | 121,538.46 | 105,128.20 |
| 07/23/04    | 18:29:39    | 120,094.42 | 129,206.35 | 111,721.61 |
| 07/23/04    | 18:31:09    | 125,506.45 | 138,925.52 | 92,722.84  |
| 07/23/04    | 18:32:39    | 121,037.04 | 124,786.33 | 117,216.12 |
| 07/23/04    | 18:34:09    | 116,039.88 | 122,564.10 | 111,672.77 |

EVR0001  
07/28/04

BAYOU STEEL CORPORATION  
FURNACE #1 & #2 TOTAL FLOW (SCFM) - EVERY 15 MIN

15  
08:11

| END<br>DATE | END<br>TIME | AVG        | MAX        | MIN        |
|-------------|-------------|------------|------------|------------|
| ----        | ----        | ---        | ---        | ---        |
| 07/23/04    | 18:35:38    | 111,347.45 | 112,796.09 | 109,426.13 |
| 07/23/04    | 18:37:08    | 112,019.80 | 114,456.66 | 108,766.79 |
| 07/23/04    | 18:38:39    | 111,362.91 | 114,676.44 | 107,179.48 |
| 07/23/04    | 18:40:09    | 108,899.74 | 113,577.53 | 105,885.23 |
| 07/23/04    | 18:41:40    | 107,539.82 | 113,577.53 | 101,733.82 |
| 07/23/04    | 18:43:10    | 100,975.17 | 111,037.85 | 93,943.84  |
| 07/23/04    | 18:44:40    | 107,283.13 | 122,661.78 | 88,131.87  |
| 07/23/04    | 18:46:10    | 112,533.45 | 117,753.36 | 109,230.77 |
| 07/23/04    | 18:47:39    | 108,729.34 | 110,256.41 | 106,031.74 |
| 07/23/04    | 18:49:09    | 108,799.35 | 112,356.53 | 105,641.02 |
| 07/23/04    | 18:50:40    | 111,210.42 | 115,384.62 | 106,837.61 |
| 07/23/04    | 18:52:10    | 107,594.63 | 109,059.83 | 105,836.38 |
| 07/23/04    | 18:53:41    | 106,409.71 | 110,109.89 | 91,892.55  |
| 07/23/04    | 18:55:11    | 100,905.98 | 112,112.34 | 91,892.55  |
| 07/23/04    | 18:56:40    | 111,978.56 | 120,488.40 | 87,179.48  |
| 07/23/04    | 18:58:11    | 111,371.32 | 116,190.48 | 108,620.27 |
| 07/23/04    | 18:59:41    | 112,009.23 | 113,870.57 | 108,522.59 |
| 07/23/04    | 19:01:11    | 112,795.55 | 116,166.05 | 106,471.30 |
| 07/23/04    | 19:02:42    | 111,658.12 | 113,675.21 | 108,034.19 |
| 07/23/04    | 19:04:12    | 109,704.25 | 113,577.53 | 105,518.92 |
| 07/23/04    | 19:05:42    | 107,653.51 | 112,844.93 | 104,566.55 |
| 07/23/04    | 19:07:12    | 110,639.53 | 112,136.75 | 108,424.91 |
| 07/23/04    | 19:08:41    | 107,879.26 | 110,964.59 | 104,322.34 |
| 07/23/04    | 19:10:11    | 105,643.47 | 107,130.65 | 103,663.00 |
| 07/23/04    | 19:11:42    | 108,230.09 | 112,576.31 | 105,250.30 |
| 07/23/04    | 19:13:12    | 110,144.08 | 116,483.52 | 104,932.84 |
| 07/23/04    | 19:14:43    | 104,355.17 | 115,164.84 | 96,166.05  |
| 07/23/04    | 19:16:13    | 107,405.51 | 111,843.71 | 100,683.76 |
| 07/23/04    | 19:17:43    | 113,401.44 | 125,738.70 | 107,545.79 |
| 07/23/04    | 19:19:13    | 119,060.38 | 127,643.47 | 110,231.99 |
| 07/23/04    | 19:20:42    | 119,051.69 | 131,990.23 | 94,871.80  |
| 07/23/04    | 19:22:12    | 128,472.39 | 139,096.45 | 94,871.80  |
| 07/23/04    | 19:23:43    | 120,271.34 | 125,152.63 | 115,140.41 |
| 07/23/04    | 19:25:13    | 113,765.02 | 115,824.18 | 111,159.95 |
| 07/23/04    | 19:26:44    | 113,598.70 | 116,923.08 | 110,769.23 |
| 07/23/04    | 19:28:14    | 114,606.43 | 117,997.55 | 111,013.43 |
| 07/23/04    | 19:29:44    | 111,629.09 | 114,603.17 | 107,179.48 |
| 07/23/04    | 19:31:14    | 110,212.73 | 115,409.04 | 106,984.13 |
| 07/23/04    | 19:32:43    | 105,153.16 | 112,551.89 | 92,649.57  |
| 07/23/04    | 19:34:13    | 103,707.23 | 121,196.58 | 86,080.59  |
| 07/23/04    | 19:35:44    | 115,170.27 | 121,929.18 | 107,912.09 |
| 07/23/04    | 19:37:14    | 110,060.23 | 115,311.35 | 105,787.55 |
| 07/23/04    | 19:38:45    | 107,283.68 | 111,306.47 | 105,299.15 |
| 07/23/04    | 19:40:15    | 109,061.73 | 114,017.09 | 105,079.37 |
| 07/23/04    | 19:41:45    | 109,078.82 | 113,455.43 | 105,567.77 |
| 07/23/04    | 19:43:15    | 104,174.74 | 112,063.49 | 86,862.02  |
| 07/23/04    | 19:44:44    | 99,473.88  | 111,501.83 | 78,705.74  |
| 07/23/04    | 19:46:14    | 114,310.13 | 121,562.88 | 78,705.74  |
| 07/23/04    | 19:47:45    | 112,059.96 | 115,579.98 | 105,567.77 |
| 07/23/04    | 19:49:15    | 107,781.85 | 113,235.66 | 101,391.94 |
| 07/23/04    | 19:50:46    | 112,417.31 | 114,652.02 | 109,914.53 |
| 07/23/04    | 19:52:16    | 109,349.07 | 113,943.84 | 104,810.74 |
| 07/23/04    | 19:53:46    | 106,407.27 | 110,573.87 | 100,781.44 |

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07/28/04

BAYOU STEEL CORPORATION  
FURNACE #1 & #2 TOTAL FLOW (SCFM) - EVERY 15 MIN

16  
08:11

| END<br>DATE | END<br>TIME | AVG        | MAX        | MIN        |
|-------------|-------------|------------|------------|------------|
| ----        | ----        | ---        | ---        | ---        |
| 07/23/04    | 19:55:16    | 104,103.11 | 107,594.63 | 101,343.10 |
| 07/23/04    | 19:56:45    | 103,071.23 | 109,035.41 | 101,001.22 |
| 07/23/04    | 19:58:15    | 107,409.85 | 110,354.09 | 104,078.14 |
| 07/23/04    | 19:59:46    | 105,034.32 | 108,864.47 | 101,269.84 |
| 07/23/04    | 20:01:16    | 105,811.70 | 107,594.63 | 103,736.27 |
| 07/23/04    | 20:02:47    | 105,173.52 | 107,716.73 | 101,147.74 |
| 07/23/04    | 20:04:17    | 100,169.31 | 106,715.51 | 89,719.17  |
| 07/23/04    | 20:05:46    | 104,745.09 | 112,454.21 | 96,923.08  |
| 07/23/04    | 20:07:16    | 109,973.41 | 121,587.30 | 96,141.63  |
| 07/23/04    | 20:08:47    | 113,518.66 | 118,534.80 | 108,107.45 |
| 07/23/04    | 20:10:17    | 119,150.45 | 130,451.77 | 84,908.42  |
| 07/23/04    | 20:11:48    | 120,589.61 | 124,908.42 | 117,118.44 |
| 07/23/04    | 20:13:18    | 114,776.55 | 119,120.88 | 111,575.09 |
| 07/23/04    | 20:14:48    | 111,870.84 | 116,019.54 | 107,960.93 |
| 07/23/04    | 20:16:18    | 112,860.40 | 116,361.41 | 109,914.53 |
| 07/23/04    | 20:17:47    | 112,480.80 | 119,389.50 | 108,083.03 |
| 07/23/04    | 20:19:17    | 112,175.28 | 116,043.95 | 108,034.19 |
| 07/23/04    | 20:20:48    | 104,120.20 | 115,384.62 | 94,334.55  |
| 07/23/04    | 20:22:18    | 115,071.50 | 125,177.05 | 93,260.07  |
| 07/23/04    | 20:23:49    | 115,303.48 | 118,608.06 | 111,330.89 |
| 07/23/04    | 20:25:19    | 110,711.16 | 113,699.63 | 107,179.48 |
| 07/23/04    | 20:26:49    | 110,741.28 | 114,407.81 | 108,253.97 |
| 07/23/04    | 20:28:19    | 110,771.95 | 113,772.89 | 107,594.63 |
| 07/23/04    | 20:29:48    | 103,291.01 | 111,135.53 | 89,865.69  |
| 07/23/04    | 20:31:18    | 104,560.03 | 121,538.46 | 82,637.36  |
| 07/23/04    | 20:32:49    | 113,827.70 | 120,024.42 | 109,768.01 |
| 07/23/04    | 20:34:19    | 107,632.88 | 111,965.81 | 100,024.42 |
| 07/23/04    | 20:35:50    | 109,064.45 | 114,993.90 | 100,024.42 |
| 07/23/04    | 20:37:20    | 111,369.15 | 114,041.52 | 107,692.30 |
| 07/23/04    | 20:38:50    | 100,669.65 | 110,061.05 | 91,892.55  |
| 07/23/04    | 20:40:20    | 111,874.10 | 121,733.82 | 87,912.09  |
| 07/23/04    | 20:41:49    | 112,616.74 | 116,800.98 | 109,890.11 |
| 07/23/04    | 20:43:19    | 109,485.28 | 111,111.11 | 105,421.24 |
| 07/23/04    | 20:44:50    | 111,805.73 | 115,140.41 | 107,350.43 |
| 07/23/04    | 20:46:20    | 110,833.54 | 113,870.57 | 103,736.27 |
| 07/23/04    | 20:47:51    | 108,562.48 | 112,454.21 | 104,786.33 |
| 07/23/04    | 20:49:21    | 108,036.90 | 110,866.91 | 104,835.16 |
| 07/23/04    | 20:50:51    | 109,716.73 | 114,188.03 | 107,057.39 |
| 07/23/04    | 20:52:21    | 108,387.46 | 111,770.45 | 103,223.45 |
| 07/23/04    | 20:53:50    | 103,033.24 | 108,669.11 | 94,432.23  |
| 07/23/04    | 20:55:20    | 106,444.72 | 117,558.00 | 95,531.13  |
| 07/23/04    | 20:56:51    | 108,938.81 | 113,333.34 | 106,080.59 |
| 07/23/04    | 20:58:21    | 113,204.45 | 125,323.56 | 98,632.48  |
| 07/23/04    | 20:59:52    | 118,041.24 | 122,173.38 | 113,772.89 |
| 07/23/04    | 21:01:22    | 119,050.06 | 123,565.32 | 114,481.08 |
| 07/23/04    | 21:02:51    | 123,560.71 | 139,804.64 | 99,340.66  |
| 07/23/04    | 21:04:22    | 128,216.52 | 137,264.95 | 121,782.66 |
| 07/23/04    | 21:05:52    | 119,187.63 | 124,542.13 | 116,263.73 |
| 07/23/04    | 21:07:21    | 113,819.02 | 118,241.76 | 110,793.65 |
| 07/23/04    | 21:08:52    | 113,374.30 | 119,829.06 | 109,474.97 |
| 07/23/04    | 21:10:22    | 110,581.47 | 113,064.71 | 109,181.93 |
| 07/23/04    | 21:11:53    | 108,501.42 | 111,477.41 | 106,862.02 |
| 07/23/04    | 21:13:23    | 102,845.48 | 108,595.85 | 93,406.59  |

EVR0001  
07/28/04

BAYOU STEEL CORPORATION  
FURNACE #1 & #2 TOTAL FLOW (SCFM) - EVERY 15 MIN

17  
08:11

| END<br>DATE | END<br>TIME | AVG        | MAX        | MIN        |
|-------------|-------------|------------|------------|------------|
| 07/23/04    | 21:14:52    | 102,020.63 | 116,312.58 | 89,963.37  |
| 07/23/04    | 21:16:23    | 107,284.49 | 118,901.10 | 87,619.05  |
| 07/23/04    | 21:17:53    | 111,514.59 | 117,851.04 | 109,548.23 |
| 07/23/04    | 21:19:22    | 111,843.98 | 114,481.08 | 107,374.84 |
| 07/23/04    | 21:20:53    | 111,025.10 | 113,992.67 | 107,032.97 |
| 07/23/04    | 21:22:23    | 107,787.27 | 109,206.35 | 106,446.88 |
| 07/23/04    | 21:23:54    | 110,460.18 | 113,675.21 | 107,179.48 |
| 07/23/04    | 21:25:24    | 103,884.95 | 110,500.61 | 92,161.17  |
| 07/23/04    | 21:26:53    | 107,760.14 | 112,014.65 | 103,833.95 |
| 07/23/04    | 21:28:23    | 116,789.31 | 130,695.97 | 94,432.23  |
| 07/23/04    | 21:29:54    | 122,822.68 | 128,083.03 | 117,728.94 |
| 07/23/04    | 21:31:24    | 114,788.23 | 118,705.74 | 111,184.38 |
| 07/23/04    | 21:32:54    | 114,922.53 | 118,852.26 | 111,086.69 |
| 07/23/04    | 21:34:24    | 110,988.74 | 113,284.49 | 108,693.53 |
| 07/23/04    | 21:35:55    | 109,104.33 | 113,675.21 | 105,763.13 |
| 07/23/04    | 21:37:25    | 108,919.28 | 113,260.07 | 105,421.24 |
| 07/23/04    | 21:38:54    | 110,824.31 | 116,068.38 | 106,202.69 |
| 07/23/04    | 21:40:24    | 107,574.28 | 111,941.39 | 102,246.64 |
| 07/23/04    | 21:41:55    | 105,990.23 | 109,670.33 | 102,905.98 |
| 07/23/04    | 21:43:25    | 110,513.91 | 113,772.89 | 107,399.27 |
| 07/23/04    | 21:44:55    | 110,089.54 | 113,675.21 | 102,490.84 |
| 07/23/04    | 21:46:25    | 105,729.21 | 112,210.02 | 96,385.84  |
| 07/23/04    | 21:47:56    | 109,216.93 | 110,695.97 | 104,566.55 |
| 07/23/04    | 21:49:26    |            |            |            |

Records selected: 958  
Records sorted: 958  
Lines printed: 1053  
Pages printed: 19

|            |            |            |            |            |
|------------|------------|------------|------------|------------|
| 108,765.43 | 116,190.48 | 97,680.10  |            |            |
| 07/23/04   | 21:50:55   | 106,868.81 | 112,234.43 | 96,410.26  |
| 07/23/04   | 21:52:25   | 112,163.62 | 126,422.47 | 100,122.10 |
| 07/23/04   | 21:53:56   | 123,698.27 | 134,334.55 | 91,623.93  |
| 07/23/04   | 21:55:27   | 117,146.38 | 125,836.38 | 114,188.03 |
| 07/23/04   | 21:56:56   | 113,416.09 | 116,605.62 | 110,476.19 |
| 07/23/04   | 21:58:26   | 109,487.72 | 112,429.79 | 105,445.66 |
| 07/23/04   | 21:59:57   | 109,169.72 | 113,504.27 | 106,202.69 |
| 07/23/04   | 22:01:27   | 109,208.25 | 111,697.20 | 107,081.80 |
| 07/23/04   | 22:02:56   | 103,207.70 | 109,279.61 | 88,766.79  |
| 07/23/04   | 22:04:26   | 102,681.05 | 116,678.88 | 97,753.36  |
| 07/23/04   | 22:05:57   | 111,611.18 | 128,864.47 | 96,874.23  |
| 07/23/04   | 22:07:27   | 116,079.50 | 119,633.70 | 112,991.45 |
| 07/23/04   | 22:08:58   | 112,771.95 | 117,460.32 | 111,257.63 |
| 07/23/04   | 22:10:28   | 113,903.41 | 118,315.02 | 109,426.13 |
| 07/23/04   | 22:11:58   | 112,065.94 | 114,163.62 | 110,695.97 |
| 07/23/04   | 22:13:28   | 112,230.36 | 116,605.62 | 108,766.79 |
| 07/23/04   | 22:14:57   | 109,118.98 | 115,164.84 | 89,597.07  |
| 07/23/04   | 22:16:27   | 100,432.77 | 112,527.47 | 88,498.17  |
| 07/23/04   | 22:17:58   | 111,454.08 | 132,161.17 | 88,498.17  |
| 07/23/04   | 22:19:28   | 117,751.19 | 122,490.84 | 113,968.26 |
| 07/23/04   | 22:20:59   | 116,745.35 | 119,780.22 | 112,014.65 |
| 07/23/04   | 22:22:29   | 114,721.48 | 117,484.73 | 111,306.47 |
| 07/23/04   | 22:23:59   | 111,945.19 | 114,432.23 | 109,108.67 |

|          |          |            |            |            |
|----------|----------|------------|------------|------------|
| 07/23/04 | 22:25:29 | 115,035.14 | 118,803.42 | 112,429.79 |
| 07/23/04 | 22:26:58 | 113,157.23 | 117,435.90 | 108,840.05 |
| 07/23/04 | 22:28:28 | 108,179.89 | 111,086.69 | 103,492.06 |
| 07/23/04 | 22:30:00 | 105,510.24 | 108,840.05 | 100,146.52 |
| 07/23/04 | 22:31:29 | 109,427.76 | 112,185.59 | 106,422.47 |
| 07/23/04 | 22:32:99 | 108,233.62 | 112,551.89 | 103,174.60 |

EVR0001  
07/28/04

BAYOU STEEL CORPORATION  
FURNACE #1 & #2 TOTAL FLOW (SCFM) - EVERY 15 MIN

18  
08:11

| END<br>DATE | END<br>TIME | AVG        | MAX        | MIN        |
|-------------|-------------|------------|------------|------------|
| 07/23/04    | 22:34:30    | 107,986.98 | 114,603.17 | 92,307.70  |
| 07/23/04    | 22:36:00    | 104,042.60 | 109,816.85 | 99,780.22  |
| 07/23/04    | 22:37:30    | 109,126.03 | 123,516.48 | 95,042.73  |
| 07/23/04    | 22:39:00    | 113,108.94 | 119,242.98 | 95,042.73  |
| 07/23/04    | 22:40:29    | 116,178.27 | 119,242.98 | 113,186.81 |
| 07/23/04    | 22:42:01    | 117,638.31 | 122,271.06 | 114,358.98 |
| 07/23/04    | 22:43:30    | 121,811.97 | 129,597.07 | 116,117.22 |
| 07/23/04    | 22:45:00    | 129,148.83 | 141,611.72 | 98,339.44  |
| 07/23/04    | 22:46:31    | 127,097.27 | 135,335.78 | 120,659.34 |
| 07/23/04    | 22:48:01    | 120,265.63 | 122,710.63 | 117,924.30 |
| 07/23/04    | 22:49:31    | 118,353.82 | 120,854.70 | 114,993.90 |
| 07/23/04    | 22:51:01    | 117,635.05 | 122,857.14 | 114,871.80 |
| 07/23/04    | 22:52:30    | 118,845.75 | 121,440.78 | 115,970.70 |
| 07/23/04    | 22:54:02    | 113,726.23 | 117,948.72 | 97,899.88  |
| 07/23/04    | 22:55:31    | 108,694.07 | 121,245.42 | 97,948.72  |
| 07/23/04    | 22:57:01    | 118,847.91 | 129,890.11 | 97,484.73  |
| 07/23/04    | 22:58:32    | 117,127.66 | 120,048.84 | 113,553.12 |
| 07/23/04    | 23:00:02    | 117,249.49 | 118,949.94 | 114,822.95 |
| 07/23/04    | 23:01:31    | 118,067.84 | 121,733.82 | 113,284.49 |
| 07/23/04    | 23:03:01    | 117,727.31 | 121,733.82 | 114,700.85 |
| 07/23/04    | 23:04:32    | 114,283.27 | 117,167.27 | 112,356.53 |
| 07/23/04    | 23:06:02    | 104,751.32 | 113,284.49 | 93,162.39  |
| 07/23/04    | 23:07:33    | 108,471.03 | 120,488.40 | 95,628.81  |
| 07/23/04    | 23:09:03    | 115,176.23 | 128,644.69 | 99,365.08  |
| 07/23/04    | 23:10:33    | 117,513.50 | 129,304.03 | 106,813.19 |
| 07/23/04    | 23:12:03    | 128,677.25 | 134,432.23 | 122,051.28 |
| 07/23/04    | 23:13:32    | 122,102.29 | 126,886.45 | 118,119.66 |
| 07/23/04    | 23:15:02    | 117,980.73 | 121,611.72 | 113,821.73 |
| 07/23/04    | 23:16:33    | 119,446.21 | 121,074.48 | 116,971.91 |
| 07/23/04    | 23:18:03    | 119,287.20 | 122,368.74 | 116,605.62 |
| 07/23/04    | 23:19:34    | 122,757.56 | 126,642.25 | 117,069.59 |
| 07/23/04    | 23:21:04    | 122,189.12 | 125,543.34 | 119,072.04 |
| 07/23/04    | 23:22:34    | 119,045.72 | 121,953.60 | 117,142.86 |
| 07/23/04    | 23:24:04    | 116,332.93 | 118,046.40 | 114,334.55 |
| 07/23/04    | 23:25:33    | 114,345.13 | 117,167.27 | 111,721.61 |
| 07/23/04    | 23:27:03    | 110,720.66 | 114,285.71 | 104,884.01 |
| 07/23/04    | 23:28:34    | 111,976.39 | 115,921.86 | 105,665.45 |
| 07/23/04    | 23:30:04    | 103,021.57 | 112,332.11 | 95,531.13  |
| 07/23/04    | 23:31:35    | 107,314.88 | 116,507.94 | 103,345.55 |
| 07/23/04    | 23:33:05    | 115,334.69 | 119,511.60 | 102,783.88 |
| 07/23/04    | 23:34:35    | 118,216.25 | 124,639.80 | 112,380.95 |
| 07/23/04    | 23:36:05    | 123,540.09 | 139,633.70 | 98,974.36  |
| 07/23/04    | 23:37:34    | 123,894.72 | 133,772.89 | 119,829.06 |
| 07/23/04    | 23:39:04    | 125,883.60 | 130,036.63 | 120,903.54 |
| 07/23/04    | 23:40:35    | 122,930.41 | 125,763.13 | 118,803.42 |
| 07/23/04    | 23:42:05    | 120,017.37 | 121,831.50 | 117,069.59 |
| 07/23/04    | 23:43:36    | 117,132.55 | 121,221.00 | 115,018.31 |
| 07/23/04    | 23:45:06    | 120,105.28 | 123,907.20 | 116,019.54 |
| 07/23/04    | 23:46:36    | 112,464.80 | 119,218.56 | 100,659.34 |
| 07/23/04    | 23:48:06    | 109,968.26 | 126,886.45 | 97,509.16  |
| 07/23/04    | 23:49:35    | 122,827.84 | 128,278.39 | 117,704.52 |
| 07/23/04    | 23:51:07    | 117,981.82 | 119,804.64 | 115,286.94 |
| 07/23/04    | 23:52:36    | 116,102.29 | 119,438.34 | 113,260.07 |

EVR0001  
07/28/04

B A Y O U   S T E E L   C O R P O R A T I O N  
FURNACE #1 & #2 TOTAL FLOW (SCFM) - EVERY 15 MIN

19  
08:11

| END<br>DATE<br>---- | END<br>TIME<br>---- | AVG<br>--- | MAX<br>--- | MIN<br>--- |
|---------------------|---------------------|------------|------------|------------|
| 07/23/04            | 23:54:06            | 116,503.87 | 119,951.16 | 113,406.59 |
| 07/23/04            | 23:55:37            | 115,567.77 | 117,924.30 | 112,185.59 |
| 07/23/04            | 23:57:07            | 114,627.59 | 116,727.72 | 111,770.45 |
| 07/23/04            | 23:58:37            | 104,412.43 | 114,139.20 | 94,700.85  |

## VII. APPENDIX

The following appendices are presented as supporting documentation to the emission test report.

- A. Resumes of Test Personnel
- B. Test Equipment Calibrations
- C. Correspondence, Bayou Steel and LDEQ
- D. Permit Number 885 (M-2) Excerpts

Troy W. LeSage  
Assistant Manager  
Senior Project Team Leader  
Emission Testing Services, Incorporated  
Baton Rouge, Louisiana

## EDUCATION

U. S. EPA Round Robin sample integrity audits  
Completed Emission Testing Services Air Sampling Techniques Seminar  
Participates in on going Air-Pollution Training Institute Courses (APTI)  
EPA - Sampling and evaluation of Airborne Asbestos, Temple University  
NIOSH - Supervision of Asbestos Abatement Projects, Texas A & M  
High School Graduate

## CERTIFICATIONS

EPA Certified Opacity Reader (Method 9)  
General Safety & Health Orientation Program  
Respiratory Equipment Medical Certification  
MSA Qualitative Fit Test Record

## EXPERIENCE

1992 to Present - Senior Project Team Leader.  
Responsibilities include planning and performing source testing projects.

1987 to 1992 - Testing Specialist for Emission Testing Services, Inc.  
Performs EPA approved reference methods for compliance testing as well as other non-routine source evaluations. Responsibilities also include job preparation, equipment calibration, and equipment maintenance.

1985 to 1987 - Industrial Hygiene Technician for an environmental firm.  
Performed metal analysis with atomic adsorption spectrophotometer, fiber analysis for asbestos and overseeing asbestos abatement projects.

**Ronald L. McCabe, II**  
Senior Sampling Specialist  
Emission Testing Services, Incorporated  
Baton Rouge, Louisiana

#### EDUCATION

Louisiana State University  
B.S. ---- Environmental Engineering

#### CERTIFICATIONS

General Safety & Health Orientation Program  
Respiratory Equipment Medical Certification  
MSA Qualitative Fit Test Record  
EPA Certified Opacity Reader (Method 9)

#### EXPERIENCE

#### EXPERIENCE

08/98 to Present - Sampling Specialist for Emission Testing Services, Inc.

Performs EPA approved reference methods for compliance testing as well as other non-routine source evaluations.

Responsibilities also include job preparation, equipment calibration, and equipment maintenance.

Responsibilities include planning and performing source testing projects.

**Joel S. Richard**  
Sampling Technician Grade 2  
Emission Testing Services, Incorporated  
Baton Rouge, Louisiana

## EDUCATION

High School Graduate

## CERTIFICATIONS

General Safety & Health Orientation Program  
Respiratory Equipment Medical Certification  
MSA Qualitative Fit Test Record

## EXPERIENCE

### 09/01 to Present -- Sampling Technician Grade 2

Able to perform all procedures required in 40 CFR 60, Method 2 and Method 4 testing without the use of a computer. Able to prepare and load for an emission test which requires a sample train. Proficient in completion of project field logs and data sheets. Responsible for the calibration and maintenance of consoles, pitot tubes, thermacouples and barometers. Proficient in the collection of organ samples by EPA Reference Method 18. Is well-versed in the calculation of stack gas flow rates with and without the use of a computer. Helps in training a Grade 1 technician. Will have accumulated, at least, 240 field hours as a Sampling Technician Grade 1.

### 05/00 to 09/01 -- Sampling Technician Grade 1

Able to perform all procedures required in 40 CFR 60, Method 1 without use of a computer. All to perform all procedures required in 40 CFR 60, Method 3 (orsat analysis). Competent in the calibration of consoles, pitot tubes, thermal couples and barometers. Able to setup and assist in leak-check as well as weigh-in of a M4 sample train. Will have accumulated, at least, 480 hours of field experience.

10/99 to 05/00 - Testing trainee technician for Emission Testing Services, Inc. Supports in performing EPA approved reference methods for compliance testing as well as other non-routine source evaluations. Responsibilities also include job preparation, equipment calibration and equipment maintenance.

# ETS

EMISSION TESTING SERVICES

## METER BOX CALIBRATION DATA AND CALCULATIONS FORM (English Units)

|                    |                                                     |
|--------------------|-----------------------------------------------------|
| Gas meter Reads in |                                                     |
| liters             | <input checked="" type="checkbox"/> ft <sup>3</sup> |

One Revolution of meter = 0.1 ft<sup>3</sup>  
 Leak Check Good @: 0.0123  
 Barometric Pres., Pb: 29.821

Wet Test Meter Cal Factor: 1.007  
 Meter Box Number: 3  
 Date Calibrated: 6/15/04

| Orifice Setting<br>ΔH<br>in. H <sub>2</sub> O | Wet Test Meter Reading<br>(V <sub>w</sub> m),<br>ft <sup>3</sup> | Dry Gas Meter Readings                            |                                                 |                                                 | Wet Test Meter Reading<br>(T <sub>w</sub> m),<br>ft <sup>3</sup> | Wet Test Meter Pressure<br>(P <sub>w</sub> ),<br>in. H <sub>2</sub> O | Dry Gas Meter                          |                                         |                                      | Run Time<br>(Θ),<br>Min. |
|-----------------------------------------------|------------------------------------------------------------------|---------------------------------------------------|-------------------------------------------------|-------------------------------------------------|------------------------------------------------------------------|-----------------------------------------------------------------------|----------------------------------------|-----------------------------------------|--------------------------------------|--------------------------|
|                                               |                                                                  | Initial<br>(V <sub>d</sub> i),<br>ft <sup>3</sup> | Final<br>(V <sub>d</sub> f),<br>ft <sup>3</sup> | Total<br>(V <sub>d</sub> m),<br>ft <sup>3</sup> |                                                                  |                                                                       | Inlet<br>(T <sub>d</sub> i),<br>deg. F | Outlet<br>(T <sub>d</sub> f),<br>deg. F | Avg<br>(T <sub>d</sub> m),<br>deg. F |                          |
| 0.50                                          | 5                                                                | 839.575                                           | 844.628                                         | 5.053                                           | 74                                                               | 0.5                                                                   | 86.5                                   | 83.0                                    | 84.8                                 | 13.15                    |
| 1.00                                          | 5                                                                | 844.628                                           | 849.678                                         | 5.050                                           | 74                                                               | 1.125                                                                 | 97.0                                   | 85.5                                    | 91.3                                 | 9.02                     |
| 1.50                                          | 5                                                                | 849.678                                           | 854.734                                         | 5.056                                           | 74                                                               | 1.5                                                                   | 98.5                                   | 86.5                                    | 92.5                                 | 7.32                     |
| 2.00                                          | 5                                                                | 854.734                                           | 859.768                                         | 5.034                                           | 74                                                               | 2.125                                                                 | 100.0                                  | 87.0                                    | 93.5                                 | 6.37                     |
| 3.00                                          | 5                                                                | 859.768                                           | 864.788                                         | 5.020                                           | 74                                                               | 2.875                                                                 | 101.0                                  | 88.0                                    | 94.5                                 | 5.25                     |

| Dry Gas Meter Gauge Pressure<br>in. H <sub>2</sub> O<br>(Gp) | Dry Gas Meter Gp<br>P <sub>d</sub> m = — + P <sub>b</sub><br>13.6<br>(P <sub>d</sub> m) | Wet Test Meter Pw<br>P <sub>w</sub> m = — + P <sub>b</sub><br>13.6<br>(P <sub>w</sub> m) | Y <sub>d</sub> m = $\frac{(V_{wm}) \cdot (Y_{wm}) \cdot (T_{wm}) \cdot (P_{wm})}{(V_{dm}) \cdot (T_{dm}) \cdot (P_{dm})}$ |           | ΔH@ = $\frac{0.0317 \cdot \Delta H}{P_b \cdot (t_d + 460)} \cdot \frac{(T_w + 460)^2}{V_w}$ |           |
|--------------------------------------------------------------|-----------------------------------------------------------------------------------------|------------------------------------------------------------------------------------------|---------------------------------------------------------------------------------------------------------------------------|-----------|---------------------------------------------------------------------------------------------|-----------|
|                                                              |                                                                                         |                                                                                          | Y <sub>d</sub> m                                                                                                          | Tolerance | ΔH@                                                                                         | Tolerance |
| 0.5                                                          | 29.8578                                                                                 | 29.8578                                                                                  | 1.0165                                                                                                                    | 0.0144    | 1.9244                                                                                      | -0.1117   |
| 1.0                                                          | 29.8945                                                                                 | 29.9037                                                                                  | 1.0296                                                                                                                    | 0.0014    | 1.7896                                                                                      | 0.0232    |
| 1.5                                                          | 29.9313                                                                                 | 29.9313                                                                                  | 1.0303                                                                                                                    | 0.0006    | 1.7638                                                                                      | 0.0489    |
| 2.0                                                          | 29.9681                                                                                 | 29.9773                                                                                  | 1.0370                                                                                                                    | -0.0061   | 1.7778                                                                                      | 0.0350    |
| 3.0                                                          | 30.0416                                                                                 | 30.0324                                                                                  | 1.0412                                                                                                                    | -0.0103   | 1.8081                                                                                      | 0.0047    |
| Average                                                      |                                                                                         |                                                                                          | 1.0309                                                                                                                    |           | 1.8127                                                                                      |           |

Y<sub>d</sub>m = Ratio of reading of wet test meter to dry test meter; tolerance for individual values "0.02 from average.

ΔH@ = Orifice pressure differential that equates to 0.75 cfm of air @ 68°F and 29.92 inches of mercury, in H<sub>2</sub>O: tolerance for individual values "0.20 from average.

|                      |               |      |
|----------------------|---------------|------|
| Serial #:            | <u>10-006</u> |      |
| Calibration:         | <u>pass</u>   | fail |
| +/- 5% from previous |               |      |

Calibrated by:

*Bryd Barber*

### THERMOCOUPLE CALIBRATION

Meter Box Number: 3  
 Barometric Pressure: 29.821  
 Serial #: 0

Date: 06/15/04  
 Calibrated By: Boyd Barbier  
 +/- 1.5% from previous: ☒ PASS ☐ FAIL

#### LOW CHECK POINT

|              | Omega CL27 Reading |         |              |         | Thermocouple Reading |                                 |         |         |
|--------------|--------------------|---------|--------------|---------|----------------------|---------------------------------|---------|---------|
| Channel Type | Trial 1            | Trial 2 | Trial 3      | Average | Trial 1              | Trial 2                         | Trial 3 | Average |
| Stack        | 100                | 100     | 100          | 100     | 100                  | 100                             | 100     | 100.00  |
| Probe        | 100                | 100     | 100          | 100     | 100                  | 100                             | 101     | 100.33  |
| Hot Box      | 100                | 100     | 100          | 100     | 100                  | 101                             | 100     | 100.33  |
| Umbilical    | 100                | 100     | 100          | 100     | 100                  | 100                             | 100     | 100.00  |
|              | Average Reading    |         |              |         |                      | % Error (Diff / Avg CL27) * 100 |         |         |
| Channel Type | Omega CL27         |         | Thermocouple |         | Difference           | -1.5 % < %Error < +1.5 %        |         |         |
| Stack        | 100                |         | 100.00       |         | 0.00                 | 0.00                            |         |         |
| Probe        | 100                |         | 100.33       |         | 0.33                 | 0.33                            |         |         |
| Hot Box      | 100                |         | 100.33       |         | 0.33                 | 0.33                            |         |         |
| Umbilical    | 100                |         | 100.00       |         | 0.00                 | 0.00                            |         |         |

#### MID CHECK POINT

| Channel Type | Omega CL27 Reading |              |         |            | Thermocouple Reading            |         |         |         |
|--------------|--------------------|--------------|---------|------------|---------------------------------|---------|---------|---------|
|              | Trial 1            | Trial 2      | Trial 3 | Average    | Trial 1                         | Trial 2 | Trial 3 | Average |
| Stack        | 500                | 500          | 500     | 500        | 500                             | 500     | 500     | 500.00  |
| Probe        | 500                | 500          | 500     | 500        | 500                             | 500     | 501     | 500.33  |
| Hot Box      | 500                | 500          | 500     | 500        | 500                             | 501     | 500     | 500.33  |
| Umbilical    | 500                | 500          | 500     | 500        | 500                             | 500     | 500     | 500.00  |
| Channel Type | Average Reading    |              |         | Difference | % Error (Diff / Avg CL27) * 100 |         |         |         |
|              | Omega CL27         | Thermocouple |         |            | -1.5 % < %Error < +1.5 %        |         |         |         |
| Stack        | 500                | 500.00       |         | 0.00       | 0.00                            |         |         |         |
| Probe        | 500                | 500.33       |         | 0.33       | 0.07                            |         |         |         |
| Hot Box      | 500                | 500.33       |         | 0.33       | 0.07                            |         |         |         |
| Umbilical    | 500                | 500.00       |         | 0.00       | 0.00                            |         |         |         |

#### HIGH CHECK POINT

|              | Omega CL27 Reading |         |              |         | Thermocouple Reading |                                 |         |         |
|--------------|--------------------|---------|--------------|---------|----------------------|---------------------------------|---------|---------|
| Channel Type | Trial 1            | Trial 2 | Trial 3      | Average | Trial 1              | Trial 2                         | Trial 3 | Average |
| Stack        | 950                | 950     | 950          | 950     | 950                  | 950                             | 951     | 950.33  |
| Probe        | 950                | 950     | 950          | 950     | 950                  | 950                             | 950     | 950.00  |
| Hot Box      | 950                | 950     | 950          | 950     | 951                  | 951                             | 951     | 951.00  |
| Umbilical    | 950                | 950     | 950          | 950     | 951                  | 950                             | 951     | 950.67  |
|              | Average Reading    |         |              |         |                      | % Error (Diff / Avg CL27) * 100 |         |         |
| Channel Type | Omega CL27         |         | Thermocouple |         | Difference           | -1.5 % < %Error < +1.5 %        |         |         |
| Stack        | 950                |         | 950.33       |         | 0.33                 | 0.04                            |         |         |
| Probe        | 950                |         | 950.00       |         | 0.00                 | 0.00                            |         |         |
| Hot Box      | 950                |         | 951.00       |         | 1.00                 | 0.11                            |         |         |
| Umbilical    | 950                |         | 950.67       |         | 0.67                 | 0.07                            |         |         |

# ETS

EMISSION TESTING SERVICES, INC.

Pitot Tube Number: P-10-5  
Calibrated By: B.Barbier

CP(std): STD - 0.99  
Date Calibrated: 06/18/04

| Point Number | Standard Pitot *P (in. H2O) | "S" Type Pitot *P, in H2O<br>Impact Side | Static Side  |
|--------------|-----------------------------|------------------------------------------|--------------|
| Low          | <u>0.280</u>                | <u>0.410</u>                             | <u>0.400</u> |
| Mid          | <u>0.580</u>                | <u>0.810</u>                             | <u>0.800</u> |
| High         | <u>0.740</u>                | <u>1.050</u>                             | <u>1.050</u> |

## CALCULATIONS

$$Cp(s) = Cp(std) \times \left( \frac{P(std)^{1/2}}{P(s)} \right)$$

$$Deviation = |Cp(s) - Cp| \quad (\text{Impact Side or Static Side})$$

$$Avg. Dev. = \frac{Low deviation + Mid deviation + High deviation}{3} \quad (\text{Impact Side or Static Side})$$

|      | Impact Side<br>Cp (s) | Deviation    | Static Side<br>Cp(s) | Deviation    |
|------|-----------------------|--------------|----------------------|--------------|
| Low  | <u>0.8181</u>         | <u>0.011</u> | <u>0.8283</u>        | <u>0.006</u> |
| Mid  | <u>0.8377</u>         | <u>0.009</u> | <u>0.8430</u>        | <u>0.009</u> |
| High | <u>0.8311</u>         | <u>0.002</u> | <u>0.8311</u>        | <u>0.003</u> |
| Cp = | <u>0.8290</u>         |              | Cp = <u>0.8341</u>   |              |

|                                       |   |              |                   |
|---------------------------------------|---|--------------|-------------------|
| * Cp(Static Side) - Cp(Impact Side) * | = | <u>0.005</u> | (Must be <= 0.01) |
| Average Deviation (Impact Side)       | = | <u>0.007</u> | (Must be <= 0.01) |
| Average Deviation (Static Side)       | = | <u>0.006</u> | (Must be <= 0.01) |

$$Cp = \underline{0.832}$$

Pitot Tube Leak Check ☒ PASSED ☐ FAILED

# ETS

EMISSION TESTING SERVICES, INC.

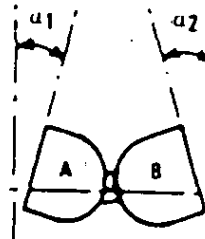
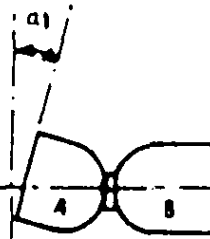
TUBE NUMBER P-10-5

DATE 7-23-04

INSPECTOR NAME Joel Richard

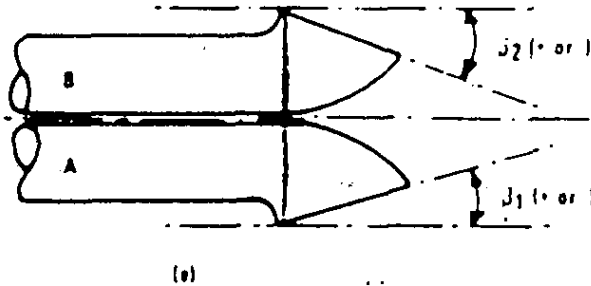
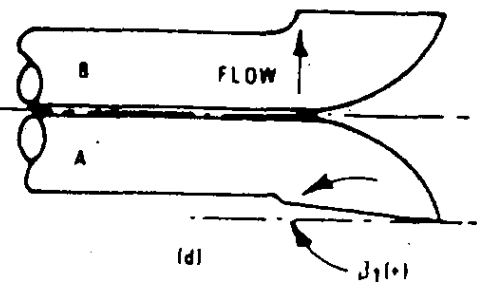
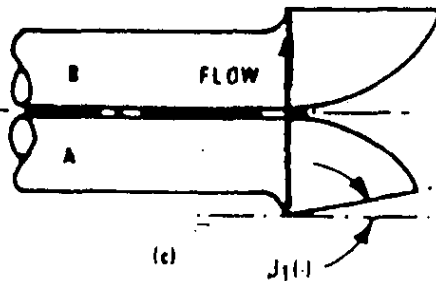
1 YES ☒ NO ☐  $a_1$  and  $a_2 \leq 10^\circ$

TRANSVERSE  
TUBE AXIS

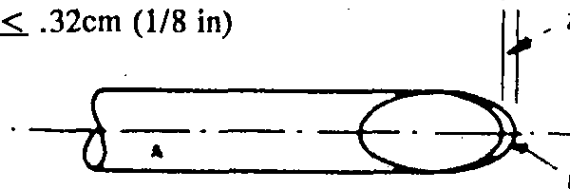


2 YES ☒ NO ☐  $B_1$  and  $B_2 \leq 5^\circ$

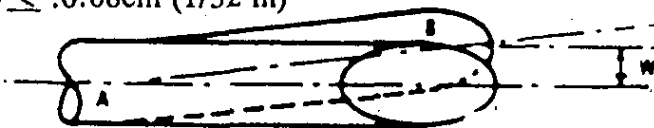
LONGITUDINAL  
TUBE AXIS



3 YES ☒ NO ☐  $Z \leq .32\text{cm} (1/8 \text{ in})$



4 YES ☒ NO ☐  $W \leq .08\text{cm} (1/32 \text{ in})$



SIGNATURE Joel Richard

C:\WS\FORMS\TUBE

# ETS

EMISSION TESTING SERVICES, INC.

## SAMPLING NOZZLE CALIBRATION DATA FORM

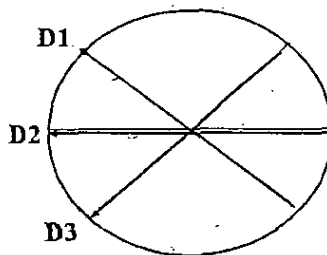
NOZZLE I.D. NO. .170  
COMPANY NAME Bayer Steel  
SOURCE I.D. Baghouse Stack

| DATE CALIBRATED | CALIBRATED BY | NOZZLE MEASUREMENTS <sup>a</sup> |      |      | MAXIMUM $\Delta$ <sup>b</sup> | D avg. <sup>c</sup> |
|-----------------|---------------|----------------------------------|------|------|-------------------------------|---------------------|
|                 |               | D1                               | D2   | D3   |                               |                     |
| 7-23-04         | Joel Richard  | .170                             | .170 | .170 | $\emptyset$                   | .170                |

<sup>a</sup>CORRECT NOZZLE DIAMETER MEASUREMENTS AS INDICATED IN THE DIAGRAM TO THE NEAREST 0.001 INCH

<sup>b</sup>MAXIMUM DIFFERENCE BETWEEN ANY TWO DIAMETERS. ACCEPTANCE LIMIT: MAXIMUM  $\Delta \leq 0.004$  INCH

<sup>c</sup>AVERAGE OF D1 PLUS D2 PLUS D3.



SIGNATURE

*[Handwritten Signature]*

APPENDIX B

7.2.5

**ETS<sub>R</sub>**

EMISSION TESTING SERVICES, INC.

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**BAROMETER CALIBRATION SHEET**

---

CLIENT: BAYOU STEEL

DATE: 7-22-04

SOURCE ID: BAGHOUSE STACK

OPERATOR: RON MCCABE

\*\*\*\*\*BAROMETER\*\*\*\*\*

BAROMETER ID: UNIT #1

CALIBRATION DATA:

INITIAL CALIBRATION: 29.95 INITIAL 29.95 FINAL

ADJUSTMENT: ☐ Yes

☒ No

\*\*\*\*\*CALIBRATION REFERENCE\*\*\*\*\*

ID: PRINCO, HG

ELEVATION: BATON ROUGE

ELEVATION DIFF: N/A

BAROMETER READING: 29.96

COMMENTS: \_\_\_\_\_  
\_\_\_\_\_  
\_\_\_\_\_

**BAYOU STEEL CORPORATION**

July 12, 2004

**FAXSIMILE  
225/219-3474**

Mr. Jim Courville  
Office of Environmental Assessment  
Louisiana Department of Environmental Quality  
P.O. Box 4314  
Baton Rouge, LA 70821-4314

**RE: Bayou Steel Corporation Notification of Intent to Test and Summary of  
Pretest Meeting**

Dear Mr. Courville:

This is a summary of the pretest meeting held the DEQ office on July 12, 2004. The list of meeting attendees is appended as Exhibit 1.

On Friday, July 23, 2004, ETS will perform a stack test at Bayou Steel Corporation on the main stack, source 1-77, for mercury and lead. The test methods to be utilized are EPA Methods 1-4 and Method 29. The detection limit for mercury will be 0.1 lbs/hr. The plant operating data at the time of the test to be supplied includes: tons/hour of scrap melted, the scrap mix utilized, the electrical power, natural gas, carbon and oxygen utilized. The testing duration will be 3 hours and will include one complete melting cycle from charge to tap per hour.

At the time of the test a sample will also be collected from the Secondary Dust Collection System, sources 2-77A-F. This sample will be analyzed for mercury and the results will be provided to DEQ.

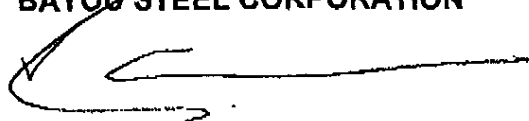
Bayou Steel will also investigate previous sampling events at the shredder cyclones and will provide DEQ with an estimated mercury value.

Attached is the Notification of Intent to Test for the stack test to occur on July 23.

**APPENDIX C**

If you have any questions or require additional information, please do not hesitate to contact me.

Respectfully,  
**BAYOU STEEL CORPORATION**



Wendy Stehling  
Manager, Environmental, Health & Safety

c: Barry Gipson, ETS  
Linda Brown, LDEQ  
Freddie Touro, LDEQ  
Jennifer Pelloat, LDEQ  
Al Pulliam, Bayou Steel Corporation

**NOTIFICATION OF INTENT TO TEST****FACILITY INFORMATION**

Facility Name: Bayou Steel Corporation  
Street Address: 138 Highway 3217 70068  
Post Office Box: PO Box 5000  
City/State/Zip: LaPlace LA 70069  
Contact name for testing purposes: Wendy Stehling  
Contact's phone number: 985/652-0322  
Contact's fax number: 985/652-0373  
E-Mail: wendys@bayousteel.com  
Type of Permit: State ☒ NSPS ☐ Other ☐  
State Permit Number: 885 (m-2)  
State Permit Writer: Gus Von Bodungen - issued permit  
Federal Permit Number: \_\_\_\_\_  
Federal Permit Writer: \_\_\_\_\_  
If Other, Explain: \_\_\_\_\_

**NOTIFICATION**

30-Day Notice Given: Yes ☒ No ☐  
TO Whom: LA DEQ  
Was a pretest meeting required: Yes ☒ No ☐ (if answer was yes, see Exhibit 1)

**PROPOSED TEST DATE(S):** JULY 23, 2004

**TEST COMPANY INFORMATION**

Emission Testing Services, Inc. (ETS)  
Post Office Box 15075  
Baton Rouge, LA 70895

10461 Mammoth Drive  
Baton Rouge, LA 70814

Contact Person: Barry Gipson  
General Manager  
Phone No. (225)925-8405  
Fax No. (225)925-2343  
E-Mail: bgipson@emissiontesting.com  
Home Page: www.Emissiontesting.com

File:\forms\NOTI-TEST

**EXHIBIT 1****PRETEST MEETING ATTENDEES**DATE OF MEETING: 7/12/04Bayou Steel

| <u>NAME</u>      | <u>PHONE</u>   | <u>AFFILIATION</u>       |
|------------------|----------------|--------------------------|
| Jennifer Pelloat | 225-219-3432   | LDEQ / Eng Group 1       |
| Cedric Mallon    | 225-219-3999   | DEQ - EED - TEDI         |
| Nicholas LaCroix | 225-219-9501   | DEQ - EED - TRI          |
| Timothy Bergeron | 225/219-3431   | LDEQ / Eng 1             |
| Fredrick Toura   | (225) 291-7122 | LDEQ / Permits           |
| Denise Bennett   | (225) 219-3086 | LDEQ / Permits - Air     |
| Clay Robinson    | (225) 219-3760 | LDEQ / Enforcement - Air |
| Jim Courville    | (225) 219-3428 | LDEQ / Eng #1            |
| Jim ORGERON      | (225) 275-3231 | LDEQ / PLANS             |
| Trevor Telle     | (225) 219-3105 | LDEQ / PERMITS           |
| BARRY GIPSON     | (225) 925-8405 | ETS                      |
| Wendy Stehling   | 985/652-0322   | Bayou Steel Corp.        |
| Linda Brown      | (225) 219-3535 | DEQ / EED / TRI + TEDI   |
| Al Pulliam       | 985 652-0409   | Bayou Steel              |
|                  |                |                          |
|                  |                |                          |
|                  |                |                          |



State of Louisiana  
Department of Environmental Quality



Edwin W. Edwards  
Governor

William A. Kucharski  
Secretary

Mr. Al Pulliam  
Environmental Manager  
Bayou Steel Corporation  
P. O. Box 5000  
LaPlace LA 70069

Dear Mr. Pulliam:

RE: Permit modification, Bayou Steel Corporation, LaPlace,  
St. John the Baptist Parish, Louisiana

This is to inform you that the permit modification requested for the above referenced facility has been approved under LAC 33:III.501. The submittal was approved on the basis of the emissions reported and the approval in no way guarantees the design scheme presented will be capable of controlling the emissions to the types and quantities stated. A revised application must be submitted if the reported emissions are exceeded after operation begins. The synopsis, data sheets, and conditions are attached herewith.

