AP32 Section:	12.5.1
Background Chapter	3
Reference:	31
Title:	Emissions Test Report for Sulfur Dioxide and Oxides of Nitrogen, Gallatin Steel Company, Ghent, KY (Permit Number F-96-009 Revision 1). May 4, 2000. Ambient Air Services, Inc., Starke, FL.

JAMES E. BICKFORD
SECRETARY

PAUL E. PATTON
GOVERNOR

31

COMMONWEALTH OF KENTUCKY
NATURAL RESOURCES AND ENVIRONMENTAL PROTECTION CABINET
DEPARTMENT FOR ENVIRONMENTAL PROTECTION
DIVISION FOR AIR QUALITY
803 SCHENKEL LN
FRANKFORT KY 40601-1403

June 19, 2000

Ms. Valerie A. Hudson, Manager
Environmental Systems
Gallatin Steel
R.R. #1, Box 320
Ghent, Kentucky 41045-9704

Dear Ms. Hudson:

On May 4, 2000, NO_x, and SO_2 compliance tests were performed on the Electric Arc Furnace baghouse at your Ghent facility. Ambient Air Services, Inc performed the testing. Gerald Slucher observed testing for the Division for Air Quality. Proper test methods were followed, and the test report was checked for completeness and accuracy. The results are summarized below.

PARAMETER	TEST RESULTS	PERMIT LIMIT
Sulfur Dioxide	0.10lb/ton, 19.0 lb/hr	0.2 lb/ton, 40 lb/hr
Nitrogen Oxides (as NO_2)	0.19lb/ton, 36.1 lb/hr	0.51 lb/ton, 102 lb/hr

Therefore, this test report is accepted as proof of compliance for sulfur dioxide and nitrogen oxides. A copy of this letter is being sent to the Florence Regional Office for review. If you have any questions, please contact me at (502) 573-3382.

Sincerely,

Gerald H. Slucher

Gerald Slucher, Supervisor
Source Testing Section
Technical Services Branch

GHS/mlp

cc: Edd Frazier
W. A. Clements
Florence Regional Office

EDUCATION PAYS

bcc: File: ID# 21-077-00018

Facility	Gallatin Steel					
Source Type	Electric Arc Furnace					
Performed By	Ambient Air Services	Req. by		E. Frazier	Rvwed. By	Slucher
Date Performed	5/4/2000	Received	5/4/00	Reviewed	6/15/00	

PARTICULATE

	Run #1	Run #2	Run #3
Cp	0.84	0.84	0.84
Theta,min.	252	252	252
As1,ft2	201.062	201.062	201.062
Ts1,degF	132.3	135	119.3
Ps1,in.Hg.	29.8	29.85	29.87
DELP1sqrt	1.3231	1.3321	1.3087
As2,ft2	78.54	78.54	78.54
Ts2,degF	168.9	106.9	98.4
Ps2,in.Hg.	29.88	29.89	29.89
DELP2sqrt	0.3231	0.2778	0.307
As3,ft2	78.54	78.54	78.54
Ts3,degF	469.1	478.7	356.9
Ps3,in.Hg.	29.68	29.63	29.57
DELP3sqrt	1.119	1.1309	1.1406
Asout,ft2	12069.79	12069.79	12069.79
Gamma	1	1	1
Ts,degF	0	151.4	151.4
Tm,degF	85.6	89	86
Ps,in.Hg.	30.03	30	30.03
Pbar,in.Hg.	30.03	30	30.03
Vlc,ml.	9	13.4	12.5
Vm.ft3.	31.4	31.79	31.196
DELH,in.H2O	1.5	1.5	1.5
CO2%	0	0	0
O2%	20.9	20.9	20.9
CO%	0	0	0
N2%	79.1	79.1	79.1
Vwstd,ft3	0.4239	0.63114	0.58875
Vmstd,ft3.	30.5985857	30.7561352	30.3775214
Bws	0.01366428	0.02010815	0.01901262
Md	28.836	28.836	28.836
Ms	28.6879338	28.6181081	28.6299792
vs1,ft/sec	79.0861386	79.8357274	77.3496481
vs2,ft/sec	19.8738692	16.2403975	17.8086996
vs3,ft/sec	83.9410382	85.4468251	80.4592981
Q1std,dscf/hr.	50130616.8	50130979.1	49975464.6
Q2std,dscf/hr.	4646976.42	4186571.79	4665953.62
Q3std,dscf/hr.	13196684	13186914.6	14255628.6

Qtotal,dscf/min	1132904.62	1125074.43	1148284.11
vs,out ft/sec	1.56438046	1.55356808	1.58561736

NITROGEN OXIDES			
ppm	6.4	3.4	3.4
tons/hr	182	198	199
lb/scf	7.645E-07	4.0616E-07	4.062E-07
lb/hr	51.969304	27.4178724	27.983489
lbs/ton	0.2855456	0.1384741	0.1406205
Avg lbs/ton	0.1882134		

SULFUR DIOXIDE			
ppm	1.1	1.15	2.8
tons/hr	182	198	199
lb/scf	1.83E-07	1.9127E-07	4.657E-07
lb/hr	12.436389	12.9118174	32.086007
lb/ton	0.0683318	0.0652112	0.1612362
Avg lbs/ton	0.0982597		

interoffice
MEMORANDUM

to: Jerry Slucher
from: Edd Frazier
subject: Stack test review
date: June 15, 2000

Re: Gallatin Steel
21-077-00018/5

Please review the attached test report. This test was performed on May 4, 2000, and the NOx and SO2 emissions from the baghouse for the EAF were determined. Please inform me of your findings when your review is done.

cc: Dan Gray

attachment

GALLATIN
STEEL
A Co-Steel Dofasco Partnership

June 14, 2000

Mr. Daniel Gray, Manager
Permit Review Branch
Division for Air Quality
803 Schenkel Lane
Frankfort, KY 40601-1403

RE: Air Emissions Performance Testing – May 2000
Gallatin Steel Company, Warsaw, Kentucky
I.D. # 079-1380-0018, Permit # F-96-009

Dear Mr. Gray:

Enclosed is the test report prepared by Ambient Air Services, Inc. for the air emissions performance testing conducted at Gallatin Steel Company on May 4, 2000 for SO_2 and NOx.

Data sheets for the baghouse pressure drops, furnace shell pressures, fan amperes and damper positions are included in Appendix F of the report with the production data. The sulfur content of the charge carbon used during the test was 0.57%.

If you have any questions regarding this report, please feel free to contact me at (606) 567-3141.