It will be considered a violation of the permit if all proposed control measures and/or equipment are not installed and properly operated and maintained as specified in the application.

The permit number cited below should be referenced in future correspondence regarding this subject.

Done this 5<sup>th</sup> day of MAY, 1995.

Permit No.: 885 (M-2)

Very truly yours,

*Gustave A. Von Bodungen*  
Gustave A. Von Bodungen, P.E.  
Assistant Secretary

GVB/WL

c: Southeast Regional Office



OFFICE OF AIR QUALITY P.O. BOX 82135 BATON ROUGE, LOUISIANA 70884-2135  
AN EQUAL OPPORTUNITY EMPLOYER

APPENDIX D  
7.4.1

AIR PERMIT BRIEFING SHEET  
AIR QUALITY DIVISION  
LOUISIANA DEPARTMENT OF ENVIRONMENTAL QUALITY

BAYOU STEEL CORPORATION  
LAPLACE, ST. JOHN THE BAPTIST PARISH, LOUISIANA

**I. BACKGROUND**

Bayou Steel Corporation operates an Electric Arc Furnace (EAF) steel mill in LaPlace, Louisiana. It was originally permitted on February 28, 1978 (Permit No. 885). A PSD permit (PSD-LA-66), issued February 15, 1983, for NO<sub>x</sub> emissions, was later rescinded. Permit No. 885(M-1) was issued October 28, 1983. Nitrogen oxides (NO<sub>x</sub>) emissions from the electric arc furnace (EAF) during melting and refining operations were not included in the referenced permit as NO<sub>x</sub> was not recognized as a precursor to ozone formation at that time. Accounting for fugitive emissions in permitting began only after 1990. The application for the present modification was first submitted in December, 1993, but later withdrawn because fugitive emissions were not included. The revised submittal was dated August 4, 1994. Supplemental information was received March 22, 1995.

**II. ORIGIN**

A permit application and Emission Inventory Questionnaire for this modification was received August 5, 1994. The commitment to submit an updated air permit application and EIQ was made in response to a Notice of Violation (NOV), issued by DEQ on June 3, 1994. The purpose of this submittal is to provide speciation of hazardous air pollutants (HAP) and to include fugitive emissions. Electric arc furnace (EAF) NO<sub>x</sub> emissions, missing from the previous permit modification, are included in this modification.

**III. DESCRIPTION**

Bayou Steel operates two separate EAFs. Scrap steel, coke lime, flux, and alloys are melted in a refractory-lined kettle using three high-voltage electrodes to produce a recovered steel product.

In preparation for charging and melting of the steel, the furnace electrodes are aligned and the furnace lining is coated with a protective layer of gunite at the slag zone. The furnace is loaded with the initial charge of scrap steel and other materials. The roof, in which the electrodes are

AIR PERMIT BRIEFING SHEET  
AIR QUALITY DIVISION  
LOUISIANA DEPARTMENT OF ENVIRONMENTAL QUALITY

BAYOU STEEL CORPORATION  
LAPLACE, ST. JOHN THE BAPTIST PARISH, LOUISIANA

housed, is placed onto the furnace and the electrical current is applied. After the first charge is melted, the EAF roof is removed from the furnace and a second charge of scrap steel, coke, lime and flux is added. The furnace roof is lowered onto the furnace and current again applied to melt the second charge. A third charge is added repeating the steps of the second charge. After the final meltdown, the molten steel is subjected to an oxygen injection period to further oxidize impurities and combine with any excess carbon to form carbon dioxide.

In a final refining stage, oxygen flow is discontinued with the electrical current still applied. The EAF vessel is first tilted backwards to empty slag into the slag pot, where it is water cooled and then placed on a slag pile. Liquid molten steel is poured into a teeming ladle when the vessel is tilted forward, completing a single EAF heat.

Molten steel is poured from the ladle to the continuous casting machine via an overhead crane. The ladle is placed on a turret which rotates to position the ladle over the continuous casting tundish. The ladle empties into four individual water-cooled copper billet molds. Steel leaves the mold as a solid steel casing with a liquid core. A continuous strand of steel is further cooled by water sprays as it is drawn from the mold and cut into various lengths by an oxygen cutting torch. The billets are transferred to the finishing area where they are allowed to cool.

Billets are sold or further processed in the hot forming rolling mill into angles, channels and I beams. A maximum of 600,000 tons of billets is anticipated to be produced, requiring 1.4 MM BTU of natural gas for each ton of billets charged.

Particulate emissions from the slag piles are controlled by wetting with water.

The Primary Dust Collection system (Emission Point No. 1-77) captures particulates during melting and refining operations (when the roof and electrodes are in place). The Secondary Dust Collection System (Emission Points 2-77A through F) collects particulates during charging and tapping operations (when the roof is removed). A canopy system around the EAF

AIR PERMIT BRIEFING SHEET  
AIR QUALITY DIVISION  
LOUISIANA DEPARTMENT OF ENVIRONMENTAL QUALITY

BAYOU STEEL CORPORATION  
LAPLACE, ST. JOHN THE BAPTIST PARISH, LOUISIANA

captures emissions from the uncovered furnace and routes them to the Secondary Dust Collection System baghouse for collection. Although it has been shown as a single point source in previous EIQ submittals, this baghouse actually has six separate vents. The furnace house vacuuming operations collects dust from the furnace house floor. Baghouse filters and vacuum bags are periodically dumped into an EAF during a routine charging sequence.

Bayou Steel's operation is regulated under New Source Performance Standards, 40 CFR 60 Subpart AA-Standards of Performance for Steel Plants: Electric Arc Furnaces Constructed After October 21, 1974 and on or Before August 17, 1983, for particulate emissions. Compliance with 0.0052 gr/dscf limit for the Primary Dust Collection System was demonstrated during a stack test performed during March, 1984. The average value obtained was 0.0029 gr/dscf which corresponds to an average rate of 2.15 pounds per hour total suspended particulates (TSP or 1.63 for PM<sub>10</sub>).

EIQ sheets were submitted for five diesel and two gasoline storage tanks ranging in size from 200 to 9,000 gallons. Total emission from the seven tanks is less than one ton. All of the tanks storing VOCs are equipped with submerged fill pipes. Only the two gasoline tanks are included in this permit. The diesel tanks meet the criteria for insignificant sources and, therefore, are not included in the permit.

Emissions summary, in tons per year (TPY), is as follows:

| <u>Pollutant</u> | <u>Permitted Before</u> | <u>Proposed</u> | <u>Change</u> |
|------------------|-------------------------|-----------------|---------------|
| TSP*             | 62.9                    | 58.2            | - 4.7         |
| PM <sub>10</sub> | -                       | 37.2            | + 37.2        |
| SO <sub>2</sub>  | 0.9                     | 0.3             | - 0.6         |
| NO <sub>x</sub>  | 119.7**                 | 149.1           | + 29.4        |
| VOC              | 1.0                     | 2.2             | + 1.2         |
| CO               | 5.4                     | 15.0            | + 9.6         |

\*See Attachment A for speciation of solid HAPs. Total particulates only were permitted previously.

\*\*This figure is adjusted for inclusion of NO<sub>x</sub> emissions omitted in error from the M-1 modification of Permit No. 885.

AIR PERMIT BRIEFING SHEET  
AIR QUALITY DIVISION  
LOUISIANA DEPARTMENT OF ENVIRONMENTAL QUALITY

BAYOU STEEL CORPORATION  
LAPLACE, ST. JOHN THE BAPTIST PARISH, LOUISIANA

Increases are due to increase in operating hours which results in an increase in the annual charge rate to the furnace. Since there was no modification, PSD review is not triggered. Decreases are due to differences in emission factors.

IV. TYPE OF REVIEW

The permit was reviewed for compliance with the Louisiana Air Quality Regulations and NSPS. Prevention of Significant Deterioration and NESHAP do not apply.

This facility is a major source of toxic air pollutants (TAP) because their potential to emit is above the 10/25 threshold. The compliance plan for the facility was approved April 13, 1995. This permit establishes limits within the constraints of said compliance plan.

V. PUBLIC NOTICE

Public notice is not required for a minor modification to an existing source.

SPECIFIC CONDITIONS

BAYOU STEEL CORPORATION  
LAPLACE, ST. JOHN THE BAPTIST PARISH, LOUISIANA

1. Permittee shall comply with all applicable provisions of 40 CFR 60 Subpart AA - Steel Plants: Electric Arc Furnaces Constructed After October 21, 1974 and on or Before August 17, 1983.
2. Permittee shall maintain the dust filters of the baghouse, Emission Point No. 1-77, and the baghouse serving Emission Point Nos. 2-77A thru F, so that particulate removal efficiencies of 99% are maintained. Filter vents shall be visually inspected for opacity on a daily basis. The filter elements (bags) shall be inspected every six months and changed as necessary. Records of opacity checks and maintenance inspections of the dust filters shall be kept on site and available for inspection by the Air Quality Division.

BAYOU STEEL CORPORATION  
LAPLACE, ST. JOHN THE BAPTIST PARISH, LOUISIANA

ATTACHMENT A

HAP Speciation in tons per year  $\times 10^{-2}$  (TPY  $\times 10^{-2}$ ):

| Emission Pt.No. | As    | Ba    | Cd    | Cr    | Cu    | Pb    | Mn    | Ni    | Zn    | Total |
|-----------------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|
| 1-77            | 0.042 | 0.323 | 0.444 | 3.099 | 2.834 | 19.72 | 29.66 | 0.399 | 134.3 | 190.8 |
| 2-77A           | 0.005 | 0.041 | 0.056 | 0.391 | 0.358 | 2.490 | 3.744 | 0.050 | 16.96 | 24.1  |
| 2-77B           | 0.005 | 0.041 | 0.056 | 0.391 | 0.358 | 2.490 | 3.744 | 0.050 | 16.96 | 24.1  |
| 2-77C           | 0.005 | 0.041 | 0.056 | 0.391 | 0.358 | 2.490 | 3.744 | 0.050 | 16.96 | 24.1  |
| 2-77D           | 0.005 | 0.041 | 0.056 | 0.391 | 0.358 | 2.490 | 3.744 | 0.050 | 16.94 | 24.1  |
| 2-77E           | 0.005 | 0.041 | 0.056 | 0.391 | 0.358 | 2.490 | 3.744 | 0.050 | 16.94 | 24.1  |
| 2-77F           | 0.005 | 0.041 | 0.056 | 0.391 | 0.358 | 2.490 | 3.744 | 0.050 | 16.94 | 24.1  |
| 1-94            | 0.178 | 1.360 | 1.871 | 13.06 | 11.94 | 83.10 | 124.9 | 1.682 | 565.9 | 804.0 |
| 2-94            | 0.003 | 0.021 | 0.029 | 0.204 | 0.187 | 1.299 | 1.954 | 0.026 | 8.85  | 12.6  |
| Totals          | 0.253 | 1.95  | 2.68  | 18.7  | 17.1  | 119.1 | 179.0 | 2.4   | 810.8 | 1152  |

\*The concentrations were derived from analyses of baghouse dust averaged over a 21-month period. They are amounts contained in total suspended particulates (TSP), not just  $PM_{10}$ .

AIR QUALITY DATA SHEET  
PAGE 1

BAYOU STEEL CORPORATION  
LAPLACE, ST. JOHN THE BAPTIST PARISH, LOUISIANA

Location of plant: 15 UTM: 744.7 km E 3325.5 km N

Description of location: Between River Road and Airline Highway approximately  
2 miles south of LaPlace

Estimated starting date Estimated starting operation  
of construction operating will begin \_\_\_\_\_

Dispersion Model(s) Used: NA

NEW \_\_\_\_\_ OR MODIFIED X EMISSION SOURCES Scrap Metal Recovery  
(Type of Source)

| Emission<br>Point No. | Description                      | Operating<br>Rate (Max)<br>or Tank Capacity | Operating Schedule |     |     |
|-----------------------|----------------------------------|---------------------------------------------|--------------------|-----|-----|
|                       |                                  |                                             | H/D                | D/W | W/Y |
| 1-77                  | Primary Dust Collection System   | 292,000 cu ft/min                           | 24                 | 7   | 52  |
| 2-77A                 | Secondary Dust Collection System | 68,333 cu ft/min                            | 24                 | 7   | 52  |
| 2-77B                 | Secondary Dust Collection System | 68,333 cu ft/min                            | 24                 | 7   | 52  |
| 2-77C                 | Secondary Dust Collection System | 68,333 cu ft/min                            | 24                 | 7   | 52  |
| 2-77D                 | Secondary Dust Collection System | 68,333 cu ft/min                            | 24                 | 7   | 52  |
| 2-77E                 | Secondary Dust Collection System | 68,333 cu ft/min                            | 24                 | 7   | 52  |
| 2-77F                 | Secondary Dust Collection System | 68,333 cu ft/min                            | 24                 | 7   | 52  |
| 4-77                  | Rolling Mill Furnace             | 77.2 MM BTU/hr                              | 24                 | 7   | 52  |
| 1-94                  | Furnace House Fugitives          | N/A                                         | 24                 | 7   | 52  |
| 2-94                  | Slag Pile Fugitives              | N/A                                         | 24                 | 7   | 52  |
| 3-94                  | A Bay Heater No. 1               | 1.5 MM BTU/hr                               | 24                 | 7   | 22  |
| 4-94                  | A Bay Heater No. 2               | 1.5 MM BTU/hr                               | 24                 | 7   | 22  |

AIR QUALITY DATA SHEET  
PAGE 1 (CONTINUED)

BAYOU STEEL CORPORATION  
LAPLACE, ST. JOHN THE BAPTIST PARISH, LOUISIANA

| Emission<br>Point No. | Description                      | Operating<br>Rate (Max)<br>or Tank Capacity | Operating Schedule |     |     |
|-----------------------|----------------------------------|---------------------------------------------|--------------------|-----|-----|
|                       |                                  |                                             | H/D                | D/W | W/Y |
| 5-94                  | A Bay Heater No. 3               | 1.5 MM BTU/hr                               | 24                 | 7   | 22  |
| 6-94                  | B Bay Heater No. 4               | 3.0 MM BTU/hr                               | 24                 | 7   | 22  |
| 7-94                  | B Bay Heater No. 5               | 3.0 MM BTU/hr                               | 24                 | 7   | 52  |
| 8-94                  | B Bay Heater No. 6               | 3.0 MM BTU/hr                               | 24                 | 7   | 52  |
| 11-94                 | Mechanic Shop Gasoline Tank No.3 | 1100 gal                                    | 24                 | 7   | 52  |
| 14-94                 | IMS Gasoline Tank No. 6          | 800 gal                                     | 24                 | 7   | 52  |

AIR QUALITY DATA SHEET  
PAGE 2

BAYOU STEEL CORPORATION  
LAPLACE, ST. JOHN THE BAPTIST PARISH, LOUISIANA  
MAXIMUM/AVERAGE EMISSIONS ARE LISTED IN LBS/HR

| Emission Point No. | PM <sub>10</sub> | SO <sub>2</sub> | Permitted Emissions<br>NO <sub>x</sub> | VOC         | CO        | OTHER | HEIGHT<br>Feet | TEMP<br>°F | FLOW RATE<br>CFM |
|--------------------|------------------|-----------------|----------------------------------------|-------------|-----------|-------|----------------|------------|------------------|
| 1-77               | 2.93/1.63        | 0.01/0.01       | 20.36/20.36                            | -           | -         | -     | 162.5          | 257        | 292,000          |
| 2-77A              | 0.258/0.21       | -               | -                                      | -           | -         | -     | 143.2          | 104        | 68,333           |
| 2-77B              | 0.258/0.21       | -               | -                                      | -           | -         | -     | 143.2          | 104        | 68,333           |
| 2-77C              | 0.258/0.21       | -               | -                                      | -           | -         | -     | 143.2          | 104        | 68,333           |
| 2-77D              | 0.258/0.21       | -               | -                                      | -           | -         | -     | 143.2          | 104        | 68,333           |
| 2-77E              | 0.258/0.21       | -               | -                                      | -           | -         | -     | 143.2          | 104        | 68,333           |
| 2-77F              | 0.258/0.21       | -               | -                                      | -           | -         | -     | 143.2          | 104        | 68,333           |
| 4-77               | 0.44/0.28*       | 0.09/0.06       | 20.36/12.91                            | 0.41/0.26   | 5.08/3.22 | -     | 143.3          | 700        | 44,490           |
| 1-94               | 6.57/5.25        | -               | -                                      | -           | -         | -     | NA             | ambient    | NA               |
| 2-94               | 0.064/0.064      | -               | -                                      | -           | -         | -     | NA             | ambient    | NA               |
| 3-94               | 0.004/0.004      | <0.01/0.01      | 0.20/0.20                              | <0.01/<0.01 | 0.05/0.05 | -     | NA             | 375        | 285              |
| 4-94               | 0.004/0.004      | <0.01/0.01      | 0.20/0.20                              | <0.01/<0.01 | 0.05/0.05 | -     | NA             | 375        | 285              |
| 5-94               | 0.004/0.004      | <0.01/0.01      | 0.20/0.20                              | <0.01/<0.01 | 0.05/0.05 | -     | NA             | 375        | 285              |
| 6-94               | 0.01/0.01        | <0.01/0.01      | 0.40/0.40                              | 0.01/0.01   | 0.10/0.10 | -     | NA             | 375        | 570              |
| 7-94               | 0.01/0.01        | <0.01/0.01      | 0.40/0.40                              | 0.01/0.01   | 0.10/0.10 | -     | NA             | 375        | 570              |
| 8-94               | 0.01/0.01        | <0.01/0.01      | 0.40/0.40                              | 0.01/0.01   | 0.10/0.10 | -     | NA             | 375        | 570              |
| 11-94              | -                | -               | -                                      | 0.12/0.12   | -         | -     | NA             | ambient    | NA               |
| 14-94              | -                | -               | -                                      | 0.09/0.09   | -         | -     | NA             | ambient    | NA               |

\*PM<sub>10</sub> emissions due to combustion of natural gas and process.

AIR QUALITY DATA SHEET  
PAGE 3

BAYOU STEEL CORPORATION  
LAPLACE, ST. JOHN THE BAPTIST PARISH, LOUISIANA

| Permitted emissions are listed in tons per year |                    |                 |                 |      |      |       |
|-------------------------------------------------|--------------------|-----------------|-----------------|------|------|-------|
| Emission Point No.                              | PM <sub>10</sub> * | SO <sub>2</sub> | NO <sub>x</sub> | VOC  | CO   | OTHER |
| 1-77                                            | 7.2                | 0.04            | 89.2            | -    | -    | -     |
| 2-77A                                           | 0.90               | -               | -               | -    | -    | -     |
| 2-77B                                           | 0.90               | -               | -               | -    | -    | -     |
| 2-77C                                           | 0.90               | -               | -               | -    | -    | -     |
| 2-77D                                           | 0.90               | -               | -               | -    | -    | -     |
| 2-77E                                           | 0.90               | -               | -               | -    | -    | -     |
| 2-77F                                           | 0.90               | -               | -               | -    | -    | -     |
| 4-77                                            | 1.22               | 0.24            | 56.5            | 1.13 | 14.1 | -     |
| 1-94                                            | 23.0               | -               | -               | -    | -    | -     |
| 2-94                                            | 0.28               | -               | -               | -    | -    | -     |
| 3-94                                            | 0.01               | <0.01           | 0.37            | 0.01 | 0.09 | -     |
| 4-94                                            | 0.01               | <0.01           | 0.37            | 0.01 | 0.09 | -     |
| 5-94                                            | 0.01               | <0.01           | 0.37            | 0.01 | 0.09 | -     |
| 6-94                                            | 0.02               | <0.01           | 0.75            | 0.02 | 0.19 | -     |
| 7-94                                            | 0.02               | <0.01           | 0.75            | 0.02 | 0.19 | -     |
| 8-94                                            | 0.02               | <0.01           | 0.75            | 0.02 | 0.19 | -     |
| 11-94                                           | -                  | -               | -               | 0.54 | -    | -     |
| 14-94                                           | -                  | -               | -               | 0.41 | -    | -     |
| TOTALS                                          | 37.2               | 0.28            | 149.1           | 2.2  | 15.0 | -     |

\*See Attachment A for speciation of HAP in particulates.

SPECIFIC CONDITIONS

BAYOU STEEL CORPORATION  
LAPLACE, ST. JOHN THE BAPTIST PARISH, LOUISIANA

1. Permittee shall comply with all applicable provisions of 40 CFR 60 Subpart AA - Steel Plants: Electric Arc Furnaces Constructed After October 21, 1974 and on or Before August 17, 1983.
2. Permittee shall maintain the dust filters of the baghouse, Emission Point No. 1-77, and the baghouse serving Emission Point Nos. 2-77A thru F, so that particulate removal efficiencies of 99% are maintained. Filter vents shall be visually inspected for opacity on a daily basis. The filter elements (bags) shall be inspected every six months and changed as necessary. Records of opacity checks and maintenance inspections of the dust filters shall be kept on site and available for inspection by the Air Quality Division.

STONE, PIGMAN, WALTHER, WITTMANN & HUTCHINSON

COUNSELLORS AT LAW

1000 WHITNEY BANK BUILDING

NEW ORLEANS, LOUISIANA 70130-2662

(504) 581-3200 TELEX 584128

SAUL STONE\*  
PAUL O. H. PIGMAN\*  
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DAVID L. STONE\*  
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PAUL L. ZIMMERING  
JOHN M. LANDIS  
STEPHEN H. KUPPERMAN  
JO HARRIET STRICKLER\*  
STEPHEN G. BULLOCK  
SARAH S. VANCE

\*A PROFESSIONAL CORPORATION

KYLE SCHONEKAS  
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DOUGLAS D. DODD  
RANDALL A. SMITH  
CHARLES R. PENOT, JR.  
LINDA R. GALLAGHER  
NOEL J. DARCE

November 9, 1983

OUR FILE NUMBER

40,728-D

Mr. Dietmar Sainitzer  
Mr. Bruce Eskew  
Mr. Mike McEarl  
Bayou Steel Corporation  
P. O. Box 5000  
LaPlace, Louisiana 70068

Re: Louisiana Permit 885-M-1

Gentlemen:

I enclose herewith a copy of State Air Permit 885-M-1. Larry Schumer of Waldemar S. Nelson and Company advises that this permit is an interim step toward rescission and replacement of the PSD Permit.

Before the PSD Permit can be rescinded by the Environmental Protection Agency, an operating permit must be in place, and therefore Permit 885-M-1 has been issued. If, and after, the PSD Permit is rescinded, Larry advises that we can anticipate issuance of a more stringent and more detailed state permit as the permanent Air Quality Permit.

Sincerely,

Original Signed

CLINTON W. SHINN

Clinton W. Shinn

CWS/sh  
Encl.

cc: Larry Schumer  
Harold Himmelman, Esq.  
John Guttmann, Esq.  
Paul Shorb, Esq.

APPENDIX D  
7.4.13



FRANK P. SIMONEAUX  
SECRETARY

B. JIM PORTER  
ASSISTANT SECRETARY

DEPARTMENT OF NATURAL RESOURCES  
OFFICE OF ENVIRONMENTAL AFFAIRS  
AIR QUALITY DIVISION

GUSTAVE VON BODUNGEN  
PROGRAM ADMINISTRATOR

October 28, 1983

Mr. Ewell P. Walther, Jr.  
Bayou Steel Corporation  
Post Office Box 5000  
LaPlace, Louisiana 70068

Dear Mr. Walther:

RE: Revision of State Permit 885 issued February 28, 1978. Total Emissions: Particulates 65.98 TPY, Sulfur Dioxide 1.002 TPY, Oxides of Nitrogen 77.80 TPY, Hydrocarbons 1.58 TPY, and Carbon Monoxide 9.22 TPY.

This is to confirm that the permit request for the above referenced project at the LaPlace Facility, LaPlace, St. John the Baptist Parish, Louisiana has been approved by the Assistant Secretary, Office of Environmental Affairs, Department of Natural Resources, under Air Quality Regulation 6.1.1. The submittal was approved on the basis of the emissions reported and the approval in no way guarantees the design scheme presented will be capable of controlling the emissions to the types and quantities stated. A new application must be submitted if the reported emissions are exceeded after operation begins. The emission and operating limitations are described in attached synopsis, data sheets and conditions.

It will be considered a violation of the permit if all proposed control measures and/or equipment are not installed and properly operated and maintained as specified in the application, and/or the attached condition are not satisfied.

The permit number cited below should be referenced in future correspondence regarding this subject.

Date: October 28, 1983  
Permit No.: 885-M-1

Approved by:

*Gustave Von Bodungen for*  
B. JIM PORTER  
Assistant Secretary

BJP/PD/bap

Enclosures

cc: Southeast Regional Office  
U.S. EPA, Region  
Waldmar S. Nelsen and Company

LOUISIANA AIR CONTROL COMMISSION

BAYOU STEEL CORPORATION

LaPlace (St. John the Baptist)

Bayou Steel Corporation requests a permit to construct and operate a steel manufacturing and forming facility on the Mississippi River in St. John the Baptist Parish, Louisiana. The facility will process scrap steel and produce billets, sections, rods, rounds and angles for both export and domestic purposes.

The process units will consist of two Electric Arc Furnaces, two Continuous Casting Units and Hot Rolling Mill Equipment.

Scrap steel and scale recovered from within the steel works will be recycled to the furnaces whereas the environmentally stable slag, wastewater treatment sludge and dust from the fabric filters will be used as landfill on Bayou Steel's property. A variance to start construction was approved by the Commission at the January 24, 1978 hearing.

Overall emissions of the facility are summarized as follows:

|                 |                 |
|-----------------|-----------------|
| Particulate     | 65.98 tons/year |
| HC              | 1.58 tons/year  |
| SO <sub>2</sub> | 1.002 tons/year |
| CO              | 9.22 tons/year  |
| NO <sub>x</sub> | 77.80 tons/year |

The greatest sources of air pollution in the steel mill will be the electric arc furnaces when power is on and/or when oxygen is injected.

To control and limit the emissions, the company will install:

- 1) A primary dust control system which will provide for carbon monoxide incineration, cooling, and high efficiency (99%) dust removal by means of a fabric filter baghouse.

- 2) A secondary dust control system with fabric filter baghouses to collect dust emissions when the primary dust control system is disengaged during the electric arc furnaces charging and tapping operations.

Fugitive dust emissions primarily due to lime and additive receiving, transferring and feeding system will be collected and cleaned by a fabric filter baghouse.

Sulfur dioxide emissions will be controlled by firing the rolling mill furnace with natural gas, a clean fuel.

Hydrocarbon emissions will consist of those associated with storing kerosene (a non-volatile organic compound), which is required for auxiliary heat input to the electric arc furnaces, in a 1500 barrel cone roof tank.

The company has stated that all the mentioned emission control schemes and equipment will comply with both LACC Regulations and EPA New Source Performance Standards and will also conduct necessary tests, monitoring and reporting as required.

A significant air quality deterioration analysis for particulate and sulfur dioxide area increments was submitted to EPA and indicate that the standards will be met.

Submitted dispersion calculations indicate that ambient air quality standards will not be violated.

BAYOU STEEL CORPORATION

LaPlace (St. John the Baptist)

RECOMMENDATION:

Approval provided the following conditions are met.

- 1) The synopsis sheets and the attached data sheets establish the emission and operating limitations and are a part of the permit. The synopsis and data sheets are based on the application for approval of emissions dated June 21, 1983 with supplemental information submitted July 15, 1983. The application and supplemental information are also considered part of this permit be reference.
- 2) Construction must commence within two years after the date of approval.
- 3) The permittee will submit to the Technical Secretary seminannual reports of progress defining the status of construction, noting any design changes, modifications or alterations in the construction schedule which have or may have an effect upon the emission rates or ambient air quality levels. Such reports shall continue to be submitted until such time as construction is certified as being complete.
- 4) Any emission testing performed for purposes of demonstrating compliance with the limitations set forth in Condition 1 shall be conducted in accordance with the methods described and referenced in Table 4 of the current Louisiana Air Control Commission Regulations.
- 5) The permittee shall, within 180 days after certifying the completion of construction prepare and submit to the Technical Secretary a report detailing the actual emission rates as compared to those limitations specified in Condition 1. The report shall also include, but not be limited to, malfunctions and upsets.

- 6) The permittee shall comply with all applicable New Source Performance Standards for Electric Arc Furnaces (40 CFR, Subpart AA).
- 7) The permittee shall maintain records of the hours of operation per calendar year for each source. These records shall be kept at the plant site for at least two years and made available to Air Quality Division.

## LOUISIANA ENVIRONMENTAL CONTROL COMMISSION

## Air Quality Data Sheet

Page 1

Bayou Steel Corporation

LaPlace, St. John the Baptist Parish

Location of plant: 15 UTM 744.7 Km E 3325.5 Km N

Description of location: The facility is located between River Road and

Airline Highway, approximately 2 miles south of LaPlace, and 2.3 miles north of Montz.

Estimated starting date

Estimated date operation will begin:

of construction: Existing

Type of Dispersion Calculations Used: Computer calculations using dispersion model PTMAX

## EFFECTS ON AMBIENT AIR

| Pollutant       | Time Period | Calculated Maximum Ground Level Concentration | Louisiana Air Quality Standard |
|-----------------|-------------|-----------------------------------------------|--------------------------------|
| Particulate     | Annual      | 43 ug/m <sup>3</sup>                          | 60 ug/m <sup>3</sup>           |
|                 | 24 hour     | 100 ug/m <sup>3</sup>                         | 150 ug/m <sup>3</sup>          |
| SO <sub>2</sub> | Annual      | 1.86 ug/m <sup>3</sup>                        | 60ug/m <sup>3</sup>            |
|                 | 24 hour     | 34.1 ug/m <sup>3</sup>                        | 260 ug/m <sup>3</sup>          |
| NO <sub>x</sub> | Annual      | 18.5 ug/m <sup>3</sup>                        | 100ug/m <sup>3</sup>           |
|                 |             |                                               |                                |
|                 |             |                                               |                                |
|                 |             |                                               |                                |

NEW ☐ OR MODIFIED ☒ EMISSION SOURCES

Steel Mill

(Type of Source)

| Stack I.D. # | Description               | Operating Rate (Maximum) | Operating Schedule |         |        |
|--------------|---------------------------|--------------------------|--------------------|---------|--------|
|              |                           |                          | Hrs/Day            | Days/Wk | Wks/Yr |
| 1-77         | Primary Dust Collection   | 203,580 lbs.hr           | 24                 | 7       | 42.5   |
| 2-77         | Secondary Dust Collection |                          | 8                  | 7       | 42.5   |
| 4-77         | Rolling Mill Furnace      | 145.5 mscf/hr            | 24                 | 6       | 50     |
|              |                           |                          |                    |         |        |
|              |                           |                          |                    |         |        |
|              |                           |                          |                    |         |        |
|              |                           |                          |                    |         |        |
|              |                           |                          |                    |         |        |
|              |                           |                          |                    |         |        |
|              |                           |                          |                    |         |        |

## Air Quality Data Sheet - Page 2

Bayou Steel Corporation

La Place, St. John the Baptist

(Company's Name)

(Nearest Town)

(Parish)

## EMISSIONS ARE LISTED USING THE UNITS LBS/HR

[illegible]

# Air Quality Data Sheet

[illegible]

8.1

**BAYOU STEEL CORPORATION**  
**P.O. BOX 5000**  
**LA PLACE, LOUISIANA 70069-1156**

**EMISSION COMPLIANCE TESTS**

**BAGHOUSE STACK** (source ID 1-77)

**JULY 23,2004**

**PERMIT NUMBER : 885 (M-2)**

Testing conducted by :

**E T S**

**EMISSION TESTING SERVICES, INC.**

**P.O. BOX 15075**

**BATON ROUGE, LOUISIANA 70895**

**(225) 925-8405**

FINAL File : 24104 issued 09-07-04 (117 pages)  
Draft File : 24104 issued 08-19-04 (95 pages)

# EMISSION TEST REPORT CERTIFICATION

for

BAYOU STEEL CORPORATION

EMISSION COMPLIANCE TESTS

BAGHOUSE STACK (source ID 1-77)

JULY 23, 2004

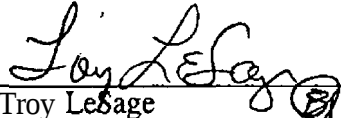
Testing conducted by :

EMISSION TESTING SERVICES, INC.

Emission Testing Services, Inc. is certified by the Louisiana Department of Environmental Quality (LDEQ) as a qualified environmental testing laboratory under the Louisiana Environmental Laboratory Accreditation Program (LELAP).

I certify that I have personally examined and am familiar with the information submitted herein, and based on my inquiries of those individuals immediately responsible for obtaining the information, I believe the submitted information is true, accurate, and complete.

\_\_\_\_\_  
Wendy Stehling  
Bayou Steel Corporation  
Plant Representative

  
\_\_\_\_\_  
Troy LeSage  
Emission Testing Services, Inc.  
Project Leader

  
\_\_\_\_\_  
Barry Gipson  
Emission Testing Services, Inc.  
Manager

# TABLE of CONTENTS

|      |                                                                       |        |
|------|-----------------------------------------------------------------------|--------|
| I.   | Introduction .....                                                    | 1.1    |
| II.  | Summary                                                               |        |
|      | Test Results Summary .....                                            | 2.1    |
|      | Test Method Modifications, Deviations, and Unusual Conditions .....   | 2.1    |
|      | Test Conclusions .....                                                | 2.1    |
|      | Process Description .....                                             | 2.3    |
| III. | Procedure .....                                                       | 3.1    |
| IV.  | Analytical Technique .....                                            | 4.1    |
| V.   | Quality Assurance/Quality Control .....                               | 5.1    |
|      | Chain of Custody .....                                                | 5.2    |
| VI.  | Test Data and Calculations .....                                      | 6.0.1  |
|      | <u>Baghouse Stack</u> .....                                           | 6.1.1  |
|      | Sample Point Location                                                 |        |
|      | EPA Methods 2, 4, and 29 .....                                        | 6.1.2  |
|      | EPA Method 3 .....                                                    | 6.1.3  |
|      | EPA Method 1, Verification of Absence of Cyclonic Flow .....          | 6.1.4  |
|      | EPA Methods 2, 3, and 4 (stack gas flow rate, mole wt., and moisture) |        |
|      | Test Data & Calculations, Runs 1-3 .....                              | 6.1.5  |
|      | EPA Method 29 (lead and mercury)                                      |        |
|      | Data Summary & Calculations, Runs 1-3 .....                           | 6.1.11 |
|      | Analyses of Samples .....                                             | 6.1.15 |
|      | Unit Operating Data .....                                             | 6.1.26 |
| VII. | Appendix .....                                                        | 7.0.1  |
|      | A. Resumes of Test Personnel .....                                    | 7.1.1  |
|      | B. Test Equipment Calibrations .....                                  | 7.2.1  |
|      | C. Correspondence, Bayou Steel and LDEQ .....                         | 7.3.1  |
|      | D. Permit Number 885 (M-2) Excerpts .....                             | 7.4.1  |

## LIST of TABLES

|    |                                                            |     |
|----|------------------------------------------------------------|-----|
| I. | Emission Test Results Summary, <b>Baghouse</b> Stack ..... | 2.2 |
|----|------------------------------------------------------------|-----|

## LIST of FIGURES

|      |                                                       |       |
|------|-------------------------------------------------------|-------|
| I.   | Schematic Drawing of Process .....                    | 2.4   |
| II.  | Sample Point Location, EPA Methods 2, 4, and 29 ..... | 6.1.2 |
| III. | Sample Point Location, EPA Method 3 .....             | 6.1.3 |

## LIST of STANDARD RESULT NOTATIONS

- $\leq$  or  $<$  **None** detected. Stated **result** is the minimum detection limit. Actual result may be less including the result 0.
- $\Delta$  or ! **Stated** result is the sum or average of multiple component **results**; or a result based on the sum of individual component results from a multi-part sampling train. At least one of the component results has a detectable quantity and at least one of the component results has a none **detectable** quantity; and the **value** of the minimum detection limit for the none detectable **component(s)** is significant in comparison with the value of the detectable **component(s)**. The actual result may be less; however, not less than the result computed with the detectable **component(s)** only.

## I. INTRODUCTION

Emission Testing Services, Inc. (**ETS**) was contracted by Bayou Steel Corporation (Bayou **Steel**) to conduct emission testing at Bayou Steel's plant located **near** the town of **LaPlace**, Louisiana in **St. James** Parish, Louisiana. Emissions from the **Baghouse Stack** were **tested** to **determine** the emission rates of lead and mercury. Tests were conducted in **order** to **demonstrate** compliance with emission permit limits. The **Baghouse Stack**, source ID 1-77, operates under permit number 885 (M-2) issued by the Louisiana Department of Environmental Quality (LDEQ).

All tests were **conducted** using EPA test methods. The emission rates of lead and mercury were determined using EPA Method **29**. EPA Methods 1 - 4 were used to determine the number and location of sample **points**, **and** the velocity, moisture, molecular weight, and volumetric flow rate of the stack gas.

The ETS test **team** consisted of Project Leader Troy **LeSage** and a test crew consisting of Ronald **McCabe** and Joel **Richard**. Wendy Stehling represented Bayou Steel and coordinated testing with plant operations. During the emission tests, the LDEQ was represented **onsite** by Jim Stone (SERO), Tim Bergeron (ECS-Technology) and Cedric **Mellion** (EED-TRI).

Emissions from the **Baghouse Stack** were tested on **July**, 23, 2004. Three, 72-min duration tests were conducted.

## II. SUMMARY

### Test Results Summary

On July 23, 2004 emissions from the **Baghouse** Stack at Bayou Steel were tested to determine the emission rates of lead and mercury. Results of the tests are presented in Table I.

### Test Method Modifications, Deviations and Unusual Conditions

EPA methods were used to determine all pollutant and stack gas data. All modifications to and deviations from the standard test methods have been documented above. All unusual conditions have been noted above.

### Test Conclusions

Quality assurance procedures meeting EPA and LDEQ requirements were used during the emission tests. All quality indicators, with the exception of those noted above, were within the range of acceptable results. Test data are complete, accurate, and representative of source conditions. Overall, the quality of data gathered are acceptable to meet project objectives.

**TABLE I**  
**EMISSION TEST RESULTS SUMMARY**

**BAYOU STEEL CORPORATION**

**BAGHOUSE STACK** (source ID 1-77)

| <u>PARAMETER</u>      | <u>Permit Limit<br/>Max./Avg.</u> | <u>RUN 1</u> | <u>RUN2</u> | <u>RUN 3</u> | <u>AVERAGE</u> |
|-----------------------|-----------------------------------|--------------|-------------|--------------|----------------|
| <b>DATE</b>           |                                   | 7-23-04      | 7-23-04     | 7-23-04      |                |
| <b>TIME</b>           |                                   | 0934-1047    | 1158-1314   | 1605-1723    |                |
| <b>MERCURY</b>        |                                   |              |             |              |                |
| ug/dscf               |                                   | 0.0670       | 0.0696      | 0.1908       | 0.1091         |
| lb/hr                 |                                   | 0.00133      | 0.00140     | 0.00403      | 0.00225        |
| <b>LEAD</b>           |                                   |              |             |              |                |
| ug/dscf               |                                   | 9.735        | 10.66       | 10.53        | 10.31          |
| lb/hr                 |                                   | 0.1938       | 0.2151      | 0.2124       | 0.2071         |
| <b>STACK GAS DATA</b> |                                   |              |             |              |                |
| Temperature, F        |                                   | 241          | 241         | 240          | 241            |
| Moisture, vol %       |                                   | 4.08         | 3.05        | 4.64         | 3.92           |
| Velocity, ft/sec      |                                   | 66.33        | 66.43       | 67.52        | 66.76          |
| Flow Rate, acfm       |                                   | 208477       | 208786      | 212216       | 209826         |
| , dscfm               |                                   | 150510       | 152492      | 152533       | 151845         |

## PROCESS DESCRIPTION

Bayou Steel operates a steel mill, which includes two separate Electric Arc Furnaces (EAF) and a Ladle Metallurgical Facility (LMF). The EAF steel melting process consists of melting scrap steel, carbon sources, lime, **flux**, alloys, **and** other iron bearing material **in a** refractory lined vessel using three high voltage electrodes to produce a recovered steel product. Liquid steel is transferred either to the LMF for further refining or, to the continuous casting area where it is poured into the billet molds. The continuous strand is cooled and cut into various lengths. Billets are either sold as products or processed in the Rolling Mill by reheating followed by shaping using various rolling operations. Steel sections, angles, channels, and I-beams are cut or sheared to various lengths and transferred to the shipping warehouse for storage and loading.

### ELECTRIC ARC FURNACE STEEL MILL

The EAF steel melting process is a batch operation. Each batch is called a heat and requires approximately 60 minutes. A heat consists of the following steps:

EAF Preparation – In preparation for charging and melting the scrap steel, the furnace electrodes are aligned and the **furnace** is coated with a protective layer of **gunnite** at the slag zone.

First Charge and Melt – The **furnace** is loaded **with** the initial charge of scrap steel and other materials. The roof is placed on the furnace and electrical current is applied to the electrodes to melt the first **charge** of scrap material.;

Potential **Intermediate** Charges and Melts – The **furnace** roof is removed and the **intermediate** charge of scrap material **and** additives **are** added to the furnace. The roof is lowered onto the **furnace** and current is applied to melt the second charge of material.

Final Charge and Melt – The furnace roof is removed and the **final** charge of scrap material and additives **are** added to the furnace. The roof is lowered onto the **furnace** and current is applied to melt **the final** charge of material.

Oxidizing and Refining – Oxygen is injected into the molten steel to oxidize impurities and carbon. **Electrical** current is applied to **refine** the molten steel to meet product specifications.

Slagging and Tapping – The **EAF** is tilted backward to empty slag into a slag pot. Slag is cooled and **transferred** to a material stockpile. Following **slagging**, the EAF is tilted forward to pour the molten steel into a **teeming** ladle:

Figure -1  
Bayou Steel  
Process Flow Diagram

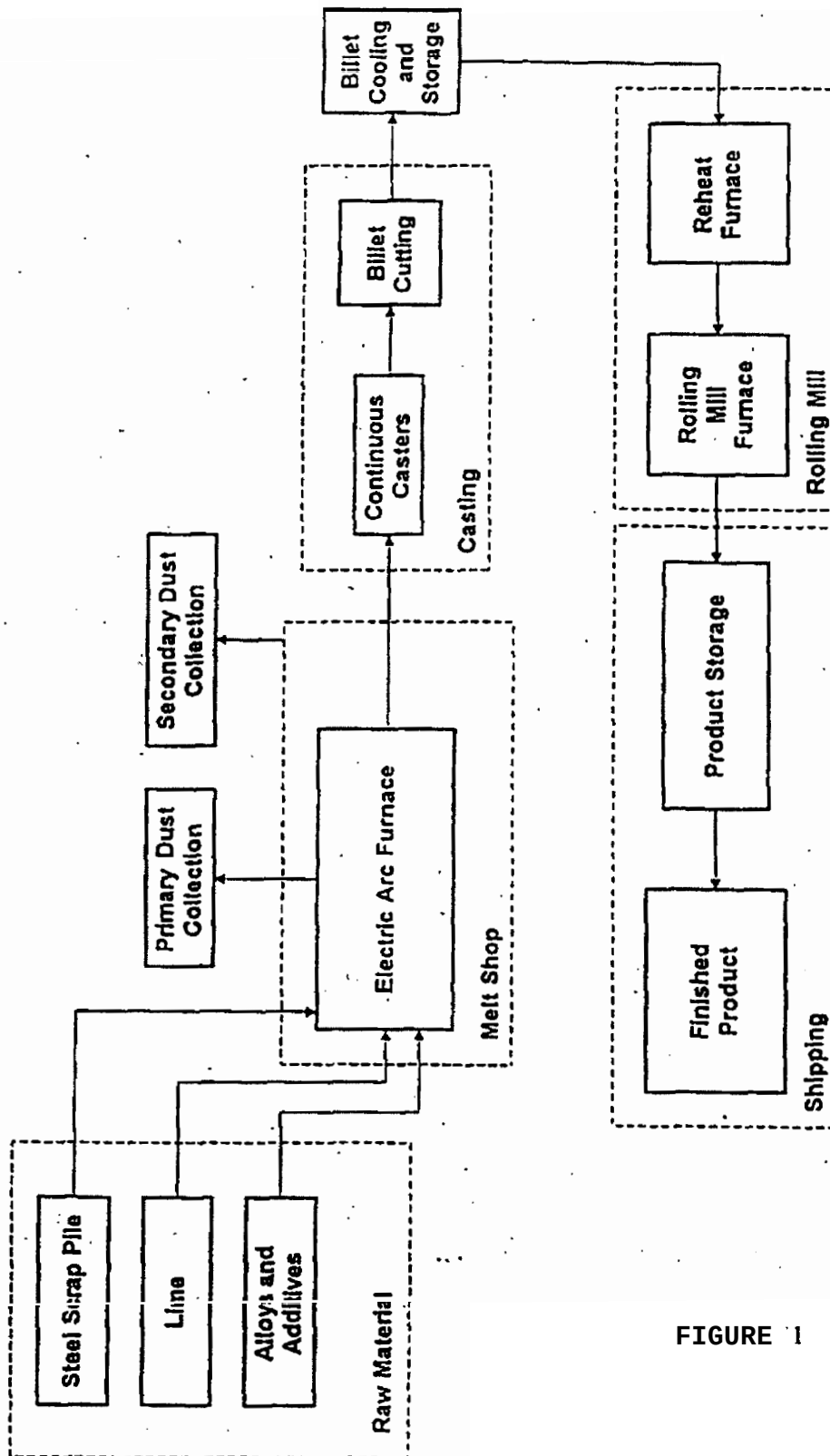


FIGURE 1

Bayou Steel Title V Draft 8/21/98 f:\users\title5\bayou\title5genfig.vsd

### III. PROCEDURE

Emissions were determined using EPA methods found in Appendix A, Part 60, Title 40 of the Code of Federal Regulations. A brief description of each method used follows.

#### LOCATION of SAMPLE POINTS

Stack gas flow rate, moisture, lead, and mercury determinations were conducted at test points selected per EPA Method 1.

Oxygen and carbon dioxide samples were collected from a point located at the center of the stack. This test point is in conformance with the applicable test methods.

#### EPA METHOD 1:

##### SAMPLE and VELOCITY TRAVERSES for STATIONARY SOURCES

Method 1 is applicable to stacks having a diameter greater than 12 in. The method recommends that sampling points be located 8 diameters downstream and 2 diameters upstream from the nearest flow disturbances; however, any distances greater than the minimum 2 diameters downstream and 0.5 diameters upstream are acceptable. These distances help insure the collection of a representative sample in the absence of cyclonic flow. Cyclonic flow is detected by measuring the stack gas flow Yaw angle at each test point. The average yaw angle is required to be less than 20 degrees.

The **Baghouse** Stack has a stack diameter of 98.0 in. The sampling point was located 6.73 stack diameters downstream and 7.96 **stack diameters** upstream from the nearest flow disturbances. During testing, 16 sample points were used, divided into 8 traverse points located across 2 perpendicular diameters of the stack with access to the points through 2 sampling ports. Cyclonic flow was not detected.

#### EPA METHOD 2:

##### DETERMINATION of STACK GAS VELOCITY and VOLUMETRIC FLOW RATE ( Type S **pitot** tube )

The average gas velocity in the stack was determined from the gas molecular weight, moisture content, and the average velocity head measured using a type S **pitot** tube. Volumetric flow rate was determined from the velocity and stack cross-sectional area.

#### **EPA METHOD 3:**

##### **GAS ANALYSIS FOR CARBON DIOXIDE, OXYGEN, EXCESS AIR, and DRY MOLECULAR WEIGHT**

Molecular weight of the stack gas was calculated from the oxygen, carbon dioxide, moisture, and nitrogen concentration data. Oxygen concentration data were obtained using EPA Method 3A and moisture concentration data were obtained using EPA Method 4. Balance of the stack gas composition was assumed to be nitrogen.

#### **GRAB SAMPLE**

Carbon dioxide concentration data were obtained from an analysis of stack gas samples using an Orsat analyzer. A sample of the stack gas was continuously extracted from the stack and was transferred through a heated, Teflon sample line to a sample conditioning unit where particulate and moisture was removed. A portion of the conditioned sample was introduced to the Orsat for analysis.

#### **EPA METHOD 4:**

##### **DETERMINATION of MOISTURE CONTENT in STACK GASES**

Moisture of the stack gas was determined by extracting a gas sample from the stack throughout the duration of the test while traversing the stack with the sample probe. Sample gas passed from the heated probe, through a heated sample line to a particulate filter and a series of four impingers immersed in an ice bath. The first two impingers initially contained known weights of water, the third was empty; and the fourth contained a known weight of silica gel. Water vapor in the gas sample was condensed and trapped in the impingers. Sample volume was measured using a dry gas meter located downstream of the impinger train.

#### **EPA METHOD 29 :**

##### **DETERMINATION of METALS EMISSIONS from STATIONARY SOURCES**

A gas sample was extracted from the stack isokinetically using a heated glass probe fitted with a particulate filter. Sample gas passed from the probe, through a series of four impingers immersed in an ice bath. The first and second impingers contained a nitric acid solution, the third was empty, and the fourth impinger contained silica gel. Sample flow rate was established using a diaphragm pump and was controlled using a valve. A calibrated dry gas meter was used to determine the total gas sample volume.

After sampling, the filter was recovered from the filter holder. The front half of the filter holder and probe were washed and the washings were collected as the probe wash sample. The contents of the first, second, and third impingers were collected as a single impinger sample. The impingers and connecting glassware were washed with the washings added to the impinger sample. Sample containers were labeled and sealed for shipment to the laboratory for analyses.

## **IV. ANALYTICAL TECHNIQUE**

All sample analyses were conducted following EPA methodology. Presented below are brief descriptions of **each** method used.

### **EPA METHOD 3:**

#### **GAS ANALYSIS FOR CARBON DIOXIDE, OXYGEN, EXCESS AIR, and DRY MOLECULAR WEIGHT**

The concentration of carbon dioxide in the stack gas **was** determined **using** an Orsat analyzer. Analysis **was** based on the **differential** sample volume of the gas sample before and after passing the sample through an oxygen absorbing reagent.

Oxygen concentration **was** determined **using** EPA Method 3A.

### **EPA METHOD 4:**

#### **DETERMINATION of MOISTURE CONTENT in STACK GASES**

The mass of water vapor **condensed** from the sample gas was determined gravimetrically.

### **EPA METHOD 29 :**

#### **DETERMINATION of METALS EMISSIONS from STATIONARY SOURCES**

Prior to analysis, the filter was digested in nitric acid. The mass of metals collected in the various samples was analyzed using an atomic adsorption spectrometer (AA).

## V. QUALITY ASSURANCE/ QUALITY CONTROL

Test results have been validated by following rigorous quality assurance (QA) and quality control (QC) procedures **documented** in ETS' Standard Operating Procedures. These procedures meet and/or **exceed** EPA requirements **and have approval by the LDEQ under the Louisiana Environmental Laboratory Accreditation Program (LELAP)**.

The QA/QC programs ensure that the test data are representative of the source conditions by verifying the completeness, accuracy, and precision of the test data. QA/QC functions cover all aspects of the test including field testing, sampling, and analysis, sample transport and **laboratory analysis**, and data processing and reporting.

Emission testing at Bayou Steel included a series of QA/QC functions. **All QA/QC** functions were completed satisfactorily within the required limits.

## CHAIN of CUSTODY

For those samples being transported to the laboratory for analysis, a Chain of Custody form was prepared during the sample recovery process. The sample ID, number of samples, **liquid** level when applicable, name of the sample recovery supervisor, name of the person responsible for sample recovery and the signature of the sample trustee were recorded on the custody **form**.

**During** all subsequent handing, the custody form accompanied the samples. As personnel relinquished responsibility for the samples, the receiving sample trustee verified the number and integrity of the samples and signed **the** custody form.