Sincerely yours,

Valerie A. Hudson

Valerie A. Hudson, P.E.
Process Manager – Environmental Systems

R.R. #1, Box 320, Ghent, KY 41045-9704 PHONE 606.567.3100 FAX 606.567.3165

EMISSIONS TEST REPORT FOR SULFUR DIOXIDE AND OXIDES OF NITROGEN

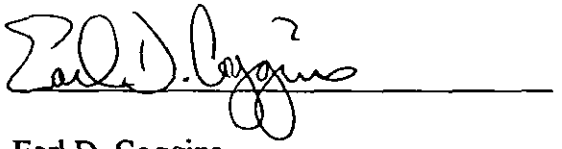
GALLATIN STEEL COMPANY
GHENT, KENTUCKY
(PERMIT NUMBER F-96-009 REVISION 1)

MAY 4, 2000

AMBIENT AIR SERVICES, INC.
106 AMBIENT AIR WAY
STARKE, FLORIDA 32091
(904) 964-8440

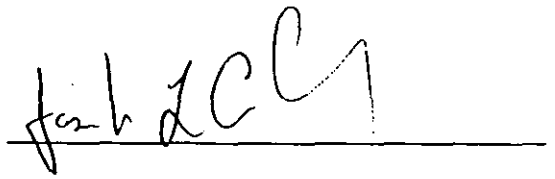
Ambient Air Services, Inc. of Starke, Florida, has completed the testing described in this report for the Gallatin Steel Company, Ghent, Kentucky facility. To the best of our knowledge and abilities we certify that all information, facts and test data are true and correct. Information supplied to AASI for use in this report from Gallatin Steel is perceived to be accurate and is used as such where necessary.

Test Team Leader:



Earl D. Coggins

Project Manager:



Joseph L. Cooksey

1.0 EXECUTIVE SUMMARY

On May 4, 2000 emission tests were conducted at the Gallatin Steel mill located in Warsaw, Kentucky. The emission testing was conducted in accordance with the requirements listed in the Kentucky Department of Environmental Protection, Division of Air Quality, PSD Permit F-96-009. In accordance with Permit F-96-009 (Revision 1) Gallatin Steel was required to test for NO_x and SO_2 emissions. Based on results from testing conducted in the previous 2 years (1998 and 1999) testing was not required for VOC, PM, CO and lead emissions. The results from this test indicate compliance with the NO_x and SO_2 permit limitations. Table 1 summarizes the results of these testing efforts.

TABLE 1

SUMMARY OF EMISSION TEST RESULTS

GALLATIN STEEL COMPANY - WARSAW, KENTUCKY MILL
GHENT, KENTUCKY

May 4, 2000

EMISSION POINT	PARAMETER	TEST RESULTS	PERMIT LIMIT
EAF/CASTER LMF Baghouse	Sulfur Dioxide (SO_2)	0.10 lbs/ton 18.6 lbs/hr.	0.20 lbs/ton 40 lbs/hr.
Emission Point E1 (01)	Oxides of Nitrogen	0.19 lbs/ton 36.1 lbs/hr.	0.51 lbs/ton 102.0 lbs/hr.

TABLE OF CONTENTS

2.0 INTRODUCTION

On May 4, 2000 Ambient Air Services, Inc. conducted air emission testing at Gallatin Steel Company's, Ghent, Kentucky mill. Prior to starting these tests, Kentucky Department of Environmental Protection personnel were notified of the testing schedule and provided a testing protocol for review. A copy of the Notification Letter is included in the Appendix section of this report.

Testing methods and time duration are summarized in Table 2.

TABLE 2

SUMMARY OF TESTING METHODS

GALLATIN STEEL COMPANY

GHENT, KENTUCKY

MAY 4, 2000

POLLUTANT-SOURCE	EPA REFERENCE METHOD	TIME DURATION
Sulfur Dioxide - E1 (01)	Method 6C	3 runs, 3 heats each, 2 compartments tested simultaneously per run
Oxides of Nitrogen - E1 (01)	Method 7E	3 runs, 3 heats each All tests conducted in Compartment 7

3.0 PROCESS DESCRIPTION

At the Ghent, Kentucky facility of Gallatin Steel, the overall objective is to reclaim scrap steel of various forms, refining this material to create rolled steel coils. This type of mill is commonly referred to as a "mini" mill. The particular aspect of this mill examined by these testing efforts were the Electric Arc Furnace (EAF) operations. The EAF by introducing heat primarily in the form of an electric arc provides the energy necessary to melt the scrap steel. Once melted and refined, the furnace is tapped and the product is transferred to the caster/tunnel furnace to be formed into rolled steel. To control the amount of particulate escaping from the melt shop building, during all operations, a baghouse filter system is employed. This system exhausts the furnace directly through fourth hole and canopy hood ducts.

4.0 GASEOUS EMISSION SAMPLING

4.1 Methodology

Continuous instruments were used to measure SO_2 and NO_x emissions. The arc furnace shop sample was obtained from the baghouse. A dilution extraction system was utilized to convey the sample gas to the sulfur dioxide analytical instruments. A fully extractive system was utilized for the NO_x instrument. The sample was obtained from a representative middle point among the bag filter banks on the clean side of the baghouse. The sample probe for the NO_x instrument was positioned in Compartment 7 of the baghouse for the duration of the test. The probe for the SO_2 sample was positioned in 6 different compartments, 2 per test run.

Gaseous emission sampling consisted of three runs, each run covering three furnace "heats". Utilizing the flow rates (SCFM) measured during each run, mass emissions were calculated in lbs/hr. and in lbs/ton.

As described in the test protocol, in order to sample a maximum number of compartments per test run, two SO_2 instruments were utilized. The sample probe for each instrument was positioned in separate compartments. Thus, a total of six compartments were tested for three heats each over the test period. The compartments were selected so that one inner and one outer compartment were sampled during each run. The compartments were randomly selected.

Historically all SO_2 measurements were conducted in Compartment Number 7. This originated at the request of the State of Kentucky. Compartment 7 was selected by the State due to the location of the installed CEMS probe. Through a baghouse consultant, Gallatin learned that the sulfur dioxide

may be different in concentration in different compartments within the baghouse. This stratification is due in part to the design of the duct work and fan configuration.

As can be seen in the results summary, SO_2 concentrations vary considerably from compartment to compartment within the baghouse. In order to achieve a more statistically valid average, compartments were selected so that one "inner" and one "outer" compartment were sampled per test run. The inner and outer compartments were selected to achieve a cross-sectional average of all compartments based on engineering judgements.

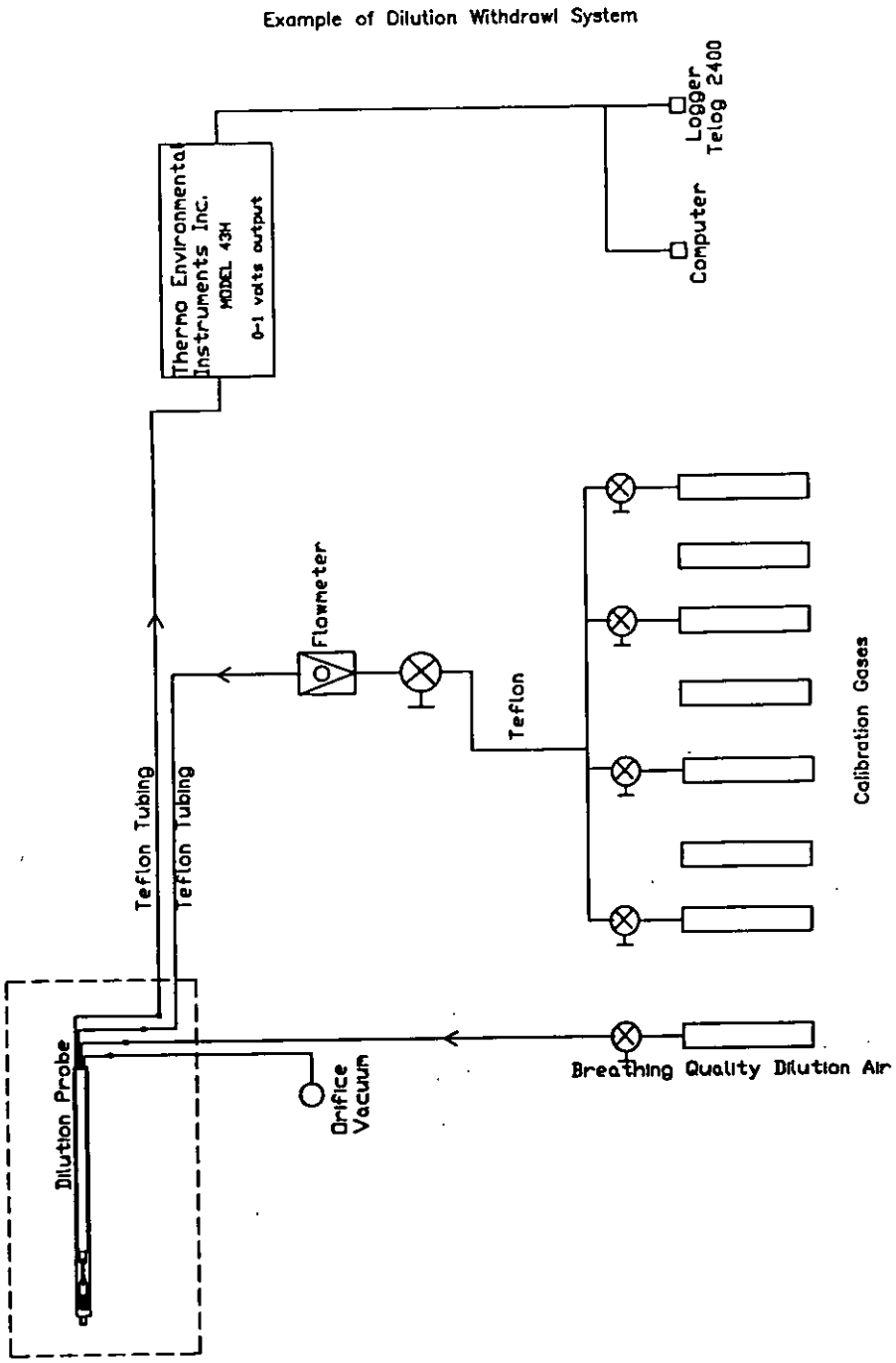

Example of Dilution Withdrawl System
Logger
Telog 2400
Computer
Therma Environmental
Instruments Inc.
MODEL 43H
0-1 volts output
Flowmeter
Teflon
Calibration Gases
Teflon Tubing
Teflon Tubing
Dilution Probe
Orifice
Vacuum
Breathing Quality Dilution Air