Upon receipt at the analytical laboratory, the lab sample trustee verified the number, type, and integrity of the samples. These data were **recorded** on the custody form **along** with the date of receipt and **lab** sample trustees signature.

At the time of analysis, the **laboratory** analyst recorded the analysis date and the laboratory supervisors name on the custody **form**. The analyst signed the custody form and attached it to the analytical results.

Chain of Custody forms for samples collected during testing' follow on the next pages along with the **analytical** q u e s t forms.

CLIENT: BAYOU STEEL SOURCE: BAGHOUSE STACK

| ETS SAMPLE ID   | LAB ID   | NUMBER | DESCRIPTION    | COLLECTION DATE | SAMPLE MEDIA | PRESERVATIVE/TYPE & AMOUNT | STORE ON ICE | VOLUME MARKED | SEALED |
|-----------------|----------|--------|----------------|-----------------|--------------|----------------------------|--------------|---------------|--------|
| PW-R1           | P4070973 |        | PROBE WASH     | 7/23/2004       | 0.1N HNO3    | N/A                        | Y            | Y             | Y      |
| PW-R2           | P4070974 |        | PROBE WASH     | 7/23/2004       | 0.1N HNO3    | N/A                        | Y            | Y             | Y      |
| PW-R3           | P4070975 |        | PROBE WASH     | 7/23/2004       | 0.1N HNO3    | N/A                        | Y            | Y             | Y      |
| IMP 1&2-R1      | P4070976 |        | IMPINGER CATCH | 7/23/2004       | HNO3/H2O2    | N/A                        | Y            | Y             | Y      |
| IMP 1&2-R2      | P4070977 |        | IMPINGER CATCH | 7/23/2004       | HNO3/H2O2    | N/A                        | Y            | Y             | Y      |
| IMP 1&2-R3      | P4070978 |        | IMPINGER CATCH | 7/23/2004       | HNO3/H2O2    | N/A                        | Y            | Y             | Y      |
| IMP 3-R1        | P4070979 |        | IMPINGER CATCH | 7/23/2004       | 0.1N HNO3    | N/A                        | Y            | Y             | Y      |
| IMP 3-R2        | P4070980 |        | IMPINGER CATCH | 7/23/2004       | 0.1N HNO3    | N/A                        | Y            | Y             | Y      |
| IMP 3-R3        | P4070981 |        | IMPINGER CATCH | 7/23/2004       | 0.1N HNO3    | N/A                        | Y            | Y             | Y      |
| BLANK 0.1N HNO3 | P4070982 |        | BLANK          | 7/23/2004       | 0.1N HNO3    | N/A                        | Y            | Y             | Y      |
| BLANK DI H2O    | P4070983 |        | BLANK          | 7/23/2004       | DI H2O       | N/A                        | Y            | Y             | Y      |
| BLANK HNO3/H2O2 | P4070984 |        | BLANK          | 7/23/2004       | HNO3/H2O2    | N/A                        | Y            | Y             | Y      |

3.5

|                                                         |                                                |                                  |
|---------------------------------------------------------|------------------------------------------------|----------------------------------|
| TOTAL NUMBER of SAMPLES including BLANKS and SPIKES: 12 | FIELD SAMPLE RECOVERY SUPERVISOR: Ron McCabe   | SAMPLES COLLECTED BY: Ron McCabe |
|                                                         | SAMPLE TRUSTEE FROM SAMPLE POINT: Joel Richard |                                  |

| SAMPLES TRANSFERRED TO (LAB NAME) | TRANSFER DATE | METHOD  | NUMBER OF SAMPLES | CONDITION OF SAMPLES | NOTES | RECEIVING SAMPLE TRUSTEE SIGNATURE |
|-----------------------------------|---------------|---------|-------------------|----------------------|-------|------------------------------------|
| CHEMTEX                           | 07/25/04      | By hand | 12                | Good                 |       | Kerley                             |
|                                   |               |         |                   |                      |       |                                    |
|                                   |               |         |                   |                      |       |                                    |
|                                   |               |         |                   |                      |       |                                    |
|                                   |               |         |                   |                      |       |                                    |

|                                                          |                            |                  |                       |                         |
|----------------------------------------------------------|----------------------------|------------------|-----------------------|-------------------------|
| ANALYSIS REQUIRED: LEAD AND MERCURY AS PER EPA METHOD 29 | DATE of ANALYSIS: 07/29/04 | ANALYST: 148 CHA | REPORT DATE: 08/02/04 | REPORT NUMBER: P4070973 |
|----------------------------------------------------------|----------------------------|------------------|-----------------------|-------------------------|

NOTES

# SLIDE

ANALYSIS REQUIRED: MERCURY AS PER EPA METHOD 29

5860 Lohd

ITARUSA

|   |   |   |   |   |   |
|---|---|---|---|---|---|
| 0 | 7 | 2 | 9 | 0 | 4 |
|---|---|---|---|---|---|

**NG SAMPLE TRUSTEE**  
**SIGNATURE**

**FIELD SAMPLE RECOVERY SUPERVISOR: Ron McCabe**  
**SAMPLE TRUSTEE FROM SAMPLE POINT: Joel Richard**

| ETS SAMPLE ID | LAB ID | SAMPLE DESCRIPTION | COLLECTION DATE | SAMPLE MEDIA | PRESERVATIVE/TYPE & AMOUNT | STORE ON ICE | VOLUME MARKED | SEALED |
|---------------|--------|--------------------|-----------------|--------------|----------------------------|--------------|---------------|--------|
|---------------|--------|--------------------|-----------------|--------------|----------------------------|--------------|---------------|--------|

**SOURCE: BAGHOUSE STACK**



EMISSION TESTING SERVICES, INC.

## CHAIN of CUSTODY and ANALYTICAL REQUIREMENTS

CLIENT: BAYOU STEEL

SOURCE: BAGHOUSE STACK

| ETS SAMPLE ID- | LAB ID<br>NUMBER | SAMPLE<br>DESCRIPTION | COLLECTION<br>DATE | SAMPLE<br>MEDIA | PRESERVATIVE/<br>TYPE & AMOUNT | STORE<br>ON ICE | VOLUME<br>MARKED | SEALED |
|----------------|------------------|-----------------------|--------------------|-----------------|--------------------------------|-----------------|------------------|--------|
| FILTER-R1      | 14070943         | #5396                 | 7/23/2004          | QUARTZ          | N/A                            | N/A             | N/A              | Y      |
| FILTER-R2      | 14070944         | #5243                 | 7/23/2004          | QUARTZ          | N/A                            | N/A             | N/A              | Y      |
| FILTER-R3      | 14070945         | #5246                 | 7/23/2004          | QUARTZ          | N/A                            | N/A             | N/A              | Y      |
| BLANK FILTER   | 14070946         | #5249                 | 7/23/2004          | QUARTZ          | N/A                            | N/A             | N/A              | Y      |
|                |                  |                       |                    |                 |                                |                 |                  |        |
|                |                  |                       |                    |                 |                                |                 |                  |        |
|                |                  |                       |                    |                 |                                |                 |                  |        |
|                |                  |                       |                    |                 |                                |                 |                  |        |
|                |                  |                       |                    |                 |                                |                 |                  |        |
|                |                  |                       |                    |                 |                                |                 |                  |        |
|                |                  |                       |                    |                 |                                |                 |                  |        |
|                |                  |                       |                    |                 |                                |                 |                  |        |
|                |                  |                       |                    |                 |                                |                 |                  |        |

on  
inTOTAL NUMBER of SAMPLES including BLANKS and SPIKES: 4  
SAMPLES COLLECTED BY: Ron McCabeFIELD SAMPLE RECOVERY SUPERVISOR: Ron McCabe  
SAMPLE TRUSTEE FROM SAMPLE POINT: Joel Richard

| SAMPLES TRANSFERRED<br>TO<br>(LABNAME) | TRANSFER<br>DATE | TRANSFER<br>METHOD | NUMBER<br>OF SAMPLES | CONDITION<br>OF SAMPLES | NOTES | RECEIVING SAMPLE TRUSTEE<br>SIGNATURE |
|----------------------------------------|------------------|--------------------|----------------------|-------------------------|-------|---------------------------------------|
| CHEMTREX                               | 07/25/04         | By hand            | 4                    | Good                    |       | KC Robely                             |
|                                        |                  |                    |                      |                         |       |                                       |
|                                        |                  |                    |                      |                         |       |                                       |

ANALYSIS REQUIRED: MERCURY AND LEAD AS PER EPA REFERENCE  
METHOD 29

DATE of ANALYSIS: \_\_\_\_\_

ANALYST: - \_\_\_\_\_  
REPORT DATE: \_\_\_\_\_  
REPORT NUMBER: \_\_\_\_\_NOTES \_\_\_\_\_  
\_\_\_\_\_  
\_\_\_\_\_

## VI. TEST DATA and CALCULATIONS

All emission test field data, unit **operations** data, and laboratory **data** are presented in this section along with the associated data reduction calculations.

Data from the field data **forms** were manually input into a computer for data processing and calculations. Integrity of data input is maintained by using a double entry system. The computer performed all calculations and produced the calculations and results summary pages. Input data accuracy were further verified by comparison of raw field data to the computer data printed on the summary pages. Computer program integrity and calculations verification are validated by processing a known set of data. Further **controls** on the computer program are **conducted** by comparison of **manual** spot calculations of the raw data input to computer **calculations** results.

## **EMISSION TESTS**

### **on the BAGHOUSE STACK**

Emission tests were conducted on the **Baghouse** Stack to determine the concentration of oxygen and carbon dioxide; and the concentration and mass emission rates of lead and mercury.

Flow rate, lead, and mercury emissions were determined following **EPA** Methods 2, 4, and 29 using a combined sampling train. Oxygen and carbon dioxide emissions were determined using **EPA** Method 3. Prior to the emission tests, the absence of cyclonic flow at the sampling point was determined using **EPA** Method 1.

Lead, mercury, stack gas velocity, and moisture samples and measurements were obtained at sample traverse points, Figure **II**, selected per **EPA** Method 1. Oxygen and carbon dioxide samples and measurements were obtained from a single sample point, Figure **III**, located near the center of the stack.

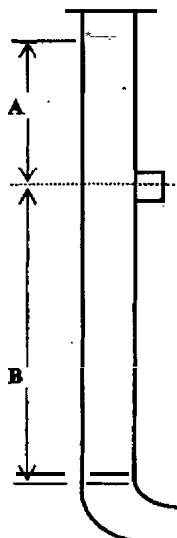
Test data and associated calculations are presented on the following pages.

# ETS

EMISSION TESTING SERVICES INC.

## TRAVERSE POINT LAYOUT

METHODS-1-4 & 29



CLIENT:

BAYOU STEEL

DATE:

7/22/2004

UNIT TESTED:

BAGHOUSE STACK

LOCATION:

LAPLACE, LA

UPSTREAM DIST. (A): (INCHES)

780

DIAMETERS: 7.96

DOWNSTREAM DIST. (B): (INCHES)

660

DIAMETERS: 6.73

INSIDE DIAMETER (INCHES):

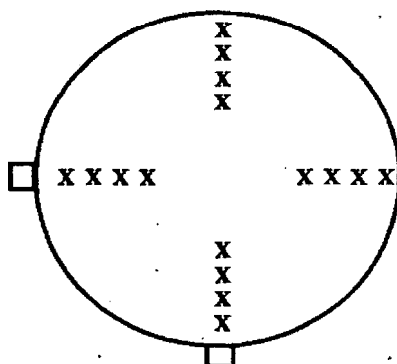
98

COUPLING LENGTH (INCHES):

6

COUPLING TYPE:

4" SCREW ON



CROSS SECTIONAL LAYOUT

FIGURE 11

TOTAL TRAVERSE POINTS. 16

| TRAVERSE POINT | DISTANCE<br>% OF DIAMETER | STACK<br>DIAMETER | COUPLING<br>LENGTH | TRAVERSE<br>POINTS |
|----------------|---------------------------|-------------------|--------------------|--------------------|
| 1              | 3.2                       | 98                | 6                  | 9.14               |
| 2              | 10.5                      | 98                | 6                  | 16.29              |
| 3              | 19.4                      | 98                | 6                  | 25.01              |
| 4              | 32.3                      | 98                | 6                  | 37.65              |
| 5              | 67.7                      | 98                | 6                  | 72.35              |
| 6              | 80.6                      | 98                | 6                  | 84.99              |
| 7              | 89.5                      | 98                | 6                  | 93.71              |
| 8              | 98.8                      | 98                | 6                  | 100.86             |

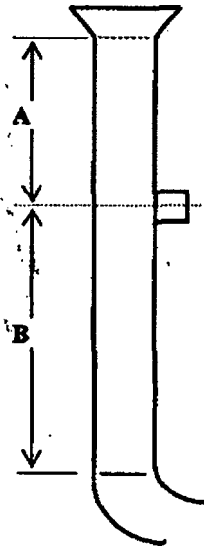
SIGNATURE: Tom McCabe

# ETS

EMISSION TESTING SERVICES INC.

## TRAVERSE POINT LAYOUT

### METHODS 3



CLIENT:

DATE:

UNIT TESTED:

LOCATION:

UPSTREAM DIST. (A):

DOWNSTREAM DIST. (B):

INSIDE DIAMETER (INCHES):

COUPLING LENGTH (INCHES):

COUPLING TYPE:

BAYOU STEEL

07/22/04

BAGHOUSE STACK

LAPLACE, LA

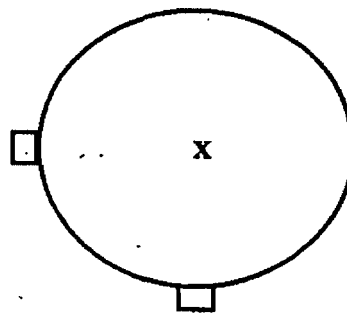
780

660

98

6

4" SCREW ON



CROSS SECTIONAL LAYOUT

FIGURE 111

TOTAL TRAVERSE POINTS-

1

TRAVERSE  
POINT  
1

DISTANCE  
% OF DIAMETER  
0.500

STACK  
DIAMETER  
98

COUPLING  
LENGTH  
6

TRAVERSE  
POINTS  
55.00

SIGNATURE:

*Ronald M. Cate*

# ETS

EMISSION TESTING SERVICES, INC.

## VERIFICATION OF ABSENCE of CYCLONIC FLOW

COMPANY: Bayer Steel

DATE: 7-23-04

SOURCE: Bqhouse Stack

STACK DIAMETER 98"

LOCATION: Norco, La.

OPERATOR: Joe Richard

| REFERENCE<br>ANGLE |          | REFERENCE<br>ANGLE |           |
|--------------------|----------|--------------------|-----------|
| 1                  | <u>0</u> | 13                 | <u>1</u>  |
| 2                  | <u>1</u> | 14                 | <u>2</u>  |
| 3                  | <u>2</u> | 15                 | <u>1</u>  |
| 4                  | <u>1</u> | 16                 | <u>1</u>  |
| 5                  | <u>2</u> | 17                 | <u>  </u> |
| 6                  | <u>0</u> | 18                 | <u>  </u> |
| 7                  | <u>1</u> | 19                 | <u>  </u> |
| 8                  | <u>2</u> | 20                 | <u>  </u> |
| 9                  | <u>1</u> | 21                 | <u>  </u> |
| 10                 | <u>2</u> | 22                 | <u>  </u> |
| 11                 | <u>0</u> | 23                 | <u>  </u> |
| 12                 | <u>1</u> | 24                 | <u>  </u> |
| AVERAGE            |          | <u>1.125</u> *     |           |

\* THE AVERAGE IS THE ABSOLUTE VALUE OF EACH DEGREE POINT DIVIDED BY THE NUMBER OF POINTS.

REFERENCE ANGLE CANNOT EXCEED 26 DEGREES OF AVERAGE OVERALL VALUE.

FORMS: CYCLONIC

# ETS<sup>®</sup> EMISSION TESTING SERVICES, INC., FIELD DATA, METHOD(S) 1-4 + 29

PLANT: Bayou Steel SAMPLE BOX NO.: 35<sup>th</sup> RM PITOT TUBE ID.: P-105 STACK DIAMETER, in.: .98"  
 DATE: 7-23-04 METER BOX NO.: 3 PITOT TUBE FACTOR: .832 METER Δ H@: 1.8127  
 LOCATION: Norco, La. BAROMETRIC PRESSURE: 29.95 FILTER ID.: METER D.G.M.F.: 1.0309  
 STACK ID.: Baghouse Stack AMBIENT TEMP.: 81°F FILTER TYPE: K-FACTOR: .6580  
 RUN NO.: 1 OPERATOR: Joe Richard NOZZLE DIAMETER, IN: .170 T-FACTOR: 461.91

| Traverse Point Number | Sampling Time (θ), min. | Static Pressure (in. H <sub>2</sub> O) | Stack Temp. (T <sub>s</sub> ), °F | Velocity Head |        | Pressure Differential Across Orifice Meter (ΔH) in., H <sub>2</sub> O |         | Dry Gas Meter Volume (V <sub>m</sub> ), ft <sup>3</sup> | Gas Sample Temperature at Dry Gas Meter |                                | Probe Temp. °F | Sample Box Temp. °F | Temp of Gas Leaving Last Impinger °F | Pump Vacuum in. Hg gauge |
|-----------------------|-------------------------|----------------------------------------|-----------------------------------|---------------|--------|-----------------------------------------------------------------------|---------|---------------------------------------------------------|-----------------------------------------|--------------------------------|----------------|---------------------|--------------------------------------|--------------------------|
|                       |                         |                                        |                                   | (ΔPs)         | (VAPs) | Actual                                                                | Desired |                                                         | Inlet (T <sub>min</sub> ), °F           | Outlet (T <sub>max</sub> ), °F |                |                     |                                      |                          |
| 1                     | 9:34                    | .650                                   | 234                               | 1.20          | 1.095  | .800                                                                  | .798    | 879.203                                                 | 105                                     | 97                             | 242            | 245                 | 58                                   | 3.5                      |
| 2                     | 9:38.5                  |                                        | 246                               | 1.10          | 1.048  | .720                                                                  | .719    | 881.510                                                 | 108                                     | 97                             | 242            | 245                 | 57                                   | 3.5                      |
| 3                     | 9:43                    |                                        | 251                               | 1.00          | 1.000  | .650                                                                  | .649    | 883.810                                                 | 110                                     | 98                             | 241            | 244                 | 56                                   | 3.5                      |
| 4                     | 9:47.5                  |                                        | 253                               | .940          | .9695  | .610                                                                  | .608    | 885.810                                                 | 112                                     | 99                             | 245            | 240                 | 56                                   | 3.5                      |
| 5                     | 9:52                    |                                        | 258                               | .960          | .9797  | .620                                                                  | .617    | 887.825                                                 | 114                                     | 101                            | 242            | 247                 | 56                                   | 3.5                      |
| 6                     | 9:56.5                  |                                        | 248                               | 1.05          | 1.024  | .690                                                                  | .685    | 889.820                                                 | 116                                     | 104                            | 245            | 248                 | 57                                   | 3.5                      |
| 7                     | 10:01                   |                                        | 231                               | 1.20          | 1.095  | .800                                                                  | .802    | 892.050                                                 | 117                                     | 105                            | 247            | 251                 | 56                                   | 3.5                      |
| 8                     | 10:05.5                 |                                        | 230                               | 1.10          | 1.048  | .740                                                                  | .736    | 894.350                                                 | 118                                     | 104                            | 243            | 250                 | 56                                   | 3.5                      |
| 9                     | 10:16                   |                                        | 233                               | 1.10          | 1.048  | .730                                                                  | .733    | 896.553                                                 | 118                                     | 104                            | 242            | 248                 | 57                                   | 3.5                      |
| 10                    | 10:20.5                 |                                        | 238                               | 1.20          | 1.095  | .790                                                                  | .794    | 898.875                                                 | 121                                     | 110                            | 242            | 248                 | 57                                   | 3.5                      |
| 11                    | 10:25                   |                                        | 240                               | 1.20          | 1.095  | .790                                                                  | .790    | 901.210                                                 | 119                                     | 107                            | 242            | 249                 | 58                                   | 3.5                      |
| 12                    | 10:29.5                 |                                        | 236                               | 1.05          | 1.024  | .6700                                                                 | .696    | 903.670                                                 | 121                                     | 111                            | 243            | 250                 | 58                                   | 3.5                      |
| 13                    | 10:34                   |                                        | 237                               | .900          | .948   | .600                                                                  | .596    | 905.515                                                 | 122                                     | 112                            | 242            | 253                 | 59                                   | 3.5                      |
| 14                    | 10:38.5                 |                                        | 245                               | .940          | .969   | .620                                                                  | .615    | 907.505                                                 | 119                                     | 109                            | 240            | 256                 | 60                                   | 3.5                      |
| 15                    | 10:43                   |                                        | 238                               | .960          | .979   | .640                                                                  | .635    | 909.520                                                 | 121                                     | 109                            | 242            | 255                 | 60                                   | 3.5                      |
| 16                    | 10:47.5                 |                                        | 240                               | .980          | .989   | .650                                                                  | .646    | 911.735                                                 | 120                                     | 109                            | 241            | 253                 | 60                                   | 3.5                      |
| 17                    | 10:52                   |                                        |                                   |               |        |                                                                       |         | 913.670                                                 |                                         |                                |                |                     |                                      |                          |
| 18                    | 10:56.5                 |                                        |                                   |               |        |                                                                       |         |                                                         |                                         |                                |                |                     |                                      |                          |
| AVERAGE 10 min        |                         | .650                                   | 241.125                           | 1.025         | .709   |                                                                       |         | 34.467                                                  | 110.53                                  |                                |                |                     |                                      |                          |

| LIQUID COLLECTED | IMPINGER WEIGHTS |   |   |   |      |
|------------------|------------------|---|---|---|------|
|                  | 1                | 2 | 3 | 4 | 5    |
| FINAL            |                  |   |   |   | 29.7 |
| INITIAL          |                  |   |   |   |      |
| TOTAL WEIGHT     |                  |   |   |   |      |

| ORSAT MEASUREMENT                                    |      |    |    |  |
|------------------------------------------------------|------|----|----|--|
| C02                                                  | 02   | CO | N2 |  |
| 0.1                                                  | 19.8 |    |    |  |
| Orsat leak check <input checked="" type="checkbox"/> |      |    |    |  |
| Method (3 or 3A) <u>3</u>                            |      |    |    |  |
| Barometer ID <u>1</u>                                |      |    |    |  |

## COMMENTS:

Pitot tube leak check, impact side good @ 3.5" H<sub>2</sub>O  
 Pitot tube leak check, static side good @ 4.0" H<sub>2</sub>O  
 Pre-leak Rate @ 10 in.Hg 0.001 ft<sup>3</sup>/min.  
 Post-leak Rate @ 10 in.Hg 0.002 ft<sup>3</sup>/min.

## DETERMINATION of STACK GAS MOISTURE, MOLECULAR WEIGHT, VELOCITY, and VOLUMETRIC FLOW RATE

|                   |                                                             |                |                                                   |                  |                                                     |
|-------------------|-------------------------------------------------------------|----------------|---------------------------------------------------|------------------|-----------------------------------------------------|
| A                 | - Cross-sectional area of the stack, ft <sup>2</sup>        | Pbar           | - Barometric pressure, in. Hg                     | Vi               | - Water vapor condensed, impinger 1, g              |
| Acf               | - Stack gas flow rate, actual, acfm                         | Pa             | - Stack gas static pressure, in. H <sub>2</sub> O | Vii              | - Water vapor condensed, impinger 2, g              |
| Bws               | - Stack gas moisture fraction, %/100                        | P <sub>s</sub> | - Stack gas absolute pressure, in. Hg             | Viii             | - Water vapor condensed, impinger 3, g              |
| Cp                | - Pitot tube coefficient                                    | Pstd           | - Standard absolute pressure, 29.92 in. Hg        | Viv              | - Water vapor condensed, impinger 4, g              |
| dH                | - Meter orifice pressure differential, in. H <sub>2</sub> O | Qsd            | - Stack gas volumetric flow rate, dry acfm        | Vm               | - Gas meter sample volume, dry ft <sup>3</sup>      |
| dP                | - Stack gas velocity head, in. H <sub>2</sub> O             | R              | - Ideal gas constant, 21.85                       | Vmstd            | - Gas meter sample volume, dry std. ft <sup>3</sup> |
| F1                | - Conversion factor, 13.6 in. H <sub>2</sub> O/in. Hg       | Tm             | - Meter temperature, R                            | Vs               | - Stack gas velocity, ft/sec                        |
| Kp                | - Pitot tube constant, 85.49                                | Ts             | - Stack gas temperature, R                        | Vw               | - Total water vapor condensed, ft <sup>3</sup>      |
| MCO <sub>2</sub>  | - Molecular weight of CO <sub>2</sub> , 44.01 lb/lb mole    | Tstd           | - Standard temperature, 528 R                     | Y                | - Dry gas meter calibration factor                  |
| Md                | - Stack gas molecular weight, dry lb/lb mole                |                |                                                   | %CO <sub>2</sub> | - Stack gas CO concentration, %/100                 |
| MH <sub>2</sub> O | - Molecular weight of water, 18.02 lb/lb mole               |                |                                                   | %N <sub>2</sub>  | - Stack gas N <sub>2</sub> concentration, %/100     |
| MN <sub>2</sub>   | - Molecular weight of N <sub>2</sub> , 28.01 lb/lb mole     |                |                                                   | O <sub>2</sub>   | - Stack gas O <sub>2</sub> concentration, %/100     |
| MO <sub>2</sub>   | - Molecular weight of O <sub>2</sub> , 32.00 lb/lb mole     |                |                                                   |                  |                                                     |
|                   | - Stack gas molecular weight, wet lb/lb mole                |                |                                                   |                  |                                                     |

$$V_w = \left\{ \frac{(V_i + V_{ii} + V_{iii} + V_{iv}) R T_{std}}{(453.6 \text{ g/lb.}) P_{std} M_{H_2O}} \right\} = \left\{ \frac{(23.9 + 1.1 + -2.9 + 7.6)(21.85)(528)}{(453.6)(29.92)(18.02)} \right\} = 1.40105$$

$$V_{mstd} = V_m Y \left\{ \frac{(P_b - dH/F1) T_{std}}{P_{std} T_m} \right\} = (34.467)(1.0309) \left\{ \frac{(29.950 + .6969/13.6)(528)}{(29.92)(571)} \right\} = 32.97250$$

$$B_{ws} = \left\{ \frac{V_w}{V_w + V_{mstd}} \right\} = \left\{ \frac{(1.40105)}{(1.40105 + 32.97250)} \right\} = .0408$$

$$M_d = (M_{CO_2})(\%CO_2) + (M_{O_2})(\%O_2) + (M_{N_2})(\%N_2) \\ = (44.01)(.001) + (32.00)(.198) + (28.01)(.801) = 28.816$$

$$M_s = M_d(1 - B_{ws}) + (M_{H_2O} B_{ws}) = (28.816)(1 - .0408) + (18.02)(.0408) = 28.376$$

$$V_s = K_p C_p (dP)^{1/2} \left\{ \frac{T_s}{P_s M_s} \right\}^{1/2} = (85.49)(.8320)(1.0259) \left\{ \frac{(701)}{(29.902)(28.376)} \right\}^{1/2} = 66.3327$$

$$Acf = (60 \text{ sec/min})(V_s A) = (60)(66.3327)(52.3817) = 208476.9$$

$$Q_{sd} = (3600 \text{ sec/hr})(1 - B_{ws})(V_s A) \left\{ \frac{T_{std} P_s}{T_s P_{std}} \right\} \\ = (3600)(1 - .0408)(66.3327)(52.3817) \left\{ \frac{(528)(29.902)}{(701)(29.92)} \right\} = \begin{matrix} 9030603.0 \text{ dscf/hr} \\ 150510.0 \text{ dscf/min} \end{matrix}$$

# ETS

## EMISSION TESTING SERVICES, INC., FIELD DATA, METHOD(S) 1-4+29

PLANT: Bryan Steel SAMPLE BOX NO.: 8 A1 PITOT TUBE ID.: P-10-5 STACK DIAMETER, in.: 98"  
 DATE: 7-23-04 METER BOX NO.: 3 PITOT TUBE FACTOR: .832 METER A HQ: 1-8127  
 LOCATION: Verco, La. BAROMETRIC PRESSURE: 29.95 FILTER ID.: 1-0309 METER D.G.M.F.: 1-0309  
 STACK ID.: Bayou Steel Stack AMBIENT TEMP.: 91°F FILTER TYPE: NOZZLE DIAMETER, IN.: .170 K-FACTOR: .6750  
 RUN NO.: 3 OPERATOR: Joel Richard T-FACTOR: 473.27

| Traverse Point Number | Sampling Time (h), min. | Static Pressure (in. H <sub>2</sub> O) | Stack Temp. (T <sub>s</sub> ), °F | Velocity Head |                    | Pressure Differential Across Orifice Meter (ΔH) in. H <sub>2</sub> O |         | Dry Gas Meter Volume (V <sub>m</sub> ), ft <sup>3</sup> | Gas Sample Temperature at Dry Gas Meter |                                | Probe Temp. °F | Sample Box Temp. °F | Temp of Gas Leaving Last Impinger °F | Pump Vacuum in. Hg gauge |
|-----------------------|-------------------------|----------------------------------------|-----------------------------------|---------------|--------------------|----------------------------------------------------------------------|---------|---------------------------------------------------------|-----------------------------------------|--------------------------------|----------------|---------------------|--------------------------------------|--------------------------|
|                       |                         |                                        |                                   | (ΔPs) (APs)   | (ΔP <sub>g</sub> ) | Actual                                                               | Desired |                                                         | Inlet (T <sub>in</sub> ), °F            | Outlet (T <sub>out</sub> ), °F |                |                     |                                      |                          |
| 1                     | 11:58                   | -640                                   | 233                               | 1.30          | 1.14               | .890                                                                 | .887    | 919.715                                                 | 111                                     | 104                            | 243            | 245                 | 55                                   | 3.0                      |
| 2                     | 12:02.5                 |                                        | 243                               | 1.05          | 1.02               | .710                                                                 | .706    | 921.950                                                 | 115                                     | 103                            | 240            | 248                 | 55                                   | 3.5                      |
| 3                     | 12:07                   |                                        | 240                               | .980          | .989               | .660                                                                 | .647    | 924.350                                                 | 117                                     | 105                            | 241            | 250                 | 55                                   | 3.5                      |
| 4                     | 12:10.5                 |                                        | 243                               | .960          | .979               | .650                                                                 | .647    | 926.430                                                 | 117                                     | 106                            | 245            | 251                 | 55                                   | 3.5                      |
| 5                     | 12:16                   |                                        | 246                               | 1.05          | 1.024              | .700                                                                 | .703    | 928.470                                                 | 116                                     | 106                            | 242            | 253                 | 56                                   | 3.5                      |
| 6                     | 12:20.5                 |                                        | 243                               | 1.00          | 1.000              | .670                                                                 | .673    | 930.680                                                 | 117                                     | 106                            | 242            | 252                 | 56                                   | 3.5                      |
| 7                     | 12:25                   |                                        | 242                               | .970          | .984               | .650                                                                 | .653    | 932.748                                                 | 117                                     | 107                            | 243            | 250                 | 56                                   | 3.0                      |
| 8                     | 12:29.5                 |                                        | 247                               | .990          | .994               | .600                                                                 | .662    | 934.875                                                 | 118                                     | 107                            | 244            | 249                 | 56                                   | 3.0                      |
| 9                     | 12:34                   |                                        |                                   |               |                    |                                                                      |         | 936.960                                                 |                                         |                                |                |                     |                                      |                          |
| 10                    | 12:38                   |                                        | 241                               | 1.25          | 1.118              | .840                                                                 | .843    | 936.960                                                 | 118                                     | 107                            | 242            | 250                 | 57                                   | 3.0                      |
| 11                    | 12:42.5                 |                                        | 243                               | 1.20          | 1.095              | .810                                                                 | .807    | 939.330                                                 | 118                                     | 107                            | 240            | 247                 | 57                                   | 3.5                      |
| 12                    | 12:47                   |                                        | 231                               | 1.15          | 1.072              | .790                                                                 | .787    | 941.810                                                 | 121                                     | 109                            | 241            | 248                 | 57                                   | 3.5                      |
| 13                    | 12:51.5                 |                                        | 235                               | 1.10          | 1.048              | .750                                                                 | .749    | 944.020                                                 | 121                                     | 109                            | 243            | 252                 | 58                                   | 3.5                      |
| 14                    | 12:56                   |                                        | 243                               | 1.05          | 1.024              | .710                                                                 | .707    | 946.250                                                 | 122                                     | 110                            | 242            | 251                 | 58                                   | 3.5                      |
| 15                    | 13:00.5                 |                                        | 240                               | .980          | .989               | .660                                                                 | .662    | 948.460                                                 | 122                                     | 110                            | 240            | 250                 | 59                                   | 3.5                      |
| 16                    | 13:05                   |                                        | 239                               | .960          | 1.00               | .680                                                                 | .677    | 949.610                                                 | 123                                     | 111                            | 239            | 251                 | 59                                   | 3.0                      |
| 17                    | 13:09.5                 |                                        | 241                               | .990          | .994               | .670                                                                 | .668    | 952.680                                                 | 123                                     | 113                            | 240            | 252                 | 59                                   | 3.0                      |
| 18                    | 13:14                   |                                        |                                   |               |                    |                                                                      |         | 954.865                                                 |                                         |                                |                |                     |                                      |                          |
| AVERAGE               | 12 min                  | -1440                                  | 240.5                             |               | 1.029              | .718                                                                 |         | 350.150                                                 |                                         | 112.96                         |                |                     |                                      |                          |

| IMPINGER WEIGHTS |   |   |   |   |
|------------------|---|---|---|---|
| LIQUID COLLECTED | 1 | 2 | 3 | 4 |
| FINAL            |   |   |   |   |
| INITIAL          |   |   |   |   |
| TOTAL WEIGHT     |   |   |   |   |

| ORSAT MEASUREMENT                                    |                |    |                |
|------------------------------------------------------|----------------|----|----------------|
| CO <sub>2</sub>                                      | O <sub>2</sub> | CO | N <sub>2</sub> |
| 0.2                                                  | 19.8           |    |                |
| Orsat leak check <input checked="" type="checkbox"/> |                |    |                |
| Method (3 or 3A) <u>3</u>                            |                |    |                |
| Barometer ID <u>1</u>                                |                |    |                |

COMMENTS:

Pilot tube leak check, impact side good 4.0" H<sub>2</sub>O  
 Pilot tube leak check, static side good 0.3.5" H<sub>2</sub>O  
 Pre-leak Rate @ 10 in.Hg 0.00 ft<sup>3</sup>/min.  
 Post-leak Rate @ 10 in.Hg 0.00 ft<sup>3</sup>/min.

## DETERMINATION of STACK GAS MOISTURE, MOLECULAR WEIGHT, VELOCITY, and VOLUMETRIC FLOW RATE

|                   |                                                             |      |                                                   |                  |                                                     |
|-------------------|-------------------------------------------------------------|------|---------------------------------------------------|------------------|-----------------------------------------------------|
| A                 | - Cross-sectional area of the stack, ft <sup>2</sup>        | Pbar | - Barometric pressure, in. Hg                     | Vi               | - Water vapor condensed, impinger 1, g              |
| Acf               | - Stack gas flow rate, actual, acfm                         | Pa   | - Stack gas static pressure, in. H <sub>2</sub> O | Vii              | - Water vapor condensed, impinger 2, g              |
| Bws               | - Stack gas moisture fraction, %/100                        | Ps   | - Stack gas absolute pressure, in. Hg             | Viii             | - Water vapor condensed, impinger 3, g              |
| Cp                | - Pitot tube coefficient                                    | Pstd | - Standard absolute pressure, 29.92 in. Hg        | Viv              | - Water vapor condensed, impinger 4, g              |
| dH                | - Meter orifice pressure differential, in. H <sub>2</sub> O | Qad  | - Stack gas volumetric flow rate, dry acfm        | Vm               | - Gas meter sample volume, dry ft <sup>3</sup>      |
| dP                | - Stack gas velocity based, in. H <sub>2</sub> O            | R    | - Ideal gas constant, 21.85                       | Vmstd            | - Gas meter sample volume, dry std. ft <sup>3</sup> |
| F1                | - Conversion factor, 13.6 in. H <sub>2</sub> O/in. Hg       | Tm   | - Meter temperature, R                            | Vs               | - Stack gas velocity, ft/sec                        |
| Kp                | - Pitot tube constant, 85.49                                | Ts   | - Stack gas temperature, R                        | Vw               | - Total water vapor condensed, ft <sup>3</sup>      |
| MCO <sub>2</sub>  | - Molecular weight of CO <sub>2</sub> , 44.01 lb/lb mole    | Tstd | - Standard temperature, 528 R                     | Y                | - Dry gas meter calibration factor                  |
| Md                | - Stack gas molecular weight, dry lb/lb mole                |      |                                                   | %CO <sub>2</sub> | - Stack gas CO concentration, %/100                 |
| MH <sub>2</sub> O | - Molecular weight of water, 18.02 lb/lb mole               |      |                                                   | %N <sub>2</sub>  | - Stack gas N <sub>2</sub> concentration, %/100     |
| MN <sub>2</sub>   | - Molecular weight of N <sub>2</sub> , 28.01 lb/lb mole     |      |                                                   | O <sub>2</sub>   | - Stack gas O <sub>2</sub> concentration, %/100     |
| MO <sub>2</sub>   | - Molecular weight of O <sub>2</sub> , 32.00 lb/lb mole     |      |                                                   |                  |                                                     |
| Ms                | - Stack gas molecular weight, wet lb/lb mole                |      |                                                   |                  |                                                     |

$$Vw = \left\{ \frac{(Vi + Vii + Viii + Viv) R Tstd}{(453.6 \text{ g/lb}) Pstd MH_2O} \right\} = \left\{ \frac{(19.4 + 1.9 + -3.7 + 4.7)(21.85)(528)}{(453.6)(29.92)(18.02)} \right\} = 1.05196$$

$$Vmstd = Vm Y \left\{ \frac{(Pb + dH F1) Tstd}{Pstd Tm} \right\} = (35.150)(1.0309) \left\{ \frac{(29.950 + .7188/13.6)(528)}{(29.92)(573)} \right\} = 33.48461$$

$$Bws = \left\{ \frac{Vw}{Vw + Vmstd} \right\} = \left\{ \frac{(1.05196)}{(1.05196 + 33.48461)} \right\} = .0305$$

$$Md = (MCO_2)(\%CO_2) + (MO_2)(\%O_2) + (MN_2)(\%N_2) \\ = (44.01)(.002) + (32.00)(.198) + (28.01)(.800) = 28.832$$

$$Ms = Md(1 - Bws) + (MH_2O Bws) = (28.832)(1 - .0305) + (18.02)(.0305) = 28.503$$

$$Vs = Kp Cp (dP)^{1/2} \left\{ \frac{Ts}{Ps Ms} \right\}^{1/2} = (85.49)(.8320)(1.0302) \left\{ \frac{(701)}{(29.903)(28.503)} \right\}^{1/2} = 66.4312$$

$$Acf = (60 \text{ sec/min})(Vs A) = (60)(66.4312)(52.3817) = 208786.4$$

$$Qsd = (3600 \text{ sec/hr})(1 - Bws)(Vs A) \left\{ \frac{Tstd Ps}{Ts Pstd} \right\} \\ = (3600)(1 - .0305)(66.4312)(52.3817) \left\{ \frac{(528)(29.903)}{(701)(29.92)} \right\} = 9149506.0 \text{ dscf/hr} \\ = 152491.8 \text{ dscf/min}$$

# ETS EMISSION TESTING SERVICES, INC., FIELD DATA, METHOD(S) 1-4 + 29

PLANT: B Steel SAMPLE BOX NO.: X A1<sup>st</sup> PITOT TUBE ID.: P-10-5 STACK DIAMETER, in.: 98"  
 DATE: 7-23-64 METER BOX NO.: 3 PITOT TUBE FACTOR: .832 METER A H@: 1.8127  
 LOCATION: Norco, La. BAROMETRIC PRESSURE: 24.95 FILTER ID.: METER D.G.M.F.: 1.0309  
 STACK ID.: Baghouse Stack AMBIENT TEMP.: 90°F FILTER TYPE: K-FACTOR: 6750  
 RUN NO.: 3 OPERATOR: Joel R. Harsh NOZZLE DIAMETER, IN: .17 T-FACTOR: 473.27

| Traverse Point Number | Sampling Time (t), min. | Static Pressure (in. H <sub>2</sub> O) | Stack Temp. (T <sub>s</sub> ), °F | Velocity Head       |                     | Pressure Differential Across Orifice Meter (ΔH) in., H <sub>2</sub> O |         | Dry Gas Meter Volume (V <sub>m</sub> ), ft <sup>3</sup> | Gas Sample Temperature at Dry Gas Meter  |                                            | Probe Temp. °F | Sample Box Temp. °F | Temp of Gas Leaving Last Impinger °F | Pump Vacuum in. Hg gauge |
|-----------------------|-------------------------|----------------------------------------|-----------------------------------|---------------------|---------------------|-----------------------------------------------------------------------|---------|---------------------------------------------------------|------------------------------------------|--------------------------------------------|----------------|---------------------|--------------------------------------|--------------------------|
|                       |                         |                                        |                                   | (VAP <sub>s</sub> ) | (VAP <sub>s</sub> ) | Actual                                                                | Desired |                                                         | Inlet (T <sub>m<sub>in</sub></sub> ), °F | Outlet (T <sub>m<sub>out</sub></sub> ), °F |                |                     |                                      |                          |
| one 1                 | 16:05                   | -650                                   | 240                               | 1.40                | 1.18                | .950                                                                  | .946    | 973.448                                                 | 97                                       | 88                                         | 243            | 253                 | 53                                   | 3.0                      |
| 2                     | 16:09.5                 |                                        | 238                               | 1.30                | 1.14                | .880                                                                  | .881    | 975.890                                                 | 100                                      | 88                                         | 242            | 252                 | 53                                   | 3.5                      |
| 3                     | 16:14                   |                                        | 235                               | 1.10                | 1.04                | .750                                                                  | .749    | 978.285                                                 | 102                                      | 88                                         | 240            | 251                 | 54                                   | 3.0                      |
| 4                     | 16:18.5                 |                                        | 238                               | 1.05                | 1.02                | .710                                                                  | .711    | 980.600                                                 | 102                                      | 88                                         | 245            | 250                 | 54                                   | 3.5                      |
| 5                     | 16:23                   |                                        | 240                               | 1.10                | 1.04                | .740                                                                  | .743    | 982.785                                                 | 102                                      | 90                                         | 247            | 249                 | 54                                   | 3.5                      |
| 6                     | 16:27.5                 |                                        | 241                               | 1.10                | 1.04                | .740                                                                  | .743    | 984.915                                                 | 104                                      | 90                                         | 242            | 250                 | 55                                   | 3.0                      |
| 7                     | 16:32                   |                                        | 240                               | 1.00                | 1.00                | .680                                                                  | .676    | 987.150                                                 | 107                                      | 92                                         | 241            | 252                 | 55                                   | 3.0                      |
| 8                     | 16:36.5                 |                                        | 237                               | 1.05                | 1.02                | .710                                                                  | .712    | 989.350                                                 | 108                                      | 92                                         | 240            | 257                 | 56                                   | 3.0                      |
| inlet                 | 16:41                   |                                        |                                   |                     |                     |                                                                       |         | 991.476                                                 |                                          |                                            |                |                     |                                      |                          |
| 9                     | 16:47                   |                                        | 238                               | 1.20                | 1.09                | .810                                                                  | .813    | 991.476                                                 | 99                                       | 91                                         | 239            | 256                 | 56                                   | 3.0                      |
| 10                    | 16:51.5                 |                                        | 240                               | 1.10                | 1.04                | .740                                                                  | .743    | 993.770                                                 | 103                                      | 93                                         | 240            | 253                 | 57                                   | 3.5                      |
| 11                    | 16:56                   |                                        | 242                               | 1.10                | 1.04                | .740                                                                  | .743    | 996.000                                                 | 104                                      | 92                                         | 242            | 254                 | 57                                   | 3.0                      |
| 12                    | 17:00.5                 |                                        | 241                               | 1.00                | 1.00                | .680                                                                  | .675    | 998.240                                                 | 106                                      | 92                                         | 241            | 252                 | 58                                   | 3.0                      |
| 13                    | 17:05                   |                                        | 247                               | 1.05                | 1.02                | .700                                                                  | .702    | 1000.330                                                | 106                                      | 93                                         | 243            | 251                 | 59                                   | 3.0                      |
| 14                    | 17:09.5                 |                                        | 243                               | 1.00                | 1.00                | .670                                                                  | .673    | 1002.490                                                | 108                                      | 93                                         | 242            | 250                 | 60                                   | 3.0                      |
| 15                    | 17:14                   |                                        | 240                               | .970                | .984                | .660                                                                  | .655    | 1004.610                                                | 110                                      | 93                                         | 241            | 250                 | 60                                   | 3.0                      |
| 16                    | 17:18.5                 |                                        | 241                               | .960                | .979                | .650                                                                  | .648    | 1006.565                                                | 110                                      | 94                                         | 240            | 252                 | 60                                   | 3.0                      |
| 17                    | 17:23                   |                                        |                                   |                     |                     |                                                                       |         | 1008.673                                                |                                          |                                            |                |                     |                                      |                          |
| AVERAGE               | 12 min                  | -650                                   | 240.06                            | 1.039               | .738                |                                                                       |         | 35.225                                                  |                                          | 92.03                                      |                |                     |                                      |                          |

| LIQUID COLLECTED | IMPINGER WEIGHTS |   |   |   |      |
|------------------|------------------|---|---|---|------|
|                  | 1                | 2 | 3 | 4 | 5    |
| FINAL            |                  |   |   |   | 35.6 |
| INITIAL          |                  |   |   |   |      |
| TOTAL WEIGHT     |                  |   |   |   |      |

| ORSAT MEASUREMENT         |                |    |                |
|---------------------------|----------------|----|----------------|
| CO <sub>2</sub>           | O <sub>2</sub> | CO | N <sub>2</sub> |
| 0.2                       | 19.2           |    |                |
| Orsat leak check          |                |    |                |
| Method (3 or 3A) <u>3</u> |                |    |                |
| Barometer ID <u>1</u>     |                |    |                |

## COMMENTS:

Pitot tube leak check, impact side good @ 4.0" 14.0  
 Pitot tube leak check, static side good @ 4.5" 17.0  
 Pre-leak Rate @ 10' in. Hg 0.002 ft<sup>3</sup>/min.  
 Post-leak Rate @ 10' in. Hg 0.001 ft<sup>3</sup>/min.

# ETS

Emission Testing Services, Inc.

Client : BAYOU STEEL  
Source : BAGHOUSE STACK  
Test Date : 7-23-04  
Run No. : 3

## DETERMINATION of STACK GAS MOISTURE, MOLECULAR WEIGHT, VELOCITY, and VOLUMETRIC FLOW RATE

|                   |                                                             |      |                                                   |                  |                                                     |
|-------------------|-------------------------------------------------------------|------|---------------------------------------------------|------------------|-----------------------------------------------------|
| A                 | - Cross-sectional area of the stack, ft <sup>2</sup>        | Pbar | - Barometric pressure, in. Hg                     | Vi               | - Water vapor condensed, impinger 1, g              |
| Acf               | - Stack gas flow rate, actual, acfm                         | Pa   | - Stack gas static pressure, in. H <sub>2</sub> O | Vii              | - Water vapor condensed, impinger 2, g              |
| Bwr               | - Stack gas moisture fraction, %/100                        | Ps   | - Stack gas absolute pressure, in. Hg             | Viii             | - Water vapor condensed, impinger 3, g              |
| Cp                | - Pitot tube coefficient                                    | Pstd | - Standard absolute pressure, 29.92 in. Hg        | Viv              | - Water vapor condensed, impinger 4, g              |
| dH                | - Meter orifice pressure differential, in. H <sub>2</sub> O | Qsd  | - Stack gas volumetric flow rate, dry scfm        | Vm               | - Gas meter sample volume, dry ft <sup>3</sup>      |
| dP                | - Stack gas velocity head, in. H <sub>2</sub> O             | R    | - Ideal gas constant, 21.85                       | Vmstd            | - Gas meter sample volume, dry std, ft <sup>3</sup> |
| F1                | - Conversion factor, 13.6 in. H <sub>2</sub> O/ in. Hg      | Tm   | - Meter temperature, R                            | Vs               | - Stack gas velocity, ft/sec                        |
| Kp                | - P i i tube constant, 85.49                                | Ts   | - Stack gas temperature, R                        | Vw               | - Total water vapor condensed, ft <sup>3</sup>      |
| MCO <sub>2</sub>  | - Molecular weight of CO <sub>2</sub> , 44.01 lb/ lb mole   | Tstd | - Standard temperature, 528 R                     | Y                | - Dry gas meter calibration factor                  |
| Md                | - Stack gas molecular weight, dry lb/ lb mole               |      |                                                   | %CO <sub>2</sub> | - Stack gas CO concentration, %/100                 |
| MH <sub>2</sub> O | - Molecular weight of water, 18.02 lb/ lb mole              |      |                                                   | %N <sub>2</sub>  | - Stack gas N <sub>2</sub> concentration, %/100     |
| MN <sub>2</sub>   | - Molecular weight of N <sub>2</sub> , 28.01 lb/ lb mole    |      |                                                   | O <sub>2</sub>   | - Stack gas O <sub>2</sub> concentration, %/100     |
| MO <sub>2</sub>   | - Molecular weight of O <sub>2</sub> , 32.00 lb/ lb mole    |      |                                                   |                  |                                                     |
| Ms                | - Stack gas molecular weight, wet lb/ lb mole               |      |                                                   |                  |                                                     |

$$Vw = \left\{ \frac{(Vi + Vii + Viii + Viv) R Tstd}{(453.6 \text{ g/lb}) Pstd MH_2O} \right\} = \left\{ \frac{(31.1 + .8 + .0 + 3.7)(21.85)(528)}{(453.6)(29.92)(18.02)} \right\} = 1.67937$$

$$Vmstd = Vm Y \left\{ \frac{(Pb + dH/ F1) Tstd}{Pstd Tm} \right\} = (35.225)(1.0309) \left\{ \frac{(29.950 + .7381/13.6)(528)}{(29.92)(558)} \right\} = 34.47911$$

$$Bws = \left\{ \frac{Vw}{Vw + Vmstd} \right\} = \left\{ \frac{(1.67937)}{(1.67937 + 34.47911)} \right\} = .0464$$

$$Md = (MCO_2)(\%CO_2) + (MO_2)(\%O_2) + (MN_2)(\%N_2) \\ = (44.01)(.002) + (32.00)(.192) + (28.01)(.806) = 28.808$$

$$Ms = Md(1 - Bws) + (MH_2O Bws) = (28.808)(1 - .0464) + (18.02)(.0464) = 28.307$$

$$Vs = Kp Cp (dP)^{1/2} \left\{ \frac{Ts}{Ps Ms} \right\}^{1/2} = (85.49)(.8320)(1.0439) \left\{ \frac{(700)}{(29.902)(28.307)} \right\}^{1/2} = 67.5224$$

$$Acf = (60 \text{ sec/min})(Vs A) = (60)(67.5224)(52.3817) = 212216.0$$

$$Qsd = (3600 \text{ sec/hr})(1 - Bws)(Vs A) \left\{ \frac{Tstd Ps}{Ts Pstd} \right\} \\ = (3600)(1 - .0464)(67.5224)(52.3817) \left\{ \frac{(528)(29.902)}{(700)(29.92)} \right\} = 9151957.0 \text{ dscf/hr} \\ 152532.6 \text{ dscf/min}$$

## **METALS EMISSIONS per EPA METHOD 29**

During emission tests for the metals, lead and mercury samples were collected in sampling train combined with the moisture and flow rate sample train. Sample volume, etc, are recorded on test data sheets presented beginning on page 6.1.5.