FIGURE 4-1

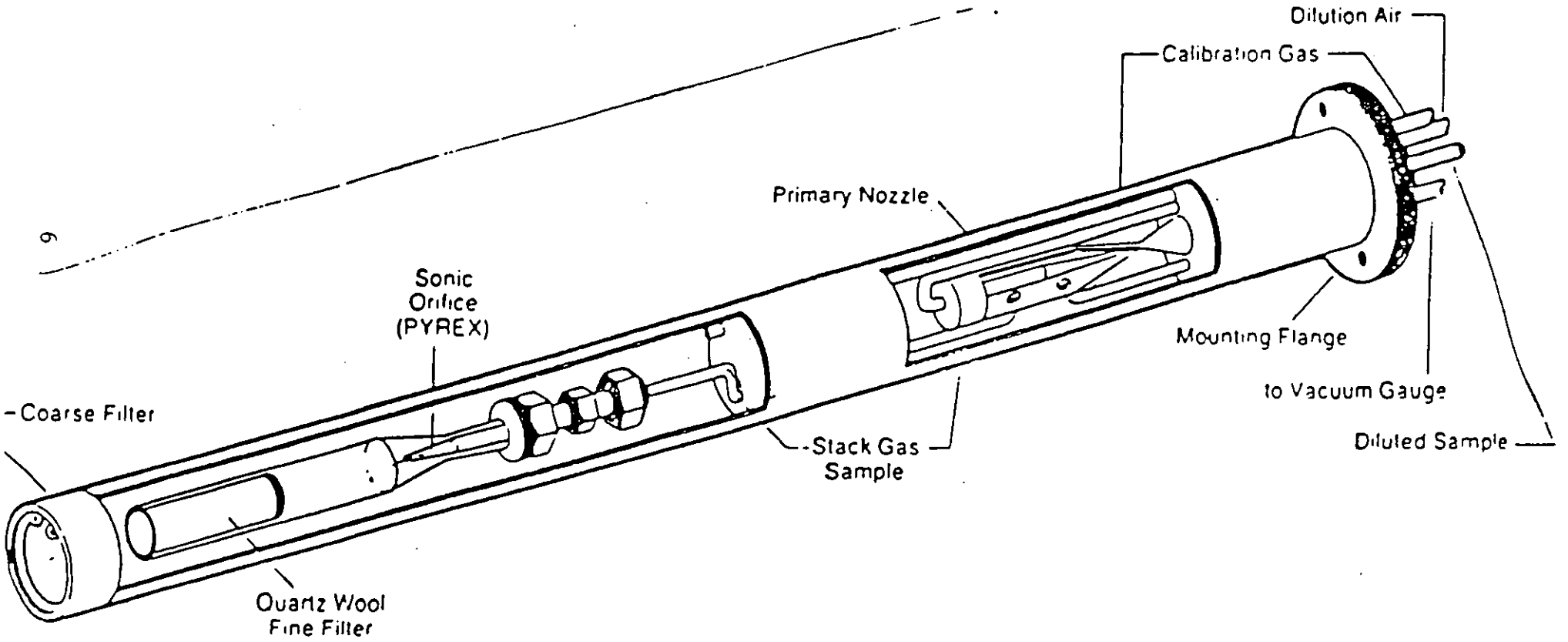

Dilution Air
Calibration Gas
Primary Nozzle
Sonic
Orifice
(PYREX)
Mounting Flange
to Vacuum Gauge
Coarse Filter
Stack Gas
Sample
Diluted Sample
Quartz Wool
Fine Filter

FIGURE 4-2

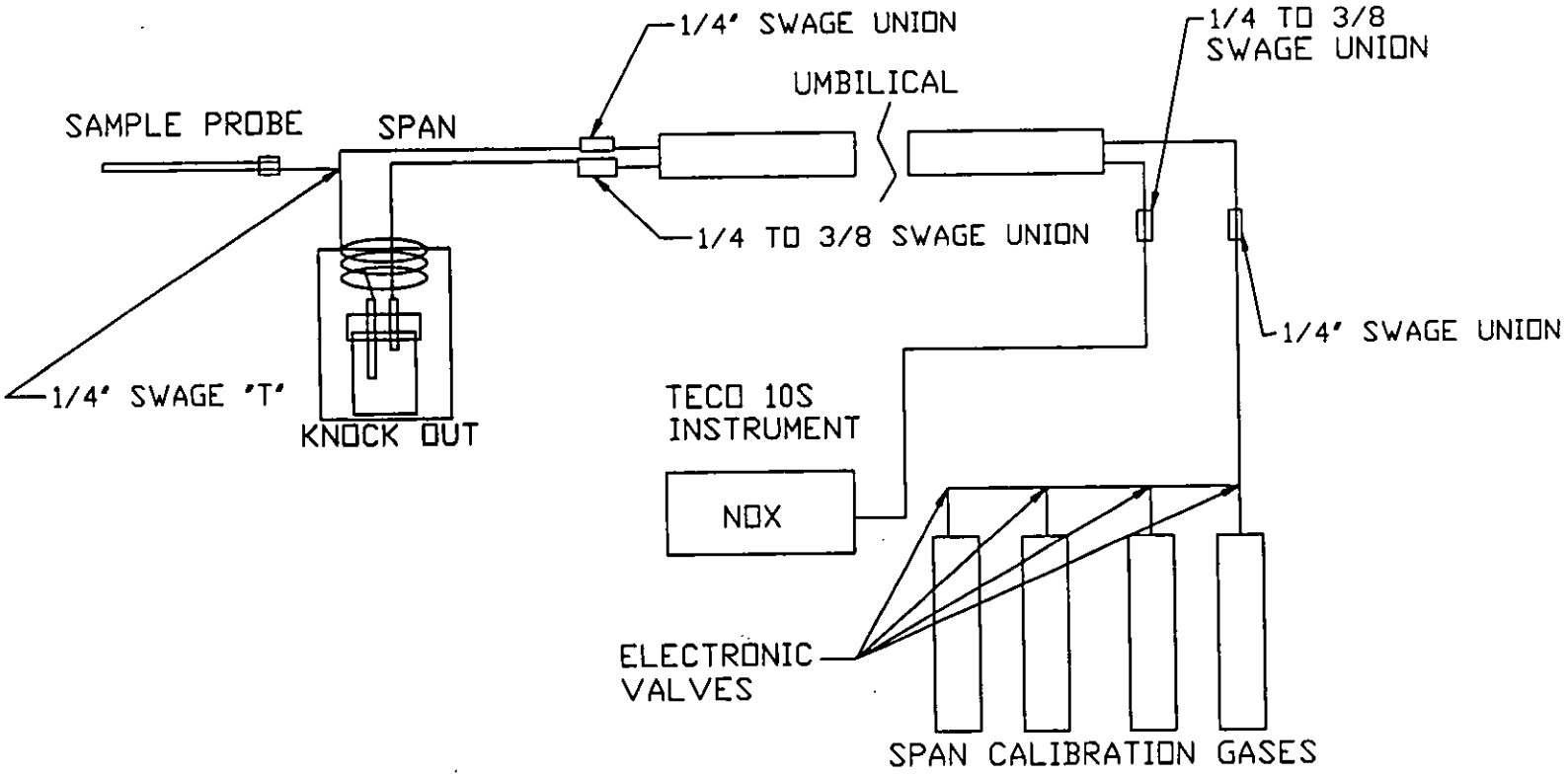


FIGURE 4-3

FULLY EXTRACTIVE WITHDRAWAL SYSTEM - NOx

Data Recording

The primary data recorder was a Telog Model 2400 electronic data recorder which is based on micro-processor technology. This recorder interrogates each analytical instrument signal on a once-every-one-second basis and for this test was instructed to accumulate 60 of these one-second readings and store the average into recorder memory. The data bank consists of a series of one minute averages. In retrieving the data from the computerized database, scaling factors were entered to reflect the appropriate calibrations which occurred immediately before and after collecting the data set of current interest. The analysis of SO_2 gaseous species was carried out as follows:

Sulfur Dioxide

Sulfur Dioxide concentrations were determined by EPA Method 6C. Two Thermo Environmental Instruments (TEI) Model 43H instruments were used. EPA protocol calibration gases of SO_2 in air were used at nominal levels of 0, 12.5, and 25.0 ppm (instrument range 0-25 ppm). Calibrations were performed before and after each test run. EPA Method 6C required correction factors were applied to the data based on the results of the calibrations.

Table 4-1 summarizes the TEI Model 43H versus those required by Method 6C.

TABLE 4-1

SULFUR DIOXIDE SYSTEM PERFORMANCE SPECIFICATIONS METHOD 6C VS THERMO ENVIRONMENTAL INSTRUMENTS MODEL 43H		
	METHOD 6C	TECO 43H
Calibration error zero, mid and high gases	Less than ±2% span	±1% of full scale
Sampling system bias for zero, mid and high gases	Less than ±5% span	±1% of full scale
Interference Check	Less than ±7% of Method 6 result	NO < 3 ppb M-Xylene <2 ppb H2O < 2% of reading
Calibration Drift	Less than ±3% of span over the run period	±1% of full scale

Oxides of Nitrogen - Oxides of Nitrogen were measured using EPA Method 7E. Table 4-2 relates the required performance specifications of Method 7E to those presented by the manufacturer of the TEI Model 10S used in these tests. The instrument was calibrated over a nominal range of 0-50 ppm.

Results from the test are expressed in mass per unit time with all NO_x converted to the species NO_2.

At the beginning and end of each test series zero gas plus two calibration gases were used to perform calibration checks. At intermediate periods between the three runs, zero gas plus one calibration gas was used as a calibration check.

TABLE 4-2

OXIDES OF NITROGEN SYSTEM PERFORMANCE SPECIFICATIONS METHOD 7E VS THERMO ENVIRONMENTAL INSTRUMENTS MODEL 10S		
	METHOD 7E	TECO 10S
Calibration error zero, mid and high gases	Less than ±2% span	±1% of full scale
Sampling system bias for zero, mid and high gases	Less than ±5% span	±1% of full scale
Zero Drift	Less than ±3% of span over the run period	Negligible
Calibration Drift	Less than ±3% of span over the run period	±1% of full scale

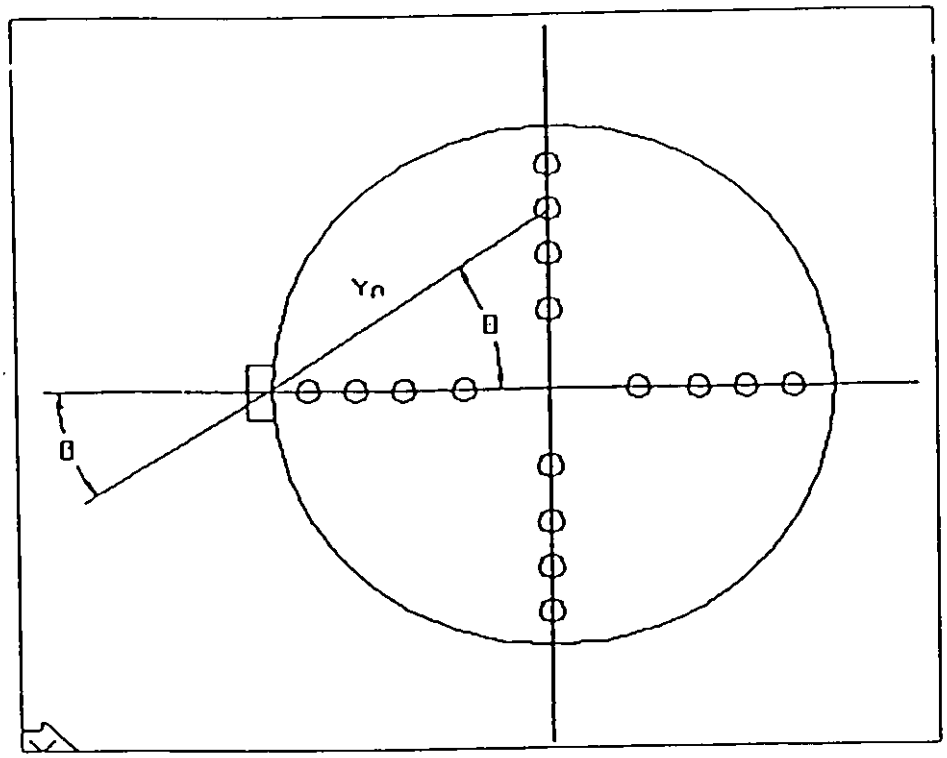
Flow, Moisture, Oxygen and Carbon Dioxide - In order to convert concentration values of parts per million NO_x and SO_2 into pounds per hour it was necessary to determine the effluent flow rate. The effluent flow rate was determined in accordance with EPA Methods 1-4.

Since the baghouse exhaust does not meet the criteria of Method 1, the flow was determined on the baghouse inlet. Specifically, there are three inlet ducts to the baghouse. Flow was measured on each of the inlet ducts and added together to get the total flow. All fresh air inlets to the compartments tested were blocked during the test. This prevented the influence of dilution air on the gas emission concentrations. Figures 4-4 and 4-5 depict the traverse points used.

In addition to the traverse data, moisture runs were conducted in accordance with EPA Method 4.

Oxygen and carbon dioxide levels were confirmed to be essentially ambient air (0% CO_2, 20.9% O_2) using Method 3. A fyrite type analyzer was used for this purpose.

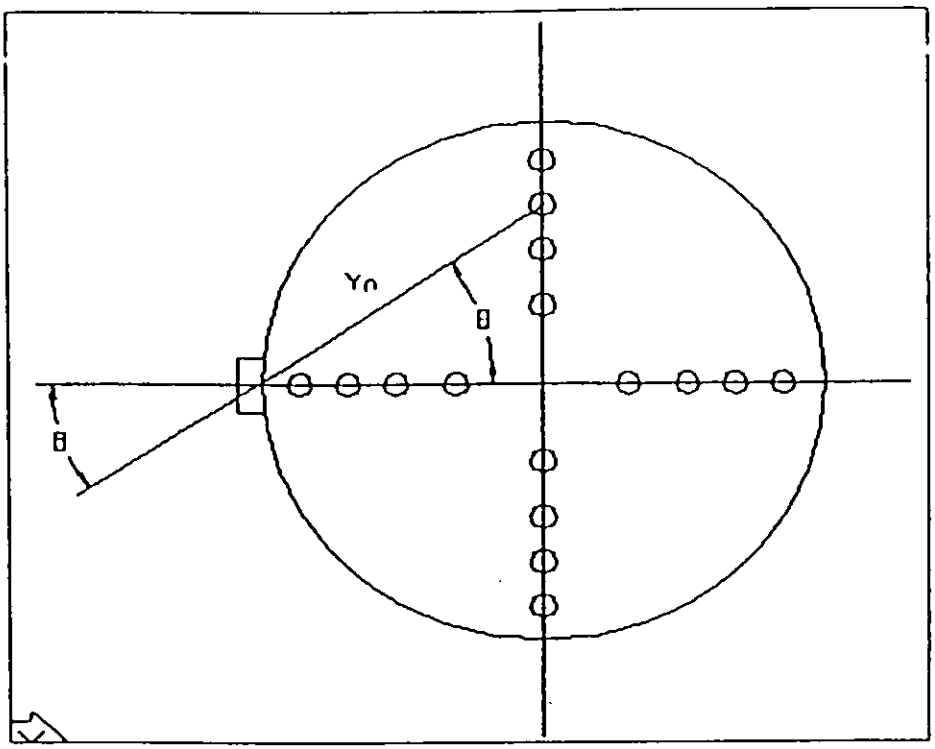
NO. 1 DUCT -- DIAMETER = 192", 16 TRAVERSE POINTS