A summary of the metals sample collection data and the emission concentration and emission rate calculations are presented on the following pages.

## METALS EMISSIONS per EPA METHOD 29

|      |                                                           |       |                                                           |
|------|-----------------------------------------------------------|-------|-----------------------------------------------------------|
| An   | • Cross-sectional area of sampler nozzle, ft <sup>2</sup> | St    | • Total sampling time, min                                |
| Bws  | • Stack gas moisture fraction, %/100                      | Tm    | • Average dry gas meter temperature, deg R                |
| Csi  | • Conc. of metals emissions, ug/dscf                      | Ts    | • Stack gas temperature, deg R                            |
| dH   | • Dry gas meter orifice press. diff., in-H <sub>2</sub> O | Tstd  | • Std. absolute temp, EPA, 528 R                          |
| Eri  | • Emission rate of metals emissions, lb/hr                | Vm    | • Volume of gas sample, actual dry ft <sup>3</sup>        |
| F1   | • Conversion factor, 2.2046 X 10 <sup>-9</sup> lb/ug      | Vmstd | • Sample vol, dry, std ft <sup>3</sup> , 68F, 29.92 in.Hg |
| I    | • Percent isokinetic, % of ideal sampling rate            |       |                                                           |
| Msi  | • Mass of metal detected in sample, ug                    | Vs    | • Stack gas velocity, ft/sec                              |
| Pbar | • Barometric press. at sampling site, in. Hg              | Y     | • Dry gas meter calibration factor                        |
| Ps   | • Stack gas pressure, absolute, in. Hg                    |       |                                                           |
| Pstd | • Standard absolute press., 29.92 in. Hg                  |       |                                                           |
| Qsd  | • Stack gas volumetric flow rate, dry ft <sup>3</sup> /hr |       |                                                           |

$$Vmstd = Vm Y \left\{ \frac{(Tstd)(Pbar + dH/13.6)}{(Tm)(Pstd)} \right\} = (34.467)(1.0309) \left\{ \frac{(528)(29.950 + .6969/13.6)}{(571)(29.92)} \right\} = 32.97250$$

$$I = \left\{ \frac{Ts Vmstd Pstd (100)}{Tstd Vs An St Ps (60)(1 - Bws)} \right\} = \left\{ \frac{(701)(32.97250)(29.92)(100)}{(528)(66.3327)(.00015762)(72.00)(29.902) 60 (1 - .0408)} \right\} = 101.11$$

----- LEAD -----

$$Csi = (Msi / Vmstd) = (321.00 / 32.97250) = 9.7354$$

$$Eri = (Msi F1 Qsd) / (Vmstd) = [(321.00)(2.2046 \times 10^{-9})(9030603.0)] / (32.97250) = 1.19382$$

----- MERCURY -----

$$Csi = (Msi / Vmstd) = (2.21 / 32.97250) = 0.0670$$

$$Eri = (Msi F1 Qsd) / (Vmstd) = [(2.21)(2.2046 \times 10^{-9})(9030603.0)] / (32.97250) = 0.00133$$

# ETS

Emission Testing Services, Inc.

Client : BAYOU STEEL  
Source : BAGHOUSE STACK  
Test Date : 7-23-04  
Run NO. : 2

## METALS EMISSIONS per EPA METHOD 29

|      |                                                           |       |                                                           |
|------|-----------------------------------------------------------|-------|-----------------------------------------------------------|
| An   | - Cross-sectional area of sampler nozzle, ft <sup>2</sup> | St    | - Total sampling time, min                                |
| Bus  | - Stack gas moisture fraction, %/100                      | Tm    | - Average dry gas meter temperature, deg R                |
| Csl  | - Conc. of metals emissions, ug/dscf                      | Ts    | - Stack gas temperature, deg R                            |
| dH   | - Dry gas meter orifice press. diff., in-H <sub>2</sub> O | Tstd  | - Std. absolute temp, EPA 528 R                           |
| Erf  | - Emission rate of metals emissions, lb/hr                | Vm    | - Volume of gas sample, actual dry ft <sup>3</sup>        |
| F1   | - Conversion factor, 2.2046 X 10 <sup>-9</sup> lb/ug      | Vmstd | - Sample vol, dry, std ft <sup>3</sup> , 68F, 29.92 in.Hg |
| I    | - Percent isokinetic, % of ideal sampling rate            |       |                                                           |
| Msi  | - Mass of metal detected in sample, ug                    | Vs    | - Stack gas velocity, ft/sec                              |
| Pbar | - Barometric press. at sampling site, in. Hg              | Y     | - Dry gas meter calibration factor                        |
| Ps   | - Stack gas pressure, absolute, in. Hg                    |       |                                                           |
| Pstd | - Standard absolute press., 29.92 in. Hg                  |       |                                                           |
| Qsd  | - Stack gas volumetric flow rate, dry ft <sup>3</sup> /hr |       |                                                           |

$$Vmstd = Vm Y \left\{ \frac{(Tstd)(Pbar + dH/13.6)}{(Tm)(Pstd)} \right\} = (35.150)(1.0309) \left\{ \frac{(528)(29.950 + .7188/13.6)}{(573)(29.92)} \right\} = 33.48462$$

$$\left\{ \frac{Ts Vmstd Pstd (100)}{Tstd Vs An St Ps (60)(1 - Bus)} \right\} = \left\{ \frac{(701)(33.48462)(29.92)(100)}{(528)(66.4312)(.00015762)(72.00)(29.903) 60 (1 - .0305)} \right\} = 101.35$$

### ----- LEAD -----

$$Csl = (Msi / Vmstd) = (357.00 / 33.48462) = 10.6616$$

$$Erf = (Msi F1 Qsd) / (Vmstd) = [(357.00)(2.2046 \times 10^{-9})(9149506.0)] / (33.48462) = 2.21506$$

### ----- MERCURY -----

$$Csl = (Msi / Vmstd) = (2.33 / 33.48462) = .0696$$

$$Erf = (Msi F1 Qsd) / (Vmstd) = [(2.33)(2.2046 \times 10^{-9})(9149506.0)] / (33.48462) = .00140$$

# ETS

Emission Testing Services, Inc.

Client : BAYOU STEEL  
Source : BAGHOUSE STACK  
Test Date : 7-23-04  
Run No. : 3

## METALS EMISSIONS per EPA METHOD 29

An - Cross-sectional area of sampler nozzle, ft<sup>2</sup>  
Bws - Stack gas moisture fraction, %/100  
Csi - Conc. of metals emissions, ug/dscf  
dH - Dry gas meter orifice press. diff., in-H<sub>2</sub>O  
Eri - Emission rate of metals emissions, lb/hr  
F1 - Conversion factor, 2.2046 x 10<sup>-9</sup> lb/ug  
I - Percent isokinetic, % of ideal sampling rate  
Msi - Mass of metal detected in sample, ug  
Pbar - Barometric press. at sampling site, in. Hg  
Ps - Stack gas pressure, absolute, in. Hg  
Pstd - Standard absolute press., 29.92 in. Hg  
Qsd - Stack gas volumetric flow rate, dry ft<sup>3</sup>/hr  
St - Total sampling time, min  
Tm - Average dry gas meter temperature, deg R  
Ts - Stack gas temperature, deg R  
Tstd - Std. absolute temp, EPA, 528 R  
Vm - Volume of gas sample, actual dr. ft<sup>3</sup>  
Vmstd - Sample vol, dry, std ft<sup>3</sup>, 68F, 39.92 in.Hg  
Vs - Stack gas velocity, ft/sec  
Y - Dry gas meter calibration factor

$$Vmstd = Vm Y \left\{ \frac{(Tstd)(Pbar + dH/13.6)}{(Tm)(Pstd)} \right\} = (35.225)(1.0309) \left\{ \frac{(528)(29.950 + .7381/13.6)}{(558)(29.92)} \right\} = 34.47912$$

$$I = \left\{ \frac{Ts Vmstd Pstd (100)}{Tstd Vs An St Ps (60)(1-BUS)} \right\} = \left\{ \frac{(700)(34.47912)(29.92)(100)}{(528)(67.5224)(.00015762)(72.00)(29.902) 60 (1 - .0464)} \right\} = 104.33$$

### ----- LEAD -----

$$Csi = (Msi / Vmstd) = ( .363.00 / 34.47912 ) = .10.5281$$

$$Eri = (Msi F1 Qsd) / (Vmstd) = [( .363.00 )(2.2046 \times 10^{-9})( 9151957.0 )] / ( 34.47912 ) = .21242$$

### ----- MERCURY -----

$$Csi = (Msi / Vmstd) = ( .6.58 / 34.47912 ) = .1908$$

$$Eri = (Msi F1 Qsd) / (Vmstd) = [( .6.58 )(2.2046 \times 10^{-9})( 9151957.0 )] / ( 32.97250 ) = .00403$$

## **LABORATORY ANALYSES of METALS SAMPLES**

During the emission tests, metals samples were collected in the probe wash, filter, and impinger samples. These samples were transported to Chemtex Environmental and Industrial Hygiene Services located in Port Arthur, Texas for analyses. A summary of analytical **results** are presented on the following page followed by the complete analytical report.

Chemtex Environmental and Industrial **Hygiene** Services is certified by the Louisiana Department of Environmental **Quality (LDEQ)** as a qualified environmental testing laboratory under the Louisiana Environmental Laboratory Accreditation Program (LELAP).

# ETS

Emission Testing Services, Inc.

## Metals Analysis per EPA Method 29

Analytical Laboratory : Chemtex Environmental & Industrial Hygiene Services

Client Name : Bayou Steel  
Source Name : Baghouse Stack  
Run No. : 1

| HNO3 PROBEWASH             |              |                     |              |                     |                                        | IMPINGERS 1 & 2 HNO3/H2O2 |                     |                    |                     |                                        |
|----------------------------|--------------|---------------------|--------------|---------------------|----------------------------------------|---------------------------|---------------------|--------------------|---------------------|----------------------------------------|
| SAMPLE ID                  | SAMPLE       |                     | BLANK        |                     | SAMPLE<br>Blank Corrected<br>ug/sample | SAMPLE                    |                     | BLANK              |                     | SAMPLE<br>Blank Corrected<br>ug/sample |
|                            | VOLUME<br>ml | RESULT<br>mg/sample | VOLUME<br>ml | RESULT<br>mg/sample |                                        | VOLUME<br>ml              | RESULT<br>mg/sample | VOLUME<br>ml       | RESULT<br>mg/sample |                                        |
| Lead                       | 170.00       | 0.172000            | 210.000      | < 0.011000          | 172.000                                | 274.00                    | < 0.014000          | 102.000            | < 0.005000          | < 14.000                               |
| Mercury                    | 170.00       | 0.000187            | 210.000      | < 0.000210          | 0.187                                  | 274.00                    | < 0.000270          | 102.000            | < 0.000100          | < 0.270                                |
| IMPINGER 3, HNO3           |              |                     |              |                     |                                        | IMPINGERS 4 & 5, KMnO4    |                     |                    |                     |                                        |
| SAMPLE ID                  | SAMPLE       |                     | BLANK        |                     | SAMPLE<br>Blank Corrected<br>ug/sample | SAMPLE                    |                     | BLANK              |                     | SAMPLE<br>Blank Corrected<br>ug/sample |
|                            | VOLUME<br>ml | RESULT<br>mg/sample | VOLUME<br>ml | RESULT<br>mg/sample |                                        | VOLUME<br>ml              | RESULT<br>mg/sample | VOLUME<br>ml       | RESULT<br>mg/sample |                                        |
| Lead                       | 90.00        | < 0.005000          | 210.000      | < 0.011000          | < 5.000                                | 430.00                    | 0.022000            | 60.000             | < 0.005000          | 22.000                                 |
| Mercury                    | 90.00        | < 0.000090          | 210.000      | < 0.000210          | < 0.090                                | 430.00                    | < 0.000430          | 60.000             | < 0.000060          | < 0.430                                |
| IMPINGERS 4 & 5, HCl RINSE |              |                     |              |                     |                                        | FILTERS                   |                     |                    |                     |                                        |
| SAMPLE ID                  | SAMPLE       |                     | BLANK        |                     | SAMPLE<br>Blank Corrected<br>ug/sample | SAMPLE                    |                     | BLANK              |                     | SAMPLE<br>Blank Corrected<br>ug/sample |
|                            | VOLUME<br>ml | RESULT<br>mg/sample | VOLUME<br>ml | RESULT<br>mg/sample |                                        | RESULT<br>ug/sample       |                     | CONC.<br>ug/sample |                     |                                        |
| Lead                       | 234.00       | < 0.012000          | 105.000      | < 0.005000          | < 12.000                               | 96.00                     |                     | < 3.00             |                     | 96.00                                  |
| Mercury                    | 234.00       | < 0.000230          | 105.000      | < 0.000110          | < 0.230                                | < 1.00                    |                     | 1.00               |                     | < 1.00                                 |
| TOTAL SAMPLE               |              |                     |              |                     | Blank Corrected<br>ug/sample           |                           |                     |                    |                     |                                        |
| SAMPLE ID                  |              |                     |              |                     |                                        |                           |                     |                    |                     |                                        |
| Lead                       |              |                     |              |                     | 1321.00                                |                           |                     |                    |                     |                                        |
| Mercury                    |              |                     |              |                     | 12.21                                  |                           |                     |                    |                     |                                        |

# ETS

Emission Testing Services, Inc.

## Metals Analysis per EPA Method 29

Analytical Laboratory: Chemtox Environmental & Industrial Hygiene Services

Client Name : Bayou Steel  
Source Name : Baghouse Stack  
Run No. : 2

| HNO3 PROBEWASH             |              |                     |              |                     |                                        | IMPINGERS 1 & 2 HNO3/H2O2 |                     |                    |                     |                                        |         |
|----------------------------|--------------|---------------------|--------------|---------------------|----------------------------------------|---------------------------|---------------------|--------------------|---------------------|----------------------------------------|---------|
| SAMPLE ID                  | SAMPLE       |                     | BLANK        |                     | SAMPLE<br>Blank Corrected<br>ug/sample | SAMPLE                    |                     | BLANK              |                     | SAMPLE<br>Blank Corrected<br>ug/sample |         |
|                            | VOLUME<br>ml | RESULT<br>mg/sample | VOLUME<br>ml | RESULT<br>mg/sample |                                        | VOLUME<br>ml              | RESULT<br>mg/sample | VOLUME<br>ml       | RESULT<br>mg/sample |                                        |         |
| Lead                       | 280.00       | 0.213000            | 210.000      | < 0.011000          | 213.000                                | 284.00                    | < 0.015000          | 102.000            | < 0.005000          | < 15.000                               |         |
| Mercury                    | 260.00       | 0.000290            | 210.000      | < 0.000210          | 0.290                                  | 294.00                    | < 0.000290          | 102.000            | < 0.000100          | < 0.290                                |         |
| IMPINGER 3, HNO3           |              |                     |              |                     |                                        | IMPINGERS 4 & 5, KMnO4    |                     |                    |                     |                                        |         |
| SAMPLE ID                  | SAMPLE       |                     | BLANK        |                     | SAMPLE<br>Blank Corrected<br>ug/sample | SAMPLE                    |                     | BLANK              |                     | SAMPLE<br>Blank Corrected<br>ug/sample |         |
|                            | VOLUME<br>ml | RESULT<br>mg/sample | VOLUME<br>ml | RESULT<br>mg/sample |                                        | VOLUME<br>ml              | RESULT<br>mg/sample | VOLUME<br>ml       | RESULT<br>mg/sample |                                        |         |
| Lead                       | 90.00        | < 0.005000          | 210.000      | < 0.011000          | < 5.000                                | 430.00                    | 0.039000            | 60.000             | < 0.005000          | 39.000                                 |         |
| Mercury                    | 90.00        | < 0.000090          | 210.000      | < 0.000210          | < 0.090                                | 430.00                    | < 0.000430          | 60.000             | < 0.000060          | < 0.430                                |         |
| IMPINGERS 4 & 5, HCl RINSE |              |                     |              |                     |                                        | FILTERS                   |                     |                    |                     |                                        |         |
| SAMPLE ID                  | SAMPLE       |                     | BLANK        |                     | SAMPLE<br>Blank Corrected<br>ug/sample | SAMPLE                    |                     | BLANK              |                     | SAMPLE<br>Blank Corrected<br>ug/sample |         |
|                            | VOLUME<br>ml | RESULT<br>mg/sample | VOLUME<br>ml | RESULT<br>mg/sample |                                        | RESULT<br>ug/sample       |                     | CONC.<br>ug/sample |                     |                                        |         |
| Lead                       | 234.00       | < 0.012000          | 105.000      | < 0.005000          | < 12.000                               | 73.00                     |                     | < 3.00             |                     | 73.00                                  |         |
| Mercury                    | 234.00       | < 0.000230          | 105.000      | < 0.000110          | < 0.230                                | < 1.00                    |                     | < 1.00             |                     | < 1.00                                 |         |
| TOTAL SAMPLE               |              |                     |              |                     | Blank Corrected<br>ug/sample           |                           |                     |                    |                     |                                        |         |
| Lead                       |              |                     |              |                     |                                        |                           |                     |                    |                     |                                        | 1357.00 |
| Mercury                    |              |                     |              |                     |                                        |                           |                     |                    |                     |                                        | 12.33   |



Emission Testing Services, Inc.

## Metals Analysis per EPA Method 29

Analytical Laboratory : Chemtex Environmental & Industrial Hygiene Services

Client Name : Bayou Steel  
Source Name : Baghouse Stack  
Run No. : 3

| HNO3 PROBE WASH          |              |                     |              |                     |                                        | IMPINGERS 1 & 2, HNO3/H2O2 |                     |                    |                     |                                        |
|--------------------------|--------------|---------------------|--------------|---------------------|----------------------------------------|----------------------------|---------------------|--------------------|---------------------|----------------------------------------|
| SAMPLE ID                | SAMPLE       |                     | BLANK        |                     | SAMPLE<br>Blank Corrected<br>ug/sample | SAMPLE                     |                     | BLANK              |                     | SAMPLE<br>Blank Corrected<br>ug/sample |
|                          | VOLUME<br>ml | RESULT<br>mg/sample | VOLUME<br>ml | RESULT<br>mg/sample |                                        | VOLUME<br>ml               | RESULT<br>mg/sample | VOLUME<br>ml       | RESULT<br>mg/sample |                                        |
| Lead                     | 234.00       | 0.171000            | 210.000      | < 0.011000          | 171.000                                | 314.00                     | < 0.016000          | 102.000            | < 0.005000          | < 18.000                               |
| Mercury                  | 234.00       | 0.004450            | 210.000      | < 0.000210          | 4.450                                  | 314.00                     | < 0.000310          | 102.000            | < 0.000100          | < 0.310                                |
| IMPINGER 3, HNO3         |              |                     |              |                     |                                        | IMPINGERS 4 & 5, KMnO4     |                     |                    |                     |                                        |
| SAMPLE ID                | SAMPLE       |                     | BLANK        |                     | SAMPLE<br>Blank Corrected<br>ug/sample | SAMPLE                     |                     | BLANK              |                     | SAMPLE<br>Blank Corrected<br>ug/sample |
|                          | VOLUME<br>ml | RESULT<br>mg/sample | VOLUME<br>ml | RESULT<br>mg/sample |                                        | VOLUME<br>ml               | RESULT<br>mg/sample | VOLUME<br>ml       | RESULT<br>mg/sample |                                        |
| Lead                     | 105.00       | < 0.005000          | 210.000      | < 0.011000          | < 5.000                                | 470.00                     | 0.028000            | 60.000             | < 0.005000          | 28.000                                 |
| Mercury                  | 105.00       | < 0.000110          | 210.000      | < 0.000210          | < 0.110                                | 470.00                     | < 0.000470          | 60.000             | < 0.000060          | < 0.470                                |
| IMPINGERS 4 & 5, HMRINSE |              |                     |              |                     |                                        | FILTERS                    |                     |                    |                     |                                        |
| SAMPLE ID                | SAMPLE       |                     | BLANK        |                     | SAMPLE<br>Blank Corrected<br>ug/sample | SAMPLE                     |                     | BLANK              |                     | SAMPLE<br>Blank Corrected<br>ug/sample |
|                          | VOLUME<br>ml | RESULT<br>mg/sample | VOLUME<br>ml | RESULT<br>mg/sample |                                        | RESULT<br>ug/sample        |                     | CONC.<br>ug/sample |                     |                                        |
| Lead                     | 240.00       | < 0.012000          | 105.000      | < 0.005000          | < 12.000                               | 131.00                     |                     | < 3.00             |                     | 131.00                                 |
| Mercury                  | 240.00       | < 0.000240          | 105.000      | < 0.000110          | < 0.240                                | < 1.00                     |                     | < 1.00             |                     | < 1.00                                 |
| TOTAL SAMPLE             |              |                     |              |                     | Blank Corrected<br>ug/sample           |                            |                     |                    |                     |                                        |
| Lead                     |              |                     |              |                     | 1363.00                                |                            |                     |                    |                     |                                        |
| Mercury                  |              |                     |              |                     | 16.58                                  |                            |                     |                    |                     |                                        |

# CHEMTEX

Environmental & Industrial Hygiene Services

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138 S. Cities Service Hwy., Sulphur, Louisiana 70663 • (337) 626-2121 FAX (337) 626-0405

Client: **E T S**  
**10461 Mammoth Dr.**  
**Baton Rouge, LA 70814**

Report Date: 08/02/04  
Sample Matrix: Liquid  
Date Collected: 07/23/04  
Collected By: Ron McCabe  
Date Received: 07/25/04  
CHEMTEX FILE #: P4070973

Phone: (225) 925-8405; Fax (225) 925-2343

**AIHA** Laboratory # 101478

**NVLAP** Lab Code 200635-0

**nelap** certificate # 02077

**RESULTS OF ANALYSIS**  
**CLIENT: Bayou Steel**  
**SOURCE: Baghouse Stack**

| CHEMTEX<br># | Sample          |           | Sampling<br>Volume | Results   |        | MDL       |      |
|--------------|-----------------|-----------|--------------------|-----------|--------|-----------|------|
|              | Identification  | Parameter | (mg/l)             | mg/sample | mg/l   | mg/sample | mg/l |
| P4070973     | PW-R1           | Lead      | 170                | 0.172     | 1.01   | 0.009     | 0.05 |
| P4070974     | PW-R2           | Lead      | 260                | 0.213     | 0.82   | 0.013     | 0.05 |
| P4070975     | PW-R3           | Lead      | 234                | 0.171     | 0.73   | 0.012     | 0.05 |
| P4070976     | IMP 1&2-R1      | Lead      | 274                | < 0.014   | < 0.05 | 0.014     | 0.05 |
| P4070977     | IMP 1&2-R2      | Lead      | 294                | < 0.015   | < 0.05 | 0.015     | 0.05 |
| P4070978     | IMP 1&2-R3      | Lead      | 314                | < 0.016   | < 0.05 | 0.016     | 0.05 |
| P4070979     | IMP 3-R1        | Lead      | 90                 | < 0.005   | < 0.05 | 0.005     | 0.05 |
| P4070980     | IMP 3-R2        | Lead      | 90                 | < 0.005   | < 0.05 | 0.005     | 0.05 |
| P4070981     | IMP 3-R3        | Lead      | 105                | < 0.005   | < 0.05 | 0.005     | 0.05 |
| P4070982     | BLANK 0.1N HNO3 | Lead      | 210                | < 0.011   | < 0.05 | 0.011     | 0.05 |
| P4070983     | BLANK DI H2O    | Lead      | 184                | < 0.009   | < 0.05 | 0.009     | 0.05 |
| P4070984     | BLANK HNO3/H2O2 | Lead      | 102                | < 0.005   | < 0.05 | 0.005     | 0.05 |
| Method Blank | DI Water        | Lead      | ---                |           | < 0.05 | ---       | 0.05 |

MDL: Method Detection Limit

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138 S. Cities Service Hwy., Sulphur, Louisiana 70663 • (337) 626-2121 FAX (337) 626-0405

Client: E T S  
10461 Mammoth Dr.  
Baton Rouge, LA 70814

Report Date: 08/02/04  
Sample Matrix: Liquid  
Date Collected: 07/23/04  
Collected By: Ron McCabe  
Date Received: 07/25/04  
CHEMTEX FILE #: P4070973

Phone: (225)925-8405; Fax (225)925-2343

AIHA Laboratory # 101478

NVLAP Lab Code 200635-0

nelap certificate # 02077

RESULTS OF ANALYSIS  
CLIENT: Bayou Steel  
SOURCE: Baghouse Stack

| CHEMTEX<br># | Sample          |           | Sampling         | Results   |       | MDL       |      |
|--------------|-----------------|-----------|------------------|-----------|-------|-----------|------|
|              | Identification  | Parameter | Volume<br>(mg/l) | ug/Sample | ug/l  | ug/Sample | ug/l |
| P4070973     | PW-R1           | Mercury   | 170              | 0.19      | 1.1   | 0.17      | 1.0  |
| P4070974     | PW-R2           | Mercury   | 260              | 0.29      | 1.1   | 0.26      | 1.0  |
| P4070975     | PW-R3           | Mercury   | 234              | 4.45      | 19.0  | 0.23      | 1.0  |
| P4070976     | IMP 1&2-R1      | Mercury   | 274              | < 0.27    | < 1.0 | 0.27      | 1.0  |
| P4070977     | IMP 1&2-R2      | Mercury   | 294              | < 0.29    | < 1.0 | 0.29      | 1.0  |
| P4070978     | IMP 162-R3      | Mercury   | 314              | < 0.31    | < 1.0 | 0.31      | 1.0  |
| P4070979     | IMP 3-R1        | Mercury   | 90               | < 0.09    | < 1.0 | 0.09      | 1.0  |
| P4070980     | IMP 3-R2        | Mercury   | 90               | < 0.09    | < 1.0 | 0.09      | 1.0  |
| P4070981     | IMP 3-R3        | Mercury   | 105              | < 0.11    | < 1.0 | 0.11      | 1.0  |
| P4070982     | BLANK 0.1N HNO3 | Mercury   | 210              | < 0.21    | < 1.0 | 0.21      | 1.0  |
| P4070983     | BLANK DI H2O    | Mercury   | 184              | < 0.18    | < 1.0 | 0.18      | 1.0  |
| P4070984     | BLANK HNO3/H2O2 | Mercury   | 102              | < 0.10    | < 1.0 |           | 1.0  |
| Method Blank | DI Water        | Mercury   | ---              |           | < 1.0 | ---       | 1.0  |

MDL: Method Detection Limit

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138 S. Cities Service Hwy., Sulphur, Louisiana 70663 • (337) 626-2121 FAX (337) 626-0405

Client: **E T S**  
10461 Mammoth Dr.  
Baton Rouge, LA 70814

Report Date: 08/02/04

Phone: (225) 925-8405; Fax (225) 925-2343

CHEMTEX FILE #: P4070973

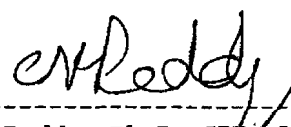
LABORATORY QUALITY ASSURANCE/QUALITY CONTROL DATA

| <u>Parameter</u> | <u>Units</u> | <u>True Value</u> | <u>Obtained Value</u> | <u>% Recovery</u> |
|------------------|--------------|-------------------|-----------------------|-------------------|
| Total Lead       | mg/l         | 0.250             | 0.268/0.299*          | 105               |
| Total Mercury    | ug/l         | 5.0               | 4.8/4.8*              | 100               |

| <u>Parameter</u> | <u>Method Reference</u> | <u>Date Analyzed/Analysts</u> |
|------------------|-------------------------|-------------------------------|
| Total Lead       | EPA Method 29           | 07/29/04 MHVR/NR              |
| Total Mercury    | EPA Method 29           | 07/29/04 MHVR/NR              |

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-----  
Dr. C. N. Reddy, Ph.D, CIA, ASP  
Director

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138 S. Cities Service Hwy., Sulphur, Louisiana 70663 • (337) 626-2121 FAX (337) 626-0405

Client: **E T S**  
10461 Mammoth Dr.  
Baton Rouge, LA 70814

Report Date: 08/02/04  
Sample Matrix: Liquid  
Date Collected: 07/23/04  
Collected By: Ron McCabe  
Date Received: 07/25/04  
CHEMTEX FILE #: P4070985

Phone: (225) 925-8405; Fax (225) 925-2343

**AIHA** Laboratory # 101478

**NVLAP** Lab Code 200635-0

**nelap** certificate # 02077

RESULTS OF ANALYSIS  
CLIENT: Bayou Steel  
SOURCE: Baghouse Stack

| CHEMTEX<br># | Sample<br>Identification              | Parameter | Sampling<br>Volume |           | Results |           | MDL  |  |
|--------------|---------------------------------------|-----------|--------------------|-----------|---------|-----------|------|--|
|              |                                       |           | (mg/l)             | mg/Sample | mg/l    | mg/Sample | mg/l |  |
| P4070985     | IMP 4&5-R1                            | Lead      | 430                | < 0.022   | < 0.05  | 0.022     | 0.05 |  |
| P4070986     | IMP 4&5- <del>R1</del> <b>R2</b>      | Lead      | 430                | 0.039     | 0.09    | 0.022     | 0.05 |  |
| P4070987     | IMP 4&5- <del>R1</del> <b>R3</b>      | Lead      | 470                | 0.028     | 0.06    | 0.024     | 0.05 |  |
| P4070988     | IMP 4&5-R1-HCL                        | Lead      | 234                | < 0.012   | < 0.05  | 0.012     | 0.05 |  |
| P4070989     | IMP 4&5- <del>R1</del> <b>R2</b> -HCL | Lead      | 234                | < 0.012   | < 0.05  | 0.012     | 0.05 |  |
| P4070990     | IMP 4&5- <del>R1</del> <b>R3</b> -HCL | Lead      | 240                | < 0.012   | < 0.05  | 0.012     | 0.05 |  |
| P4070991     | BLANK KmnO4                           | Lead      | 60                 | 0.005     | 0.08    | 0.003     | 0.05 |  |
| P4070992     | BLANK 8 N HCL                         | Lead      | 105                | < 0.005   | < 0.05  | 0.005     | 0.05 |  |
| Method Blank | DI Water                              | Lead      | ---                |           | < 0.05  | ---       | 0.05 |  |

MDL: Method Detection Limit

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138 S. Cities Service Hwy., Sulphur, Louisiana 70663 • (337) 626-2121 FAX (337) 626-0405

Client: E T S  
10461 Mammoth Dr.  
Baton Rouge, LA 70814

Report Date: 08/02/04  
Sample Matrix: Liquid  
Date Collected: 07/23/04  
Collected By: Ron McCabe  
Date Received: 07/25/04  
CHEMTEX FILE #: P4070985

Phone: (225)925-8405; Fax (225)925-2343

AIHA Laboratory # 101478

NVLAP Lab Code 200635-0

nelap certificate # 02077

RESULTS OF ANALYSIS  
CLIENT: Bayou Steel  
SOURCE: Baghouse Staak

| CHEMTEX<br># | Sample<br>Identification | Parameter | Sampling<br>Volume |           | Results |           | MDL  |
|--------------|--------------------------|-----------|--------------------|-----------|---------|-----------|------|
|              |                          |           | (mg/l)             | ug/sample | ug/l    | ug/sample | ug/l |
| P4070985     | MP 4&5-R1                | Mercury   | 430                | < 0.43    | < 1.0   | 0.43      | 1.0  |
| P4070986     | MP 4&5-R2                | Mercury   | 430                | < 0.43    | < 1.0   | 0.43      | 1.0  |
| P4070987     | IMP 4&5-R3               | Mercury   | 470                | < 0.47    | < 1.0   | 0.47      | 1.0  |
| P4070988     | IMP 4&5-R1-HCL           | Mercury   | 234                | < 0.23    | < 1.0   | 0.23      | 1.0  |
| P4070989     | IMP 4&5-R2-HCL           | Mercury   | 234                | < 0.23    | < 1.0   | 0.23      | 1.0  |
| P4070990     | IMP 4&5-R3-HCL           | Mercury   | 240                | < 0.24    | < 1.0   | 0.24      | 1.0  |
| P4070991     | BLANK KmnO4              | Mercury   | 60                 | < 0.06    | < 1.0   | 0.06      | 1.0  |
| P4070992     | BLANK 8 NHCL             | Mercury   | 105                | < 0.11    | < 1.0   | 0.11      | 1.0  |
| i            |                          |           |                    |           |         |           |      |
| Method Blank | DI Water                 | Mercury   | Blank              |           | < 1.0   | ---       | 1.0  |

MDL: Method Detection Limit

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138 S. Cities Service Hwy., Sulphur, Louisiana 70663 • (337) 626-2121 FAX(337) 626-0405

Client: **E T S**  
10461 Mammoth Dr.  
Baton Rouge, LA 70814

Report Date: 08/02/04

Phone: (225) 925-8405; Fax(225) 925-2343

CHEMTEX FILE #: P4070985

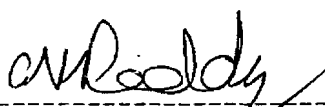
LABORATORY QUALITY ASSURANCE/QUALITY CONTROL DATA

| <u>Parameter</u> | <u>Units</u> | <u>True Value</u> | <u>Obtained Value</u> | <u>% Recovery</u> |
|------------------|--------------|-------------------|-----------------------|-------------------|
| Total Lead       | mg/l         | 0.250             | 0.268/0.299*          | 105               |
| Total Mercury    | ug/l         | 5.0               | 4.8/4.8*              | 100               |

| <u>Parameter</u> | <u>Method Reference</u> | <u>Date Analyzed/Analysts</u> |
|------------------|-------------------------|-------------------------------|
| Total Lead       | EPA Method 29           | 07/29/04 MHVR/NR              |
| Total Mercury    | EPA Method 29           | 07/29/04 MHVR/NR              |

bmb/amd/CNR

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Dr. C. El. Reddy, Ph.D., CM, ASP  
Director

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138 S. Cities Service Hwy., Sulphur, Louisiana 70663 • (337) 626-2121 FAX (337) 626-0405

Client: E T S  
10461 Mammoth Dr.  
Baton Rouge, LA 70814

Report Date: 07/30/04  
Sample Matrix: Quartz  
Date Collected: 07/23/04  
Collected By: Ron McCabe  
Date Received: 07/25/04  
CHEMTEX FILE #: P4070993

Phone: (225) 925-8405; Fax (225) 925-2343

AIHA Laboratory # 101478

NVLAP Lab Code 200635-0  
RESULTS OF ANALYSIS  
CLIENT: Bayou Steel  
SOURCE: Baghouse Stack

nelap certificate # 02077

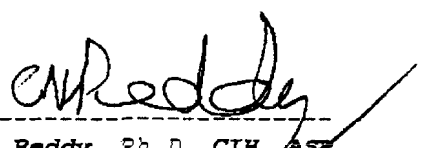
| CHEMTEX #    | Sample ID    | Parameter     | Result (ug/sample) | ML (ug/sample) |
|--------------|--------------|---------------|--------------------|----------------|
| P4070993     | Filter-R1    | Total Lead    | 96.0               | 3.0            |
|              |              | Total Mercury | < 1.0              | 1.0            |
| P4070994     | Filter-R2    | Total Lead    | 73.0               | 3.0            |
|              |              | Total Mercury | < 1.0              | 1.0            |
| P4070995     | Filter-R3    | Total Lead    | 131.0              | 3.0            |
|              |              | Total Mercury | < 1.0              | 1.0            |
| P4070996     | Blank Filter | Total Lead    | < 3.0              | 3.0            |
|              |              | Total Mercury | < 1.0              | 1.0            |
| Method Blank | Blank Filter | Total Lead    | < 3.0              | 3.0            |
|              |              | Total Mercury | < 1.0              | 1.0            |

#### LABORATORY QUALITY ASSURANCE/QUALITY CONTROL DATA

| Parameter     | Units | True Value | Obtained Value |
|---------------|-------|------------|----------------|
| Total Lead    | ug/l  | 250        | 268/302*       |
| Total Mercury | ug/l  | 5.0        | 4.8/4.8*       |

| Parameter     | Method Reference | Date Analyzed/Analysts |
|---------------|------------------|------------------------|
| Total Lead    | EPA Method 29    | 07/29/04 MHVR/NR       |
| Total Mercury | EPA Method 29    | 07/29/04 MHVR/NR       |

bmb/CNR

  
C. N. Reddy, Ph.D., CIH, ASE  
Director

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6.1.25

## UNIT OPERATING DATA

During the emission tests, unit operating data were recorded by Bayou Steel. These data are presented on the following pages.



# Bayou Steel Corporation

## Heat Record

Crew: C  
Date: 7/23/09  
Grade: A3646w

Melter: Dued  
1st Helper: W. H. H.  
Ladleman: J. H.

Heat #: 27245

| Electrodes |          |
|------------|----------|
| Ad         | Slp. Brk |
| A          |          |
| B          |          |
| C          |          |

Pulse Counter  
1st Charge 2122828  
Last Charge 2116096

Tap To Tap Time 52

Lost Time EQUALS Lost \$MONEY\$ !!!!!!!!!!!!!

| Previous Heat Tap                              |                       |
|------------------------------------------------|-----------------------|
| PON                                            | POFF                  |
| Head: <u>812</u>                               | <u>825</u> (220)      |
| 1 Back: <u>827</u>                             | <u>834</u> (220)      |
| 2 Back: <u>836</u>                             |                       |
| 3 Back:                                        |                       |
| Tap Start: <u>8:58</u> Tap Finish: <u>9:10</u> |                       |
| Power On: <u>394</u>                           | LMF                   |
| kWh: <u>31250</u>                              | kWh                   |
| kWh/Ton: <u>327</u>                            | kWh/Ton               |
| Plan: <u>(360)</u>                             | Plan: <u>(25)</u>     |
| Ladle Data:                                    | Surf Info             |
| Ladle No: <u>5</u>                             | Hts Pig: <u>9</u>     |
| Heats: <u>9</u>                                | Surf OK               |
| Temp:                                          |                       |
| Temperature Data                               |                       |
| Time                                           | kWh                   |
| 1                                              | <u>2915</u> <u>15</u> |
| 2                                              | <u>2980</u>           |
| 3                                              |                       |
| 4                                              |                       |
| 5                                              |                       |

| FAR Addition       |                   |
|--------------------|-------------------|
| Tap                | Trim              |
| Lime: <u>5000</u>  | SiMn: <u>1670</u> |
| MgO: <u>1300</u>   | FeSi: <u>338</u>  |
| Chg C:             | FeMn:             |
| Foamy: <u>7888</u> | Coke:             |
| Oxygn: <u>1048</u> | BPI:              |
| N Gas: <u>209</u>  | Lime: <u>800</u>  |
|                    | De-Sul:           |
|                    | FeV:              |
|                    | FeAl:             |
|                    | CaC: <u>50</u>    |
|                    | SiC: <u>100</u>   |
|                    | CaH: <u>200</u>   |
| Material Location  |                   |
| Amount             |                   |
| Scan Compliance    |                   |
| Charge             | Header            |
| Deviation          | 2nd Bck           |
|                    | 3rd Bck           |
|                    | TOTAL             |

Be Satisfied Always i Better Way

| Process Weights |           |
|-----------------|-----------|
| Charge lbs      | Cast Tons |
| <u>196,000</u>  |           |

| Ladle Sample                        |         |
|-------------------------------------|---------|
| To LMF                              | St to C |
| <input checked="" type="checkbox"/> |         |

| Chemistries | C     | Mn    | P  | S  | Si    | Co | Ni | Cr | Mo | Sn | V |
|-------------|-------|-------|----|----|-------|----|----|----|----|----|---|
| Alm Pin     | 13/18 | 20/85 | 40 | 50 | 18/26 | 59 |    |    |    |    |   |

### Procedure Compliance Summary

|                    | Gal | Act | Dev | Reason | (Use Delay Code & Description) |
|--------------------|-----|-----|-----|--------|--------------------------------|
| Tap                | 3   | 3   |     |        |                                |
| Turn Around        | 2   | 2   | 1   | 41-B   |                                |
| Power On           | 11  | 18  | 2   | 44-6   |                                |
| First Back Charge  | 2   | 2   |     |        |                                |
| Power On           | 8   | 7   |     |        |                                |
| Second Back Charge | 2   | 2   |     |        |                                |
| Power On           | 6   |     | 2   | AB-2   |                                |
| Third Back Charge  | 0   |     |     |        |                                |
| Power On           | 0   |     |     |        |                                |
| Refine             | 11  |     |     |        |                                |
| Total              | 45  |     |     |        |                                |

Action Items:

Maintenance Barriers:

# Bayou Steel Corporation Scrap Blend Procedure

Blend #65 3-Buckets

Heat# 27245

Date 7-22-04

Turn C

Oper Coady

Foreman Deck

## Header

| Layer | Description   | Alt Code | Sub Code | Alt   | Actual | Deviation | %   |
|-------|---------------|----------|----------|-------|--------|-----------|-----|
| 1     | Bushling      | 16       |          | 0     |        |           | 0%  |
| 2     | Home Pit      | 12       |          | 7000  | 8      |           | 9%  |
| 3     | #2 Bundles    | 5        |          | 5000  | 5      |           | 6%  |
| 4     | Turnings      | 1        |          | 12000 | 16     |           | 16% |
|       | Barge / Plate | 1        |          | 17000 | 13     |           | 22% |
|       | #1 Heavy      | 7        |          | 13000 | 15     |           | 17% |
|       | Mixed 1&2     | 11       |          | 8000  | 20     |           | 10% |
|       |               |          |          |       |        |           | 0%  |
| 6     | Shredded      | 10       |          | 15000 | 20     |           | 19% |
| Total |               |          |          | 77000 | 99     |           |     |

## First BackChg

| Layer | Description   | Alt Code | Sub Code | Alt   | Actual | Deviation | %   |
|-------|---------------|----------|----------|-------|--------|-----------|-----|
| 1     | Bushling      | 16       |          | 2000  |        |           | 3%  |
| 2     | Turnings      |          |          | 10000 | 8      |           | 15% |
| 3     | Barge / Plate | 1        |          | 14000 | 5      |           | 22% |
|       | #1 Heavy      | 1        |          | 16000 | 17     |           | 25% |
|       | Mixed 1&2     | 7        |          | 8000  | 13     |           | 12% |
|       |               |          |          |       |        |           | 0%  |
|       |               |          |          |       |        |           | 0%  |
| 5     | Shredded      | 10       |          | 15000 | 14     |           | 23% |
| Total |               |          |          | 65000 | 86     |           |     |

## Second BackChg

| Layer | Description | Alt Code | Sub Code | Alt   | Actual | Deviation | %   |
|-------|-------------|----------|----------|-------|--------|-----------|-----|
| 1     | Mixed 1&2   | 7        |          | 14000 | 15     |           | 42% |
|       | Turnings    | 11       |          | 8000  |        |           | 9%  |
|       | Mill Crop   | 15       |          | 3000  | 5      |           | 12% |
|       | #1 Heavy    | 1        |          | 4000  | 10     |           | 24% |
|       | Shredded    |          |          | 4000  | 5      |           |     |
| Total |             |          |          | 33000 | 35     |           |     |

150

# Bayou Steel Corporation

# Heat Record



Crew: C  
Date: 7/23/04  
Grade: A36

Melter: Duck  
1st Helper: Wayne  
Ladleman: Lebb

Heat #: 27246

| Electrodes | Ad | Slp | Brk |
|------------|----|-----|-----|
|            |    |     |     |
|            |    |     |     |
|            |    |     |     |

Pulse Counter:  
1st Charge 7126096  
Last Charge 7129187

Tap To Tap Time 64

Lost Time EQUALS Lost \$MONEY\$ !!!!!!!!!

|                                                |              |                  |              |
|------------------------------------------------|--------------|------------------|--------------|
| Previous Heat Tap: <u>855B</u>                 |              |                  |              |
| PON                                            | POFF         | kWh/ton          |              |
| Headr                                          | <u>9.05</u>  | <u>916</u>       | (220)        |
| 1 Back                                         | <u>918</u>   | <u>926</u>       | (220)        |
| 2 Back                                         | <u>928</u>   |                  |              |
| 3 Back                                         |              |                  |              |
| Tap Start: <u>9:52</u> Tap Finish: <u>9:55</u> |              |                  |              |
| Power On                                       | <u>27.7</u>  | LIME             |              |
| kWh                                            | <u>29810</u> | kWh              |              |
| kWh/Ton                                        | <u>321</u>   | kWh/Ton          |              |
| Plan                                           | <u>(360)</u> | Plan             |              |
| Ladle Data                                     |              |                  |              |
| Ladle No.                                      | <u>10</u>    | Hts Pig <u>5</u> |              |
| Heats                                          | <u>6</u>     | Sur OK           |              |
| Temp                                           |              |                  |              |
| Temperature Data                               |              |                  |              |
| Time                                           | kWh          | Temp             | Carbon O2ppm |
| 1                                              |              | <u>2989</u>      | <u>12</u>    |
| 2                                              |              |                  |              |
| 3                                              |              |                  |              |
| 4                                              |              |                  |              |
| Edt                                            |              |                  |              |

|                  |             |                |             |
|------------------|-------------|----------------|-------------|
| PAR Addition     |             | Ladle Addition |             |
| Tap              | Trim        | Tap            | Trim        |
| Lime             | <u>5000</u> | SIMn           | <u>1675</u> |
| MgO              | <u>1300</u> | FeSi           | <u>325</u>  |
| Chp C            |             | FeMn           |             |
| Foamy            | <u>2667</u> | Coke           |             |
| Oxgyn            | <u>996</u>  | BPL            |             |
| N Gas            | <u>207</u>  | Lime           | <u>800</u>  |
|                  |             | De-Sul         |             |
|                  |             | FeV            |             |
|                  |             | FeAl           |             |
|                  |             | CaC            | <u>50</u>   |
|                  |             | SIC            | <u>100</u>  |
|                  |             | GA1            | <u>200</u>  |
| Comments         |             |                |             |
| Material         |             | Location       |             |
| Amount           |             |                |             |
| Scrap Compliance |             |                |             |
| Charge           | Header      | 1st Bck        | 2nd Bck     |
| Deviation        |             |                |             |
|                  |             | 3rd Bck        | TOTAL       |

Never Be Satisfied Always a Better Way

|                |                |
|----------------|----------------|
| Process Weight |                |
| Charge lbs     | <u>190,000</u> |
| Tap Tons       | <u>84</u>      |
| Cast Tons      |                |

|               |          |
|---------------|----------|
| Ladle Sent To |          |
| To LMF        | <u>✓</u> |
| St to Ch      |          |

|             |              |              |           |              |              |           |
|-------------|--------------|--------------|-----------|--------------|--------------|-----------|
| Chemistries | <u>8/15</u>  | <u>15/00</u> | <u>25</u> | <u>40-50</u> | <u>10/26</u> | <u>35</u> |
|             | C            | Mn           | P         | S            | Si           | Co        |
| Alm         | <u>10/10</u> | <u>7/15</u>  | <u>16</u> | <u>50</u>    | <u>18/26</u> | <u>59</u> |
| Bin         |              |              |           |              |              |           |

## Procedure Compliance Summary

|                    | Got | Act | Dev | Reason | (Use Delay Code & Description) |
|--------------------|-----|-----|-----|--------|--------------------------------|
| Tap                | 3   | 3   |     |        |                                |
| Turn Around        | 2   | 4   | 2   | A1-B   |                                |
| Power On           | 11  | 11  |     |        |                                |
| First Back Charge  | 2   | 2   |     |        |                                |
| Power On           | 8   | 8   |     |        |                                |
| Second Back Charge | 2   |     |     |        |                                |
| Power On           | 6   |     |     |        |                                |
| Third Back Charge  | 0   |     |     | A1-2   | 9:50-9:52                      |
| Power On           | 0   |     |     |        |                                |
| Refine             | 11  |     |     |        |                                |
| Total              | 45  |     |     |        |                                |

Action Items:

Maintenance Barriers:

9434 1st Test (6.2.02)

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# Bayou Steel Corporation Scrap Blend Procedure

nd #65 3-Buckets

Mat# 37246

Date 7-22

Turn C

per Carboy

Foreman

## Header

| Layer | Description   | Alt Code | Sub Code | Alt Weight | Actual Weight | Deviation | %   |
|-------|---------------|----------|----------|------------|---------------|-----------|-----|
| 1     | Bushling      | 16       |          | 0          |               |           | 0%  |
| 2     | Home Plt      | 12       |          | 7000       |               |           | 9%  |
| 3     | #2 Bundles    | 5        |          | 5000       | 5             |           | 6%  |
| 4     | Turnings      | 1        |          | 12000      | 15            |           | 16% |
|       | Barge / Plate | 1        |          | 17000      | 20            |           | 22% |
|       | #1 Heavy      | 7        |          | 13000      | 20            |           | 17% |
|       | Mixed 1&2     | 11       |          | 8000       | 20            |           | 10% |
|       |               |          |          |            |               |           | 0%  |
| 6     | Shredded      | 10       |          | 15000      | 20            |           | 19% |
| Total |               |          |          | 77000      | 20            |           |     |

## First BackChg

| Layer | Description   | Alt Code | Sub Code | Alt Weight | Actual Weight | Deviation | %   |
|-------|---------------|----------|----------|------------|---------------|-----------|-----|
| 1     | Bushling      | 16       |          | 2000       |               |           | 3%  |
| 2     | Turnings      |          |          | 10000      |               |           | 15% |
| 3     | Barge / Plate | 1        |          | 14000      | 10            |           | 22% |
|       | #1 Heavy      | 1        |          | 16000      | 20            |           | 25% |
|       | Mixed 1&2     | 7        |          | 8000       | 10            |           | 12% |
|       |               |          |          |            |               |           | 0%  |
|       |               |          |          |            |               |           | 0%  |
| 5     | Shredded      | 10       |          | 15000      | 20            |           | 23% |
| Total |               |          |          | 65000      | 60            |           |     |

## Second BackChg

| Layer | Description | Alt Code | Sub Code | Alt Weight | Actual Weight | Deviation | %   |
|-------|-------------|----------|----------|------------|---------------|-----------|-----|
| 1     | Mixed 1&2   | 7        |          | 14000      | 20            |           | 42% |
|       | Turnings    | 11       |          | 8000       | 10            |           | 9%  |
|       | Mill Crop   | 15       |          | 3000       |               |           | 12% |
|       | #1 Heavy    | 1        |          | 4000       | 5             |           | 24% |
|       | Shredded    |          |          | 4000       | 5             |           |     |
| Total |             |          |          | 33000      | 40            |           |     |

190



# Bayou Steel Corporation

## Heat Record

Crew: C Melter: Duck  
Date: 7/23/04 1st Helper: Wayne  
Grade: A3644w Ladleman: J46

Heat #: 27247

### Pulse Counter

1st Charge 7129187

Last Charge 7132630

Tap To Tap Time 54

Lost Time EQUALS Lost \$MONEYS !!!!!!!!!!!

| Electrodes |     |     |
|------------|-----|-----|
| Ad         | Slp | Brk |
| A          |     |     |
| B          |     |     |
| C          |     |     |

Previous Heat Tap: 9:52

|        | PON          | POFF         | kWh/ton |
|--------|--------------|--------------|---------|
| Headr  | <u>10:00</u> | <u>10:11</u> | (220)   |
| 1 Back | <u>10:13</u> | <u>10:22</u> | (220)   |
| 2 Back | <u>10:24</u> |              |         |
| 3 Back |              |              |         |

Tap Start: 10:46 Tap Finish: 10:49

|          |              |         |             |
|----------|--------------|---------|-------------|
| Power On | <u>40.2</u>  | LME     |             |
| kWh      | <u>32100</u> | kWh     |             |
| kWh/Ton  | <u>345</u>   | kWh/Ton |             |
| Plan     | <u>(360)</u> | Plan    | <u>(25)</u> |

Ladle Data: Stir OK

Ladle No: 8 Hts Pig: 1

Heats: 45 Stir OK

Temp

Temperature Data

| Time | kWh | Temp        | Carbon    | O2ppm |
|------|-----|-------------|-----------|-------|
| 1    |     | <u>3026</u> | <u>11</u> |       |
| 2    |     | <u>3100</u> |           |       |
| 3    |     |             |           |       |
| 4    |     |             |           |       |
| 5    |     |             |           |       |

### PAF Additions

|        | Tap         | Trim |
|--------|-------------|------|
| Lime   | <u>5000</u> |      |
| MgO    | <u>1800</u> |      |
| ChgC   |             |      |
| Foamy  | <u>3057</u> |      |
| Oxygen | <u>1067</u> |      |
| N Gas  | <u>215</u>  |      |

### Ladle Additions

|        | Tap         | Trim |
|--------|-------------|------|
| SiMn   | <u>1678</u> |      |
| FeSi   | <u>330</u>  |      |
| FeMn   |             |      |
| Coke   | <u>50</u>   |      |
| BPI    |             |      |
| Lime   | <u>800</u>  |      |
| De-Sul |             |      |
| FeV    |             |      |
| FeAl   |             |      |
| CaC    | <u>50</u>   |      |
| SiC    | <u>100</u>  |      |
| GA1    | <u>200</u>  |      |

### Sampling Data

| Material | Location |
|----------|----------|
| Amount   |          |

### Scan Compliance

| Charge    | Header | 1st Bck | 2nd Bck | 3rd Bck | TOTAL |
|-----------|--------|---------|---------|---------|-------|
| Deviation |        |         |         |         |       |

Never Be Satisfied Always a B Way

### Process Weights

| Charge lbs   | Tap Tons  | Cast Tons |
|--------------|-----------|-----------|
| <u>19000</u> | <u>83</u> |           |

### Ladle Sampling

| To LME                              | St to C |
|-------------------------------------|---------|
| <input checked="" type="checkbox"/> |         |

### Chemistries

|     | C            | Mn           | P         | S         | Si           | Co        | N | Cr | Mo | Sn | V |
|-----|--------------|--------------|-----------|-----------|--------------|-----------|---|----|----|----|---|
| Aim | <u>13/18</u> | <u>70/85</u> | <u>40</u> | <u>50</u> | <u>18/26</u> | <u>59</u> |   |    |    |    |   |
| Rin |              |              |           |           |              |           |   |    |    |    |   |

### Procedure Compliance Summary

|                    | Go | Act | Dev | Reason      | (Use Delay Code & Description) |
|--------------------|----|-----|-----|-------------|--------------------------------|
| Tap                | 3  | 3   |     |             |                                |
| Turn Around        | 2  | 5   | 3   | <u>A1-3</u> |                                |
| Power On           | 1  | 1   |     |             |                                |
| Flrs               | 1  | 1   |     |             |                                |
| Power On           | 8  | 9   | 1   | <u>A4-6</u> |                                |
| Second Back Charge | 2  | 2   |     |             |                                |
| Power On           | 6  |     |     |             |                                |
| Third Back Charge  | 0  |     |     |             |                                |
| Power On           | 0  |     |     |             |                                |
| Refine             | 11 |     |     |             |                                |
| Total              | 45 |     |     |             |                                |

Action Items:

Maintenance Barriers:

Record  
247

# Bayou Steel Corporation Scrap Blend Procedure

Blend #65 3-Break

Heat# 87247  
Oper Cowley

Date 7-22

Turn C  
Foreman ARK

## Header

| Layer | Description   | Alt Code | Sub Code | Alt   | Actual | Deviation | %   |
|-------|---------------|----------|----------|-------|--------|-----------|-----|
| 1     | Bushling      | 16       |          | 0     |        |           | 0%  |
| 2     | Home Pit      | 12       |          | 7000  |        |           | 9%  |
| 3     | #2 Bundles    | 5        |          | 5000  |        |           | 6%  |
| 4     | Turnings      | 1        |          | 12000 | 5      |           | 16% |
|       | Barge / Plate | 1        |          | 17000 | 20     |           | 22% |
|       | #1 Heavy      | 7        |          | 13000 | 20     |           | 17% |
|       | Mixed 1&2     | 11       |          | 8000  | 20     |           | 10% |
|       |               |          |          |       |        |           | 0%  |
| 6     | Shredded      | 10       |          | 15000 | 20     |           | 19% |
| Total |               |          |          | 77000 | 95     |           |     |

## First BackChg

| Layer | Description   | Alt Code | Sub Code | Alt   | Actual | Deviation | %   |
|-------|---------------|----------|----------|-------|--------|-----------|-----|
| 1     | Bushling      | 16       |          | 2000  |        |           | 3%  |
| 2     | Turnings      |          |          | 10000 | 10     |           | 15% |
| 3     | Barge / Plate | 1        |          | 14000 | 10     |           | 22% |
|       | #1 Heavy      | 1        |          | 16000 | 10     |           | 25% |
|       | Mixed 1&2     | 7        |          | 8000  | 10     |           | 12% |
|       |               |          |          |       |        |           | 0%  |
|       |               |          |          |       |        |           | 0%  |
| 5     | Shredded      | 10       |          | 15000 | 14     |           | 23% |
| Total |               |          |          | 65000 | 54     |           |     |

## Second BackChg

| Layer | Description | Alt Code | Sub Code | Alt   | Actual | Deviation | %   |
|-------|-------------|----------|----------|-------|--------|-----------|-----|
| 1     | Mixed 1&2   | 7        |          | 14000 | 30     |           | 42% |
|       | Turnings    | 11       |          | 8000  | 20     |           | 9%  |
|       | Mill Crop   | 15       |          | 3000  |        |           | 12% |
|       | #1 Heavy    | 1        |          | 4000  | 5      |           | 24% |
|       | Shredded    |          |          | 4000  | 5      |           |     |
| Total |             |          |          | 33000 | 60     |           |     |

190



# Bayou Steel Corporation

## Heat Record

Crew: CMelter: DuckHeat #: 27248Date: 7-23-041st Helper: WSGrade: A36-44WLadleman: JB

| Electrodes |         |
|------------|---------|
| Ad         | Sip Brk |
| A          |         |
| B          |         |
| C          |         |

|                            |
|----------------------------|
| Pulse Counter              |
| 1st Charge <u>7/29/07</u>  |
| Last Charge <u>7/25/07</u> |

Tap To Tap Time 53

Lost Time EQUALS Lost \$MONEY\$ !!!!!!!!!!!!!

|                                 |       |                          |              |
|---------------------------------|-------|--------------------------|--------------|
| Previous Heat Tap: <u>10:46</u> |       |                          |              |
| Headr                           | 1053  | 11:04                    | (220)        |
| 1 Back                          | 1108  | 11:15                    | (220)        |
| 2 Back                          | 1117  |                          |              |
| 3 Back                          |       |                          |              |
| Tap Start: <u>11:39</u>         |       | Tap Finish: <u>11:43</u> |              |
| Power On                        | 37.2  | LME                      |              |
| kWh                             | 29040 | kWh                      |              |
| kWh/Ton                         | 310   | kWh/Ton                  |              |
| Plan                            | (360) | Plan                     |              |
| Ladle Data                      |       | Sift Info                |              |
| Ladle No                        | 7     | HTS Pig                  |              |
| Heats                           | 89    | Sift OK                  |              |
| Temp                            |       |                          |              |
| Temperature Data                |       |                          |              |
| Time                            | kWh   | Temp                     | Carbon O2ppm |
| 1                               |       | 3000                     | 12           |
| 2                               |       |                          |              |
| 3                               |       |                          |              |
| 4                               |       |                          |              |
| Edt                             |       |                          |              |

| FAR Addition     |          | Ladle Addition |         |
|------------------|----------|----------------|---------|
| Phs              | Tap      | Tap            | Trim    |
| Lime             | 5000     | SiMn           | 1678    |
| MgO              | 1300     | FeSi           | 325     |
| Chg C            |          | FeMn           |         |
| Foamy            | 2518     | Coke           | 50      |
| Oxgyn            | 971      | BPI            |         |
| N Gas            | 200      | Lime           | 800     |
|                  |          | De Sul         |         |
|                  |          | FeV            |         |
|                  |          | FeAl           |         |
|                  |          | CaC            | 50      |
|                  |          | SiC            | 100     |
|                  |          | QAI            | 200     |
| Ginning Data     |          |                |         |
| Material         | Location |                |         |
| Amount           |          |                |         |
| Scrap Compliance |          |                |         |
| Charge           | Header   | 1st Bck        | 2nd Bck |
| Deviation        |          |                |         |
|                  |          |                | TOTAL   |

Never Be Satisfied Always Better Way

|                 |          |           |
|-----------------|----------|-----------|
| Process Weights |          |           |
| Charge lbs      | Tap Tons | Cast Tons |
| 185,000         | 86       |           |

|              |         |
|--------------|---------|
| Ladle Sample |         |
| To LMF       | St to C |
| ✓            |         |

| Chemistries |       |       |    |    |      |    |    |    |    |    |   |  |
|-------------|-------|-------|----|----|------|----|----|----|----|----|---|--|
|             | C     | Mn    | P  | S  | Si   | Co | Ni | Cr | Mo | Sn | V |  |
| Air Rin     | 13/17 | 70/85 | 40 | 50 | 1024 | 59 |    |    |    |    |   |  |

### Procedure Compliance Summary

|                    | Go! | Act | Dev | Reason (Use Delay Code & Description) |
|--------------------|-----|-----|-----|---------------------------------------|
| Tap                | 3   | 3   |     |                                       |
| Turn Around        | 2   | 4   | 2   | A1-B                                  |
| Power On           | 11  | 11  |     |                                       |
| First Back Charge  | 2   | 4   | 2   | A4-1                                  |
| Power On           | 8   | 5   |     |                                       |
| Second Back Charge | 2   | 2   |     |                                       |
| Power On           | 6   |     |     |                                       |
| Third Back Charge  | 0   |     |     |                                       |
| Power On           | 0   |     |     |                                       |
| Refine             | 11  |     |     |                                       |
| Total              | 45  |     |     |                                       |

Action Items:

Maintenance Barriers:

# **Bayou Steel Corporation** **Scrap Blend Procedure**

Blend #65 3-Buckets

Heat# 27248

Date 7-22-08

Turn C

Oper Lowrey

Foreman Park

## **Header**

| Layer | Description   | Aim  |       | Sub  |       | Weights |        | Deviation | %   |
|-------|---------------|------|-------|------|-------|---------|--------|-----------|-----|
|       |               | Code | Units | Code | Units | Aim     | Actual |           |     |
| 1     | Bushling      | 16   |       |      |       | 0       |        |           | 0%  |
| 2     | Home Pit      | 12   |       |      |       | 7000    |        |           | 9%  |
| 3     | #2 Bundles    | 5    |       |      |       | 5000    | 5      |           | 6%  |
| 4     | Turnings      | 1    |       |      |       | 12000   | 11     |           | 16% |
|       | Barge / Plate | 1    |       |      |       | 17000   | 15     |           | 22% |
|       | #1 Heavy      | 7    |       |      |       | 13000   | 15     |           | 17% |
|       | Mixed 1&2     | 11   |       |      |       | 8000    | 20     |           | 10% |
|       |               |      |       |      |       |         |        |           | 0%  |
| 6     | Shredded      | 10   |       |      |       | 15000   | 20     |           | 19% |
| Total |               |      |       |      |       | 77000   | 86     |           |     |

## **First BackChg**

| Layer | Description   | Aim  |       | Sub  |       | Weights |        | Deviation | %   |
|-------|---------------|------|-------|------|-------|---------|--------|-----------|-----|
|       |               | Code | Units | Code | Units | Aim     | Actual |           |     |
| 1     | Bushling      | 16   |       |      |       | 2000    |        |           | 3%  |
| 2     | Turnings      |      |       |      |       | 10000   | 15     |           | 15% |
| 3     | Barge / Plate | 1    |       |      |       | 14000   | 8      |           | 22% |
|       | #1 Heavy      | 1    |       |      |       | 16000   | 15     |           | 25% |
|       | Mixed 1&2     | 7    |       |      |       | 8000    | 15     |           | 12% |
|       |               |      |       |      |       |         |        |           | 0%  |
|       |               |      |       |      |       |         |        |           | 0%  |
| 5     | Shredded      | 10   |       |      |       | 15000   | 20     |           | 23% |
| Total |               |      |       |      |       | 65000   | 73     |           |     |

## **Second BackChg**

| Layer | Description | Aim  |       | Sub  |       | Weights |        | Deviation | %   |
|-------|-------------|------|-------|------|-------|---------|--------|-----------|-----|
|       |             | Code | Units | Code | Units | Aim     | Actual |           |     |
| 1     | Mixed 1&2   | 7    |       |      |       | 14000   | 20     |           | 42% |
|       | Turnings    | 11   |       |      |       | 8000    | 8      |           | 9%  |
|       | Mill Crop   | 15   |       |      |       | 3000    |        |           | 12% |
|       | #1 Heavy    | 1    |       |      |       | 4000    |        |           | 24% |
|       | Shredded    |      |       |      |       | 4000    |        |           |     |
| Total |             |      |       |      |       | 33000   | 26     |           |     |

3 Heats



# Bayou Steel Corporation

## Heat Record

Crew: CMelter: AuekDate: 7-23-041st Helper: WSGrade: A36Ladleman: JBHeat #: 27249

### Pulse Counter

1st Charge 7135551Last Charge 7138686Tap To Tap Time 55

Lost Time EQUALS Lost \$MONEY\$ !!!!!!!!!!!

Electrodes  
Ad. Slip Br.

|   |  |  |  |
|---|--|--|--|
| A |  |  |  |
| B |  |  |  |
| C |  |  |  |

Previous Heat Tap 11:39

PON POFF kWh/ton

Headr 11:50 12:01 (220)1 Back 12:03 12:13 (220)2 Back 12:15 (220)

3 Back (220)

Tap Start 12:19 Tap Finish 12:34Power On 38.4 kWhkWh 29620 kWhkWh/ton 316 kWh/ton

Plan (360) Plan (25)

Ladle No 5 Stir OK 10Heats 10 Stir OK

Temp

Temperature Data (250) (250)

Time kWh Temp Carbon-O2ppm

1 (250) (250) (250) (250)

2 (250) (250) (250) (250)

3 (250) (250) (250) (250)

4 (250) (250) (250) (250)

Ld

FAR Additions

Tap Trim

Lime 5000 SiMn 1665MgO 1300 FeSi 330Chg C 26.97 FeMnFoamy 100 CokeOxygen 208 BPIN Gas 800 Lime

De-Sul

FeV

FeAl

CaC 50SiC 100GHL 200

Continued Data

Material Location

Amount

Start Compliance

Charge Header 1st Bck 2nd Bck 3rd Bck TOTAL

Deviation

Process Weights

Charge lbs Tap Tons Cast Tons

180,000 81

Ladle Sample

To LMF Stio C

✓

Never Be Satisfied Always a Better Way

### Chemistries

C Mn P S Si Cu Ni Cr Mo Sn V

Aim 843 7015 40 60 1826 60

Pin

### Procedure Compliance Summary

|                    | Get | Act | Dev | Reason  | (Use Delay Code & Description) |
|--------------------|-----|-----|-----|---------|--------------------------------|
| Tap                | 3   | 3   |     |         |                                |
| Turn Around        | 2   | 8   | 6   | A4-3(4) | A4-1(2)                        |
| Power On           | 11  | 11  |     |         |                                |
| First Back Charge  | 2   | 2   |     |         |                                |
| Power On           | 8   | 10  | 2   | A4-6    |                                |
| Second Back Charge | 2   | 2   |     |         |                                |
| Power On           | 6   | 6   |     |         |                                |
| Third Back Charge  | 0   | 0   |     |         |                                |
| Power On           | 0   | 0   |     |         |                                |
| Refine             | 11  | 11  |     |         |                                |
| Total              | 45  | 45  |     |         |                                |

### Action Items:

Test #2 11:58 0.8 min into Header

### Maintenance Barriers:

# Bayou Steel Corporation

## Scrap Blend Procedure

Blend #65 3-Buckets

Heat# 27219

Date. Feb

Turn C

Oper Carbo

Foreman Deck

### Header

| Layer | Description   | Alm Code | Sub Code | Alm   | Actual | Deviation | %   |
|-------|---------------|----------|----------|-------|--------|-----------|-----|
| 1     | Bushling      | 16       |          | 0     |        |           | 0%  |
| 2     | Home Pit      | 12       |          | 7000  |        |           | 8%  |
| 3     | #2 Bundles    | 5        |          | 5000  | 3      |           | 6%  |
| 4     | Turnings      | 1        |          | 12000 | 20     |           | 16% |
|       | Barge / Plate | 1        |          | 17000 | 20     |           | 22% |
|       | #1 Heavy      | 7        |          | 13000 | 25     |           | 17% |
|       | Mixed 1&2     | 11       |          | 8000  | 25     |           | 10% |
|       |               |          |          |       |        |           | 0%  |
| 6     | Shredded      | 10       |          | 15000 | 20     |           | 19% |
| Total |               |          |          | 77000 | 103    |           |     |

### First BackChg

| Layer | Description   | Alm Code | Sub Code | Alm   | Actual | Deviation | %   |
|-------|---------------|----------|----------|-------|--------|-----------|-----|
| 1     | Bushling      | 16       |          | 2000  |        |           | 3%  |
| 2     | Turnings      |          |          | 10000 |        |           | 15% |
| 3     | Barge / Plate | 1        |          | 14000 | 14     |           | 22% |
|       | #1 Heavy      | 1        |          | 16000 | 18     |           | 25% |
|       | Mixed 1&2     | 7        |          | 8000  | 12     |           | 12% |
|       |               |          |          |       |        |           | 0%  |
|       |               |          |          |       |        |           | 0%  |
| 5     | Shredded      | 10       |          | 15000 | 6      |           | 23% |
| Total |               |          |          | 65000 | 55     |           |     |

### Second BackChg

| Layer | Description | Alm Code | Sub Code | Alm   | Actual | Deviation | %   |
|-------|-------------|----------|----------|-------|--------|-----------|-----|
| 1     | Mixed 1&2   | 7        |          | 14000 | 15     |           | 42% |
|       | Turnings    | 11       |          | 8000  | 7      |           | 9%  |
|       | Mill Crop   | 15       |          | 3000  |        |           | 12% |
|       | #1 Heavy    | 1        |          | 4000  |        |           | 24% |
|       | Shredded    |          |          | 4000  |        |           |     |
| Total |             |          |          | 33000 | 22     |           |     |

180



# Bayou Steel Corporation

## Heat Record

Crew: CDate: 7-23-04Grade: 436Melter: Duck1st Helper: USLadlieman: JBHeat #: 27250**Pulse Counter**1st Charge 7438656Last Charge 7441332

Tap To Tap Time

2:38 = 158 min.

Lost Time EQUALS Lost \$MONEY\$ !!!!!!!!!

Electrodes  
Ad. Slp. Bck

|   |  |  |
|---|--|--|
| A |  |  |
| B |  |  |
| C |  |  |

Previous Heat Tap: 12:34

|        | PON       | POFF        | kWh/ton |
|--------|-----------|-------------|---------|
| Headr  | <u>1"</u> | <u>1:24</u> | (220)   |
| 1 Back |           |             | (220)   |
| 2 Back |           |             |         |
| 3 Back |           |             |         |

Tap Start: 3:12 Tap Finish:

|          |              |             |
|----------|--------------|-------------|
| Power On | <u>36.0</u>  | LMF         |
| kWh      | <u>27480</u> | kWh         |
| kWh/Ton  | <u>310</u>   | kWh/Ton     |
| Plan     | <u>(360)</u> | Plan        |
|          |              | <u>(25)</u> |

| Ladle Data | Slr Info  |
|------------|-----------|
| Ladle No   | <u>8</u>  |
| Heats      | <u>96</u> |
| Temp       |           |
|            | Slr OK    |
|            | <u>Z</u>  |

Temperature Data (250) (250) (10)

| Time | kWh | Temp        | Carbon O2ppm |
|------|-----|-------------|--------------|
| 1    |     | <u>2977</u> | <u>9</u>     |
| 2    |     | <u>3150</u> |              |
| 3    |     |             |              |
| 4    |     |             |              |
| Edr  |     |             |              |

| EA Additions | Tap         | Trim            |
|--------------|-------------|-----------------|
| Lime         | <u>5000</u> | SiMn <u>260</u> |
| MgO          | <u>1800</u> | FeSi <u>175</u> |
| Chg C        |             | FeMn            |
| Foamy        | <u>26/9</u> | Coke            |
| Oxgyn        | <u>17</u>   | BPI             |
| N Gas        | <u>128</u>  | Lime <u>800</u> |
|              |             | De-Sul          |
|              |             | FeV             |
|              |             | FeAl            |
|              |             | CaC <u>50</u>   |
|              |             | SiC <u>100</u>  |
|              |             | GAH <u>200</u>  |

|                  |          |         |         |         |       |
|------------------|----------|---------|---------|---------|-------|
| Scrap Compliance |          |         |         |         |       |
| Material         | Location |         |         |         |       |
| Amount           |          |         |         |         |       |
| Scrap Compliance |          |         |         |         |       |
| Charge           | Header   | 1st Bck | 2nd Bck | 3rd Bck | TOTAL |
| Deviation        |          |         |         |         |       |

Never Be Satisfied says a Better Way

| Process Weights |          |           |
|-----------------|----------|-----------|
| Charge lbs      | Tap Tons | Cast Tons |
| 27,000          | @1       |           |

| Ladle Sent To |         |
|---------------|---------|
| To LMF        | St to C |
| ✓             |         |

**Chemistries**

|     | C           | Mn           | P         | S         | S            | Cr        | NI | Cr | Mo | Sn | V |
|-----|-------------|--------------|-----------|-----------|--------------|-----------|----|----|----|----|---|
| Aim | <u>8/13</u> | <u>70/85</u> | <u>40</u> | <u>50</u> | <u>10/26</u> | <u>60</u> |    |    |    |    |   |
| Rin |             |              |           |           |              |           |    |    |    |    |   |

**Procedure Compliance Summary**

|                   | Gol | Act | Dev | Reason (Use Delay Code & Description)   |
|-------------------|-----|-----|-----|-----------------------------------------|
| Tap               | 3   | 4   |     |                                         |
| Turn Around       | 2   | 33  | 31  |                                         |
| Power On          | 11  | 13  | 2   | <u>Add 1 slp Bt 1st Close slow line</u> |
| First BackCharge  | 2   |     |     | <u>A4-6</u>                             |
| Power On          | 8   |     |     |                                         |
| Second BackCharge | 2   |     |     |                                         |
| Power On          | 6   |     |     | <u>A1-2 3:09</u>                        |
| Third Back Charge | 0   |     |     |                                         |
| Power On          | 0   |     |     |                                         |
| Refine            | 11  |     |     |                                         |
| Total             | 45  |     |     |                                         |

Action items:

Maintenance Barriers:

Test # 3 2:00

# **Bayou Steel Corporation** **Scrap Blend Procedure**

Blend #65 3-Buckets

Heat# 27250

Date 7-22

Turn C

Oper C. C. Long

Foreman DLK

## **Header**

| Layer | Description   | Aim  |  | Sub  |  | Weights |        | Deviation | %   |
|-------|---------------|------|--|------|--|---------|--------|-----------|-----|
|       |               | Code |  | Code |  | Aim     | Actual |           |     |
| 1     | Bushling      | 16   |  |      |  | 0       |        |           | 0%  |
| 2     | Home Pit      | 12   |  |      |  | 7000    |        |           | 9%  |
| 3     | #2 Bundles    | 5    |  |      |  | 5000    |        |           | 6%  |
| 4     | Turnings      | 1    |  |      |  | 12000   |        |           | 16% |
|       | Barge / Plate | 1    |  |      |  | 17000   | 13     |           | 22% |
|       | #1 Heavy      | 7    |  |      |  | 13000   | 25     |           | 17% |
|       | Mixed 1&2     | 11   |  |      |  | 8000    | 17     |           | 10% |
|       |               |      |  |      |  |         |        |           | 0%  |
| 6     | Shredded      | 10   |  |      |  | 15000   | 15     |           | 19% |
| Total |               |      |  |      |  | 77000   | 60     |           |     |

## **First BackChg**

| Layer | Description   | Aim  |  | Sub  |  | Weights |        | Deviation | %   |
|-------|---------------|------|--|------|--|---------|--------|-----------|-----|
|       |               | Code |  | Code |  | Aim     | Actual |           |     |
| 1     | Bushling      | 16   |  |      |  | 2000    | 2      |           | 3%  |
| 2     | Turnings      |      |  |      |  | 10000   |        |           | 15% |
| 3     | Barge / Plate | 1    |  |      |  | 14000   | 19     |           | 22% |
|       | #1 Heavy      | 1    |  |      |  | 16000   | 21     |           | 25% |
|       | Mixed 1&2     | 7    |  |      |  | 8000    | 8      |           | 12% |
|       |               |      |  |      |  |         |        |           | 0%  |
|       |               |      |  |      |  |         |        |           | 0%  |
| 5     | Shredded      | 10   |  |      |  | 15000   | 15     |           | 23% |
| Total |               |      |  |      |  | 65000   | 65     |           |     |

## **Second BackChg**

| Layer | Description | Aim  |  | Sub  |  | Weights |        | Deviation | %   |
|-------|-------------|------|--|------|--|---------|--------|-----------|-----|
|       |             | Code |  | Code |  | Aim     | Actual |           |     |
| 1     | Mixed 1&2   | 7    |  |      |  | 14000   | 20     |           | 42% |
|       | Turnings    | 11   |  |      |  | 8000    |        |           | 8%  |
|       | Mill Crop   | 15   |  |      |  | 3000    |        |           | 12% |
|       | #1 Heavy    | 1    |  |      |  | 4000    |        |           | 24% |
|       | Shredded    |      |  |      |  | 4000    | 5      |           |     |
| Total |             |      |  |      |  | 33000   | 25     |           |     |

180



# Bayou Steel Corporation

## Heat Record

Crew: CDate: 7-23-04Grade: A36Melter: Duck1st Helper: WSLadleman: SBHeat #: 27251Electrodes  
Add Slip Bck

|   |  |  |  |
|---|--|--|--|
| A |  |  |  |
| B |  |  |  |
| C |  |  |  |

Pulse Counter

1st Charge 7141532Last Charge 7142634Tap To Tap Time 46

Lost Time EQUALS Lost \$MONEY\$ !!!!!!!!!

Previous Heat Tap: 3:12

|        | PON | POFF | kWh/ton |
|--------|-----|------|---------|
| Headr  |     |      | (220)   |
| 1 Back |     |      | (220)   |
| 2 Back |     |      |         |
| 3 Back |     |      |         |

Tap Start: 3:57 Tap Finish: 2:54

|          |              |         |      |
|----------|--------------|---------|------|
| Power On | <u>12.7</u>  | LMF     |      |
| kWh      | <u>10630</u> | kWh     |      |
| kWh/Ton  |              | kWh/Ton |      |
| Plan     | (360)        | Plan    | (25) |

|            |           |
|------------|-----------|
| Ladle Data | Stir OK   |
| Ladle No.  | <u>8</u>  |
| Heats      | <u>44</u> |
| Temp       |           |

Temperature Data: 1250 10

| Time | kWh | Temp        | Carbon    | O2ppm |
|------|-----|-------------|-----------|-------|
| 1    |     | <u>3069</u> | <u>10</u> |       |
| 2    |     | <u>3150</u> |           |       |
| 3    |     |             |           |       |
| 4    |     |             |           |       |
| Ldl  |     |             |           |       |

| EA Additions | Ladle Additions |
|--------------|-----------------|
| Lime         | 5000            |
| MgO          | 1800            |
| Chg C        |                 |
| Foamy        | 1026            |
| Oxygen       | 352             |
| N Gas        | 106             |
| SiMn         | 575             |
| FeSi         | 176             |
| FeMn         |                 |
| Coke         |                 |
| BPI          |                 |
| Lime         | 800             |
| De-Sul       |                 |
| FeV          |                 |
| FeAl         |                 |
| CaC          | 50              |
| SiC          | 100             |
| Al           | 200             |

| Material        | Location                             |
|-----------------|--------------------------------------|
| Amount          |                                      |
| Scan Compliance |                                      |
| Charge          | Header 1st Bck 2nd Bck 3rd Bck TOTAL |
| Deviation       |                                      |

Never Be Satisfied Always a Better Way

| Process Weights |          |           |
|-----------------|----------|-----------|
| Charge lbs      | Tap Tons | Cast Tons |
| 27,000          | 8.5      |           |

|              |         |
|--------------|---------|
| Ladle Sample |         |
| To LMF       | St to C |
| ✓            |         |

| Chemistries | C           | Mn           | P         | S         | Si           | CU        | Ni | Cr | Mo | Sn | V |
|-------------|-------------|--------------|-----------|-----------|--------------|-----------|----|----|----|----|---|
| Aim         | <u>8/13</u> | <u>70/65</u> | <u>40</u> | <u>50</u> | <u>18/26</u> | <u>50</u> |    |    |    |    |   |
| Rin         |             |              |           |           |              |           |    |    |    |    |   |

### Procedure Compliance Summary

|                    | Gal | Act | Dev | Reason | (Use Delay Code & Description) |
|--------------------|-----|-----|-----|--------|--------------------------------|
| Tap                | 3   |     |     |        |                                |
| Turn Around        | 2   |     |     |        |                                |
| Power On           | 11  |     |     |        |                                |
| First Back Charge  | 2   |     |     |        |                                |
| Power On           | 8   |     |     |        |                                |
| Second Back Charge | 2   |     |     |        |                                |
| Power On           | 6   |     |     |        |                                |
| Third Back Charge  | 0   |     |     |        |                                |
| Power On           | 0   |     |     |        |                                |
| Refine             | 11  |     |     |        |                                |
| Total              | 45  |     |     |        |                                |

Action Items:

Maintenance Barriers:

# **Bayou,Steel Corporation** **Scrap Blend Procedure**

Blend #65 3-Buckets

Heat# 27257

Date 7-22

Turn C

Oper Chris S.

Foreman. DUK

| Header |               | Alm  | Sub  | Weights |        |           |     |
|--------|---------------|------|------|---------|--------|-----------|-----|
| Layer  | Description   | Code | Code | Alm     | Actual | Deviation | %   |
| 1      | Bushling      | 16   |      | 0       |        |           | 0%  |
| 2      | Home Pit      | 12   |      | 7000    | ←      |           | 9%  |
| 3      | #2 Bundles    | 5    |      | 5000    |        |           | 6%  |
| 4      | Turnings      | 1    |      | 12000   | 15     |           | 16% |
|        | Barge / Plate | 1    |      | 17000   | 20     |           | 22% |
|        | #1 Heavy      | 7    |      | 13000   | 20     |           | 17% |
|        | Mixed 1&2     | 11   |      | 8000    | 20     |           | 10% |
|        |               |      |      |         |        |           | 0%  |
| 6      | Shredded      | 10   |      | 15000   | 16     |           | 19% |
| Total  |               |      |      | 77000   | 96     |           |     |

| First BackChg |               | Alm  | Sub  | Weights |        |           |     |
|---------------|---------------|------|------|---------|--------|-----------|-----|
| Layer         | Description   | Code | Code | Alm     | Actual | Deviation | %   |
| 1             | Bushling      | 16   |      | 2000    | 3      |           | 3%  |
| 2             | Turnings      |      |      | 10000   | 7      |           | 15% |
| 3             | Barge / Plate | 1    |      | 14000   | 2      |           | 22% |
|               | #1 Heavy      | 1    |      | 16000   | 15     |           | 25% |
|               | Mixed 1&2     | 7    |      | 8000    | 15     |           | 12% |
|               |               |      |      |         |        |           | 0%  |
|               |               |      |      |         |        |           | 0%  |
| 5             | Shredded      | 10   |      | 15000   | 11     |           | 23% |
| Total         |               |      |      | 65000   | 57     |           |     |

| Second BackChg |             | Alm  | Sub  | Weights |        |           |     |
|----------------|-------------|------|------|---------|--------|-----------|-----|
| Layer          | Description | Code | Code | Alm     | Actual | Deviation | %   |
| 1              | Mixed 1&2   | 7    |      | 14000   | 14     |           | 42% |
|                | Turnings    | 11   |      | 8000    |        |           | 9%  |
|                | Mill Crop   | 15   |      | 3000    | 6      |           | 12% |
|                | #1 Heavy    | 1    |      | 4000    | 4      |           | 24% |
|                | Shredded    |      |      | 4000    | 3      |           |     |
| Total          |             |      |      | 33000   | 27     |           |     |



# Bayou Steel Corporation

# Heat Record

Crew: CMelter: DuckDate: 7-23-041st Helper: WSGrade: A3652960Ladleman: TBHeat #: 27252

|            |         |
|------------|---------|
| Electrodes |         |
| Ad         | Slp/Brk |
| A          |         |
| B          |         |
| C          |         |

|                            |
|----------------------------|
| Pulse Counter              |
| 1st Charge <u>7142634</u>  |
| Last Charge <u>7144603</u> |

Tap To Tap Time 135

Lost Time EQUALS Lost \$MONEY\$ !!!!!!!!!!!!!

|                                |                       |
|--------------------------------|-----------------------|
| Previous Heat Tap: <u>3167</u> |                       |
| PON                            | POFF kWh/ton          |
| Headr <u>4:03</u>              | (220)                 |
| 1 Back                         | (220)                 |
| 2 Back                         |                       |
| 3 Back                         |                       |
| Tap Start <u>4:32</u>          | Tap Finish            |
| Power On <u>22.6</u>           | LME                   |
| kWh <u>17840</u>               | kWh                   |
| kWh/Ton                        | kWh/Ton               |
| Plan (360)                     | Plan (25)             |
| Ladle Data                     | Stir Info             |
| Ladle No. <u>4</u>             | Hts Pig <u>392</u>    |
| Heats <u>87</u>                | Stir OK               |
| Temp                           |                       |
| Temperature Data (300-1500)    |                       |
| Time kWh Temp Carbon O2ppm     |                       |
| 1 <u>4:24</u>                  | <u>3050</u> <u>7</u>  |
| 2                              |                       |
| 3                              | <u>3010</u> <u>10</u> |
| 4                              |                       |
| End                            |                       |

|                  |                  |                 |         |
|------------------|------------------|-----------------|---------|
| EAF Additions    |                  | Ladle Additions |         |
| Fe               | Tap              | Trim            |         |
| Lime <u>5000</u> | SiMn <u>1400</u> |                 |         |
| MgO <u>1300</u>  | FeSi <u>320</u>  |                 |         |
| Chg C            | FeMn             |                 |         |
| Foamy <u>928</u> | Coke             |                 |         |
| Oxygn <u>392</u> | BPI              |                 |         |
| N Gas <u>95</u>  | Lime <u>800</u>  |                 |         |
|                  | De Sul           |                 |         |
|                  | FeV              |                 |         |
|                  | FeAl             |                 |         |
|                  | CaC <u>50</u>    |                 |         |
|                  | SiC <u>100</u>   |                 |         |
|                  | Al <u>200</u>    |                 |         |
| Ginning Data     |                  |                 |         |
| Material         | Location         |                 |         |
| Amount           |                  |                 |         |
| Scrap Compliance |                  |                 |         |
| Charge           | Header           | 1st Bck         | 2nd Bck |
| Deviation        |                  |                 |         |
|                  | 3rd Bck          | TOTAL           |         |

Never Be Satisfied Always a Better Way

|                 |           |           |
|-----------------|-----------|-----------|
| Process Weights |           |           |
| Charge lbs      | Tap Tons  | Cast Tons |
| <u>96000</u>    | <u>74</u> |           |

|                |         |
|----------------|---------|
| Ladle Sampling |         |
| To LME         | St to C |
| <u>✓</u>       |         |

|             |            |              |           |           |              |           |    |    |    |    |              |
|-------------|------------|--------------|-----------|-----------|--------------|-----------|----|----|----|----|--------------|
| Chemistries |            |              |           |           |              |           |    |    |    |    |              |
|             | C          | Mn           | P         | S         | Si           | Cu        | Ni | Cr | Mo | Sn | V            |
| Aim         | <u>313</u> | <u>80/40</u> | <u>30</u> | <u>50</u> | <u>20/27</u> | <u>50</u> |    |    |    |    | <u>30/40</u> |
| Pin         |            |              |           |           |              |           |    |    |    |    |              |

## Procedure Compliance Summary

|                    | Got | Act | Dev | Reason | (Use Delay Code & Description) |
|--------------------|-----|-----|-----|--------|--------------------------------|
| Tap                | 3   | 3   |     |        |                                |
| Turn Around        | 2   | 3   |     |        |                                |
| Power On           | 11  |     |     |        |                                |
| First Back Charge  | 2   |     |     |        |                                |
| Power On           | 8   |     |     |        |                                |
| Second Back Charge | 2   |     |     |        |                                |
| Power On           | 6   |     |     |        |                                |
| Third Back Charge  | 0   |     |     |        |                                |
| Power On           | 0   |     |     |        |                                |
| Refine             | 11  |     |     |        |                                |
| Total              | 45  | 35  |     |        |                                |

## Action Items:

## Maintenance Barriers:

4<sup>th</sup> Test 4:04 p.m. (D.E.Q.)

# Bayou Steel Corporation Scrap Blend Procedure

Blend #65 3-Buckets

Heat# 27252

Date 7-23-04

Turn C

Oper Cowling

Foreman Over

| Header |               | Alm  | Sub  | Weights |        |           |     |
|--------|---------------|------|------|---------|--------|-----------|-----|
| Layer  | Description   | Code | Code | Alm     | Actual | Deviation | %   |
| 1      | Bushling      | 16   |      | 0       |        |           | 0%  |
| 2      | Home Plt      | 12   |      | 7000    | 6      |           | 9%  |
| 3      | #2 Bundles    | 5    |      | 5000    |        |           | 6%  |
| 4      | Turnings      | 1    |      | 12000   | 10     |           | 16% |
|        | Barge / Plate | 1    |      | 17000   | 20     |           | 22% |
|        | #1 Heavy      | 7    |      | 13000   | 20     |           | 17% |
|        | Mixed 1&2     | 11   |      | 8000    | 20     |           | 10% |
|        |               |      |      |         |        |           | 0%  |
| 6      | Shredded      | 10   |      | 15000   | 30     |           | 19% |
| Total  |               |      |      | 77000   | 96     |           |     |

See Heat # 257  
1st  
2nd

| First BackChg |               | Alm  | Sub  | Weights |        |           |     |
|---------------|---------------|------|------|---------|--------|-----------|-----|
| Layer         | Description   | Code | Code | Alm     | Actual | Deviation | %   |
| 1             | Bushling      | 16   |      | 2000    |        |           | 3%  |
| 2             | Turnings      |      |      | 10000   |        |           | 15% |
| 3             | Barge / Plate | 1    |      | 14000   |        |           | 22% |
|               | #1 Heavy      | 1    |      | 16000   |        |           | 25% |
|               | Mixed 1&2     | 7    |      | 8000    |        |           | 12% |
|               |               |      |      |         |        |           | 0%  |
|               |               |      |      |         |        |           | 0%  |
| 5             | Shredded      | 10   |      | 15000   |        |           | 23% |
| Total         |               |      |      | 65060   | 57     |           |     |

| Second BackChg |             | Alm  | Sub  | Weights |        |           |     |
|----------------|-------------|------|------|---------|--------|-----------|-----|
| Layer          | Description | Code | Code | Alm     | Actual | Deviation | %   |
| 1              | Mixed 1&2   | 7    |      | 14000   |        |           | 42% |
|                | Turnings    | 11   |      | 8000    |        |           | 8%  |
|                | Mill Crop   | 15   |      | 3000    |        |           | 12% |
|                | #1 Heavy    | 1    |      | 4000    |        |           | 24% |
|                | Shredded    |      |      | 4000    |        |           |     |
| Total          |             |      |      | 33000   | 27     |           |     |

180



# Bayou Steel Corporation

## Heat Record.

Crew: CMelter: DuckHeat #: 27253Date: 7-23-041st Helper: WSGrade: A36 (24.5)Ladleman: JBElectrodes  
Add Slip Bk

Pulse Counter

1st Charge 7144603Last Charge 7144585Tap To Tap Time 1:58

Lost Time EQUALS Lost \$MONEY\$ !!!!!!!!!!!!!

Previous Heat Tap: 432

|        | PON        | POFF       | kWh/ton          |
|--------|------------|------------|------------------|
| Headr  | <u>442</u> | <u>454</u> | (220) <u>175</u> |
| 1 Back | <u>456</u> | <u>504</u> | (220) <u>213</u> |
| 2 Back | <u>508</u> |            |                  |
| 3 Back |            |            |                  |

Tap Start 5:21 Tap Finish

|          | Power On    | kWh | kWh/Ton | Plan |
|----------|-------------|-----|---------|------|
| Power On | <u>2860</u> |     |         |      |
| kWh      | <u>319</u>  |     |         |      |
| kWh/Ton  |             |     |         |      |
| Plan     | (360)       |     |         | (25) |

|          | Ladle Data  | Slur Info |
|----------|-------------|-----------|
| Ladle No | <u>5</u>    | <u>4</u>  |
| Heats    | <u>14</u>   |           |
| Temp     | <u>1486</u> |           |

|   | Time        | kWh        | Temp        | Carbon    | O2ppm |
|---|-------------|------------|-------------|-----------|-------|
| 1 | <u>5:23</u> | <u>319</u> | <u>3010</u> | <u>12</u> |       |
| 2 |             |            |             |           |       |
| 3 |             |            | <u>3010</u> |           |       |
| 4 |             |            |             |           |       |

Never Be Satisfied Always a Better Way

| FAR Additions |             | Ladle Additions |                  |
|---------------|-------------|-----------------|------------------|
|               | Tap         | Trim            |                  |
| Lime          | <u>5000</u> |                 | SiMn <u>1765</u> |
| MgO           | <u>1000</u> |                 | FeSi <u>260</u>  |
| Chg C         |             |                 | FeMn             |
| Foamy         | <u>7256</u> |                 | Coke             |
| Oxygen        | <u>508</u>  |                 | BPI              |
| N Gas         | <u>173</u>  |                 | Lime <u>800</u>  |
|               |             |                 | De-Sul           |
|               |             |                 | FeV              |
|               |             |                 | FeAl             |
|               |             |                 | CaC <u>50</u>    |
|               |             |                 | SiC <u>100</u>   |
|               |             |                 | GA1 <u>200</u>   |

| Scrap Compliance |          |
|------------------|----------|
| Charge           | Header   |
| Deviation        | 96 57 27 |

| Process Weights |     |
|-----------------|-----|
| Charge lbs      | 170 |
| Tap Tons        | 87  |
| Cast Tons       |     |

| Ladle Sent To |   |
|---------------|---|
| To LMF        | ✓ |
| To C          |   |

| Chemistries |            |             |           |           |             |           |    |    |    |    |              |
|-------------|------------|-------------|-----------|-----------|-------------|-----------|----|----|----|----|--------------|
|             | Cl         | Mn          | P         | S         | Si          | Cu        | NI | Cr | Mo | Sn | V            |
| Aim         | <u>873</u> | <u>8450</u> | <u>30</u> | <u>50</u> | <u>2027</u> | <u>50</u> |    |    |    |    | <u>30-40</u> |
| Pin         |            |             |           |           |             |           |    |    |    |    |              |

### Procedure Compliance Summary

|                    | Gal | Act | Dev | Reason | (Use Delay Code & Description) |
|--------------------|-----|-----|-----|--------|--------------------------------|
| Tap                | 3   | 3   | -   |        |                                |
| Turn Around        | 2   | 7   | 5   | A-3    | John's                         |
| Power On           | 11  | 14  | 3   | A-4    | C                              |
| First Back Charge  | 2   | 2   | -   |        |                                |
| Power On           | 8   | 10  | 2   | A-6    | Ruro                           |
| Second Back Charge | 2   | 2   | -   |        |                                |
| Power On           | 6   |     |     |        |                                |
| Third Back Charge  | 0   | 5   | 5   | A-6    | honey bad                      |
| Power On           | 0   |     |     |        |                                |
| Refine             | 11  |     |     |        |                                |
| Total              | 45  | 58  | 13  |        |                                |

Action Items:

Maintenance Barriers:

# **Bayou Steel Corporation** **Scrap Blend Procedure**

Blend #65 3-Buckets

Heat# 27055

Date 7-23

Turn C

Oper Carroll

Foreman Ark

| Header |               | Alm  | Sub  | Weights |        |           |     |
|--------|---------------|------|------|---------|--------|-----------|-----|
| Layer  | Description   | Code | Code | Alm     | Actual | Deviation | %   |
| 1      | Bushling      | 16   |      | 0       |        |           | 0%  |
| 2      | Home Plt      | 12   |      | 7000    |        |           | 8%  |
| 3      | #2 Bundles    | 5    |      | 5000    |        |           | 6%  |
| 4      | Turnings      | 1    |      | 12000   | 10     |           | 16% |
|        | Barge / Plate | 1    |      | 17000   | 20     |           | 22% |
|        | #1 Heavy      | 7    |      | 13000   | 20     |           | 17% |
|        | Mixed 1&2     | 11   |      | 8000    | 20     |           | 10% |
|        |               |      |      |         |        |           | 0%  |
| 6      | Shredded      | 10   |      | 15000   | 20     |           | 19% |
| Total  |               |      |      | 77000   | 80     |           |     |

| First BackChg |               | Alm  | Sub  | Weights |        |           |     |
|---------------|---------------|------|------|---------|--------|-----------|-----|
| Layer         | Description   | Code | Code | Alm     | Actual | Deviation | %   |
| 1             | Bushling      | 16   |      | 2000    |        |           | 3%  |
| 2             | Turnings      |      |      | 10000   |        |           | 15% |
| 3             | Barge / Plate | 1    |      | 14000   | 16     |           | 22% |
|               | #1 Heavy      | 1    |      | 16000   | 8      |           | 25% |
|               | Mixed 1&2     | 7    |      | 8000    | 21     |           | 12% |
|               |               |      |      |         |        |           | 0%  |
|               |               |      |      |         |        |           | 0%  |
| 5             | Shredded      | 10   |      | 15000   | 17     |           | 23% |
| Total         |               |      |      | 65000   | 60     |           |     |

| Second BackChg |             | Alm  | Sub  | Weights |        |           |     |
|----------------|-------------|------|------|---------|--------|-----------|-----|
| Layer          | Description | Code | Code | Alm     | Actual | Deviation | %   |
| 1              | Mixed 1&2   | 7    |      | 14000   | 17     |           | 42% |
|                | Turnings    | 11   |      | 8000    |        |           | 9%  |
|                | Mill Crop   | 15   |      | 3000    | 10     |           | 12% |
|                | #1 Heavy    | 1    |      | 4000    | 6      |           | 24% |
|                | Shredded    |      |      | 4000    | 8      |           |     |
| Total          |             |      |      | 33000   | 41     |           |     |

191,000

EVR0001  
07/28/04

BAYOU STEEL CORPORATION  
FURNACE #1 & #2 TOTAL FLOW (SCFM) - EVERY 15 MIN

1  
08:11

| END<br>DATE<br>.... | END<br>TIME<br>.... | AVG<br>... | MAX<br>--- | MIN<br>--- |
|---------------------|---------------------|------------|------------|------------|
| 07/23/04            | 00:00:57            | 113,799.76 | 116,068.38 | 111,843.71 |
| 07/23/04            | 00:02:27            | 113,540.63 | 117,435.90 | 109,841.27 |
| 07/23/04            | 00:03:58            | 115,219.65 | 117,216.12 | 113,137.98 |
| 07/23/04            | 00:05:28            | 113,433.19 | 117,118.44 | 111,037.85 |
| 07/23/04            | 00:06:59            | 111,420.43 | 114,847.38 | 108,498.17 |
| 07/23/04            | 00:08:29            | 111,034.32 | 114,822.95 | 109,499.39 |
| 07/23/04            | 00:09:59            | 109,752.81 | 112,771.67 | 107,350.43 |
| 07/23/04            | 00:11:29            | 107,390.31 | 110,964.59 | 105,372.41 |
| 07/23/04            | 00:12:58            | 108,607.79 | 110,622.71 | 105,372.41 |
| 07/23/04            | 00:14:28            | 106,911.68 | 111,697.20 | 101,929.18 |
| 07/23/04            | 00:16:00            | 105,303.22 | 119,389.50 | 101,245.42 |
| 07/23/04            | 00:17:29            | 108,828.38 | 118,901.10 | 91,746.03  |
| 07/23/04            | 00:18:59            | 105,455.98 | 109,548.23 | 96,166.05  |
| 07/23/04            | 00:20:30            | 110,128.34 | 112,527.47 | 107,936.51 |
| 07/23/04            | 00:22:00            | 116,280.83 | 125,909.65 | 111,599.51 |
| 07/23/04            | 00:23:30            | 121,566.68 | 125,909.65 | 113,137.98 |
| 07/23/04            | 00:25:00            | 127,663.55 | 138,901.09 | 108,595.85 |
| 07/23/04            | 00:26:29            | 122,307.96 | 135,213.67 | 118,412.70 |
| 07/23/04            | 00:28:01            | 124,499.25 | 130,280.83 | 118,412.70 |
| 07/23/04            | 00:29:30            | 121,444.04 | 126,666.66 | 116,410.26 |
| 07/23/04            | 00:31:00            | 116,694.62 | 120,903.54 | 113,992.67 |
| 07/23/04            | 00:32:31            | 114,827.30 | 118,241.76 | 112,600.73 |
| 07/23/04            | 00:34:01            | 116,739.38 | 119,023.20 | 114,334.55 |
| 07/23/04            | 00:35:31            | 113,813.32 | 116,752.14 | 111,257.63 |
| 07/23/04            | 00:37:01            | 112,672.63 | 116,434.68 | 109,865.69 |
| 07/23/04            | 00:38:30            | 111,369.15 | 117,509.16 | 109,157.51 |
| 07/23/04            | 00:40:02            | 109,806.81 | 111,306.47 | 107,643.47 |
| 07/23/04            | 00:41:31            | 103,418.26 | 112,478.63 | 90,744.81  |
| 07/23/04            | 00:43:01            | 110,545.92 | 124,957.27 | 79,096.46  |
| 07/23/04            | 00:44:32            | 114,684.30 | 123,980.46 | 109,890.11 |
| 07/23/04            | 00:46:02            | 110,379.87 | 115,238.09 | 107,448.11 |
| 07/23/04            | 00:47:32            | 108,935.83 | 112,258.85 | 106,031.74 |
| 07/23/04            | 00:49:02            | 108,861.21 | 110,476.19 | 105,811.97 |
| 07/23/04            | 00:50:33            | 110,736.95 | 113,479.85 | 105,543.34 |
| 07/23/04            | 00:52:03            | 109,708.31 | 113,382.17 | 107,081.80 |
| 07/23/04            | 00:53:32            | 99,998.10  | 112,429.79 | 89,035.41  |
| 07/23/04            | 00:55:02            | 111,537.65 | 126,080.59 | 82,319.90  |
| 07/23/04            | 00:56:33            | 111,760.95 | 115,286.94 | 109,499.39 |
| 07/23/04            | 00:58:03            | 115,833.67 | 120,952.38 | 110,598.29 |
| 07/23/04            | 00:59:33            | 111,517.02 | 113,504.27 | 109,304.03 |
| 07/23/04            | 01:01:02            | 108,835.71 | 113,626.38 | 105,641.02 |
| 07/23/04            | 01:02:33            | 108,997.15 | 112,136.75 | 104,664.23 |
| 07/23/04            | 01:04:03            | 112,094.97 | 114,114.77 | 109,059.83 |
| 07/23/04            | 01:05:34            | 109,267.95 | 111,477.41 | 107,032.97 |
| 07/23/04            | 01:07:04            | 109,026.45 | 114,578.76 | 107,032.97 |
| 07/23/04            | 01:08:34            | 106,242.03 | 115,286.94 | 100,634.92 |
| 07/23/04            | 01:10:04            | 109,588.39 | 116,337.00 | 101,050.06 |
| 07/23/04            | 01:11:33            | 110,203.77 | 119,951.16 | 102,222.22 |
| 07/23/04            | 01:13:03            | 107,521.64 | 113,089.13 | 95,042.73  |
| 07/23/04            | 01:14:34            | 102,347.58 | 109,084.25 | 91,086.69  |
| 07/23/04            | 01:16:04            | 108,452.59 | 112,576.31 | 104,786.33 |
| 07/23/04            | 01:17:35            | 114,318.00 | 123,858.37 | 103,785.10 |
| 07/23/04            | 01:19:05            | 122,761.63 | 125,396.83 | 115,457.88 |