VERTICAL TRAVERSE		HORIZONTAL TRAVERSE		
POINT	DIST. FROM WALL	POINT	Θ	Yn
1	6.1"	1	43.0°	131.0"
2	20.2"	2	38.0°	122.0"
3	37.2"	3	31.5°	112.6"
4	62.0"	4	20.0°	101.8"
5	130.0"	5	-20.0°	101.8"
6	154.8"	6	-31.5°	112.6"
7	171.8"	7	-38.0°	122.0"
8	185.6"	8	-43.0°	131.0"

FIGURE 4-4

NO. 2 AND HOT DUCT -- DIAMETER = 120", 16 TRAVERSE POINTS



VERTICAL TRAVERSE		HORIZONTAL TRAVERSE		
POINT	DIST. FROM WALL	POINT	θ	Yn
1	3.84	1	43.1	82.2
2	12.6	2	38.3	76.5
3	23.3	3	31.5	70.3
4	38.76	4	19.5	63.6
5	81.24	5	-19.5	63.6
6	96.72	6	-31.5	70.3
7	107.4	7	-38.3	76.5
8	116.16	8	-43.1	82.2

FIGURE 4-5

4.2 Test Results

The results of the instrumental testing for gaseous emissions are as follows:

TABLE 4-3

SUMMARY OF OXIDES OF NITROGEN EMISSION MEASUREMENTS

GALLATIN STEEL COMPANY
GHENT, KENTUCKY

EAF/LMF/CASTER BAGHOUSE
May 4, 2000

RUN NUMBER	HEAT NUMBERS	PRODUCTION	TEST TIME	OXIDES OF NITROGEN (as NO_2)		
		TONS PER HOUR	Minutes	ppm	Lbs/hr.	Lbs/ton
1	A13562, C13217, A13563	182	180	6.4	52.0	0.29
2	A13564, C13219, A13565	198	165	3.4	28.0	0.14
3	A13566, C13221, A13567	199	148	3.4	27.4	0.14
Averages[1]		193	493	4.4	36.1	0.19

[1] Time Weighted Average

Notes: PPM = Parts per Million V.V
Lbs/Hr = Pounds per Hour
Lbs/Ton = Pounds per ton cast

All emissions measurements taken in compartment number 7 (per prior agreement/request from State of Kentucky)

TABLE 4-4

SUMMARY OF SULFUR DIOXIDE EMISSION MEASUREMENTS

GALLATIN STEEL COMPANY
GHENT, KENTUCKY

EAF/LMF/CASTER BAGHOUSE

May 4, 2000

RUN NUMBER	HEAT NUMBERS	PRODUCTION	TEST TIME	OUTER COMPARTMENT SO_2		INNER COMPARTMENT SO_2		AVERAGE	
		TONS PER HOUR	Minutes	ppm	Lb/Hr	ppm	Lb/Hr	Lb/Hr	Lb/Ton
1	A13562, C13217, A13563	182	180	1.3	14.5	0.9	10.5	12.5	0.07
2	A13564, C13219, A13565	198	165	1.8	20.8	0.5	5.9	13.4	0.07
3	A13566, C13221, A13567	199	148	2.9	32.2	2.7	30.0	31.1	0.16
Averages[1]		193	493	2.0	22.2	1.3	14.9	18.6 / 19.0	0.10

[1] Time Weighted Average

Notes: PPM = Parts per Million V.V
Lb/Hr = Pounds per Hour
Lb/Ton = Pounds per ton cast

Run 1 = Compartments 2 (outer) and 14 (inner)
Run 2 = Compartments 4 (outer) and 16 (inner)
Run 3 = Compartments 19 (outer) and 7 (inner)

4.3 Testing Compromises

In the test protocol/notification letter dated March 31, 2000 it was proposed to conduct 4 test runs of 3 heats each. The logic was to obtain the most representative average SO_2 data possible from the baghouse. After discussing this with Mr. Gerald Slucher on site it was decided that three test runs of three heats each would be acceptable.

Three test runs were conducted over a total of nine heats.

A second compromise - approximately 20 minutes prior to the end of the ninth heat the plant encountered a problem. The problem resulted in an undetermined amount of down time. Again, Mr. Slucher was consulted and he suggested that a representative portion of the heat had been sampled and suggested that we end the test run at that point.

APPENDICES

APPENDIX A - Sample Calculations - Gaseous Emissions

APPENDIX B - Instrument Calibration Data - Baghouse Testing

APPENDIX C - Gaseous Emission Data - Baghouse Testing

APPENDIX D - Flow Rates

APPENDIX E - Field Data Sheets

APPENDIX F - Production Data, Test Notification Letter

APPENDIX G - Project Participants

APPENDIX A

SAMPLE CALCULATIONS

Gaseous Emissions Sample Calculations

I. Concentrations as calculated from method 6c

A. Co, Average of initial and final system calibration bias check responses for the zero gas, ppm.

Run 1, SO2
Co = (.037+.078)/2 = 0.057

B. Cm, Average of initial and final system calibration bias check responses for the upscale calibration gas.

Run 1, SO2
Cm = (8.876+8.937)/2 = 8.907

C. Cma, Actual concentration of the upscale calibration gas ppm.

Run 1, SO2
Cma = 8.95

D. Cgas, Effluent gas concentration, dry basis, ppm.

Run 1, SO2
Cgas = (Cbar-Co)(Cma/(Cm-Co))

A. SO2 Emissions

$$lb/hr. = \frac{(ppm)*(Mol.Wt.)}{385e6} * (flowrate)(60\ \text{min}/hr)$$

Example: Mol. Wt. = 64, ppm = 2.15, flowrate = 1145162 SCFMD

lb/hr SO2 = 24.56

IV. Emission Rates (lb/ton)

Lb/ton = (lb/hr)/(lb/ton)