EVR0001  
07/28/04

BAYOU STEEL CORPORATION  
FURNACE #1 & #2 TOTAL FLOW (SCFM) - EVERY 15 MIN

2  
08:11

| END<br>DATE<br>.... | END<br>TIME<br>.... | AVG<br>... | MAX<br>... | MIN        |
|---------------------|---------------------|------------|------------|------------|
| 07/23/04            | 01:20:35            | 125,521.09 | 137,753.36 | 105,006.10 |
| 07/23/04            | 01:22:05            | 126,494.91 | 133,455.44 | 122,197.80 |
| 07/23/04            | 01:23:34            | 119,804.09 | 123,467.64 | 115,628.81 |
| 07/23/04            | 01:25:06            | 115,115.45 | 117,704.52 | 112,039.07 |
| 07/23/04            | 01:26:35            | 118,042.05 | 122,783.88 | 114,188.03 |
| 07/23/04            | 01:28:05            | 116,005.97 | 118,998.78 | 113,308.91 |
| 07/23/04            | 01:29:36            | 116,844.39 | 119,780.22 | 114,310.13 |
| 07/23/04            | 01:31:06            | 115,585.40 | 119,560.44 | 111,965.81 |
| 07/23/04            | 01:32:36            | 117,140.14 | 120,048.84 | 114,285.71 |
| 07/23/04            | 01:34:06            | 113,241.89 | 120,317.46 | 103,418.80 |
| 07/23/04            | 01:35:37            | 116,621.90 | 132,674.00 | 100,244.20 |
| 07/23/04            | 01:37:07            | 128,470.22 | 134,139.19 | 122,442.00 |
| 07/23/04            | 01:38:36            | 119,835.57 | 127,032.97 | 114,871.80 |
| 07/23/04            | 01:40:06            | 116,649.03 | 120,952.38 | 114,896.22 |
| 07/23/04            | 01:41:37            | 116,735.59 | 120,952.38 | 111,819.29 |
| 07/23/04            | 01:43:07            | 116,562.74 | 122,026.86 | 114,236.88 |
| 07/23/04            | 01:44:37            | 115,189.52 | 117,338.22 | 113,431.02 |
| 07/23/04            | 01:46:07            | 107,330.08 | 119,169.72 | 93,919.41  |
| 07/23/04            | 01:47:38            | 112,600.19 | 127,374.84 | 98,144.08  |
| 07/23/04            | 01:49:08            | 118,873.70 | 124,737.48 | 114,114.77 |
| 07/23/04            | 01:50:37            | 115,863.52 | 119,316.24 | 112,136.75 |
| 07/23/04            | 01:52:07            | 175,333.60 | 119,218.56 | 111,941.39 |
| 07/23/04            | 01:53:38            | 115,762.85 | 118,559.22 | 113,137.98 |
| 07/23/04            | 01:55:08            | 115,648.08 | 118,021.98 | 110,622.71 |
| 07/23/04            | 01:56:38            | 116,897.30 | 118,852.26 | 113,211.23 |
| 07/23/04            | 01:58:08            | 114,200.52 | 118,779.00 | 110,549.45 |
| 07/23/04            | 01:59:39            | 113,815.22 | 117,020.76 | 108,937.73 |
| 07/23/04            | 02:01:09            | 113,255.73 | 116,288.16 | 109,719.17 |
| 07/23/04            | 02:02:38            | 112,691.36 | 116,874.23 | 109,865.69 |
| 07/23/04            | 02:04:08            | 117,175.15 | 120,830.28 | 113,015.88 |
| 07/23/04            | 02:05:39            | 121,146.66 | 125,689.87 | 116,385.84 |
| 07/23/04            | 02:07:09            | 119,957.40 | 124,371.19 | 114,554.34 |
| 07/23/04            | 02:08:38            | 114,070.27 | 120,366.30 | 106,666.66 |
| 07/23/04            | 02:10:08            | 119,374.84 | 126,837.61 | 115,360.20 |
| 07/23/04            | 02:11:40            | 115,308.91 | 121,416.36 | 107,277.16 |
| 07/23/04            | 02:13:10            | 117,237.28 | 120,781.44 | 111,452.99 |
| 07/23/04            | 02:14:39            | 105,604.94 | 118,632.48 | 95,848.59  |
| 07/23/04            | 02:16:09            | 113,497.22 | 117,509.16 | 110,989.01 |
| 07/23/04            | 02:17:40            | 119,636.41 | 130,085.47 | 108,034.19 |
| 07/23/04            | 02:19:10            | 125,164.29 | 129,279.61 | 118,827.84 |
| 07/23/04            | 02:20:39            | 129,477.41 | 141,953.61 | 103,003.66 |
| 07/23/04            | 02:22:11            | 127,739.25 | 134,798.53 | 121,660.56 |
| 07/23/04            | 02:23:41            | 120,086.55 | 125,299.15 | 116,776.55 |
| 07/23/04            | 02:25:11            | 118,068.10 | 126,178.27 | 116,190.48 |
| 07/23/04            | 02:26:40            | 118,913.85 | 126,178.27 | 115,018.31 |
| 07/23/04            | 02:28:10            | 117,956.86 | 119,926.74 | 114,676.44 |
| 07/23/04            | 02:29:41            | 115,074.21 | 120,537.24 | 112,722.84 |
| 07/23/04            | 02:31:11            | 112,335.64 | 118,852.26 | 109,987.79 |
| 07/23/04            | 02:32:40            | 103,516.48 | 116,263.73 | 92,039.07  |
| 07/23/04            | 02:34:12            | 107,429.66 | 120,610.50 | 94,261.30  |
| 07/23/04            | 02:35:42            | 125,435.90 | 137,680.09 | 107,741.15 |
| 07/23/04            | 02:37:12            | 117,657.58 | 124,224.66 | 114,969.48 |
| 07/23/04            | 02:38:41            | 113,782.12 | 117,777.78 | 111,623.93 |

EVRO001  
07/28/04

BAYOU STEEL CORPORATION  
FURNACE #1 & #2 TOTAL FLOW (SCFM) - EVERY 15 MIN

3  
08:11

| END<br>DATE<br>---- | END<br>TIME<br>---- | AVG<br>--- | MAX<br>--- | MIN<br>--- |
|---------------------|---------------------|------------|------------|------------|
| 07/23/04            | 02:40:11            | 114,029.30 | 116,996.34 | 111,062.27 |
| 07/23/04            | 02:41:42            | 112,124.00 | 114,505.49 | 108,766.79 |
| 07/23/04            | 02:43:12            | 102,842.77 | 114,505.49 | 92,551.89  |
| 07/23/04            | 02:44:41            | 107,334.96 | 110,891.33 | 103,614.16 |
| 07/23/04            | 02:46:13            | 114,573.09 | 128,083.03 | 105,152.63 |
| 07/23/04            | 02:47:42            | 121,482.84 | 123,394.38 | 115,213.67 |
| 07/23/04            | 02:49:13            | 120,795.28 | 126,080.59 | 117,411.48 |
| 07/23/04            | 02:50:43            | 122,256.14 | 128,742.37 | 118,192.92 |
| 07/23/04            | 02:52:12            | 123,604.66 | 127,008.55 | 120,146.52 |
| 07/23/04            | 02:53:43            | 118,111.79 | 121,221.00 | 114,749.70 |
| 07/23/04            | 02:55:13            | 115,936.23 | 117,948.72 | 114,090.35 |
| 07/23/04            | 02:56:44            | 114,987.66 | 117,240.54 | 110,964.59 |
| 07/23/04            | 02:58:14            | 115,524.63 | 121,758.24 | 112,087.91 |
| 07/23/04            | 02:59:43            | 116,120.47 | 121,758.24 | 112,210.02 |
| 07/23/04            | 03:01:13            | 113,608.20 | 116,361.41 | 110,549.45 |
| 07/23/04            | 03:02:44            | 112,603.45 | 117,362.64 | 110,354.09 |
| 07/23/04            | 03:04:14            | 110,460.45 | 117,362.64 | 104,102.56 |
| 07/23/04            | 03:05:44            | 110,706.01 | 120,683.76 | 97,313.80  |
| 07/23/04            | 03:07:14            | 110,806.95 | 115,824.18 | 106,910.87 |
| 07/23/04            | 03:08:45            | 117,554.20 | 123,125.77 | 112,478.63 |
| 07/23/04            | 03:10:15            | 122,218.15 | 131,819.30 | 111,721.61 |
| 07/23/04            | 03:11:44            | 124,764.62 | 129,792.43 | 119,755.80 |
| 07/23/04            | 03:13:14            | 129,368.61 | 141,465.20 | 109,181.93 |
| 07/23/04            | 03:14:45            | 127,805.73 | 133,357.75 | 124,981.69 |
| 07/23/04            | 03:16:15            | 124,209.20 | 129,157.51 | 120,439.56 |
| 07/23/04            | 03:17:45            | 119,557.18 | 124,420.02 | 116,459.09 |
| 07/23/04            | 03:19:15            | 118,425.72 | 122,612.95 | 115,579.98 |
| 07/23/04            | 03:20:46            | 121,082.08 | 123,492.06 | 117,631.26 |
| 07/23/04            | 03:22:16            | 121,606.84 | 126,617.83 | 118,266.18 |
| 07/23/04            | 03:23:45            | 121,071.50 | 124,078.14 | 117,753.36 |
| 07/23/04            | 03:25:15            | 118,800.16 | 120,879.12 | 115,677.66 |
| 07/23/04            | 03:26:46            | 110,345.41 | 119,072.04 | 98,852.26  |
| 07/23/04            | 03:28:16            | 115,062.54 | 119,682.54 | 109,865.69 |
| 07/23/04            | 03:29:47            | 123,608.47 | 137,118.44 | 104,664.23 |
| 07/23/04            | 03:31:17            | 120,651.74 | 125,641.02 | 118,779.00 |
| 07/23/04            | 03:32:47            | 128,875.32 | 137,655.67 | 119,511.60 |
| 07/23/04            | 03:34:17            | 123,997.55 | 129,768.01 | 118,925.52 |
| 07/23/04            | 03:35:46            | 119,812.23 | 121,587.30 | 117,826.62 |
| 07/23/04            | 03:37:18            | 121,281.51 | 123,956.05 | 117,216.12 |
| 07/23/04            | 03:38:47            | 124,694.62 | 126,446.88 | 121,514.04 |
| 07/23/04            | 03:40:17            | 118,707.91 | 123,467.64 | 112,380.95 |
| 07/23/04            | 03:41:48            | 109,639.67 | 118,754.58 | 99,462.76  |
| 07/23/04            | 03:43:18            | 118,132.41 | 129,059.83 | 99,316.24  |
| 07/23/04            | 03:44:48            | 125,266.86 | 131,062.27 | 120,170.94 |
| 07/23/04            | 03:46:18            | 118,773.03 | 121,904.77 | 116,483.52 |
| 07/23/04            | 03:47:49            | 117,366.71 | 120,952.38 | 109,328.45 |
| 07/23/04            | 03:49:19            | 119,162.94 | 123,223.45 | 114,358.98 |
| 07/23/04            | 03:50:48            | 115,132.00 | 117,558.00 | 110,134.31 |
| 07/23/04            | 03:52:18            | 115,501.29 | 118,974.36 | 110,647.13 |
| 07/23/04            | 03:53:49            | 117,460.05 | 123,052.50 | 114,920.63 |
| 07/23/04            | 03:55:19            | 114,487.86 | 118,412.70 | 112,673.99 |
| 07/23/04            | 03:56:49            | 113,637.50 | 115,433.45 | 112,283.27 |
| 07/23/04            | 03:58:19            | 113,780.22 | 117,069.59 | 112,234.43 |

EVR0001  
07/28/04

B A Y O U S T E E L C O R P O R A T I O N  
FURNACE #1 & #2 TOTAL FLOW (SCFM) - EVERY 15 MIN

4  
08:11

| END<br>DATE<br>---- | END<br>TIME<br>---- | AVG<br>--- | MAX<br>--- | MIN<br>--- |
|---------------------|---------------------|------------|------------|------------|
| 07/23/04            | 03:59:50            | 113,397.91 | 115,311.35 | 108,693.53 |
| 07/23/04            | 04:01:19            | 103,785.65 | 108,693.53 | 96,581.20  |
| 07/23/04            | 04:02:50            | 109,491.79 | 115,238.09 | 106,959.70 |
| 07/23/04            | 04:04:20            | 117,574.28 | 131,282.05 | 109,890.11 |
| 07/23/04            | 04:05:50            | 122,492.20 | 125,592.19 | 115,604.40 |
| 07/23/04            | 04:07:20            | 126,603.99 | 133,064.72 | 121,343.10 |
| 07/23/04            | 04:08:49            | 129,477.41 | 133,431.02 | 124,053.73 |
| 07/23/04            | 04:10:19            | 128,084.38 | 131,746.03 | 123,223.45 |
| 07/23/04            | 04:11:50            | 133,962.56 | 136,581.20 | 129,670.33 |
| 07/23/04            | 04:13:20            | 133,937.33 | 137,191.70 | 131,135.53 |
| 07/23/04            | 04:14:51            | 134,768.69 | 139,194.14 | 132,503.05 |
| 07/23/04            | 04:16:21            | 135,828.78 | 138,901.09 | 131,550.67 |
| 07/23/04            | 04:17:51            | 135,926.47 | 138,949.94 | 132,576.31 |
| 07/23/04            | 04:19:21            | 137,007.19 | 138,779.00 | 135,360.20 |
| 07/23/04            | 04:20:50            | 135,910.73 | 140,390.72 | 132,796.09 |
| 07/23/04            | 04:22:20            | 136,193.45 | 141,050.06 | 130,451.77 |
| 07/23/04            | 04:23:51            | 136,063.77 | 139,633.70 | 132,991.45 |
| 07/23/04            | 04:25:21            | 136,757.56 | 143,174.61 | 133,601.95 |
| 07/23/04            | 04:26:52            | 138,527.20 | 150,280.83 | 119,633.70 |
| 07/23/04            | 04:28:22            | 139,115.19 | 148,669.11 | 133,089.14 |
| 07/23/04            | 04:29:52            | 130,961.34 | 134,822.95 | 127,301.59 |
| 07/23/04            | 04:31:22            | 126,419.21 | 130,256.41 | 121,880.34 |
| 07/23/04            | 04:32:51            | 124,495.45 | 126,788.77 | 122,271.06 |
| 07/23/04            | 04:34:23            | 127,247.32 | 130,378.51 | 125,250.30 |
| 07/23/04            | 04:35:52            | 122,821.60 | 125,860.80 | 120,341.88 |
| 07/23/04            | 04:37:22            | 121,609.01 | 126,105.01 | 119,072.04 |
| 07/23/04            | 04:38:53            | 113,595.71 | 121,245.42 | 99,194.14  |
| 07/23/04            | 04:40:23            | 115,921.59 | 121,709.40 | 110,769.23 |
| 07/23/04            | 04:41:53            | 122,726.36 | 137,777.78 | 117,118.44 |
| 07/23/04            | 04:43:23            | 132,191.30 | 144,786.33 | 107,887.66 |
| 07/23/04            | 04:44:52            | 125,062.54 | 129,841.27 | 121,978.02 |
| 07/23/04            | 04:46:24            | 121,745.49 | 124,493.28 | 120,317.46 |
| 07/23/04            | 04:47:53            | 123,188.98 | 126,275.95 | 117,924.30 |
| 07/23/04            | 04:49:23            | 122,789.85 | 126,349.20 | 118,656.90 |
| 07/23/04            | 04:50:54            | 116,648.76 | 120,268.62 | 112,551.89 |
| 07/23/04            | 04:52:24            | 111,313.80 | 120,317.46 | 96,043.95  |
| 07/23/04            | 04:53:54            | 107,668.98 | 115,042.73 | 92,893.77  |
| 07/23/04            | 04:55:24            | 122,594.22 | 130,989.01 | 92,893.77  |
| 07/23/04            | 04:56:53            | 118,329.40 | 121,123.32 | 114,529.91 |
| 07/23/04            | 04:58:25            | 116,601.82 | 120,366.30 | 112,307.70 |
| 07/23/04            | 04:59:54            | 116,614.84 | 119,145.30 | 113,455.43 |
| 07/23/04            | 05:01:24            | 115,254.10 | 119,194.14 | 111,452.99 |
| 07/23/04            | 05:02:55            | 112,373.63 | 116,849.82 | 109,914.53 |
| 07/23/04            | 05:04:25            | 112,185.32 | 115,482.30 | 109,694.75 |
| 07/23/04            | 05:05:54            | 112,016.55 | 115,482.30 | 109,426.13 |
| 07/23/04            | 05:07:25            | 113,930.54 | 116,849.82 | 112,161.17 |
| 07/23/04            | 05:08:56            | 109,194.68 | 115,384.62 | 105,421.24 |
| 07/23/04            | 05:10:26            | 111,262.52 | 118,510.38 | 106,959.70 |
| 07/23/04            | 05:11:55            | 104,779.81 | 111,819.29 | 98,485.96  |
| 07/23/04            | 05:13:25            | 102,627.05 | 112,112.34 | 85,225.88  |
| 07/23/04            | 05:14:56            | 113,902.86 | 118,437.12 | 103,882.78 |
| 07/23/04            | 05:16:26            | 112,200.52 | 117,191.70 | 102,808.30 |
| 07/23/04            | 05:17:55            | 112,662.05 | 116,459.09 | 109,157.51 |

EVR0001  
07/28/04

BAYOU STEEL CORPORATION  
FURNACE #1 & #2 TOTAL FLOW (SCFM) - EVERY 15 MIN

5  
08:11

| END<br>DATE | END<br>TIME | AVG        | MAX        | MIN        |
|-------------|-------------|------------|------------|------------|
| ----        | ----        | ---        | ---        | ---        |
| 07/23/04    | 05:19:25    | 116,338.35 | 121,172.16 | 111,501.83 |
| 07/23/04    | 05:20:57    | 124,637.09 | 131,404.16 | 114,798.53 |
| 07/23/04    | 05:22:27    | 125,795.96 | 128,595.85 | 121,587.30 |
| 07/23/04    | 05:23:56    | 127,941.39 | 141,001.22 | 123,492.06 |
| 07/23/04    | 05:25:26    | 131,479.31 | 143,003.66 | 105,689.87 |
| 07/23/04    | 05:26:57    | 126,696.24 | 133,260.08 | 122,490.84 |
| 07/23/04    | 05:28:27    | 119,833.67 | 123,907.20 | 117,020.76 |
| 07/23/04    | 05:29:56    | 120,957.80 | 123,931.63 | 118,388.28 |
| 07/23/04    | 05:31:26    | 122,754.58 | 128,034.19 | 117,631.26 |
| 07/23/04    | 05:32:58    | 121,644.28 | 126,031.74 | 119,413.92 |
| 07/23/04    | 05:34:28    | 116,209.20 | 120,000.00 | 113,040.30 |
| 07/23/04    | 05:35:57    | 108,928.77 | 118,437.12 | 96,825.40  |
| 07/23/04    | 05:37:27    | 115,045.72 | 120,293.04 | 109,304.03 |
| 07/23/04    | 05:38:58    | 119,555.55 | 124,932.84 | 114,065.94 |
| 07/23/04    | 05:40:28    | 128,306.88 | 137,680.09 | 109,523.81 |
| 07/23/04    | 05:41:57    | 128,254.78 | 133,382.17 | 124,542.13 |
| 07/23/04    | 05:43:27    | 122,107.99 | 126,715.51 | 118,608.06 |
| 07/23/04    | 05:44:58    | 121,359.38 | 125,763.13 | 117,899.88 |
| 07/23/04    | 05:46:29    | 121,842.09 | 125,152.63 | 119,316.24 |
| 07/23/04    | 05:47:58    | 118,023.06 | 124,688.65 | 113,772.89 |
| 07/23/04    | 05:49:28    | 116,163.07 | 119,877.90 | 98,290.60  |
| 07/23/04    | 05:50:59    | 107,594.36 | 114,139.20 | 98,266.18  |
| 07/23/04    | 05:52:29    | 112,798.80 | 117,704.52 | 103,931.63 |
| 07/23/04    | 05:53:58    | 118,792.30 | 122,393.16 | 113,748.48 |
| 07/23/04    | 05:55:30    | 122,115.86 | 135,824.17 | 106,813.19 |
| 07/23/04    | 05:57:00    | 131,442.14 | 141,050.06 | 124,029.30 |
| 07/23/04    | 05:58:30    | 122,860.40 | 127,203.91 | 117,289.38 |
| 07/23/04    | 05:59:99    | 122,309.59 | 126,349.20 | 116,166.05 |
| 07/23/04    | 06:01:30    | 122,949.66 | 126,788.77 | 120,610.50 |
| 07/23/04    | 06:03:00    | 120,799.62 | 124,981.69 | 117,484.73 |
| 07/23/04    | 06:04:30    | 116,792.56 | 119,072.04 | 114,505.49 |
| 07/23/04    | 06:06:00    | 115,095.10 | 116,703.30 | 112,527.47 |
| 07/23/04    | 06:07:31    | 113,915.07 | 115,677.66 | 111,330.89 |
| 07/23/04    | 06:09:01    | 112,256.14 | 115,091.58 | 107,155.07 |
| 07/23/04    | 06:10:30    | 110,850.36 | 114,505.49 | 107,155.07 |
| 07/23/04    | 06:12:00    | 111,699.63 | 113,431.02 | 108,937.73 |
| 07/23/04    | 06:13:31    | 112,302.80 | 115,311.35 | 110,061.05 |
| 07/23/04    | 06:15:01    | 109,930.81 | 112,063.49 | 106,642.25 |
| 07/23/04    | 06:16:31    | 102,446.62 | 107,301.59 | 94,017.09  |
| 07/23/04    | 06:18:01    | 104,700.59 | 107,838.83 | 99,438.34  |
| 07/23/04    | 06:19:32    | 110,501.97 | 116,776.55 | 103,369.96 |
| 07/23/04    | 06:21:02    | 116,377.42 | 119,926.74 | 112,576.31 |
| 07/23/04    | 06:22:31    | 119,053.32 | 124,151.41 | 114,920.63 |
| 07/23/04    | 06:24:01    | 121,437.52 | 124,957.27 | 117,264.96 |
| 07/23/04    | 06:25:32    | 126,727.45 | 146,788.77 | 103,809.52 |
| 07/23/04    | 06:27:02    | 129,346.36 | 134,285.72 | 123,247.86 |
| 07/23/04    | 06:28:32    | 128,137.30 | 132,503.05 | 123,980.46 |
| 07/23/04    | 06:30:03    | 122,983.86 | 126,568.98 | 118,192.92 |
| 07/23/04    | 06:31:33    | 119,580.79 | 121,636.14 | 117,655.68 |
| 07/23/04    | 06:33:03    | 118,641.70 | 122,173.38 | 116,361.41 |
| 07/23/04    | 06:34:32    | 119,060.38 | 122,173.38 | 116,727.72 |
| 07/23/04    | 06:36:02    | 117,685.52 | 122,466.42 | 114,358.98 |
| 07/23/04    | 06:37:33    | 116,027.95 | 119,780.22 | 113,235.66 |

EVR0001  
07/28/04

B A Y O U S T E E L C O R P O R A T I O N  
FURNACE #1 & #2 TOTAL FLOW (SCFM) - EVERY 15 MIN

6  
08:11

| END<br>DATE<br>.... | END<br>TIME<br>.... | AVG<br>... | MAX<br>... | MIN<br>... |
|---------------------|---------------------|------------|------------|------------|
| 07/23/04            | 06:39:03            | 113,168.36 | 116,141.63 | 109,621.49 |
| 07/23/04            | 06:40:33            | 103,337.95 | 114,432.23 | 95,091.58  |
| 07/23/04            | 06:42:04            | 112,558.41 | 126,886.45 | 96,239.31  |
| 07/23/04            | 06:43:34            | 116,668.30 | 121,611.72 | 111,282.05 |
| 07/23/04            | 06:45:04            | 113,954.15 | 116,996.34 | 108,913.31 |
| 07/23/04            | 06:46:33            | 113,741.42 | 115,457.88 | 111,697.20 |
| 07/23/04            | 06:48:03            | 115,058.20 | 118,119.66 | 111,575.09 |
| 07/23/04            | 06:49:34            | 116,249.09 | 118,070.82 | 114,627.59 |
| 07/23/04            | 06:51:04            | 113,222.09 | 118,534.80 | 109,474.97 |
| 07/23/04            | 06:52:34            | 102,605.34 | 110,183.15 | 91,159.95  |
| 07/23/04            | 06:54:05            | 112,049.38 | 128,327.23 | 95,555.55  |
| 07/23/04            | 06:55:35            | 117,648.35 | 122,930.41 | 114,481.08 |
| 07/23/04            | 06:57:05            | 111,670.05 | 114,481.08 | 108,424.91 |
| 07/23/04            | 06:58:34            | 116,317.73 | 119,658.12 | 112,625.16 |
| 07/23/04            | 07:00:05            | 115,629.09 | 118,803.42 | 112,600.73 |
| 07/23/04            | 07:01:35            | 112,051.28 | 114,969.48 | 109,450.55 |
| 07/23/04            | 07:03:05            | 110,574.41 | 113,846.16 | 106,910.87 |
| 07/23/04            | 07:04:34            | 108,220.05 | 111,159.95 | 105,909.65 |
| 07/23/04            | 07:06:06            | 110,206.48 | 112,796.09 | 106,446.88 |
| 07/23/04            | 07:07:35            | 107,519.20 | 110,769.23 | 105,128.20 |
| 07/23/04            | 07:09:05            | 107,140.69 | 111,819.29 | 103,809.52 |
| 07/23/04            | 07:10:36            | 97,324.11  | 105,909.65 | 89,328.45  |
| 07/23/04            | 07:12:06            | 98,616.74  | 107,985.35 | 89,328.45  |
| 07/23/04            | 07:13:36            | 105,886.85 | 112,625.16 | 100,512.82 |
| 07/23/04            | 07:15:06            | 113,240.80 | 120,781.44 | 107,301.59 |
| 07/23/04            | 07:16:37            | 116,539.14 | 127,301.59 | 112,063.49 |
| 07/23/04            | 07:18:07            | 124,595.58 | 133,528.69 | 86,739.93  |
| 07/23/04            | 07:19:36            | 121,367.25 | 128,107.45 | 116,581.20 |
| 07/23/04            | 07:21:06            | 115,913.98 | 118,119.66 | 113,162.39 |
| 07/23/04            | 07:22:37            | 114,758.65 | 118,827.84 | 112,503.05 |
| 07/23/04            | 07:24:07            | 113,874.91 | 119,365.08 | 109,206.35 |
| 07/23/04            | 07:25:37            | 113,205.80 | 117,631.26 | 109,133.09 |
| 07/23/04            | 07:27:07            | 113,395.20 | 118,144.08 | 109,499.39 |
| 07/23/04            | 07:28:38            | 114,295.21 | 117,387.05 | 111,184.38 |
| 07/23/04            | 07:30:08            | 114,439.56 | 119,877.90 | 110,964.59 |
| 07/23/04            | 07:31:37            | 108,165.78 | 115,482.30 | 96,630.04  |
| 07/23/04            | 07:33:07            | 112,335.37 | 116,971.91 | 108,009.77 |
| 07/23/04            | 07:34:38            | 113,587.30 | 118,656.90 | 109,670.33 |
| 07/23/04            | 07:36:08            | 119,418.80 | 122,051.28 | 116,605.62 |
| 07/23/04            | 07:37:38            | 125,200.38 | 143,174.61 | 108,058.61 |
| 07/23/04            | 07:39:08            | 129,942.75 | 143,174.61 | 122,979.24 |
| 07/23/04            | 07:40:39            | 120,599.65 | 125,470.09 | 117,704.52 |
| 07/23/04            | 07:42:09            | 118,339.71 | 122,832.73 | 114,822.95 |
| 07/23/04            | 07:43:38            | 119,320.58 | 123,833.95 | 115,995.12 |
| 07/23/04            | 07:45:08            | 118,421.38 | 122,832.73 | 115,360.20 |
| 07/23/04            | 07:46:39            | 114,745.90 | 116,947.50 | 112,380.95 |
| 07/23/04            | 07:48:09            | 108,437.12 | 115,921.86 | 92,087.91  |
| 07/23/04            | 07:49:39            | 104,813.19 | 116,849.82 | 89,768.01  |
| 07/23/04            | 07:51:10            | 119,514.86 | 123,565.32 | 111,575.09 |
| 07/23/04            | 07:52:40            | 113,758.24 | 118,046.40 | 112,063.49 |
| 07/23/04            | 07:54:10            | 112,538.87 | 117,875.46 | 108,009.77 |
| 07/23/04            | 07:55:39            | 115,720.26 | 118,876.68 | 111,379.73 |
| 07/23/04            | 07:57:09            | 112,066.20 | 118,632.48 | 108,498.17 |

EVR0001  
07/28/04

BAYOU STEEL CORPORATION  
FURNACE #1 & #2 TOTAL FLOW (SCFM) - EVERY 15 MIN

7  
08:11

| END<br>DATE | END<br>TIME | AVG        | MAX        | MIN        |
|-------------|-------------|------------|------------|------------|
| 07/23/04    | 07:58:40    | 111,698.82 | 115,409.04 | 108,766.79 |
| 07/23/04    | 08:00:10    | 108,213.00 | 112,503.05 | 104,664.23 |
| 07/23/04    | 08:01:39    | 109,128.20 | 112,967.03 | 105,030.52 |
| 07/23/04    | 08:03:11    | 108,121.83 | 110,085.47 | 106,202.69 |
| 07/23/04    | 08:04:41    | 103,032.97 | 109,719.17 | 98,876.68  |
| 07/23/04    | 08:06:11    | 101,964.45 | 105,836.38 | 99,511.60  |
| 07/23/04    | 08:07:40    | 106,322.62 | 111,868.13 | 101,831.50 |
| 07/23/04    | 08:09:10    | 97,921.86  | 104,908.42 | 93,504.27  |
| 07/23/04    | 08:10:41    | 100,797.45 | 107,765.57 | 96,947.50  |
| 07/23/04    | 08:12:11    | 107,000.13 | 109,133.09 | 104,420.02 |
| 07/23/04    | 08:13:40    | 110,661.51 | 122,612.95 | 91,990.23  |
| 07/23/04    | 08:15:12    | 122,735.59 | 133,724.05 | 81,416.36  |
| 07/23/04    | 08:16:41    | 117,785.38 | 124,200.24 | 114,652.02 |
| 07/23/04    | 08:18:12    | 114,354.63 | 117,826.62 | 107,203.91 |
| 07/23/04    | 08:19:41    | 108,720.12 | 114,700.85 | 102,148.96 |
| 07/23/04    | 08:21:11    | 110,897.57 | 116,166.05 | 104,981.69 |
| 07/23/04    | 08:22:42    | 112,626.78 | 116,678.88 | 109,328.45 |
| 07/23/04    | 08:24:12    | 108,273.51 | 111,282.05 | 104,713.06 |
| 07/23/04    | 08:25:41    | 108,065.12 | 110,109.89 | 105,909.65 |
| 07/23/04    | 08:27:13    | 100,245.55 | 108,205.13 | 89,255.19  |
| 07/23/04    | 08:28:42    | 103,292.63 | 118,779.00 | 83,858.37  |
| 07/23/04    | 08:30:13    | 108,862.02 | 116,825.40 | 99,609.28  |
| 07/23/04    | 08:31:44    | 109,329.27 | 113,333.34 | 100,683.76 |
| 07/23/04    | 08:33:15    | 106,704.66 | 112,796.09 | 99,658.12  |
| 07/23/04    | 08:34:45    | 107,605.48 | 111,965.81 | 99,169.72  |
| 07/23/04    | 08:36:15    | 109,801.93 | 112,405.38 | 107,350.43 |
| 07/23/04    | 08:37:44    | 96,913.58  | 110,427.35 | 85,885.23  |
| 07/23/04    | 08:39:14    | 108,495.45 | 118,363.86 | 82,222.22  |
| 07/23/04    | 08:40:45    | 115,126.85 | 117,167.27 | 112,234.43 |
| 07/23/04    | 08:42:15    | 110,062.41 | 114,456.66 | 108,498.17 |
| 07/23/04    | 08:43:46    | 110,648.48 | 114,529.91 | 107,374.84 |
| 07/23/04    | 08:45:16    | 107,231.04 | 109,523.81 | 104,786.33 |
| 07/23/04    | 08:46:46    | 106,837.61 | 109,670.33 | 103,760.69 |
| 07/23/04    | 08:48:16    | 106,005.97 | 109,890.11 | 103,101.34 |
| 07/23/04    | 08:49:45    | 101,265.77 | 105,665.45 | 96,239.31  |
| 07/23/04    | 08:51:17    | 105,438.88 | 111,990.23 | 96,019.54  |
| 07/23/04    | 08:52:46    | 103,950.62 | 106,813.19 | 101,025.64 |
| 07/23/04    | 08:54:16    | 102,862.57 | 107,326.01 | 98,461.54  |
| 07/23/04    | 08:55:47    | 104,375.26 | 110,354.09 | 95,262.52  |
| 07/23/04    | 08:57:17    | 97,711.30  | 107,106.23 | 90,671.55  |
| 07/23/04    | 08:58:47    | 102,041.79 | 116,190.48 | 80,903.54  |
| 07/23/04    | 09:00:16    | 108,582.28 | 115,335.77 | 101,123.32 |
| 07/23/04    | 09:01:47    | 96,357.34  | 105,689.87 | 81,611.72  |
| 07/23/04    | 09:03:18    | 101,543.89 | 109,963.37 | 86,691.09  |
| 07/23/04    | 09:04:48    | 109,563.16 | 115,213.67 | 105,030.52 |
| 07/23/04    | 09:06:17    | 111,918.33 | 124,273.51 | 97,313.80  |
| 07/23/04    | 09:07:48    | 120,888.62 | 130,622.71 | 93,284.49  |
| 07/23/04    | 09:09:18    | 119,507.53 | 124,468.87 | 116,874.23 |
| 07/23/04    | 09:10:47    | 114,287.07 | 119,487.18 | 110,915.75 |
| 07/23/04    | 09:12:17    | 113,743.05 | 117,020.76 | 111,037.85 |
| 07/23/04    | 09:13:48    | 110,061.05 | 112,429.79 | 106,666.66 |
| 07/23/04    | 09:15:18    | 109,957.95 | 113,162.39 | 102,783.88 |
| 07/23/04    | 09:16:49    | 111,183.02 | 117,704.52 | 106,544.57 |

EVR0001  
07/28/04

B A Y O U S T E E L C O R P O R A T I O N  
FURNACE #1 & #2 TOTAL FLOW (SCFM) - EVERY 15 MIN

8  
08:11

| END<br>DATE<br>.... | END<br>TIME<br>.... | AVG<br>--- | MAX<br>---  | MIN<br>--- |
|---------------------|---------------------|------------|-------------|------------|
| 07/23/04            | 09:18:18            | 105,410.39 | log, 694.75 | 88,669.11  |
| 07/23/04            | 09:19:49            | 99,342.02  | 102,954.82  | 91,208.79  |
| 07/23/04            | 09:21:19            | 110,014.92 | 115,897.44  | 84,884.01  |
| 07/23/04            | 09:22:48            | 111,999.73 | 114,803.17  | 110,500.61 |
| 07/23/04            | 09:24:18            | 109,461.41 | 112,234.43  | 104,957.27 |
| 07/23/04            | 09:25:49            | 105,882.52 | 111,379.73  | 101,294.26 |
| 07/23/04            | 09:27:19            | 112,606.16 | 120,170.94  | 107,399.27 |
| 07/23/04            | 09:28:50            | 107,841.54 | 116,630.04  | 93,357.75  |
| 07/23/04            | 09:30:20            | 107,286.66 | 121,245.42  | 94,163.62  |
| 07/23/04            | 09:31:50            | 119,618.77 | 125,738.70  | 113,089.13 |
| 07/23/04            | 09:33:20            | 115,504.00 | 119,169.72  | 110,647.13 |
| 07/23/04            | 09:34:49            | 110,291.69 | 113,333.34  | 107,155.07 |
| 07/23/04            | 09:36:19            | 109,160.22 | 112,112.34  | 104,688.65 |
| 07/23/04            | 09:37:50            | 107,054.87 | 112,722.84  | 99,780.22  |
| 07/23/04            | 09:39:20            | 104,396.96 | 109,865.69  | 97,728.94  |
| 07/23/04            | 09:40:51            | 107,855.11 | 110,061.05  | 105,543.34 |
| 07/23/04            | 09:42:21            | 104,661.51 | 110,451.77  | 94,554.34  |
| 07/23/04            | 09:43:51            | 101,014.79 | 108,278.39  | 96,556.77  |
| 07/23/04            | 09:45:21            | 105,691.22 | 108,840.05  | 101,489.63 |
| 07/23/04            | 09:46:50            | 104,376.61 | 107,936.51  | 99,658.12  |
| 07/23/04            | 09:48:20            | 104,592.32 | 109,670.33  | 101,001.22 |
| 07/23/04            | 09:49:51            | 102,737.76 | 107,252.75  | 94,822.95  |
| 07/23/04            | 09:51:21            | 97,983.99  | 102,979.24  | 94,725.27  |
| 07/23/04            | 09:52:52            | 92,553.25  | 106,031.74  | 77,558.00  |
| 07/23/04            | 09:54:22            | 94,566.55  | 105,838.38  | 67,448.11  |
| 07/23/04            | 09:55:52            | 102,448.79 | 112,893.77  | 90,573.87  |
| 07/23/04            | 09:57:22            | 108,038.26 | 115,604.40  | 102,564.10 |
| 07/23/04            | 09:58:51            | 109,325.73 | 114,945.05  | 104,664.23 |
| 07/23/04            | 10:00:21            | 117,286.66 | 121,880.34  | 109,523.81 |
| 07/23/04            | 10:01:52            | 115,757.70 | 128,766.79  | 93,333.34  |
| 07/23/04            | 10:03:22            | 127,383.99 | 134,529.92  | 111,452.99 |
| 07/23/04            | 10:04:53            | 118,521.23 | 122,954.82  | 113,455.43 |
| 07/23/04            | 10:06:23            | 117,171.34 | 121,001.22  | 113,821.73 |
| 07/23/04            | 10:07:52            | 112,307.70 | 115,506.72  | 109,084.25 |
| 07/23/04            | 10:09:23            | 110,123.45 | 115,653.23  | 101,294.26 |
| 07/23/04            | 10:10:52            | 112,383.66 | 118,876.68  | 105,763.13 |
| 07/23/04            | 10:12:22            | 109,918.60 | 111,990.23  | 105,177.05 |
| 07/23/04            | 10:13:53            | 103,880.07 | 111,721.61  | 94,407.81  |
| 07/23/04            | 10:15:23            | 100,009.50 | 102,002.45  | 94,725.27  |
| 07/23/04            | 10:16:54            | 96,058.88  | 118,412.70  | 46,837.61  |
| 07/23/04            | 10:18:24            | 114,074.07 | 119,389.50  | 109,426.13 |
| 07/23/04            | 10:19:53            | 109,023.20 | 113,894.99  | 102,661.78 |
| 07/23/04            | 10:21:24            | 113,808.16 | 116,727.72  | 108,888.89 |
| 07/23/04            | 10:22:54            | 112,010.58 | 116,923.08  | 106,739.93 |
| 07/23/04            | 10:24:25            | 109,959.30 | 117,460.32  | 105,470.09 |
| 07/23/04            | 10:25:54            | 100,127.52 | 109,670.33  | 93,601.95  |
| 07/23/04            | 10:27:24            | 108,134.58 | 116,971.91  | 90,109.89  |
| 07/23/04            | 10:28:55            | 113,021.03 | 114,896.22  | 109,816.85 |
| 07/23/04            | 10:30:25            | 112,719.58 | 115,702.08  | 107,838.83 |
| 07/23/04            | 10:31:56            | 109,467.64 | 113,113.55  | 106,666.66 |
| 07/23/04            | 10:33:26            | 110,204.31 | 112,820.52  | 107,765.57 |
| 07/23/04            | 10:34:56            | 110,859.86 | 114,749.70  | 108,400.49 |
| 07/23/04            | 10:36:26            | 108,195.36 | 111,452.99  | 105,909.65 |

EVR0001  
07/28/04

BAYOU STEEL CORPORATION  
FURNACE #1 & #2 TOTAL FLOW (SCFM) - EVERY 15 MIN

9  
08:11

| END<br>DATE<br>---- | END<br>TIME<br>---- | AVG<br>--- | MAX<br>--- | MIN<br>--- |
|---------------------|---------------------|------------|------------|------------|
| 07/23/04            | 10:37:55            | 106,339.44 | 109,108.67 | 102,930.41 |
| 07/23/04            | 10:39:25            | 105,823.63 | 108,693.53 | 102,124.54 |
| 07/23/04            | 10:40:56            | 105,244.34 | 110,061.05 | 99,853.48  |
| 07/23/04            | 10:42:26            | 102,211.37 | 107,960.93 | 94,920.63  |
| 07/23/04            | 10:43:57            | 101,326.82 | 104,639.80 | 95,995.12  |
| 07/23/04            | 10:45:27            | 102,278.66 | 105,860.80 | 97,948.72  |
| 07/23/04            | 10:46:57            | 103,480.13 | 109,279.61 | 97,191.70  |
| 07/23/04            | 10:48:27            | 103,148.55 | 110,573.87 | 94,188.03  |
| 07/23/04            | 10:49:56            | 98,348.94  | 102,759.46 | 90,866.91  |
| 07/23/04            | 10:51:28            | 97,853.75  | 103,614.16 | 88,693.53  |
| 07/23/04            | 10:52:57            | 108,947.77 | 116,923.08 | 98,705.74  |
| 07/23/04            | 10:54:27            | 112,530.73 | 124,200.24 | 105,543.34 |
| 07/23/04            | 10:55:58            | 118,811.02 | 130,818.07 | 93,431.02  |
| 07/23/04            | 10:57:28            | 113,422.60 | 123,540.91 | 97,362.64  |
| 07/23/04            | 10:58:58            | 112,289.52 | 117,387.05 | 99,145.30  |
| 07/23/04            | 11:00:27            | 111,766.11 | 115,115.99 | 107,277.16 |
| 07/23/04            | 11:01:58            | 109,178.40 | 113,040.30 | 105,128.20 |
| 07/23/04            | 11:03:28            | 108,397.23 | 112,283.27 | 103,003.66 |
| 07/23/04            | 11:04:59            | 103,261.70 | 107,277.16 | 99,096.46  |
| 07/23/04            | 11:06:29            | 103,969.88 | 111,746.03 | 96,141.63  |
| 07/23/04            | 11:07:59            | 95,055.76  | 106,398.05 | 76,971.91  |
| 07/23/04            | 11:09:29            | 107,305.38 | 117,411.48 | 100,366.30 |
| 07/23/04            | 11:11:01            | 113,014.79 | 125,616.61 | 91,306.47  |
| 07/23/04            | 11:12:30            | 110,752.95 | 115,286.94 | 106,251.52 |
| 07/23/04            | 11:14:00            | 105,558.00 | 113,382.17 | 98,217.34  |
| 07/23/04            | 11:15:31            | 107,406.32 | 110,402.93 | 102,442.00 |
| 07/23/04            | 11:17:01            | 109,349.07 | 113,846.16 | 105,738.70 |
| 07/23/04            | 11:18:30            | 96,989.55  | 109,304.03 | 81,538.46  |
| 07/23/04            | 11:20:01            | 97,898.52  | 114,822.95 | 81,440.78  |
| 07/23/04            | 11:21:31            | 106,878.04 | 112,869.35 | 98,339.44  |
| 07/23/04            | 11:23:02            | 108,009.77 | 112,918.20 | 104,004.88 |
| 07/23/04            | 11:24:31            | 105,566.41 | 111,575.09 | 98,998.78  |
| 07/23/04            | 11:26:01            | 106,792.56 | 115,238.09 | 101,978.02 |
| 07/23/04            | 11:27:32            | 106,790.66 | 110,427.35 | 104,371.19 |
| 07/23/04            | 11:29:02            | 106,808.84 | 108,937.73 | 103,272.28 |
| 07/23/04            | 11:30:31            | 103,779.68 | 108,522.59 | 100,146.52 |
| 07/23/04            | 11:32:01            | 101,603.04 | 103,882.78 | 98,827.84  |
| 07/23/04            | 11:33:32            | 103,349.07 | 106,935.29 | 99,047.62  |
| 07/23/04            | 11:35:03            | 99,651.06  | 102,319.90 | 95,409.04  |
| 07/23/04            | 11:36:32            | 101,769.09 | 107,985.35 | 96,068.38  |
| 07/23/04            | 11:38:02            | 101,152.90 | 103,980.46 | 99,023.20  |
| 07/23/04            | 11:39:33            | 98,361.15  | 102,637.36 | 91,452.99  |
| 07/23/04            | 11:41:03            | 95,039.48  | 101,587.30 | 87,326.01  |
| 07/23/04            | 11:42:32            | 97,791.34  | 105,787.55 | 88,449.33  |
| 07/23/04            | 11:44:02            | 106,493.55 | 113,992.67 | 100,586.08 |
| 07/23/04            | 11:45:33            | 107,849.41 | 114,212.45 | 103,052.50 |
| 07/23/04            | 11:47:04            | 111,359.92 | 118,388.28 | 105,250.30 |
| 07/23/04            | 11:48:33            | 117,484.47 | 124,053.73 | 109,450.55 |
| 07/23/04            | 11:50:03            | 118,073.53 | 126,398.05 | 111,599.51 |
| 07/23/04            | 11:51:34            | 115,049.52 | 132,551.89 | 104,688.65 |
| 07/23/04            | 11:53:04            | 131,892.83 | 142,319.91 | 120,854.70 |
| 07/23/04            | 11:54:33            | 120,384.48 | 123,663.00 | 113,284.49 |
| 07/23/04            | 11:56:03            | 112,704.38 | 114,017.09 | 111,111.11 |

EVR0001  
07/28/04

BAYOU STEEL CORPORATION  
FURNACE #1 8 #2 TOTAL FLOW (SCFM) - EVERY 15 MIN

10  
08:11

| END<br>DATE<br>---- | END<br>TIME<br>---- | AVG<br>--- | MAX<br>--- | MIN<br>--- |
|---------------------|---------------------|------------|------------|------------|
| 07/23/04            | 11:57:34            | 110,716.87 | 113,821.73 | 106,129.43 |
| 07/23/04            | 11:59:05            | 111,226.97 | 113,724.05 | 106,129.43 |
| 07/23/04            | 12:00:35            | 113,238.09 | 116,459.09 | 108,229.55 |
| 07/23/04            | 12:02:05            | 110,153.58 | 114,261.30 | 105,250.30 |
| 07/23/04            | 12:03:35            | 103,684.16 | 111,941.39 | 86,227.11  |
| 07/23/04            | 12:05:05            | 97,268.48  | 100,366.30 | 92,454.21  |
| 07/23/04            | 12:06:34            | 106,751.59 | 119,365.08 | 50,940.17  |
| 07/23/04            | 12:08:04            | 114,004.61 | 118,461.54 | 107,228.33 |
| 07/23/04            | 12:09:35            | 110,729.07 | 113,772.89 | 106,471.30 |
| 07/23/04            | 12:11:05            | 105,660.84 | 108,595.85 | 98,803.42  |
| 07/23/04            | 12:12:36            | 105,310.54 | 110,427.35 | 99,755.80  |
| 07/23/04            | 12:14:06            | 105,612.80 | 108,498.17 | 103,272.28 |
| 07/23/04            | 12:15:36            | 98,183.15  | 108,302.80 | 88,424.91  |
| 07/23/04            | 12:17:06            | 108,221.95 | 117,387.05 | 88,131.87  |
| 07/23/04            | 12:18:35            | 112,482.70 | 116,727.72 | 105,323.56 |
| 07/23/04            | 12:20:05            | 107,568.30 | 114,212.45 | 103,443.23 |
| 07/23/04            | 12:21:36            | 108,036.90 | 111,501.83 | 103,565.32 |
| 07/23/04            | 12:23:06            | 108,751.59 | 112,918.20 | 104,688.65 |
| 07/23/04            | 12:24:37            | 105,897.71 | 110,842.49 | 101,514.04 |
| 07/23/04            | 12:26:07            | 107,267.95 | 112,576.31 | 100,830.28 |
| 07/23/04            | 12:27:37            | 105,227.52 | 112,576.31 | 99,975.58  |
| 07/23/04            | 12:29:07            | 103,620.67 | 109,426.13 | 97,484.73  |
| 07/23/04            | 12:30:36            | 102,500.88 | 109,450.55 | 98,388.28  |
| 07/23/04            | 12:32:06            | 103,540.91 | 108,205.13 | 99,047.62  |
| 07/23/04            | 12:33:37            | 105,361.55 | 108,009.77 | 102,686.20 |
| 07/23/04            | 12:35:07            | 101,825.53 | 105,152.63 | 97,777.78  |
| 07/23/04            | 12:36:38            | 102,316.10 | 108,131.87 | 95,164.84  |
| 07/23/04            | 12:38:08            | 101,067.97 | 104,004.88 | 99,072.04  |
| 07/23/04            | 12:39:38            | 101,645.64 | 109,670.33 | 91,233.21  |
| 07/23/04            | 12:41:08            | 110,024.42 | 117,680.10 | 94,529.91  |
| 07/23/04            | 12:42:37            | 115,562.34 | 119,438.34 | 110,402.93 |
| 07/23/04            | 12:44:07            | 120,172.02 | 127,081.80 | 113,846.16 |
| 07/23/04            | 12:45:38            | 115,677.93 | 119,609.28 | 111,819.29 |
| 07/23/04            | 12:47:08            | 118,437.39 | 123,199.02 | 114,383.39 |
| 07/23/04            | 12:48:39            | 120,405.10 | 123,638.59 | 112,136.75 |
| 07/23/04            | 12:50:09            | 123,791.62 | 128,131.87 | 118,583.64 |
| 07/23/04            | 12:51:39            | 121,747.66 | 127,423.69 | 116,581.20 |
| 07/23/04            | 12:53:09            | 128,772.48 | 134,358.97 | 119,731.38 |
| 07/23/04            | 12:54:38            | 128,722.02 | 131,916.97 | 122,246.64 |
| 07/23/04            | 12:56:08            | 130,843.30 | 133,968.25 | 128,302.80 |
| 07/23/04            | 12:57:39            | 130,350.29 | 136,947.50 | 126,471.30 |
| 07/23/04            | 12:59:09            | 131,676.58 | 137,094.02 | 127,863.25 |
| 07/23/04            | 13:00:40            | 130,524.48 | 136,703.30 | 119,853.48 |
| 07/23/04            | 13:02:10            | 128,301.45 | 138,681.31 | 120,293.04 |
| 07/23/04            | 13:03:39            | 136,471.58 | 142,832.72 | 132,063.48 |
| 07/23/04            | 13:05:09            | 136,498.72 | 142,393.16 | 130,231.99 |
| 07/23/04            | 13:06:40            | 136,221.41 | 139,487.17 | 131,623.94 |
| 07/23/04            | 13:08:10            | 141,083.44 | 145,518.92 | 137,973.14 |
| 07/23/04            | 13:09:41            | 141,400.08 | 144,810.75 | 139,120.88 |
| 07/23/04            | 13:11:11            | 142,623.25 | 145,958.48 | 140,024.42 |
| 07/23/04            | 13:12:41            | 139,660.02 | 152,771.67 | 129,084.25 |
| 07/23/04            | 13:14:11            | 143,266.58 | 154,505.50 | 132,918.19 |
| 07/23/04            | 13:15:40            | 134,204.05 | 136,385.84 | 131,746.03 |

EVR0001  
07/28/04

BAYOU STEEL CORPORATION  
FURNACE #1 & #2 TOTAL FLOW (SCFM) - EVERY 15 MIN

11  
08:11

| END<br>DATE<br>---- | END<br>TIME<br>---- | AVG<br>--- | MAX<br>--- | MIN<br>--- |
|---------------------|---------------------|------------|------------|------------|
| 07/23/04            | 13:17:10            | 133,255.45 | 135,775.33 | 129,450.55 |
| 07/23/04            | 13:18:41            | 133,100.80 | 139,560.44 | 127,032.97 |
| 07/23/04            | 13:20:11            | 131,181.66 | 136,630.03 | 125,738.70 |
| 07/23/04            | 13:21:42            | 126,507.39 | 129,719.17 | 122,148.96 |
| 07/23/04            | 13:23:12            | 123,121.96 | 125,811.97 | 119,291.82 |
| 07/23/04            | 13:24:42            | 119,783.48 | 122,271.06 | 118,217.34 |
| 07/23/04            | 13:26:12            | 114,265.37 | 119,755.80 | 99,926.74  |
| 07/23/04            | 13:27:41            | 110,150.59 | 124,566.55 | 103,076.92 |
| 07/23/04            | 13:29:11            | 115,090.76 | 124,566.55 | 102,442.00 |
| 07/23/04            | 13:30:42            | 123,626.91 | 126,495.73 | 120,561.66 |
| 07/23/04            | 13:32:12            | 123,370.51 | 126,520.15 | 121,172.16 |
| 07/23/04            | 13:33:43            | 127,247.32 | 130,891.33 | 123,418.80 |
| 07/23/04            | 13:35:13            | 131,054.13 | 135,750.92 | 128,107.45 |
| 07/23/04            | 13:36:43            | 134,021.44 | 136,923.08 | 131,916.97 |
| 07/23/04            | 13:38:13            | 136,160.09 | 138,412.70 | 134,065.94 |
| 07/23/04            | 13:39:42            | 138,440.64 | 141,587.30 | 134,285.72 |
| 07/23/04            | 13:41:12            | 140,377.70 | 144,615.39 | 136,752.14 |
| 07/23/04            | 13:42:43            | 140,718.77 | 151,062.27 | 128,376.07 |
| 07/23/04            | 13:44:13            | 141,343.92 | 144,737.48 | 138,779.00 |
| 07/23/04            | 13:45:44            | 142,282.19 | 145,616.61 | 140,586.08 |
| 07/23/04            | 13:47:14            | 140,736.67 | 144,200.25 | 138,339.44 |
| 07/23/04            | 13:48:44            | 141,613.89 | 145,567.77 | 138,779.00 |
| 07/23/04            | 13:50:14            | 143,302.13 | 145,934.06 | 141,636.14 |
| 07/23/04            | 13:51:43            | 144,249.89 | 145,738.70 | 142,222.22 |
| 07/23/04            | 13:53:13            | 144,588.25 | 147,081.81 | 142,637.36 |
| 07/23/04            | 13:54:44            | 147,832.59 | 149,768.02 | 144,395.61 |
| 07/23/04            | 13:56:14            | 146,837.88 | 150,402.94 | 144,493.28 |
| 07/23/04            | 13:57:45            | 147,072.31 | 149,645.91 | 144,297.92 |
| 07/23/04            | 13:59:15            | 147,657.84 | 151,892.55 | 143,028.08 |
| 07/23/04            | 14:00:44            | 148,827.03 | 158,730.16 | 137,802.20 |
| 07/23/04            | 14:02:14            | 148,043.69 | 151,941.39 | 146,031.75 |
| 07/23/04            | 14:03:45            | 148,425.72 | 153,455.44 | 145,934.06 |
| 07/23/04            | 14:05:15            | 149,205.81 | 152,136.75 | 145,641.03 |
| 07/23/04            | 14:06:45            | 150,364.94 | 153,479.86 | 147,032.97 |
| 07/23/04            | 14:08:15            | 150,163.08 | 153,943.83 | 146,739.92 |
| 07/23/04            | 14:09:46            | 151,674.94 | 156,190.47 | 149,206.34 |
| 07/23/04            | 14:11:16            | 149,459.50 | 152,576.31 | 146,813.19 |
| 07/23/04            | 14:12:45            | 149,805.72 | 152,356.53 | 147,057.39 |
| 07/23/04            | 14:14:15            | 151,610.64 | 155,189.25 | 149,279.61 |
| 07/23/04            | 14:15:46            | 152,813.19 | 154,676.44 | 148,595.84 |
| 07/23/04            | 14:17:16            | 151,414.19 | 155,726.50 | 148,595.84 |
| 07/23/04            | 14:18:47            | 151,616.33 | 153,992.67 | 148,864.47 |
| 07/23/04            | 14:20:16            | 152,254.52 | 155,457.88 | 148,913.31 |
| 07/23/04            | 14:21:47            | 151,413.64 | 154,627.59 | 148,327.23 |
| 07/23/04            | 14:23:17            | 152,711.17 | 155,116.00 | 150,989.02 |
| 07/23/04            | 14:24:46            | 153,920.23 | 155,970.70 | 151,379.73 |
| 07/23/04            | 14:26:16            | 151,868.13 | 154,065.94 | 149,328.45 |
| 07/23/04            | 14:27:47            | 151,677.11 | 153,357.75 | 150,085.47 |
| 07/23/04            | 14:29:17            | 153,300.23 | 155,286.94 | 150,989.02 |
| 07/23/04            | 14:30:48            | 153,487.17 | 156,117.22 | 151,282.05 |
| 07/23/04            | 14:32:17            | 153,286.66 | 156,605.61 | 151,135.53 |
| 07/23/04            | 14:33:48            | 154,145.98 | 157,802.20 | 151,868.13 |
| 07/23/04            | 14:35:18            | 154,532.36 | 156,825.39 | 152,527.47 |

EVR0001  
07/28/04

BAYOU STEEL CORPORATION  
FURNACE #1 & #2 TOTAL FLOW (SCFM) - EVERY 15 MIN

12  
08:11

| END<br>DATE<br>---- | END<br>TIME<br>---- | AVG<br>--- | MAX<br>--- | MIN<br>--- |
|---------------------|---------------------|------------|------------|------------|
| 07/23/04            | 14:36:47            | 154,751.05 | 157,973.14 | 152,649.58 |
| 07/23/04            | 14:38:17            | 153,358.03 | 156,776.56 | 150,256.41 |
| 07/23/04            | 14:39:48            | 154,388.00 | 157,826.63 | 150,354.09 |
| 07/23/04            | 14:41:18            | 153,768.83 | 156,410.25 | 151,233.22 |
| 07/23/04            | 14:42:49            | 152,787.69 | 156,483.52 | 150,109.89 |
| 07/23/04            | 14:44:19            | 154,730.97 | 157,045.17 | 152,576.31 |
| 07/23/04            | 14:45:49            | 154,849.81 | 165,738.70 | 145,470.08 |
| 07/23/04            | 14:47:19            | 156,090.89 | 159,706.95 | 154,285.72 |
| 07/23/04            | 14:48:48            | 153,973.95 | 155,848.59 | 151,062.27 |
| 07/23/04            | 14:50:18            | 152,856.33 | 155,116.00 | 150,842.48 |
| 07/23/04            | 14:51:49            | 151,428.58 | 155,116.00 | 149,743.59 |
| 07/23/04            | 14:53:19            | 151,548.77 | 158,095.23 | 143,833.94 |
| 07/23/04            | 14:54:50            | 141,555.56 | 147,887.67 | 136,190.47 |
| 07/23/04            | 14:56:20            | 136,456.92 | 140,586.08 | 134,578.75 |
| 07/23/04            | 14:57:50            | 131,737.63 | 134,822.95 | 128,644.69 |
| 07/23/04            | 14:59:20            | 130,350.56 | 132,503.05 | 127,252.75 |
| 07/23/04            | 15:00:49            | 124,790.40 | 130,598.29 | 121,611.72 |
| 07/23/04            | 15:02:19            | 124,240.40 | 127,228.33 | 120,830.28 |
| 07/23/04            | 15:03:50            | 121,990.50 | 126,495.73 | 118,730.16 |
| 07/23/04            | 15:05:20            | 121,674.40 | 123,956.05 | 118,827.84 |
| 07/23/04            | 15:06:51            | 117,336.86 | 121,562.88 | 112,405.38 |
| 07/23/04            | 15:08:21            | 122,536.97 | 126,056.16 | 114,993.90 |
| 07/23/04            | 15:09:51            | 118,428.16 | 122,393.16 | 112,576.31 |
| 07/23/04            | 15:11:21            | 111,984.27 | 115,042.73 | 107,203.91 |
| 07/23/04            | 15:12:50            | 115,315.16 | 119,316.24 | 111,013.43 |
| 07/23/04            | 15:14:20            | 119,524.08 | 122,881.56 | 112,551.89 |
| 07/23/04            | 15:15:51            | 121,318.41 | 125,543.34 | 112,551.89 |
| 07/23/04            | 15:17:21            | 126,217.07 | 129,548.23 | 123,101.34 |
| 07/23/04            | 15:18:52            | 129,078.01 | 133,235.66 | 125,567.77 |
| 07/23/04            | 15:20:22            | 132,934.20 | 135,360.20 | 129,987.79 |
| 07/23/04            | 15:21:52            | 136,189.39 | 144,713.06 | 129,548.23 |
| 07/23/04            | 15:23:22            | 138,544.56 | 149,768.02 | 126,300.37 |
| 07/23/04            | 15:24:51            | 137,873.56 | 139,584.86 | 136,239.31 |
| 07/23/04            | 15:26:21            | 137,337.95 | 139,804.64 | 135,506.72 |
| 07/23/04            | 15:27:52            | 135,463.58 | 137,362.64 | 133,626.38 |
| 07/23/04            | 15:29:22            | 136,269.16 | 139,438.34 | 132,478.63 |
| 07/23/04            | 15:30:53            | 136,292.77 | 140,317.45 | 134,505.50 |
| 07/23/04            | 15:32:23            | 136,348.39 | 138,705.73 | 135,042.73 |
| 07/23/04            | 15:33:52            | 138,115.59 | 140,927.95 | 136,385.84 |
| 07/23/04            | 15:35:23            | 139,928.64 | 142,246.64 | 137,582.42 |
| 07/23/04            | 15:36:53            | 142,388.83 | 145,689.86 | 139,194.14 |
| 07/23/04            | 15:38:22            | 142,689.73 | 145,641.03 | 139,120.88 |
| 07/23/04            | 15:39:53            | 145,081.81 | 149,816.84 | 138,339.44 |
| 07/23/04            | 15:41:23            | 138,758.38 | 142,295.48 | 133,357.75 |
| 07/23/04            | 15:42:54            | 137,747.11 | 144,615.39 | 131,843.72 |
| 07/23/04            | 15:44:24            | 134,174.47 | 141,098.91 | 128,131.87 |
| 07/23/04            | 15:45:53            | 125,848.87 | 129,352.87 | 121,318.68 |
| 07/23/04            | 15:47:23            | 118,695.43 | 123,345.55 | 113,382.17 |
| 07/23/04            | 15:48:54            | 122,526.93 | 127,374.84 | 118,534.80 |
| 07/23/04            | 15:50:24            | 126,167.14 | 129,230.77 | 121,807.08 |
| 07/23/04            | 15:51:54            | 131,042.20 | 133,235.66 | 128,351.65 |
| 07/23/04            | 15:53:24            | 135,925.66 | 141,221.00 | 129,255.19 |
| 07/23/04            | 15:54:55            | 129,950.08 | 135,579.97 | 125,396.83 |

EVR0001  
07/28/04

BAYOU STEEL CORPORATION  
FURNACE #1 & #2 TOTAL FLOW (SCFM) - EVERY 15 MIN

13  
08:11

| END<br>DATE<br>---- | END<br>TIME<br>---- | AVG<br>--- | MAX<br>--- | MIN<br>--- |
|---------------------|---------------------|------------|------------|------------|
| 07/23/04            | 15:56:25            | 121,907.20 | 127,960.93 | 118,266.18 |
| 07/23/04            | 15:57:54            | 127,539.27 | 130,744.81 | 121,514.04 |
| 07/23/04            | 15:59:24            | 117,326.01 | 128,205.13 | 107,472.53 |
| 07/23/04            | 16:00:55            | 119,497.76 | 124,346.77 | 115,775.34 |
| 07/23/04            | 16:02:25            | 126,458.01 | 130,940.17 | 122,417.59 |
| 07/23/04            | 16:03:56            | 134,399.67 | 141,904.77 | 128,888.89 |
| 07/23/04            | 16:05:26            | 135,618.50 | 151,892.55 | 112,600.73 |
| 07/23/04            | 16:06:56            | 136,427.63 | 141,416.36 | 132,478.63 |
| 07/23/04            | 16:08:26            | 128,400.76 | 133,650.80 | 122,124.54 |
| 07/23/04            | 16:09:55            | 122,803.96 | 125,396.83 | 120,268.62 |
| 07/23/04            | 16:11:25            | 121,838.83 | 124,175.82 | 119,096.46 |
| 07/23/04            | 16:12:56            | 120,435.22 | 125,299.15 | 116,337.00 |
| 07/23/04            | 16:14:26            | 118,682.13 | 121,636.14 | 113,968.26 |
| 07/23/04            | 16:15:57            | 119,540.36 | 122,222.22 | 115,726.49 |
| 07/23/04            | 16:17:27            | 120,338.08 | 124,395.60 | 117,509.16 |
| 07/23/04            | 16:18:57            | 123,530.32 | 127,521.37 | 116,752.14 |
| 07/23/04            | 16:20:27            | 120,783.34 | 122,735.04 | 118,388.28 |
| 07/23/04            | 16:21:56            | 119,123.05 | 122,124.54 | 114,456.66 |
| 07/23/04            | 16:23:26            | 117,695.02 | 121,050.06 | 115,457.88 |
| 07/23/04            | 16:24:57            | 116,407.00 | 118,705.74 | 113,992.67 |
| 07/23/04            | 16:26:27            | 115,879.80 | 117,582.41 | 113,333.34 |
| 07/23/04            | 16:27:58            | 114,771.67 | 118,168.50 | 112,210.02 |
| 07/23/04            | 16:29:28            | 109,121.15 | 115,775.34 | 101,196.58 |
| 07/23/04            | 16:30:58            | 112,083.03 | 116,605.62 | 109,230.77 |
| 07/23/04            | 16:32:28            | 118,421.11 | 120,024.42 | 116,605.62 |
| 07/23/04            | 16:33:57            | 118,881.02 | 122,686.20 | 111,672.77 |
| 07/23/04            | 16:35:27            | 122,376.34 | 127,228.33 | 117,948.72 |
| 07/23/04            | 16:36:58            | 126,204.59 | 128,742.37 | 120,854.70 |
| 07/23/04            | 16:38:28            | 128,431.70 | 141,562.88 | 114,749.70 |
| 07/23/04            | 16:39:59            | 132,401.30 | 135,677.66 | 129,841.27 |
| 07/23/04            | 16:41:29            | 134,301.72 | 138,705.73 | 131,477.41 |
| 07/23/04            | 16:42:59            | 132,775.75 | 138,681.31 | 126,471.30 |
| 07/23/04            | 16:44:30            | 138,412.70 | 154,993.89 | 113,797.31 |
| 07/23/04            | 16:46:00            | 133,043.83 | 140,830.28 | 128,253.97 |
| 07/23/04            | 16:47:30            | 123,939.77 | 128,400.49 | 119,536.02 |
| 07/23/04            | 16:49:00            | 119,963.64 | 124,297.92 | 118,070.82 |
| 07/23/04            | 16:50:29            | 119,014.79 | 122,222.22 | 117,460.32 |
| 07/23/04            | 16:51:59            | 117,983.18 | 122,393.16 | 113,724.05 |
| 07/23/04            | 16:53:30            | 115,225.34 | 120,317.46 | 112,356.53 |
| 07/23/04            | 16:55:00            | 113,436.17 | 117,484.73 | 107,741.15 |
| 07/23/04            | 16:56:31            | 109,501.02 | 115,506.72 | 99,242.98  |
| 07/23/04            | 16:58:01            | 108,279.48 | 128,913.31 | 94,261.30  |
| 07/23/04            | 16:59:31            | 119,325.20 | 125,054.95 | 113,943.84 |
| 07/23/04            | 17:01:01            | 114,440.10 | 117,094.02 | 109,255.19 |
| 07/23/04            | 17:02:31            | 112,034.19 | 117,924.30 | 107,936.51 |
| 07/23/04            | 17:04:00            | 114,238.77 | 116,971.91 | 111,770.45 |
| 07/23/04            | 17:05:31            | 114,230.36 | 118,070.82 | 110,085.47 |
| 07/23/04            | 17:07:01            | 110,676.44 | 114,774.12 | 103,516.48 |
| 07/23/04            | 17:08:32            | 98,175.55  | 109,304.03 | 84,151.41  |
| 07/23/04            | 17:10:02            | 113,614.16 | 124,664.23 | 98,681.32  |
| 07/23/04            | 17:11:31            | 113,303.48 | 117,875.46 | 110,573.87 |
| 07/23/04            | 17:13:01            | 111,851.85 | 117,753.36 | 107,277.16 |
| 07/23/04            | 17:14:32            | 116,320.17 | 120,073.26 | 108,791.21 |

EVR0001  
07/28/04

BAYOU STEEL CORPORATION  
FURNACE #1 & #2 TOTAL FLOW (SCFM) - EVERY 15 MIN

14  
08:11

| END<br>DATE<br>.... | END<br>TIME<br>.... | AVG<br>... | MAX<br>... | MIN<br>... |
|---------------------|---------------------|------------|------------|------------|
| 07/23/04            | 17:16:02            | 116,794.73 | 119,584.86 | 114,456.66 |
| 07/23/04            | 17:17:32            | 112,733.69 | 115,457.88 | 110,549.45 |
| 07/23/04            | 17:19:02            | 109,785.10 | 112,112.34 | 106,715.51 |
| 07/23/04            | 17:20:33            | 109,452.18 | 111,892.55 | 105,958.48 |
| 07/23/04            | 17:22:03            | 109,854.56 | 111,013.43 | 108,034.19 |
| 07/23/04            | 17:23:32            | 105,654.87 | 110,134.31 | 102,832.73 |
| 07/23/04            | 17:25:02            | 100,882.11 | 106,666.66 | 96,288.16  |
| 07/23/04            | 17:26:33            | 101,687.70 | 104,029.30 | 98,974.36  |
| 07/23/04            | 17:28:03            | 104,982.50 | 123,467.64 | 99,731.38  |
| 07/23/04            | 17:29:33            | 110,297.92 | 116,166.05 | 100,708.18 |
| 07/23/04            | 17:31:03            | 114,514.18 | 117,704.52 | 109,719.17 |
| 07/23/04            | 17:32:34            | 115,674.13 | 119,853.48 | 110,378.51 |
| 07/23/04            | 17:34:04            | 120,828.11 | 126,227.11 | 116,874.23 |
| 07/23/04            | 17:35:33            | 123,315.16 | 127,423.69 | 117,606.84 |
| 07/23/04            | 17:37:03            | 124,858.50 | 140,708.19 | 105,958.48 |
| 07/23/04            | 17:38:34            | 127,643.20 | 132,747.25 | 122,051.28 |
| 07/23/04            | 17:40:04            | 134,703.30 | 148,791.20 | 104,737.48 |
| 07/23/04            | 17:41:35            | 124,318.00 | 129,206.35 | 118,461.54 |
| 07/23/04            | 17:43:04            | 118,973.00 | 120,879.12 | 115,848.59 |
| 07/23/04            | 17:44:35            | 115,924.02 | 119,780.22 | 112,942.61 |
| 07/23/04            | 17:46:05            | 114,907.07 | 119,780.22 | 111,037.85 |
| 07/23/04            | 17:47:34            | 114,446.07 | 117,118.44 | 111,965.81 |
| 07/23/04            | 17:49:04            | 113,784.29 | 116,800.98 | 111,746.03 |
| 07/23/04            | 17:50:35            | 104,249.36 | 112,551.89 | 95,506.72  |
| 07/23/04            | 17:52:06            | 106,455.02 | 110,964.59 | 100,537.24 |
| 07/23/04            | 17:53:36            | 116,948.85 | 126,202.69 | 83,760.69  |
| 07/23/04            | 17:55:05            | 116,797.18 | 121,440.78 | 114,456.66 |
| 07/23/04            | 17:56:36            | 110,828.92 | 114,529.91 | 107,814.41 |
| 07/23/04            | 17:58:06            | 107,986.98 | 112,332.11 | 103,980.46 |
| 07/23/04            | 17:59:35            | 111,916.43 | 113,040.30 | 110,451.77 |
| 07/23/04            | 18:01:05            | 108,444.72 | 112,332.11 | 105,787.55 |
| 07/23/04            | 18:02:36            | 101,752.55 | 110,842.49 | 88,278.39  |
| 07/23/04            | 18:04:06            | 100,187.77 | 113,821.73 | 82,881.56  |
| 07/23/04            | 18:05:37            | 114,361.96 | 120,439.56 | 109,841.27 |
| 07/23/04            | 18:07:07            | 110,591.78 | 114,407.81 | 108,595.85 |
| 07/23/04            | 18:08:37            | 110,113.41 | 113,137.98 | 106,984.13 |
| 07/23/04            | 18:10:07            | 110,627.05 | 112,722.84 | 106,324.79 |
| 07/23/04            | 18:11:36            | 106,220.32 | 109,279.61 | 102,808.30 |
| 07/23/04            | 18:13:06            | 107,906.66 | 109,914.53 | 105,323.56 |
| 07/23/04            | 18:14:37            | 103,794.88 | 105,787.55 | 100,854.70 |
| 07/23/04            | 18:16:07            | 106,727.72 | 111,355.31 | 100,854.70 |
| 07/23/04            | 18:17:38            | 106,996.88 | 109,865.69 | 104,957.27 |
| 07/23/04            | 18:19:08            | 106,260.48 | 108,498.17 | 102,808.30 |
| 07/23/04            | 18:20:38            | 98,668.30  | 103,565.32 | 93,015.88  |
| 07/23/04            | 18:22:08            | 107,813.05 | 119,291.82 | 95,555.55  |
| 07/23/04            | 18:23:37            | 108,116.13 | 119,145.30 | 98,949.94  |
| 07/23/04            | 18:25:07            | 102,784.42 | 108,791.21 | 96,971.91  |
| 07/23/04            | 18:26:38            | 111,506.98 | 119,145.30 | 100,415.14 |
| 07/23/04            | 18:28:08            | 112,983.31 | 121,538.46 | 105,128.20 |
| 07/23/04            | 18:29:39            | 120,094.42 | 129,206.35 | 111,721.61 |
| 07/23/04            | 18:31:09            | 125,506.45 | 138,925.52 | 92,722.84  |
| 07/23/04            | 18:32:39            | 121,037.04 | 124,786.33 | 117,216.12 |
| 07/23/04            | 18:34:09            | 116,039.88 | 122,564.10 | 111,672.77 |

EVR0001  
07/28/04

BAYOU STEEL CORPORATION  
FURNACE #1 & #2 TOTAL FLOW (SCFM) - EVERY 15 MIN

15  
08:11

| END<br>DATE<br>---- | END<br>TIME<br>---- | AVG<br>--- | MAX<br>--- | MIN<br>--- |
|---------------------|---------------------|------------|------------|------------|
| 07/23/04            | 18:35:38            | 111,347.45 | 112,796.09 | 109,426.13 |
| 07/23/04            | 18:37:08            | 112,019.80 | 114,456.66 | 108,766.79 |
| 07/23/04            | 18:38:39            | 111,362.91 | 114,676.44 | 107,179.48 |
| 07/23/04            | 18:40:09            | 108,899.74 | 113,577.53 | 105,885.23 |
| 07/23/04            | 18:41:40            | 107,539.82 | 113,577.53 | 101,733.82 |
| 07123104            | 18:43:10            | 100,975.17 | 111,037.85 | 93,943.84  |
| 07/23/04            | 18:44:40            | 107,283.13 | 122,661.78 | 88,131.87  |
| 07/23/04            | 18:46:10            | 112,533.45 | 117,753.36 | 109,230.77 |
| 07/23/04            | 18:47:39            | 108,729.34 | 110,256.41 | 106,031.74 |
| 07/23/04            | 18:49:09            | 108,799.35 | 112,356.53 | 105,641.02 |
| 07/23/04            | 18:50:40            | 111,210.42 | 115,384.62 | 106,837.61 |
| 07/23/04            | 18:52:10            | 107,594.63 | 109,059.83 | 105,836.38 |
| 07/23/04            | 18:53:41            | 106,409.71 | 110,109.89 | 91,892.55  |
| 07/23/04            | 18:55:11            | 100,905.98 | 112,112.34 | 91,892.55  |
| 07/23/04            | 18:56:40            | 111,978.56 | 120,488.40 | 87,179.48  |
| 07/23/04            | 18:58:11            | 111,371.32 | 116,190.48 | 108,620.27 |
| 07/23/04            | 18:59:41            | 112,009.23 | 113,870.57 | 108,522.59 |
| 07/23/04            | 19:01:11            | 112,795.55 | 116,166.05 | 106,471.30 |
| 07/23/04            | 19:02:42            | 111,658.12 | 113,675.21 | 108,034.19 |
| 07/23/04            | 19:04:12            | 109,704.25 | 113,577.53 | 105,518.92 |
| 07/23/04            | 19:05:42            | 107,653.51 | 112,844.93 | 104,566.55 |
| 07/23/04            | 19:07:12            | 110,639.53 | 112,136.75 | 108,424.91 |
| 07/23/04            | 19:08:41            | 107,879.26 | 110,964.59 | 104,322.34 |
| 07/23/04            | 19:10:11            | 105,643.47 | 107,130.65 | 103,663.00 |
| 07/23/04            | 19:11:42            | 108,230.09 | 112,576.31 | 105,250.30 |
| 07/23/04            | 19:13:12            | 110,144.08 | 116,483.52 | 104,932.84 |
| 07/23/04            | 19:14:43            | 104,355.17 | 115,164.84 | 96,166.05  |
| 07/23/04            | 19:16:13            | 107,405.51 | 111,843.71 | 100,683.76 |
| 07/23/04            | 19:17:43            | 113,401.44 | 125,738.70 | 107,545.79 |
| 07/23/04            | 19:19:13            | 119,080.38 | 127,643.47 | 110,233.99 |
| 07/23/04            | 19:20:42            | 119,051.69 | 131,990.23 | 94,871.80  |
| 07/23/04            | 19:22:12            | 128,472.39 | 139,096.45 | 94,871.80  |
| 07/23/04            | 19:23:43            | 120,271.34 | 125,152.63 | 115,140.41 |
| 07/23/04            | 19:25:13            | 113,765.02 | 115,824.18 | 111,159.95 |
| 07/23/04            | 19:26:44            | 113,598.70 | 116,923.08 | 110,769.23 |
| 07/23/04            | 19:28:14            | 114,606.43 | 117,997.55 | 111,013.43 |
| 07/23/04            | 19:29:44            | 111,629.09 | 114,603.17 | 107,179.48 |
| 07/23/04            | 19:31:14            | 110,212.73 | 115,409.04 | 106,984.13 |
| 07/23/04            | 19:32:43            | 105,153.16 | 112,551.89 | 92,649.57  |
| 07/23/04            | 19:34:13            | 103,707.23 | 121,196.58 | 86,080.59  |
| 07/23/04            | 19:35:44            | 115,170.27 | 121,929.18 | 107,912.09 |
| 07/23/04            | 19:37:14            | 110,060.23 | 115,311.35 | 105,787.55 |
| 07/23/04            | 19:38:45            | 107,283.68 | 111,306.47 | 105,299.15 |
| 07/23/04            | 19:40:15            | 109,061.73 | 114,017.09 | 105,079.37 |
| 07/23/04            | 19:41:45            | 109,078.82 | 113,455.43 | 105,567.77 |
| 07/23/04            | 19:43:15            | 104,174.74 | 112,063.49 | 86,862.02  |
| 07/23/04            | 19:44:44            | 99,473.88  | 111,501.83 | 78,705.74  |
| 07/23/04            | 19:46:14            | 114,310.13 | 121,562.88 | 78,705.74  |
| 07/23/04            | 19:47:45            | 112,059.96 | 115,579.98 | 105,567.77 |
| 07/23/04            | 19:49:15            | 107,781.85 | 113,235.66 | 101,391.94 |
| 07/23/04            | 19:50:46            | 112,417.31 | 114,652.02 | 109,914.53 |
| 07/23/04            | 19:52:16            | 109,349.07 | 113,943.84 | 104,810.74 |
| 07/23/04            | 19:53:46            | 106,407.27 | 110,573.87 | 100,781.44 |

EVR0001  
07/28/04

BAYOU STEEL CORPORATION  
FURNACE #1 & #2 TOTAL FLOW (SCFM) - EVERY 15 MIN

16  
08:11

| END<br>DATE<br>---- | END<br>TIME<br>---- | AVG<br>--- | MAX<br>--- | MIN<br>--- |
|---------------------|---------------------|------------|------------|------------|
| 07/23/04            | 19:55:16            | 104,103.11 | 107,594.63 | 101,343.10 |
| 07/23/04            | 19:56:45            | 103,071.23 | 109,035.41 | 101,001.22 |
| 07/23/04            | 19:58:15            | 107,409.85 | 110,354.09 | 104,078.14 |
| 07/23/04            | 19:59:46            | 105,034.32 | 108,864.47 | 101,269.84 |
| 07/23/04            | 20:01:16            | 105,811.70 | 107,594.63 | 103,736.27 |
| 07/23/04            | 20:02:47            | 105,173.52 | 107,716.73 | 101,147.74 |
| 07/23/04            | 20:04:17            | 100,169.31 | 106,715.51 | 89,719.17  |
| 07/23/04            | 20:05:46            | 104,745.09 | 112,454.21 | 96,923.08  |
| 07/23/04            | 20:07:16            | 109,973.41 | 121,587.30 | 96,141.63  |
| 07/23/04            | 20:08:47            | 113,518.66 | 118,534.80 | 108,107.45 |
| 07/23/04            | 20:10:17            | 119,150.45 | 130,451.77 | 84,908.42  |
| 07/23/04            | 20:11:48            | 120,589.61 | 124,908.42 | 117,118.44 |
| 07/23/04            | 20:13:18            | 114,776.55 | 119,120.88 | 111,575.09 |
| 07/23/04            | 20:14:48            | 111,870.84 | 116,019.54 | 107,960.93 |
| 07/23/04            | 20:16:18            | 112,860.40 | 116,361.41 | 109,914.53 |
| 07/23/04            | 20:17:47            | 112,480.80 | 119,389.50 | 108,083.03 |
| 07/23/04            | 20:19:17            | 112,175.28 | 116,043.95 | 108,034.19 |
| 07/23/04            | 20:20:48            | 104,120.20 | 115,384.62 | 94,334.55  |
| 07/23/04            | 20:22:18            | 115,071.50 | 125,177.05 | 93,260.07  |
| 07/23/04            | 20:23:49            | 115,303.48 | 118,608.06 | 111,330.89 |
| 07/23/04            | 20:25:19            | 110,711.16 | 113,699.63 | 107,179.48 |
| 07/23/04            | 20:26:49            | 110,741.28 | 114,407.81 | 108,253.97 |
| 07/23/04            | 20:28:19            | 110,771.95 | 113,772.89 | 107,594.63 |
| 07/23/04            | 20:29:48            | 103,291.01 | 111,135.53 | 89,865.69  |
| 07/23/04            | 20:31:18            | 104,560.03 | 121,538.46 | 82,637.36  |
| 07/23/04            | 20:32:49            | 113,827.70 | 120,024.42 | 109,768.01 |
| 07/23/04            | 20:34:19            | 107,632.88 | 111,965.81 | 100,024.42 |
| 07/23/04            | 20:35:50            | 109,064.45 | 114,993.90 | 100,024.42 |
| 07/23/04            | 20:37:20            | 111,369.15 | 114,041.52 | 107,692.30 |
| 07/23/04            | 20:38:50            | 100,669.65 | 110,061.05 | 91,892.55  |
| 07/23/04            | 20:40:20            | 111,874.10 | 121,733.82 | 87,912.09  |
| 07/23/04            | 20:41:49            | 112,616.74 | 116,800.98 | 109,890.11 |
| 07/23/04            | 20:43:19            | 109,485.28 | 111,111.11 | 105,421.24 |
| 07/23/04            | 20:44:50            | 111,805.73 | 115,140.41 | 107,350.43 |
| 07/23/04            | 20:46:20            | 110,833.54 | 113,870.57 | 103,736.27 |
| 07/23/04            | 20:47:51            | 108,562.48 | 112,454.21 | 104,786.33 |
| 07/23/04            | 20:49:21            | 108,036.90 | 110,866.91 | 104,835.16 |
| 07/23/04            | 20:50:51            | 109,716.73 | 114,188.03 | 107,057.39 |
| 07/23/04            | 20:52:21            | 108,387.46 | 111,770.45 | 103,223.45 |
| 07/23/04            | 20:53:50            | 103,033.24 | 108,669.11 | 94,432.23  |
| 07/23/04            | 20:55:20            | 106,444.72 | 117,558.00 | 95,531.13  |
| 07/23/04            | 20:56:51            | 108,938.81 | 113,333.34 | 106,080.59 |
| 07/23/04            | 20:58:21            | 113,204.45 | 125,323.56 | 98,632.48  |
| 07/23/04            | 20:59:52            | 118,041.24 | 122,173.38 | 113,772.89 |
| 07/23/04            | 21:01:22            | 119,050.06 | 123,565.32 | 114,481.08 |
| 07/23/04            | 21:02:51            | 123,560.71 | 139,804.64 | 99,340.66  |
| 07/23/04            | 21:04:22            | 128,216.52 | 137,264.95 | 121,782.66 |
| 07/23/04            | 21:05:52            | 119,187.63 | 124,542.13 | 116,263.73 |
| 07/23/04            | 21:07:21            | 113,819.02 | 118,241.76 | 110,793.65 |
| 07/23/04            | 21:08:52            | 113,374.30 | 119,829.06 | 109,474.97 |
| 07/23/04            | 21:10:22            | 110,581.47 | 113,064.71 | 109,181.93 |
| 07/23/04            | 21:11:53            | 108,501.42 | 111,477.41 | 106,862.02 |
| 07/23/04            | 21:13:23            | 102,845.48 | 108,595.85 | 93,406.59  |

EVR0001  
07/28/04

BAYOU STEEL CORPORATION  
FURNACE #1 & #2 TOTAL FLOW (SCFM) - EVERY 15 MIN

17  
08:11

| END<br>DATE<br>----   | END<br>TIME | AVG<br>--- | MAX<br>--- | MIN<br>--- |
|-----------------------|-------------|------------|------------|------------|
| 07/23/04              | 21:14:52    | 102,020.63 | 116,312.58 | 89,963.37  |
| 07/23/04              | 21:16:23    | 107,284.49 | 118,901.10 | 87,619.05  |
| 07/23/04              | 21:17:53    | 111,514.59 | 117,851.04 | 109,548.23 |
| 07/23/04              | 21:19:22    | 111,843.98 | 114,481.08 | 107,374.84 |
| 07/23/04              | 21:20:53    | 111,025.10 | 113,992.67 | 107,032.97 |
| 07/23/04              | 21:22:23    | 107,787.27 | 109,206.35 | 106,446.88 |
| 07/23/04              | 21:23:54    | 110,460.18 | 113,675.21 | 107,179.48 |
| 07/23/04              | 21:25:24    | 103,884.95 | 110,500.61 | 92,161.17  |
| 07/23/04              | 21:26:53    | 107,760.14 | 112,014.65 | 103,833.95 |
| 07/23/04              | 21:28:23    | 116,789.31 | 130,695.97 | 94,432.23  |
| 07/23/04              | 21:29:54    | 122,822.68 | 128,083.03 | 117,728.94 |
| 07/23/04              | 21:31:24    | 114,788.23 | 118,705.74 | 111,184.38 |
| 07/23/04              | 21:32:54    | 114,922.53 | 118,852.26 | 111,086.69 |
| 07/23/04              | 21:34:24    | 110,988.74 | 113,284.49 | 108,693.53 |
| 07/23/04              | 21:35:55    | 109,104.33 | 113,675.21 | 105,763.13 |
| 07/23/04              | 21:37:25    | 108,919.28 | 113,260.07 | 105,421.24 |
| 07/23/04              | 21:38:54    | 110,824.31 | 116,068.38 | 106,202.69 |
| 07/23/04              | 21:40:24    | 107,574.28 | 111,941.39 | 102,246.64 |
| 07/23/04              | 21:41:55    | 105,990.23 | 109,670.33 | 102,905.98 |
| 07/23/04              | 21:43:25    | 110,513.91 | 113,772.89 | 107,399.27 |
| 07/23/04              | 21:44:55    | 110,089.54 | 113,675.21 | 102,490.84 |
| 07/23/04              | 21:46:25    | 105,729.21 | 112,210.02 | 96,385.84  |
| 07/23/04              | 21:47:56    | 109,216.93 | 110,695.97 | 104,566.55 |
| 07/23/04              | 21:49:26    |            |            |            |
| Records selected: 958 |             |            |            |            |
| Records sorted: 958   |             |            |            |            |
| Lines printed: 1053   |             |            |            |            |
| Pages printed: 19     |             |            |            |            |

|            |            |            |            |            |
|------------|------------|------------|------------|------------|
| 108,765.43 | 116,190.48 | 97,680.10  |            |            |
| 07/23/04   | 21:50:55   | 106,868.81 | 112,234.43 | 96,410.26  |
| 07/23/04   | 21:52:25   | 112,163.62 | 126,422.47 | 100,122.10 |
| 07/23/04   | 21:53:56   | 123,698.27 | 134,334.55 | 91,623.93  |
| 07/23/04   | 21:55:27   | 117,146.38 | 125,836.38 | 114,188.03 |
| 07/23/04   | 21:56:56   | 113,416.09 | 116,605.62 | 110,476.19 |
| 07/23/04   | 21:58:26   | 109,487.72 | 112,429.79 | 105,445.66 |
| 07/23/04   | 21:59:57   | 109,169.72 | 113,504.27 | 106,202.69 |
| 07/23/04   | 22:01:27   | 109,208.25 | 111,697.20 | 107,081.80 |
| 07/23/04   | 22:02:56   | 103,207.70 | 109,279.61 | 88,766.79  |
| 07/23/04   | 22:04:26   | 102,681.05 | 116,678.88 | 97,753.36  |
| 07/23/04   | 22:05:57   | 111,611.18 | 128,864.47 | 96,874.23  |
| 07/23/04   | 22:07:27   | 116,079.50 | 119,633.70 | 112,991.45 |
| 07/23/04   | 22:08:58   | 112,771.95 | 117,460.32 | 111,257.63 |
| 07/23/04   | 22:10:28   | 113,903.41 | 118,315.02 | 109,426.13 |
| 07/23/04   | 22:11:58   | 112,065.94 | 114,163.62 | 110,695.97 |
| 07/23/04   | 22:13:28   | 112,230.36 | 116,605.62 | 108,766.79 |
| 07/23/04   | 22:14:57   | 109,118.98 | 115,164.84 | 89,597.07  |
| 07/23/04   | 22:16:27   | 100,432.77 | 112,527.47 | 88,498.17  |
| 07/23/04   | 22:17:58   | 111,454.08 | 132,161.17 | 88,498.17  |
| 07/23/04   | 22:19:28   | 117,751.19 | 122,490.84 | 113,968.26 |
| 07/23/04   | 22:20:59   | 116,745.35 | 119,780.22 | 112,014.65 |
| 07/23/04   | 22:22:29   | 114,721.48 | 117,484.73 | 111,306.47 |
| 07/23/04   | 22:23:59   | 111,945.19 | 114,432.23 | 109,108.67 |

|          |          |            |            |            |
|----------|----------|------------|------------|------------|
| 07/23/04 | 22:25:29 | 115,035.14 | 118,803.42 | 112,429.79 |
| 07/23/04 | 22:26:58 | 113,157.23 | 117,435.90 | 108,840.05 |
| 07/23/04 | 22:28:28 | 108,179.89 | 111,086.69 | 103,492.06 |
| 07/23/04 | 22:30:00 | 105,510.24 | 108,840.05 | 100,146.52 |
| 07/23/04 | 22:31:29 | 109,427.76 | 112,185.59 | 106,422.47 |
| 07/23/04 | 22:32:99 | 108,233.62 | 112,551.89 | 103,174.60 |

EVR0001  
07/28/04

BAYOU STEEL CORPORATION  
FURNACE #1 & #2 TOTAL FLOW (SCFM) - EVERY 15 MIN

18  
08:11

| END<br>DATE | END<br>TIME | AVG        | MAX        | MIN        |
|-------------|-------------|------------|------------|------------|
| 07/23/04    | 22:34:30    | 107,986.98 | 114,603.17 | 92,307.70  |
| 07/23/04    | 22:36:00    | 104,042.60 | 109,816.85 | 99,780.22  |
| 07/23/04    | 22:37:30    | 109,126.03 | 123,516.48 | 95,042.73  |
| 07/23/04    | 22:39:00    | 113,108.94 | 119,242.98 | 95,042.73  |
| 07/23/04    | 22:40:29    | 116,178.27 | 119,242.98 | 113,186.81 |
| 07/23/04    | 22:42:01    | 117,638.31 | 122,271.06 | 114,358.98 |
| 07/23/04    | 22:43:30    | 121,811.97 | 129,597.07 | 116,117.22 |
| 07/23/04    | 22:45:00    | 129,148.83 | 141,611.72 | 98,339.44  |
| 07/23/04    | 22:46:31    | 127,097.27 | 135,335.78 | 120,659.34 |
| 07/23/04    | 22:48:01    | 120,265.63 | 122,710.63 | 117,924.30 |
| 07/23/04    | 22:49:31    | 118,353.82 | 120,854.70 | 114,993.90 |
| 07/23/04    | 22:51:01    | 117,635.05 | 122,857.14 | 114,871.80 |
| 07/23/04    | 22:52:30    | 118,845.75 | 121,440.78 | 115,970.70 |
| 07/23/04    | 22:54:02    | 113,726.23 | 117,948.72 | 97,899.88  |
| 07/23/04    | 22:55:31    | 108,694.07 | 121,245.42 | 97,948.72  |
| 07/23/04    | 22:57:01    | 118,847.91 | 129,890.11 | 97,484.73  |
| 07/23/04    | 22:58:32    | 117,127.66 | 120,048.84 | 113,553.12 |
| 07/23/04    | 23:00:02    | 117,249.49 | 118,949.94 | 114,822.95 |
| 07/23/04    | 23:01:31    | 118,067.84 | 121,733.82 | 113,284.49 |
| 07/23/04    | 23:03:01    | 117,727.31 | 121,733.82 | 114,700.85 |
| 07/23/04    | 23:04:32    | 114,283.27 | 117,167.27 | 112,356.53 |
| 07/23/04    | 23:06:02    | 104,751.32 | 113,284.49 | 93,162.39  |
| 07/23/04    | 23:07:33    | 108,471.03 | 120,488.40 | 95,628.81  |
| 07/23/04    | 23:09:03    | 115,176.23 | 128,644.69 | 99,365.08  |
| 07/23/04    | 23:10:33    | 117,513.50 | 129,304.03 | 106,813.19 |
| 07/23/04    | 23:12:03    | 128,677.25 | 134,432.23 | 122,051.28 |
| 07/23/04    | 23:13:32    | 122,102.29 | 126,886.45 | 118,119.66 |
| 07/23/04    | 23:15:02    | 117,980.73 | 121,611.72 | 113,821.73 |
| 07/23/04    | 23:16:33    | 119,446.21 | 121,074.48 | 116,971.91 |
| 07/23/04    | 23:18:03    | 119,287.20 | 122,368.74 | 116,605.62 |
| 07/23/04    | 23:19:34    | 122,757.56 | 126,642.25 | 117,069.59 |
| 07/23/04    | 23:21:04    | 122,189.12 | 125,543.34 | 119,072.04 |
| 07/23/04    | 23:22:34    | 119,045.72 | 121,953.60 | 117,142.86 |
| 07/23/04    | 23:24:04    | 116,332.93 | 118,046.40 | 114,334.55 |
| 07/23/04    | 23:25:33    | 114,345.13 | 117,167.27 | 111,721.61 |
| 07/23/04    | 23:27:03    | 110,720.66 | 114,285.71 | 104,884.01 |
| 07/23/04    | 23:28:34    | 111,976.39 | 115,921.86 | 105,665.45 |
| 07/23/04    | 23:30:04    | 103,021.57 | 112,332.11 | 95,531.13  |
| 07/23/04    | 23:31:35    | 107,314.88 | 116,507.94 | 103,345.55 |
| 07/23/04    | 23:33:05    | 115,334.69 | 119,511.60 | 102,783.88 |
| 07/23/04    | 23:34:35    | 118,216.25 | 124,639.80 | 112,380.95 |
| 07/23/04    | 23:36:05    | 123,540.09 | 139,633.70 | 98,974.36  |
| 07/23/04    | 23:37:34    | 123,894.72 | 133,772.89 | 119,829.06 |
| 07/23/04    | 23:39:04    | 125,883.60 | 130,036.63 | 120,903.54 |
| 07/23/04    | 23:40:35    | 122,930.41 | 125,763.13 | 118,803.42 |
| 07/23/04    | 23:42:05    | 120,017.37 | 121,831.50 | 117,069.59 |
| 07/23/04    | 23:43:36    | 117,132.55 | 121,221.00 | 115,018.31 |
| 07/23/04    | 23:45:06    | 120,105.28 | 123,907.20 | 116,019.54 |
| 07/23/04    | 23:46:36    | 112,464.80 | 119,218.56 | 100,659.34 |
| 07/23/04    | 23:48:06    | 109,968.26 | 126,886.45 | 97,509.16  |
| 07/23/04    | 23:49:35    | 122,827.84 | 128,278.39 | 117,704.52 |
| 07/23/04    | 23:51:07    | 117,981.82 | 119,804.64 | 115,286.94 |
| 07/23/04    | 23:52:36    | 116,102.29 | 119,438.34 | 113,260.07 |

EVR0001  
07/28/04

B A Y O U   S T E E L   C O R P O R A T I O N  
FURNACE #1 & #2 TOTAL FLOW (SCFM) - EVERY 15 MIN

19  
08:11

| END<br>DATE<br>---- | END<br>TIME<br>---- | AVG<br>--- | MAX<br>--- | MIN<br>--- |
|---------------------|---------------------|------------|------------|------------|
| 07/23/04            | 23:54:06            | 116,503.87 | 119,951.16 | 113,406.59 |
| 07/23/04            | 23:55:37            | 115,567.77 | 117,924.30 | 112,185.59 |
| 07/23/04            | 23:57:07            | 114,627.59 | 116,727.72 | 111,770.45 |
| 07/23/04            | 23:58:37            | 104,412.43 | 114,139.20 | 94,700.85  |

## **VII. APPENDIX**

The following appendices are presented as supporting documentation to the emission test report.

- A. Resumes of Test Personnel
- B. Test Equipment Calibrations
- C. Correspondence, Bayou Steel and LDEQ
- D. Permit Number 885 (M-2) Excerpts

Troy **W. LeSage**  
Assistant Manager  
Senior Project Team Leader  
Emission Testing Services, Incorporated  
Baton Rouge, Louisiana

## EDUCATION

U. S. EPA Round Robin sample integrity audits  
Completed Emission Testing Services Air Sampling Techniques Seminar  
Participates in on going Air-Pollution Training Institute Courses (**APTI**)  
EPA - Sampling and evaluation of Airborne Asbestos, Temple University  
NIOSH - Supervision of Asbestos Abatement Projects, Texas A & M  
High School Graduate

## CERTIFICATIONS

EPA Certified Opacity Reader (Method 9)  
General Safety & Health Orientation Program  
Respiratory Equipment Medical Certification  
MSA Qualitative Fit Test Record

## EXPERIENCE

1992 to Present - **Senior Project** Team Leader.  
Responsibilities include planning and performing source testing projects.

1987 to 1992 - Testing Specialist for Emission Testing Services, Inc.  
Performs EPA approved reference methods for compliance testing as well as other non-routine source evaluations. Responsibilities also include job preparation, equipment calibration, and equipment maintenance.

1985 to 1987 - Industrial Hygiene Technician for an environmental firm.  
Performed metal analysis with atomic adsorption spectrophotometer, fiber analysis for asbestos and overseeing asbestos abatement projects.

**Ronald L. McCabe, II**  
Senior Sampling Specialist  
Emission Testing Services, Incorporated .  
Baton Rouge, Louisiana

#### EDUCATION

Louisiana State University  
B.S. ---- **Environmental** Engineering

#### CERTIFICATIONS

General Safety & Health Orientation Program  
Respiratory Equipment **Medical** Certification  
MSA Qualitative Fit Test Record  
EPA Certified Opacity Reader (Method 9)

#### EXPERIENCE

#### EXPERIENCE

08/98 to Present - Sampling Specialist for Emission Testing Services, **Inc.**

Performs EPA approved reference methods for compliance testing as well as other non-routine source evaluations.

Responsibilities also include job preparation, equipment calibration, and equipment maintenance.

Responsibilities include planning and **performing** source testing projects.

Joel S. Richard  
Sampling Technician Grade 2  
Emission Testing Services, Incorporated  
Baton Rouge, Louisiana

## EDUCATION

High School Graduate

## CERTIFICATIONS

General Safety & Health Orientation Program  
Respiratory Equipment Medical Certification  
MSA Qualitative Fit Test Record

## EXPERIENCE

09/01 to Present -- Sampling Technician Grade 2

Able to perform all procedures required in 40 CFR 60, Method 2 and Method 4 testing without ~~the use~~ of a computer. Able to prepare and load for an emission test which requires a sample train. Proficient in completion of project field logs and data sheets. Responsible for the calibration and maintenance of **consoles**, **pitot** tubes, **thermocouples** and barometers. Proficient in the collection of **orgain** samples by EPA Reference Method 18. Is well-versed in the calculation of stack gas flow rates with and without the use of a computer. Helps in training a Grade 1 technician. Will have accumulated, at least, 240 field hours as a Sampling Technician Grade 1.

05/00 to 09/01 -- Sampling Technician Grade 1

Able to perform all procedures required in 40 CFR 60, Method 1 without use of a computer. All to perform all procedures required in 40 CFR 60, Method 3 (**orsat** analysis). Competent in the calibration of consoles, **pitot** tubes, thermal couples and barometers. Able to setup and assist in leak-check as well as weigh-in of a M4 sample train. Will have accumulated, at least, 480 hours of field experience.

10/99 to 05/00 - Testing trainee technician for Emission Testing Services, Inc. Supports in performing EPA approved reference methods for compliance testing as well as other non-routine source evaluations. Responsibilities also **include** job preparation, equipment calibration and equipment maintenance.