Ambient Air Services, Inc.
Environmental Consultants

106 Ambient Air Way
Starke, Florida 32091

(904) 964 - 8440
(904) 964 - 6675 fax

EXAMPLE CALCULATIONS

Plant	Gallatin Steel
Location	Ghent, Kentucky
Stack	Cold Duct No. 1
Run Date	8-25-99
Run Number	1

1. Stack Pressure, PS

Where: PB = Barometric Pressure, inches Hg
PG = Static Pressure, stack, inches H2O

PS= PB + (PG ÷ 13.6)

PB= 29.54
PG= -3.2

PS= 29.3

2. Molecular Weight of stack gas, dry, MD

MD= (0.44 × %CO2) + (0.32 × %O2) + (0.28 × %N2) + (0.28 × %CO)

CO2= 0.0
O2= 21.0
N2= 79.0
CO= 0.0

MD= 28.84

3. Molecular weight of stack gas, stack conditions, MS

Where: MD = See equation 2
W = 0.037
FDA = 1 - W

MS= (MD × FDA) + (18 × W)

MD= 28.84

FDA= 0.9627039

W= 0.037

MS= 28.44

Ambient Air Services, Inc.
Environmental Consultants

106 Ambient Air Way
Starke, Florida 32091

(904) 964 - 8440
(904) 964 - 6675 fax

EXAMPLE CALCULATIONS - CONTINUED

Plant	Gallatin Steel
Location	Ghent, Kentucky
Stack	Cold Duct No. 1
Run Date	8-25-99
Run Number	1

4. Specific Gravity of Gas, relative to air, GS

Where: MS = See equation 3

GS= MS ÷ 28.99

GS= 0.981

5. Velocity of stack gas, feet per minute, U

Where: CP = Pitot Coefficient, 0.84
H = Average of the square roots of the velocity heads, in. H2O
TS = Temperature of the stack, degrees Rankin
PS = See equation 1
GS = See equation 4

$$U = 174 \times CP \times H \times \frac{TS \times 29.92}{GS \times PS}$$

U= 5106.9 FPM

6. Stack Gas Flow Rate, Stack conditions, cfm, QS

Where: AS = Cross sectional area of stack at sampling location, sq.ft.
U = See equation 5

QS= U × AS

QS= 1026804 ACFM

APPENDIX B

INSTRUMENT CALIBRATION DATA

- Calibration Gas Certificates
  - 24.9 ppm NO_x
  - 54.2 ppm NO_x
  - 12.5 ppm SO_2
  - 24.01 ppm SO_2

- Calibration Drift/Error
  - NO_x Compartment 7
  - SO_2 Inner Compartments
  - SO_2 Outer Compartments

- Field Test Log

SPECTRA GASES INC.
3434 Route 22 West • Branchburg, NJ 08876 USA Tel. (908) 252-9300 • (800) 932-0624 • Fax (908) 252-0811
Shipped From 80 Industrial Drive • Alpha, NJ 08865

CERTIFICATE OF ANALYSIS

EPA PROTOCOL MIXTURE

PROCEDURE # : G1

CUSTOMER: Gallatin Steel Company
SGI ORDER # : 144936
ITEM# : 2
P.O.# : 72399-1

CYLINDER # : CC109962
CYLINDER PRES: 2000 PSIG
CGA OUTLET: 660

CERTIFICATION DATE: 8/10/99
EXPIRATION DATE: 8/10/2001

CERTIFICATION HISTORY

COMPONENT	DATE OF ASSAY	MEAN CONCENTRATION	CERTIFIED CONCENTRATION	ANALYTICAL ACCURACY
Carbon Monoxide	8/2/99 8/10/99	24.97 ppm 25.13 ppm	25.1 ppm	+/- 1%
Nitric Oxide	8/2/99 8/10/99	24.79 ppm 24.88 ppm	24.8 ppm	+/- 1%
NOx			24.9 ppm	Reference Value Only

BALANCE Nitrogen

PREVIOUS CERTIFICATION DATES: None

REFERENCE STANDARDS

COMPONENT	SRM/NTRM#	CYLINDER#	CONCENTRATION
Carbon Monoxide	NTRM-81679	CC88366	97.4 ppm
Nitric Oxide	NTRM-81684	CC79984	98.6 ppm

INSTRUMENTATION

COMPONENT	MAKE/MODEL	SERIAL #	DETECTOR	CALIBRATION DATE(S)
Carbon Monoxide	Horiba VIA-510	570423011	NDIR	7/23/99
Nitric Oxide	Teco 10	10AR-34979-249	Chemi	7/20/99

THIS STANDARD WAS CERTIFIED ACCORDING TO THE EPA PROTOCOL PROCEDURES.
DO NOT USE THIS STANDARD IF THE CYLINDER PRESSURE IS LESS THAN 150 PSIG.

ANALYST: FRED PIKULA

DATE: 8/10/99

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CERTIFICATE OF ANALYSIS

EPA PROTOCOL MIXTURE
PROCEDURE # : G1

CUSTOMER: Gallatin Steel Company
SGI ORDER # : 144936
ITEM# : 4
P.O.# : 72399-1

CYLINDER # : CC110128
CYLINDER PRES: 2000 PSIG
CGA OUTLET: 660

CERTIFICATION DATE: 8/10/99
EXPIRATION DATE: 8/10/2001

CERTIFICATION HISTORY

COMPONENT	DATE OF ASSAY	MEAN CONCENTRATION	CERTIFIED CONCENTRATION	ANALYTICAL ACCURACY
Carbon Monoxide	8/2/99 8/10/99	54.69 ppm 54.70 ppm	54.7 ppm	+/- 1%
Nitric Oxide	8/2/99 8/10/99	53.74 ppm 54.15 ppm	53.9 ppm	+/- 1%
NOx			54.2 ppm	Reference Value Only

BALANCE Nitrogen

PREVIOUS CERTIFICATION DATES: None

REFERENCE STANDARDS

COMPONENT	SRM/NTRM#	CYLINDER#	CONCENTRATION
Carbon Monoxide	NTRM-81679	CC88366	97.4 ppm
Nitric Oxide	NTRM-81684	CC79984	98.6 ppm

INSTRUMENTATION

COMPONENT	MAKE/MODEL	SERIAL #	DETECTOR	CALIBRATION DATE(S)
Carbon Monoxide	Horiba VIA-510	570423011	NDIR	7/23/99
Nitric Oxide	Teco 10	10AR-34979-249	Chemi	7/20/99

THIS STANDARD WAS CERTIFIED ACCORDING TO THE EPA PROTOCOL PROCEDURES.
DO NOT USE THIS STANDARD IF THE CYLINDER PRESSURE IS LESS THAN 150 PSIG.