# ETS

EMISSION TESTING SERVICES

## METER BOX CALIBRATION DATA AND CALCULATIONS FORM (English Units)

|                    |      |
|--------------------|------|
| Gas meter Reads in |      |
| Man                | 0.82 |

One Revolution of meter =  
Leak Check Good @:  
Barometric Pres., Pb:

0.1 ft3  
0.0123  
29.821

Wet Test Meter Cal Factor:  
Meter Box Number:  
Date Calibrated:

1.007  
3  
6/15/04

| Orifice Setting<br>AH<br>in. H2O | Wet Test Meter Reading<br>(Vwm),<br>ft3 | Dry Gas Meter Readings   |                        |                        | Wet Test Meter Reading<br>(Twm),<br>ft3 | Wet Test Meter Pressure<br>(Pw)<br>in. H2O | Dry Gas Meter             |                            |                         | Run Time<br>(Θ),<br>Min. |
|----------------------------------|-----------------------------------------|--------------------------|------------------------|------------------------|-----------------------------------------|--------------------------------------------|---------------------------|----------------------------|-------------------------|--------------------------|
|                                  |                                         | Initial<br>(Vdi),<br>ft3 | Final<br>(Vdf),<br>ft3 | Total<br>(Vdm),<br>ft3 |                                         |                                            | Inlet<br>(Tdi),<br>deg. F | Outlet<br>(Tdf),<br>deg. F | Avg<br>(Tdm),<br>deg. F |                          |
| 0.50                             | 5                                       | 639.575                  | 844.628                | 5.053                  | 74                                      | 0.5                                        | 86.5                      | 83.0                       | 84.8                    | 13.15                    |
| 1.00                             | 5                                       | 844.628                  | 849.678                | 5.050                  | 74                                      | 1.125                                      | 97.0                      | 85.5                       | 91.3                    | 9.02                     |
| 1.50                             | 5                                       | 849.678                  | 854.734                | 5.056                  | 74                                      | 1.5                                        | 98.5                      | 86.5                       | 92.5                    | 7.32                     |
| 2.00                             | 5                                       | 854.734                  | 859.768                | 5.034                  | 74                                      | 2.125                                      | 100.0                     | 87.0                       | 93.5                    | 6.37                     |
| 3.00                             | 5                                       | 859.768                  | 864.788                | 5.020                  | 74                                      | 2.875                                      | 101.0                     | 88.0                       | 94.5                    | 5.25                     |

| Dry Gas Meter Gauge Pressure<br>in. H2O<br>(Gp) | Dry Gas Meter<br>Gp<br>Pdm = $\frac{Gp}{13.6}$ + Pb<br>(Pdm) | Wet Test Meter<br>Pwm = $\frac{Pw}{13.6}$ + Pb<br>(Pwm) | Ydm = $\frac{(Vwm) \cdot (Ywm) \cdot (Twm) \cdot (Pwm)}{(Vdm) \cdot (Tdm) \cdot (Pdm)}$ |           | ΔH@ = $\frac{0.031 PAH}{Pb \cdot (tda+460)} \cdot \frac{(TW+460)^2}{VW}$ |           |
|-------------------------------------------------|--------------------------------------------------------------|---------------------------------------------------------|-----------------------------------------------------------------------------------------|-----------|--------------------------------------------------------------------------|-----------|
|                                                 |                                                              |                                                         | Ydm                                                                                     | Tolerance | ΔH@                                                                      | Tolerance |
| 0.5                                             | 29.8578                                                      | 29.8578                                                 | 1.0165                                                                                  | 0.0144    | 1.9244                                                                   | -0.1117   |
| 1.0                                             | 29.8945                                                      | 29.9037                                                 | 1.0296                                                                                  | 0.0014    | 1.7896                                                                   | 0.0232    |
| 1.5                                             | 29.9313                                                      | 29.9313                                                 | 1.0303                                                                                  | 0.0006    | 1.7638                                                                   | 0.0489    |
| 2.0                                             | 29.9681                                                      | 29.9773                                                 | 1.0370                                                                                  | -0.0061   | 1.7778                                                                   | 0.0350    |
| 3.0                                             | 30.0416                                                      | 30.0324                                                 | 1.0412                                                                                  | -0.0103   | 1.8081                                                                   | 0.0047    |
| Average                                         |                                                              |                                                         | 1.0309                                                                                  |           | 1.8127                                                                   |           |

Ydm = Ratio of reading of wet test meter to dry test meter; tolerance for individual values "0.02 from average.

ΔH@ = Orifice pressure differential that equates to 0.75 cfm of air @ 68°F and 29.92 inches of mercury, in H2O; tolerance for individual values "0.20 from average.

|                      |        |
|----------------------|--------|
| Serial #:            | 10-006 |
| Calibration:         | pass   |
| +/- 5% from previous |        |

Calibrated by:

*Rayd Barber*

# ETS

EMISSION TESTING SERVICES, INC.

## THERMOCOUPLE CALIBRATION

Meter Box Number: 3  
 Barometric Pressure: 29.821  
 Serial #: 0

Date: 06/15/04  
 Calibrated By: Boyd Barbier  
 +/- 1.5% from previous: ☒ PASS ☐ FAIL

| LOW CHECK POINT |                    |              |         |            |                                 |         |         |         |
|-----------------|--------------------|--------------|---------|------------|---------------------------------|---------|---------|---------|
| Channel Type    | Omega CL27 Reading |              |         |            | Thermocouple Reading            |         |         |         |
|                 | Trial 1            | Trial 2      | Trial 3 | Average    | Trial 1                         | Trial 2 | Trial 3 | Average |
| Stack           | 100                | 100          | 100     | 100        | 100                             | 100     | 100     | 100.00  |
| Probe           | 100                | 100          | 100     | 100        | 100                             | 100     | 101     | 100.33  |
| Hot Box         | 100                | 100          | 100     | 100        | 100                             | 101     | 100     | 100.33  |
| Umbilical       | 100                | 100          | 100     | 100        | 100                             | 100     | 100     | 100.00  |
| Channel Type    | Average Reading    |              |         | Difference | % Error (Diff / Avg CL27) • 100 |         |         |         |
|                 | Omega CL27         | Thermocouple |         |            | -1.5 % < %Error < +1.5 %        |         |         |         |
| Stack           | 100                |              | 100.00  | 0.00       | 0.00                            |         |         |         |
| Probe           | 100                |              | 100.33  | 0.33       | 0.33                            |         |         |         |
| Hot Box         | 100                |              | 100.33  | 0.33       | 0.33                            |         |         |         |
| Umbilical       | 100                |              | 100.00  | 0.00       | 0.00                            |         |         |         |

| MID CHECKPOINT |                    |              |         |            |                                 |         |         |         |
|----------------|--------------------|--------------|---------|------------|---------------------------------|---------|---------|---------|
| Channel Type   | Omega CL27 Reading |              |         |            | Thermocouple Reading            |         |         |         |
|                | Trial 1            | Trial2       | Trial 3 | Average    | Trial 1                         | Trial 2 | Trial 3 | Average |
|                | 500                | 500          | 500     | 500        | 500                             | 500     | 500     | 500.00  |
| Probe          | 500                | 500          | 500     | 500        | 500                             | 500     | 501     | 500.33  |
| Hot Box        | 500                | 500          | 500     | 500        | 500                             | 501     | 500     | 500.33  |
| Umbilical      | 500                | 500          | 500     | 500        | 500                             | 500     | 500     | 500.00  |
| Channel Type   | Average Beading    |              |         | Difference | % Error (Diff / Avg CL27) * 100 |         |         |         |
|                | Omega CL27         | Thermocouple |         |            | -1.5 % < %Error < +1.5 %        |         |         |         |
| Stack          | 500                | 500.00       |         | 0.00       | 0.00                            |         |         |         |
| Probe          | 500                | 500.33       |         | 0.33       | 0.01                            |         |         |         |
| Hot Box        | 500                | 500.33       |         | 0.33       | 0.07                            |         |         |         |
| Umbilical      | 500                | 500.00       |         | 0.00       | 0.00                            |         |         |         |

| HIGH CHECK POINT |                    |              |         |            |                                 |         |         |         |
|------------------|--------------------|--------------|---------|------------|---------------------------------|---------|---------|---------|
| Channel Type     | Omega CL27 Reading |              |         |            | Thermocouple Reading            |         |         |         |
|                  | Trial 1            | Trial 2      | Trial 3 | Average    | Trial 1                         | Trial 2 | Trial 3 | Average |
| Stack            | 950                | 950          | 950     | 950        | 950                             | 950     | 951     | 950.33  |
| Probe            | 950                | 950          | 950     | 950        | 950                             | 950     | 950     | 950.00  |
| Hot Box          | 950                | 950          | 950     | 950        | 951                             | 951     | 951     | 951.00  |
| Umbilical        | 950                | 950          | 950     | 950        | 951                             | 950     | 951     | 950.67  |
| Channel Type     | Average Reading    |              |         | Difference | % Error (Diff / Avg CL27) * 100 |         |         |         |
|                  | Omega CL27         | Thermocouple |         |            | -1.5 % < %Error < +1.5 %        |         |         |         |
| Stack            | 950                | 950.33       |         | 0.33       | 0.04                            |         |         |         |
| Probe            | 950                | 950.00       |         | 0.00       | 0.00                            |         |         |         |
| Hot Box          | 950                | 951.00       |         | 1.00       | 0.11                            |         |         |         |
| Umbilical        | 950                | 950.67       |         | 0.67       | 0.07                            |         |         |         |

APPENDIX B  
 7.2.2

# ETS

EMISSION TESTING SERVICES, INC.

Pitot Tube Number: P-10-5  
 Calibrated By: B. Barbier

CP(std): STD - 0.99  
 Date Calibrated: 06/18/04

| Point Number | Standard Pitot *P (in. H2O) | "S" Type Pitot *P, in H2O Impact Side | Static Side  |
|--------------|-----------------------------|---------------------------------------|--------------|
| Low          | <u>0.280</u>                | <u>0.410</u>                          | <u>0.400</u> |
| Mid          | <u>0.580</u>                | <u>0.810</u>                          | <u>0.800</u> |
| High         | <u>0.740</u>                | <u>1.050</u>                          | <u>1.050</u> |

## CALCULATIONS

$$Cp(s) = Cp(std) \times \left( \frac{*P(std)}{*P(s)} \right)^{1/2}$$

$$Deviation = |Cp(s) - Cp| \quad (\text{Impact Side or Static Side})$$

$$Avg. Dev. = \frac{\text{Low deviation} + \text{Mid deviation} + \text{High deviation}}{3} \quad (\text{Impact Side or Static Side})$$

|      | Impact Side Cp (s) | Deviation    | Static Side Cp(s) | Deviation    |
|------|--------------------|--------------|-------------------|--------------|
| Low  | <u>0.8181</u>      | <u>0.011</u> | <u>0.8263</u>     | <u>0.006</u> |
| Mid  | <u>0.8377</u>      | <u>0.009</u> | <u>0.8430</u>     | <u>0.009</u> |
| High | <u>0.8311</u>      | <u>0.002</u> | <u>0.8311</u>     | <u>0.003</u> |
| Cp = | <u>0.8290</u>      |              | <u>0.8341</u>     |              |

|                                       |   |              |                   |
|---------------------------------------|---|--------------|-------------------|
| * Cp(Static Side) - Cp(Impact Side) * | = | <u>0.005</u> | (Must be <= 0.01) |
| Average Deviation (Impact Side)       | = | <u>0.007</u> | (Must be <= 0.01) |
| Average Deviation (Static Side)       | = | <u>0.006</u> | (Must be <= 0.01) |

$$Cp = \underline{\underline{0.832}}$$

Pitot Tube Leak Check ☐ PASSED ☐ FAILED

# ETS

EMISSION TESTING SERVICES, INC.

TUBE NUMBER P-10-5 DATE 7-23-04

INSPECTOR NAME Joel Richard

- YES NO
- 1 ☒ ☐  $a_1$  and  $a_2 \leq 10^\circ$
- TRANSVERSE  
TUBE AXIS
- (a) (b)
- 2 ☒ ☐  $B_1$  and  $B_2 \leq 5^\circ$
- LONGITUDINAL  
TUBE AXIS
- (c) (d)
- (e)
- 3 ☒ ☐  $Z \leq .32\text{cm (1/8 in)}$
- (f)
- 4 ☒ ☐  $W \leq .008\text{cm (1/32 in)}$  (f)
- (g)

SIGNATURE [Signature]

C:\WS\FORMS\TUBE

# ETS

EMISSION TESTING SERVICES, INC.

## SAMPLING NOZZLE CALIBRATION DATA FORM

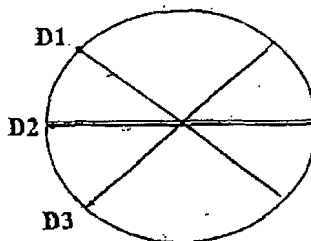
NOZZLE I.D. NO. 170  
COMPANY NAME Bayou Steel  
SOURCE LD. Baghouse Stack

| DATE CALIBRATED | CALIBRATED BY | NOZZLE MEASUREMENTS <sup>a</sup> |      |      | MAXIMUM AD <sup>b</sup> | D avg. <sup>c</sup> |
|-----------------|---------------|----------------------------------|------|------|-------------------------|---------------------|
|                 |               | D1                               | D2   | D3   |                         |                     |
| 7-23-04         | Joel Richard  | .170                             | .170 | .170 | $\emptyset$             | .170                |

<sup>a</sup>CORRECT NOZZLE DIAMETER MEASUREMENTS AS INDICATED IN THE DIAGRAM TO THE NEAREST 0.001 INCH

<sup>b</sup>MAXIMUM DEFERENCE BETWEEN ANY TWO DIAMETERS. ACCEPTANCE LIMIT: MAXIMUM  $\Delta \leq 0.004$  INCH

<sup>c</sup>AVERAGE OF D1 PLUS D2 PLUS D3.



SIGNATURE

*[Handwritten Signature]*

APPENDIX B  
7.2.5

**ETS<sub>R</sub>**

**EMISSION TESTING SERVICES, INC.**

---

**BAROMETER CALIBRATION SHEET**

---

**CLIENT: BAYOU STEEL**

**DATE: 7-22-04**

**SOURCE ID: BAGHOUSE STACK**

**OPERATOR: RON MCCABE**

**\*\*\*\*\*BAROMETER\*\*\*\*\***

**BAROMETER ID: UNIT #1**

**CALIBRATION DATA:**

**INITIAL CALIBRATION: 29.95    INITIAL    29.95    FINAL**

**ADJUSTMENT: ☐ Yes**

**☒ No**

**\*\*\*\*\*CALIBRATION REFERENCE\*\*\*\*\***

**ID: PRINCO, HG**

**ELEVATION: BATON ROUGE**

**ELEVATION DIFF: N/A**

**BAROMETER READING: 29.96**

**COMMENTS:** \_\_\_\_\_  
\_\_\_\_\_  
\_\_\_\_\_

**BAYOU STEEL CORPORATION**

July 12, 2004

**FAXSIMILE  
225/219-3474**

Mr. Jim Courville  
Office of Environmental Assessment  
Louisiana Department of Environmental Quality  
P.O. Box 4314  
Baton Rouge, LA 70821-4314

**RE: Bayou Steel Corporation Notification of Intent to Test and Summary of  
Pretest Meeting**

Dear Mr. Courville:

This is a summary of the pretest meeting held the DEQ office on July 12, 2004. The list of meeting attendees is appended as Exhibit I.

On Friday, July 23, 2004, ETS will perform a stack test at Bayou Steel Corporation on the main stack, source 1-77, for mercury and lead. The test methods to be utilized are EPA Methods 1-4 and Method 29. The detection limit for mercury will be 0.1 lbs/hr. The plant operating data at the time of the test to be supplied includes: tons/hour of scrap melted, the scrap mix utilized, the electrical power, natural gas, carbon and oxygen utilized. The testing duration will be 3 hours and will include one complete melting cycle from charge to tap per hour.

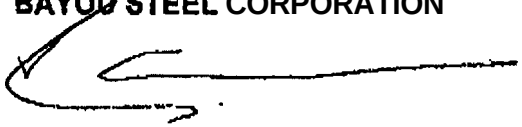
At the time of the test a sample will also be collected from the Secondary Dust Collection System, sources 2-77A-F. This sample will be analyzed for mercury and the results will be provided to DEQ.

Bayou Steel will also investigate previous sampling events at the shredder cyclones and will provide DEQ with an estimated mercury value.

Attached is the Notification of Intent to Test for the stack test to occur on July 23.

If you have any questions or require additional information, please do not hesitate to contact me,

Respectfully,  
**BAYOU STEEL CORPORATION**



Wendy Stehling  
Manager, Environmental, Health & Safety

c: Barry Gipson, ETS  
Linda Brown, LDEQ  
Freddie Touro, LDEQ  
Jennifer Pelloat, LDEQ  
Al Pulliam, Bayou Steel Corporation

## NOTIFICATION OF INTENT TO TEST

## FACILITY INFORMATION

Facility Name: Bayou Steel Corporation  
Street Address: 138 Highway 321.7 70068  
Post Office Box: Po Box 5000  
City/State/Zip: LaPlace LA 70069  
Contact name for testing purposes: Wendy Stehling  
Contact's phone number: 985/652-0322  
Contact's fax number: 985/652-0373  
E-Mail: wendys@bayousteel.com  
Type of Permit: State ☒ NSPS ☐ Other ☐  
State Permit Number: 885 (m-2)  
State Permit Writer: Gus Von Bodungen - issued permit  
Federal Permit Number: \_\_\_\_\_  
Federal Permit Writer: \_\_\_\_\_  
If Other, Explain: \_\_\_\_\_

## NOTIFICATION

30-Day Notice Given: Yes ☒ No ☐  
TO Whom: LA DEQ  
Was a pretest meeting required: Yes ☒ No ☐ (if answer was yes, see Exhibit 1)

PROPOSED TEST DATE(S): JULY 23, 2004

## TEST COMPANY INFORMATION

Emission Testing Services, Inc. (ETS)  
Post Office Box 15075  
Baton Rouge, LA 70895

10461 Mammoth Drive  
Baton Rouge, LA 70814

Contact Person: Barry Gipson  
General Manager  
Phone No. (225)925-8408  
Fax No. (225)925-2343  
E-Mail: bgipson@emissiontesting.com  
Home Page: www.Emissiontesting.com

File:\forms\NOTI-TEST

**EXHIBIT 1****PRETEST MEETING ATTENDEES**DATE OF MEETING: 7/12/04Bayou Steel

| NAME             | PHONE          | AFFILIATION              |
|------------------|----------------|--------------------------|
| Jennifer Pellaat | 225-219-3432   | LDEQ / Eng Group 1       |
| Cedric Mellon    | 225-219-3999   | DEQ - EED - TEDI         |
| Nicholas LaCroix | 225-219-3501   | DEQ - EED - TRI          |
| Timothy Bergeron | 225/219-3431   | LDEQ / Eng 1             |
| Freddie Toura    | (225) 291-7122 | LDEQ / Permits           |
| Denise Bennett   | (225) 219-3086 | LDEQ / Permits - Air     |
| Clay Robinson    | (225) 219-3760 | LDEQ / Enforcement - Air |
| Jim Courville    | (225) 219-3428 | LDEQ / Eng #1            |
| Jim ORGERON      | (225) 275-3231 | LDEQ / PLANS             |
| Trevor Telle     | (225) 219-3105 | LDEQ / PERMITS           |
| DARY GIPSON      | (225) 925-8405 | ETS                      |
| Wendy Stehling   | 985/652-0322   | Bayou Steel Corp.        |
| Linda Brown      | (225) 219-3535 | DEQ / EED / TRI + TEDI   |
| Al Pulliam       | 985 652-0409   | Bayou Steel              |
|                  |                |                          |
|                  |                |                          |
|                  |                |                          |



State of Louisiana  
Department of Environmental Quality



Edwin W. Edwards  
Governor

William A. Kucharski  
Secretary

Mr. Al Pulliam  
Environmental Manager  
Bayou Steel Corporation  
P. O. Box 5000  
LaPlace LA 70069

Dear Mr. Pulliam:

RE: Permit modification, Bayou Steel Corporation, LaPlace,  
St. John the Baptist Parish, Louisiana

This is to inform you that the permit modification requested for the above referenced facility has been approved under LAC 33:III.501. The submittal was approved on the basis of the emissions reported and the approval in no way guarantees the design scheme presented will be capable of controlling the emissions to the types and quantities stated. A revised application must be submitted if the reported emissions are exceeded after operation begins. The synopsis, data sheets, and conditions are attached herewith.

It will be considered a violation of the permit if all proposed control measures and/or equipment are not installed and properly operated and maintained as specified in the application.

The permit number cited below should be referenced in future correspondence regarding this subject.

Done this 5<sup>th</sup> day of MAY, 1995:

Permit No.: 885 (M-2)

Very truly yours,

*Gustave A. Von Bodungen*  
Gustave A. Von Bodungen, P.E.  
Assistant Secretary

GVB/WL

c: Southeast Regional Office



OFFICE OF AIR QUALITY P.O. BOX 82135 BATON ROUGE, LOUISIANA 70884-2135  
AN EQUAL OPPORTUNITY EMPLOYER

APPENDIX D  
7.4.1

AIR PERMIT BRIEFING SHEET  
AIR QUALITY DIVISION  
LOUISIANA DEPARTMENT OF ENVIRONMENTAL QUALITY

BAYOU STEEL CORPORATION  
LAPLACE, ST. JOHN THE BAPTIST PARISH, LOUISIANA

**I. BACKGROUND**

Bayou Steel Corporation operates an Electric Arc Furnace (EAF) steel mill in LaPlace, Louisiana. It was originally permitted on February 28, 1978 (Permit No. 885). A PSD permit (PSD-LA-66), issued February 15, 1983, for NO<sub>x</sub> emissions, was later rescinded. Permit No. 885(M-1) was issued October 28, 1983. Nitrogen oxides (NO<sub>x</sub>) emissions from the electric arc furnace (EAF) during melting and refining operations were not included in the referenced permit as NO<sub>x</sub> was not recognized as a precursor to ozone formation at that time. Accounting for fugitive emissions in permitting began only after 1990. The application for the present modification was first submitted in December, 1993, but later withdrawn because fugitive emissions were not included. The revised submittal was dated August 4, 1994. Supplemental information was received March 22, 1995.

**If. ORIGIN**

A permit application and Emission Inventory Questionnaire for this modification was received August 5, 1994. The commitment to submit an updated air permit application and EIQ was made in response to a Notice of Violation (NOV), issued by DEQ on June 3, 1994. The purpose of this submittal is to provide speciation of hazardous air pollutants (HAP) and to include fugitive emissions. Electric arc furnace (EAF) NO<sub>x</sub> emissions, missing from the previous permit modification, are included in this modification.

**III. DESCRIPTION**

Bayou Steel operates two separate EAFs. Scrap steel, coke lime, flux, and alloys are melted in a refractory-lined kettle using three high-voltage electrodes to produce a recovered steel product.

In preparation for charging and melting of the steel, the furnace electrodes are aligned and the furnace lining is coated with a protective layer of gunite at the slag zone. The furnace is loaded with the initial charge of scrap steel and other materials. The roof, in which the electrodes are

**AIR PERMIT BRIEFING SHEET  
AIR QUALITY DIVISION  
LOUISIANA DEPARTMENT OF ENVIRONMENTAL QUALITY**

**BAYOU STEEL CORPORATION  
LAPLACE, ST. JOHN THE BAPTIST PARISH\* LOUISIANA**

housed, is placed onto the furnace and the electrical current is applied. After the first charge is melted, the EAF roof is removed from the furnace and a second charge of scrap steel, coke, lime and flux is added. The furnace roof is lowered onto the furnace and current again applied to melt the second charge. A third charge is added repeating the steps of the second charge. After the final meltdown, the molten steel is subjected to an oxygen injection period to further oxidize impurities and combine with any excess carbon to form carbon dioxide.

In a final refining stage, oxygen flow is discontinued with the electrical current still applied. The EAF vessel is first tilted backwards to empty slag into the slag pot, where it is water cooled and then placed on a slag pile. Liquid molten steel is poured into a teeming ladle when the vessel is tilted forward, completing a single EAF heat.

Molten steel is poured from the ladle to the continuous casting machine via an overhead crane. The ladle is placed on a turret which rotates to position the ladle over the continuous casting tundish. The ladle empties into four individual water-cooled copper billet molds. Steel leaves the mold as a solid steel casing with a liquid core. A continuous strand of steel is further cooled by water sprays as it is drawn from the mold and cut into various lengths by an oxygen cutting torch. The billets are transferred to the finishing area where they are allowed to cool.

Billets are sold or further processed in the hot forming rolling mill into angles, channels and I beams. A maximum of 600,000 tons of billets is anticipated to be produced, requiring 1.4 MM BTU of natural gas for each ton of billets charged.

~articulate emissions from the slag piles are controlled by wetting with water.

The Primary Dust Collection system (Emission Point No. 1-77) captures particulates during melting and refining operations (when the roof and electrodes are in place). The Secondary Dust Collection System (Emission Points 2-77A through F) collects particulates during charging and tapping operations (when the roof is removed). A canopy system around the EAF

AIR PERMIT BRIEFING SHEET  
AIR QUALITY DIVISION  
LOUISIANA DEPARTMENT OF ENVIRONMENTAL QUALITY

BAYOU STEEL CORPORATION  
LAPLACE, ST. JOHN TEE BAPTIST PARISH, LOUISIANA

captures emissions from the uncovered furnace and routes them to the Secondary Dust Collection System baghouse for collection. Although it has been shown as a single point source in previous EIQ submittals, this baghouse actually has six separate vents. The furnace house vacuuming operations collect dust from the furnace house floor. Baghouse filters and vacuum bags are periodically dumped into an EAF during a routine charging sequence.

Bayou Steel's operation is regulated under New Source Performance Standards, 40 CFR 60 Subpart AA-Standards of Performance for Steel Plants: Electric Arc Furnaces Constructed After October 21, 1974 and on or Before August 17, 1983, for particulate emissions. Compliance with 0.0052 gr/dscf limit for the Primary Dust Collection System was demonstrated during a stack test performed during March, 1984. The average value obtained was 0.0029 gr/dscf which corresponds to an average rate of 2.15 pounds per hour total suspended particulates (TSP or 1.63 for  $PM_{10}$ ).

EIQ sheets were submitted for five diesel and two gasoline storage tanks ranging in size from 200 to 9,000 gallons. Total emission from the seven tanks is less than one ton. All of the tanks storing VOCs are equipped with submerged fill pipes. Only the two gasoline tanks are included in this permit. The diesel tanks meet the criteria for insignificant sources and, therefore, are not included in the permit.

Emissions summary, in tons per year.(TPY), is as follows:

| <u>Pollutant</u> | <u>permitted<br/>Before</u> | <u>Proposed</u> | <u>Change</u> |
|------------------|-----------------------------|-----------------|---------------|
| TSP*             | 62.9                        | 58.2            | - 4.7         |
| $PM_{10}$        | -                           | 37.2            | + 37.2        |
| SO <sub>2</sub>  | 0.9                         | 0.3             | - 0.6         |
| NO <sub>x</sub>  | 119.7**                     | 149.1           | + 29.4        |
| VOC              | 1.0                         | 2.2             | + 1.2         |
| CO               | 5.4                         | 15.0            | + 9.6         |

\*See Attachment A for speciation of solid HAPs. Total particulates only were permitted previously.

\*\*This figure is adjusted for inclusion of NO<sub>x</sub> emissions omitted in error from the M-1 modification of Permit No. 885.

AIR PERMIT BRIEFING SHEET  
AIR QUALITY DIVISION  
LOUISIANA DEPARTMENT OF ENVIRONMENTAL QUALITY

BAYOU STEEL CORPORATION  
LAPLACE, ST. JOHN THE BAPTIST PARISH, LOUISIANA

Increases are due to increase in operating hours which results in an increase in the annual charge rate to the furnace. Since, there was no modification, PSD review is not triggered. Decreases are due to differences in emission factors.

IV. TYPE OF REVIEW'

The permit was reviewed for compliance with the Louisiana Air Quality Regulations and NSPS. Prevention of Significant Deterioration and NESHAP do not apply.

This facility is a major source of toxic air pollutants (TAP) because their potential to emit is above the 10/25 threshold. The compliance plan for the facility was approved April 13, 1995. This permit establishes limits within the constraints of said compliance plan.

V. PUBLIC NOTICE

Public notice is not required for a minor modification to an existing source.

SPECIFIC CONDITIONS

BAYOU STEEL CORPORATION  
LAPLACE, ST. JOHN. THE BAPTIST PARISH, LOUISIANA

1. Permittee shall comply with all applicable provisions of 40 CFR 60 Subpart AA - Steel Plants: Electric Arc Furnaces Constructed After October 21, 1974 and on or Before August 17, 1983.
2. Permittee shall maintain the dust filters of the baghouse, Emission Point No. 1-77, and the baghouse serving Emission Point Nos. 2-77A thru F, so that particulate removal efficiencies of 99% are maintained. Filter vents shall be visually inspected for opacity on a daily basis. The filter elements (bags) shall be inspected every six months and changed as necessary. Records of opacity checks and maintenance inspections of the dust filters shall be kept on site and available for inspection by the Air Quality Division.

BAYOU STEEL CORPORATION  
LAPLACE, ST. JOHN THE BAPTIST PARISH, LOUISIANA

ATTACHMENT A

HAP speciation in tons per year  $\times 10^{-2}$  (TPY  $\times 10^{-2}$ ):

| Emission Pt.No. | As    | Ba    | Cd    | Cr    | Cu    | Pb    | Mn    | Ni    | Zn    | Total |
|-----------------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|
| 1-77            | 0.042 | 0.323 | 0.444 | 3.099 | 2.834 | 19.72 | 29.66 | 0.399 | 134.3 | 190.8 |
| 2-77A           | 0.005 | 0.041 | 0.056 | 0.391 | 0.358 | 2.490 | 3.744 | 0.050 | 16.96 | 24.1  |
| 2-77B           | 0.005 | 0.041 | 0.056 | 0.391 | 0.358 | 2.490 | 3.744 | 0.050 | 16.96 | 24.1  |
| 2-77C           | 0.005 | 0.041 | 0.056 | 0.391 | 0.358 | 2.490 | 3.744 | 0.050 | 16.96 | 24.1  |
| 2-77D           | 0.005 | 0.041 | 0.056 | 0.391 | 0.358 | 2.490 | 3.744 | 0.050 | 16.94 | 24.1  |
| 2-77E           | 0.005 | 0.041 | 0.056 | 0.391 | 0.358 | 2.490 | 3.744 | 0.050 | 16.94 | 24.1  |
| 2-77F           | 0.005 | 0.041 | 0.056 | 0.391 | 0.358 | 2.490 | 3.744 | 0.050 | 16.94 | 24.1  |
| 1-94            | 0.178 | 1.360 | 1.871 | 13.06 | 11.94 | 83.10 | 124.9 | 1.682 | 565.9 | 804.0 |
| 2-94            | 0.003 | 0.021 | 0.029 | 0.204 | 0.187 | 1.299 | 1.954 | 0.026 | 8.85  | 12.6  |
| Totals          | 0.253 | 1.95  | 2.68  | 18.7  | 17.1  | 119.1 | 179.0 | 2.4   | 810.8 | 1152  |

\*The concentrations were derived from analyses of baghouse dust averaged over a 21-month period. They are amounts contained in total suspended particulates (TSP), not just  $PM_{10}$ .

**AIR QUALITY DATA SHEET**  
PAGE 1

**BAYOU STEEL CORPORATION**  
**LAPLACE, ST. JOHN THE BAPTIST PARISH, LOUISIANA**

Location of plant: '15 UTM: 744.7 km E 3325.5 km N

Description of location: Between River Road and Airline Highway approximately 2 miles south of LaPlace

Estimated starting date of construction operating Estimated starting operation will begin \_\_\_\_\_

Dispersion Model(s) Used: NA

NEW \_\_\_\_\_ OR MODIFIED X EMISSION SOURCES Scrap Metal Recovery  
(Type of Source)

| Emission Point No. | Description                      | Operating Rate (Max) or Tank Capacity | Operating Schedule |     |     |
|--------------------|----------------------------------|---------------------------------------|--------------------|-----|-----|
|                    |                                  |                                       | H/D                | D/W | W/Y |
| 1-77               | Primary Dust Collection System   | 292,000 cu ft/min                     | 24                 | 7   | 52  |
| 2-77A              | Secondary Dust Collection System | 68,333 cu ft/min                      | 24                 | 7   | 52  |
| 2-77B              | Secondary Dust Collection System | 68,333 cu ft/min                      | 24                 | 7   | 52  |
| 2-77C              | Secondary Dust Collection System | 68,333 cu ft/min                      | 24                 | 7   | 52  |
| 2-77D              | Secondary Dust Collection System | 68,333 cu ft/min                      | 24                 | 7   | 52  |
| 2-77E              | Secondary Dust Collection System | 68,333 cu ft/min                      | 24                 | 7   | 52  |
| 2-77F              | Secondary Dust Collection System | 68,333 cu ft/min                      | 24                 | 7   | 52  |
| 4-77               | Rolling Mill Furnace             | 77.2 MM BTU/hr                        | 24                 | 7   | 52  |
| 1-94               | Furnace House Fugitives          | N/A                                   | 24                 | 7   | 52  |
| 2-94               | Slag Pile Fugitives              | N/A                                   | 24                 | 7   | 52  |
| 3-94               | A Bay Heater No. 1               | 1.5 MM BTU/hr                         | 24                 | 7   | 22  |
| 4-94               | A Bay Heater No. 2               | 1.5 MM BTU/hr                         | 24                 | 7   | 22  |

APPENDIX D  
7.4.8

**AIR QUALITY DATA SHEET**

PAGE 1 (CONTINUED)

BAYOU STEEL CORPORATION  
**LAPLACE, ST. JOHN THE BAPTIST PARISH, LOUISIANA**

| Emission<br>Point No. | Description                       | Operating<br>Rate (Max)<br>or Tank Capacity | Operating Schedule |     |     |
|-----------------------|-----------------------------------|---------------------------------------------|--------------------|-----|-----|
|                       |                                   |                                             | H/D                | D/W | W/Y |
| 5-94                  | A Bay Heater No. 3                | 1.5 MM BTU/hr                               | 24                 | 7   | 22  |
| 6-94                  | B Bay Heater No. 4                | 3.0 MM BTU/hr                               | 24                 | 7   | 22  |
| 7-94                  | B Bay Heater No. 5                | 3.0 MM BTU/hr                               | 24                 | 7   | 52  |
| 8-94                  | B Bay Heater No. 6                | 3.0 MM BTU/hr                               | 24                 | 7   | 52  |
| 11-94                 | Mechanic Shop Gasoline Tank No. 3 | 1100 gal                                    | 24                 | 7   | 52  |
| 14-94                 | IMS Gasoline Tank No. 6           | 800 gal                                     | 24                 | 7   | 52  |

APPENDIX D  
7.4.9

**AIR QUALITY DATA SHEET**  
**PAGE 2**

**BAYOU STEEL CORPORATION**  
**LAPLACE, ST. JOHN THE BAPTIST, PARISH, LOUISIANA**

**MAXIMUM/AVERAGE EMISSIONS ARE LISTED IN LBS/HR**

| Emission<br>Point No. | PM <sub>10</sub> | SO <sub>2</sub> | Permitted Emissions<br>NOx | VOC         | CO        | OTHER | HEIGHT<br>Feet | TEMP<br>°F | FLOW RATE<br>CFM |
|-----------------------|------------------|-----------------|----------------------------|-------------|-----------|-------|----------------|------------|------------------|
| <b>1-N</b>            | 2.93/1.63        | 0.01/0.01       | 20.36/20.36                |             | -         | -     | 162.5          | 257        | 292,000          |
| 2-TIA                 | 0.258/0.21       |                 |                            |             | -         | -     | 143.2          | 104        | 68,333           |
| 2-77B                 | 0.258/0.21       |                 |                            |             | -         | -     | 143.2          | 104        | 68,333           |
| 2-TIC                 | 0.258/0.21       |                 |                            |             | -         | -     | 143.2          | 104        | 68,333           |
| 2-77D                 | 0.258/0.21       |                 |                            |             | -         | -     | 143.2          | 104        | 68,333           |
| 2-77E                 | 0.258/0.21       |                 |                            |             | -         | -     | 143.2          | 104        | 68,333           |
| 2-77F                 | 0.258/0.21       |                 |                            |             | -         | -     | 143.2          | 104        | 68,333           |
| 4-77                  | 0.44/0.28*       | 0.09/0.06       | 20.36/12.91                | 0.41/0.26   | 5.08/3.22 |       | 143.3          | 700        | 44,490           |
| 1-94                  | 6.57/5.25        | -               |                            |             | -         | -     | NA             | ambient    | NA               |
| 2-94                  | 0.064/0.064      |                 |                            |             | -         | -     | NA             | ambient    | NA               |
| 3-94                  | 0.004/0.004      | <0.01/0.01      | 0.20/0.20                  | <0.01/<0.01 | 0.05/0.05 | -     | NA             | 375        | 285              |
| 4-94                  | 0.004/0.004      | <0.01/0.01      | 0.20/0.20                  | <0.01/<0.01 | 0.05/0.05 | -     | NA             | 375        | 285              |
| 5-94                  | 0.004/0.004      | <0.01/0.01      | 0.20/0.20                  | <0.01/<0.01 | 0.05/0.05 | -     | NA             | 375        | 285              |
| 6-94                  | 0.01/0.01        | <0.01/0.01      | 0.40/0.40                  | 0.01/0.01   | 0.10/0.10 |       | NA             | 375        | 570              |
| 7-94                  | 0.01/0.01        | <0.01/0.01      | 0.40/0.40                  | 0.01/0.01   | 0.10/0.10 | -     | NA             | 375        | 570              |
| 8-94                  | 0.01/0.01        | <0.01/0.01      | 0.40/0.40                  | 0.01/0.01   | 0.10/0.10 | -     | NA             | 375        | 570              |
| 11-94                 |                  |                 |                            | 0.12/0.12   | -         | -     | NA             | ambient    | NA               |
| 14-94                 |                  |                 |                            | 0.09/0.09   | -         | -     | NA             | ambient    | NA               |

\*PM<sub>10</sub> emissions due to combustion of natural gas and process.

# AIR QUALITY DATA SHEET

PAGE 3

BAYOU STEEL CORPORATION  
LAPLACE, ST. JOHN THE BAPTIST PARISH, LOUISIANA

| Permitted emissions are listed in tons per year |                    |                 |                 |      |      |       |
|-------------------------------------------------|--------------------|-----------------|-----------------|------|------|-------|
| Emission Point No.                              | PM <sub>10</sub> * | SO <sub>2</sub> | NO <sub>x</sub> | VOC  | CO   | OTHER |
| 1-77                                            | 7.2                | 0.04            | 89.2            | -    | -    | -     |
| 2-77A                                           | 0.90               | -               | -               | -    | -    | -     |
| 2-77B                                           | 0.90               | -               | -               | -    | -    | -     |
| 2-77C                                           | 0.90               | -               | -               | -    | -    | -     |
| 2-77D                                           | 0.90               | -               | -               | -    | -    | -     |
| 2-77E                                           | 0.90               | -               | -               | -    | -    | -     |
| 2-77F                                           | 0.90               | -               | -               | -    | -    | -     |
| 4-77                                            | 1.22               | 0.24            | 56.5            | 1.13 | 14.1 | -     |
| 1-94                                            | 23.0               | -               | -               | -    | -    | -     |
| 2-94                                            | 0.28               | -               | -               | -    | -    | -     |
| 3-94                                            | 0.01               | <0.01           | 0.37            | 0.01 | 0.09 | -     |
| 4-94                                            | 0.01               | <0.01           | 0.37            | 0.01 | 0.09 | -     |
| 5-94                                            | 0.01               | <0.01           | 0.37            | 0.01 | 0.09 | -     |
| 6-94                                            | 0.02               | <0.01           | 0.75            | 0.02 | 0.19 | -     |
| 7-94                                            | 0.02               | <0.01           | 0.75            | 0.02 | 0.19 | -     |
| 8-94                                            | 0.02               | <0.01           | 0.75            | 0.02 | 0.19 | -     |
| 11-94                                           | -                  | -               | -               | 0.54 | -    | -     |
| 14-94                                           | -                  | -               | -               | 0.41 | -    | -     |
| TOTALS                                          | 37.2               | 0.28            | 149.1           | 2.2  | 15.0 | -     |

\*See Attachment A for speciation of HAP in particulates.

885 M-2

**SPECIFIC CONDITIONS**

**BAYOU STEEL CORPORATION**  
**LAPLACE, ST. JOHN THE BAPTIST PARISH, LOUISIANA**

1. Permittee shall comply with all applicable provisions of 40 CFR 60 Subpart AA - Steel Plants: Electric Arc Furnaces Constructed After October 21, 1974 and on or Before August 17, 1983.
2. Permittee shall maintain the dust filters of the baghouse, Emission Point No. 1-77, and the baghouse serving Emission Point Nos. 2-77A thru F, so that particulate removal efficiencies of 99% are maintained. Filter vents shall be visually inspected for opacity on a daily basis. The filter elements (bags) shall be inspected every six months and changed as necessary. Records of opacity checks and maintenance inspections of the dust filters shall be kept on site and available for inspection by the Air Quality Division.

STONE, PIGMAN, WALTHER, WITTMANN & HUTCHINSON

SAUL STONE\*  
PAUL O. H. PIGMAN\*  
EWELL A. WALTHER, JR.\*  
PHILLIP A. WITTMANN  
CAMPELLE C. HUTCHINSON\*  
DAVID L. STONE\*  
WILLIAM D. TREEBY\*  
HIRSCHEL T. ABBOTT, JR.\*  
MICHAEL R. FORTHAM\*  
ANTHONY M. DILEO\*  
WAYNE J. LEE\*  
CLINTON W. SHINN\*  
JAMES C. GULOTTA, JR.\*  
PAUL L. ZIMMERING  
JOHN M. LANDIS  
STEPHEN M. KUPPERMAN  
JO HARRIET STRICKLER\*  
STEPHEN G. BULLOCK  
SARAH S. VANCE

\*A PROFESSIONAL CORPORATION

COUNSELLORS AT LAW  
1000 WHITNEY BANK BUILDING  
NEW ORLEANS, LOUISIANA 70130-2662  
(504) 581-3200 TELEX 564126

November 9, 1983

KYLE SCHONEKAS  
CHARLES L. STERN, JR.  
KAY W. EAGAN  
BRUCE SPIZER  
CATHY O. GLASER  
STEVEN W. USOH  
JUDY Y. BARRASSO  
SUSAN G. TALLEY  
WILLIAM C. BROWN  
DAVID W. GRUNING  
SHEILA M. LAMBERT  
DOUGLAS D. DODD  
RANDALL A. SMITH  
CHARLES R. PENOT, JR.  
LONDA R. GALLAGHER  
NOEL J. DANCE

OUR FILE NUMBER

40,728-D

Mr. Dietmar Sainitzer  
Mr. Bruce Eskew  
Mr. Mike McEarl  
Bayou Steel Corporation  
P. O. Box 5000  
LaPlace, Louisiana 70068

Re: Louisiana Permit 885-M-1

Gentlemen:

I enclose herewith a copy of State Air Permit 885-M-1. Larry Schumer of Waldemar S. Nelson and Company advises that this permit is an interim step toward rescission and replacement of the PSD Permit.

Before the PSD Permit can be rescinded by the Environmental Protection Agency, an operating permit must be in place, and therefore Permit 885-M-1 has been issued. If, and after, the PSD Permit is rescinded, Larry advises that we can anticipate issuance of a more stringent and more detailed state permit as the permanent Air Quality Permit.

Sincerely,

Original Signed

CLINTON W. SHINN

Clinton W. Shinn

CWS/sh  
Encl.

cc: Larry Schumer  
Harold Himmelman, Esq.  
John Guttman, Esq.  
Paul Shorb, Esq.

APPENDIX D  
7.4.13



FRANK P. SIMONEAUX  
SECRETARY

B. JIM PORTER  
ASSISTANT SECRETARY

DEPARTMENT OF NATURAL RESOURCES  
OFFICE OF ENVIRONMENTAL AFFAIRS  
AIR QUALITY DIVISION

GUSTAVE VON BODUNGEN  
PROGRAM ADMINISTRATOR

October 28, 1983

Mr. Ewell P. Walther, Jr.  
Bayou Steel Corporation  
Post Office Box 5000  
LaPlace, Louisiana 70068

Dear Mr. Walther:

RE: Revision of State Permit 885 issued February 28, 1978. Total Emissions: Particulates 65.98 TPY, Sulfur Dioxide 1.002 TPY, Oxides of Nitrogen **77.80** TPY, Hydrocarbons **1.5** TPY, and Carbon Monoxide 9.22 TPY.

**This** is to confirm that the permit request for the above referenced project at the **LaPlace** Facility, **LaPlace, St. John the Baptist Parish, Louisiana** has been approved by the Assistant Secretary, **Office** of Environmental Affairs, Department of Natural Resources, under Air Quality Regulation **6.1.1**. The submittal was approved on the **basis** of the emissions reported and the approval in no way guarantees the design scheme presented will be capable of controlling the emissions to the types and quantities stated. A new application must be submitted if the reported emissions are exceeded after operation **begins**. The emission and operating limitations are described in attached synopsis, data sheets and conditions.

It **will** be considered a violation of the permit if all proposed **control** measures and/or equipment **are** not installed and properly operated and maintained as specified in the application, **and/or** the attached condition are not **satisfied**.

The permit number cited below should be referenced in, future correspondence regarding this subject.

Date: October 28, 1983  
Permit No: 885-M-1

Approved by:

*Gustave Von Bodungen*  
B. JIM PORTER

Assistant Secretary

BJP/PD/bap

Enclosures

cc: Southeast Regional Office  
U.S. EPA, Region  
Waldmar S. Nelsen and Company

LOUISIANA AIR CONTROL COMMISSION

BAYOU STEEL CORPORATION

LaPlace (St John the Baptist)

Bayou Steel Corporation requests a permit to construct and operate a steel manufacturing and forming facility on the Mississippi River in St John the Baptist Parish, Louisiana. The facility will process scrap steel and produce billets, sections, rods, rounds and angles for both export and domestic purposes.

The process units will consist of two Electric Arc Furnaces, two Continuous Casting Units and Hot Rolling Mill Equipment.

Scrap steel and scale recovered from within the steel works will be recycled to the furnaces whereas the environmentally stable slag, wastewater treatment sludge and dust from the fabric filters will be used as landfill on Bayou Steel's property. A variance to start construction was approved by the Commission at the January 24, 1978 hearing.

Overall emissions of the facility are summarized as follows:

|                 |                 |
|-----------------|-----------------|
| Particulate     | 65.98 tons/year |
| HC              | 1.58 tons/year  |
| SO <sub>2</sub> | 1.002 tons/year |
| CO              | 9.22 tons/year  |
| NO <sub>x</sub> | 77.80 tons/year |

The greatest sources of air pollution in the steel mill will be the electric arc furnaces when power is on and/or when oxygen is injected.

To control and limit the emissions, the company will install:

- 1) A primary dust control system which will provide for carbon monoxide incineration, cooling, and high efficiency (99%) dust removal by means of a fabric filter baghouse.

- 2) A secondary dust control system with fabric filter **baghouses** to collect dust emissions when the primary dust control system is disengaged during the electric arc furnaces charging and tapping operations.

Fugitive dust emissions primarily due to lime and additive receiving, transferring and feeding system will be collected **and** cleaned by a fabric filter baghouse.

Sulfur dioxide emissions will be controlled by firing the **rolling** mill furnace with natural gas, a clean **fuel**.

Hydrocarbon emissions will consist of those associated with storing kerosene (a non-volatile organic **compound**), which is required for auxiliary heat input to the electric arc furnaces, in a **1500** barrel cone roof tank.

The company has stated that all the mentioned emission control schemes and equipment will **comply** with both **LACC** Regulations and **EPA** New Source **Performance** Standards and will also **conduct** necessary tests, monitoring **and** reporting as required.

A significant air quality deterioration analysis for particulate and sulfur dioxide area increments **was** submitted to EPA and indicate that the standards will be met.

Submitted dispersion **calculations** indicate that ambient air quality standards **will** not be violated.

**BAYOU STEEL CORPORATION**

**LaPlace (St. John the Baptist)**

**RECOMMENDATION:**

Approval provided the following conditions are met.

- 1) The synopsis sheets and the attached data sheets establish the emission and operating limitations and are a part of the permit. **The** synopsis and data sheets are based on the application for **approval** of emissions dated June 21, 1983 with supplemental information submitted July 15, 1983. **The** application and supplemental **information** **ark** also considered part of this permit be reference.
- 2) Construction must commence within two years after the date of **approval**.
- 3) The permittee will submit to the Technical Secretary **seminannual** reports of progress defining the status of construction, noting any design **changes, modifications** or alterations in the construction schedule which have or may have an effect upon the **emission** rates or ambient air **quality levels**. Such reports shall continue to be submitted until such time as construction is certified **as** being complete.
- 4) Any emission testing performed for **purposes** of demonstrating **compliance** with the limitations set forth in Condition 1 shall be conducted in accordance with the methods described and referenced in Table 4 of the current Louisiana Air Control Commission Regulations.
- 5) The permittee **shall**, within **180** days after certifying the completion of **construction** prepare and **submit** to **the** Technical Secretary a report detailing the actual emission rates as **compared** to those limitations specified in Condition 1. The report shall also **include**, but not be limited to, malfunctions and upsets.

- 6) The permittee shall comply with all applicable New Source Performance Standards for Electric Arc Furnaces (40 CFR, Subpart AA).
- 7) The permittee shall maintain records of the hours of operation per calendar year for each source. These records shall be kept at the plant site for at least two years and made available to Air Quality Division.

LOUISIANA ENVIRONMENTAL CONTROL COMMISSION

Air Quality Data Sheet

Page 1

Bayou Steel Corporation

LaPlace, St. John the Baptist Parish

Location of plant: 15 UTM 744.7 Km E 3325.5 Km N

Description of location: The facility is located between River Road and

Airline Highway, approximately 2 miles south of LaPlace, and 2.3 miles  
north of Montz.

Estimated starting date

Estimated date opera-

of construction: Existing

tion will begin: \_\_\_\_\_

Type of Dispersion Calculations Used: Computer calculations using dispersion  
model PTMAX

EFFECTS ON AMBIENT AIR

| Pollutant       | Time Period | Calculated Maximum Ground Level Concentration | Louisiana Air Quality Standard |
|-----------------|-------------|-----------------------------------------------|--------------------------------|
| Particulate     | Annual      | 43 ug/m <sup>3</sup>                          | 60 ug/m <sup>3</sup>           |
|                 | 24 hour     | 100 ug/m <sup>3</sup>                         | 150 ug/m <sup>3</sup>          |
| SO <sub>2</sub> | Annual      | 1.86 ug/m <sup>3</sup>                        | 60ug/m <sup>3</sup>            |
|                 | 24 hour     | 34.1 ug/m <sup>3</sup>                        | 260 ug/m <sup>3</sup>          |
| NO <sub>x</sub> | Annual      | 18.5 ug/m <sup>3</sup>                        | 100ug/m <sup>3</sup>           |
|                 |             |                                               |                                |
|                 |             |                                               |                                |
|                 |             |                                               |                                |

NEW ☐ OR MODIFIED ☒ EMISSION SOURCES

Steel Mill

(Type of Source)

| Stack I.D. # | Description               | Operating Rate (Maximum) | Operating Schedule |         |        |
|--------------|---------------------------|--------------------------|--------------------|---------|--------|
|              |                           |                          | Hrs/Day            | Days/Wk | WKS/Yr |
| 1-77         | Primary Dust Collection   | 203,580 lbs.hr           | 24                 | 7       | 42.5   |
| 2-77         | Secondary Dust Collection |                          | 8                  | 7       | 42.5   |
| 4-77         | Rolling Mill Furnace      | 145.5 mscf/hr            | 24                 | 6       | 50     |
|              |                           |                          |                    |         |        |
|              |                           |                          |                    |         |        |
|              |                           |                          |                    |         |        |
|              |                           |                          |                    |         |        |
|              |                           |                          |                    |         |        |
|              |                           |                          |                    |         |        |
|              |                           |                          |                    |         |        |

## Air Quality Data Sheet - Page 2

Bayou Steel Corporation

(Company's Name)

**La Place, St. John the Baptist**

(Nearest Town)

(Parish)

EMISSIONS ARE LISTED USING THE UNITS LBS/HR

[illegible]

## Page 3

APPENDIX D  
7.4.21