ANALYST: FRED PIKULA

DATE: 8/10/99

Airgas
Specialty Gases

1 Hamilton Blvd.
.odore, AL 36582
P.O. Box 190969
Mobile, AL 36619
Phone: (334) 653-2500
FAX: (334) 653-2530

Certificate of Analysis: E.P.A. Protocol Gas Mixture

Cylinder No :	CC13785	Order No.	382975
Cylinder Pressure:	2000 PSIG	Expiration Date:	9/30/00
Certification Date	3/31/00	Laboratory:	ASG-MOBILE

Reference Standard Information:

Type	Component	Cyl. Number	Concentration
NTRM81661	SULFUR DIOXIDE	CC31252	494.4PPM

Instrumentation:

Instrument/Model/Serial No.	Analytical Principle
SIEMENS ULTRAMAT 5E K3-685	NDIR

Analytical Methodology does not require correction for analytical interferences.

Certified Concentrations:

Component	Concentration	Accuracy	Procedure
SULFUR DIOXIDE	12.50 PPM	+/-1%	G1
NITROGEN	Balance		

Analytical Results:

1st Component: SULFUR DIOXIDE

1st Analysis Date: 3/24/00

R	494.0	S	12.50	Z	0.000	Conc	12.51
S	12.50	Z	0.000	R	494.5	Conc	12.50
Z	0.000	R	494.5	S	12.50	Conc	12.50
						AVG:	12.50

2nd Analysis Date: 3/31/00

R	494.5	S	12.50	Z	0.000	Conc	12.50
S	12.50	Z	0.000	R	494.5	Conc	12.50
Z	0.000	R	494.5	S	12.50	Conc	12.50
						AVG:	12.50

Certification performed in accordance with "EPA Traceability Protocol (Sept. 1997)" using the assay procedures listed.

Do not use cylinder below 150 psig.

Bridget M. Richerson
Approved for Release

Airgas
Specialty Gases

) Hamilton Blvd.
.odore, AL 36582
P.O. Box 190969
Mobile, AL 36619
Phone: (334) 653-2500
FAX: (334) 653-2530

Certificate of Analysis: E.P.A. Protocol Gas Mixture

Cylinder No :	CC13853	Order No.	382975
Cylinder Pressure:	2000 PSIG	Expiration Date:	9/30/00
Certification Date	3/31/00	Laboratory:	ASG-MOBILE

Reference Standard Information:

Type	Component	Cyl. Number	Concentration
NTRM81661	SULFUR DIOXIDE	CC31252	494.4PPM

Instrumentation:

Instrument/Model/Serial No.	Analytical Principle
SIEMENS ULTRAMAT 5E K3-685	NDIR

Analytical Methodology does not require correction for analytical interferences.

Certified Concentrations:

Component	Concentration		Accuracy	Procedure
SULFUR DIOXIDE	24.01	PPM	+/-1%	G1
NITROGEN	Balance			

Analytical Results:

1st Component: SULFUR DIOXIDE

1st Analysis Date:		3/24/00					
R	494.0	S	24.00	Z	0.000	Conc	24.02
S	24.00	Z	0.000	R	494.5	Conc	24.00
Z	0.000	R	494.5	S	24.00	Conc	24.00
						AVG:	24.01

2nd Analysis Date:		3/31/00					
R	494.5	S	24.00	Z	0.000	Conc	24.00
S	24.00	Z	0.000	R	494.5	Conc	24.00
Z	0.000	R	494.5	S	24.00	Conc	24.00
						AVG:	24.00

Certification performed in accordance with "EPA Traceability Protocol (Sept. 1997)" using the assay procedures listed.

Do not use cylinder below 150 psig.

Bridget M. Pickens
Approved for Release

GALLATIN STEEL COMPANY

GHENT, KENTUCKY

SUMMARY OF OXIDES OF NITROGEN INSTRUMENT CALIBRATIONS

4-May-00

INSTRUMENT RANGE, PPM	60			
CALIBRATION GAS PPM	INITIAL CALIBRATION	END RUN 1	END RUN 2	END RUN 3
0.0 24.9 54.2	0.0 24.8 54.2	0.1 24.5 N/A	0.0 24.3 N/A	-0.1 25.6 54.4
CALIBRATION ERROR		((INSTRUMENT RESPONSE-CALIBRATION GAS VALUE)/INSTRUMENT RANGE)X100		
0.0 24.9 54.2	0.0 -0.2 0.0	0.2 -0.7 #VALUE!	0.0 -1.0 #VALUE!	-0.2 1.2 0.3
CALIBRATION DRIFT		((FINAL CALIBRATION - INITIAL CALIBRATION)/INSTRUMENT RANGE)X100		
0.0 24.9 54.2	N/A N/A N/A	0.2 -0.5 #VALUE!	-0.2 -0.3 #VALUE!	-0.2 2.2 #VALUE!

ZERO BIAS CHECKS		(SAMPLE SYSTEM-DIRECT)/RANGEX100	
SAMPLE ZERO	DIRECT ZERO	BIAS	
0.0	0.0	0.0	INITIAL
-0.1	-0.1	0.0	FINAL

CALIBRATION BIAS CHECKS			
CALIBRATION GAS, PPM	54.2		
SAMPLE	DIRECT	BIAS	
54.1	54.2	-0.2	INITIAL
54.4	54.5	-0.2	FINAL

GALLATIN STEEL COMPANY

GHENT, KENTUCKY

SUMMARY OF SULFUR DIOXIDE CALIBRATIONS

5/4/2000 - INNER COMPARTMENTS

INSTRUMENT RANGE, PPM	25			
CALIBRATION GAS PPM	INITIAL CALIBRATION	END RUN 1	END RUN 2	END RUN 3
0.0 12.5 24.0	0.1 12.2 24.2	0.1 12.3 N/A	0.1 12.2 N/A	0.1 12.4 23.9
CALIBRATION ERROR	**((INSTRUMENT RESPONSE-CALIBRATION GAS VALUE)/INSTRUMENT RANGE)X100**			
0.0 12.5 24.0	0.4 -1.2 0.8	0.4 -0.8 #VALUE!	0.4 -1.2 #VALUE!	0.3 -0.4 -0.4
CALIBRATION DRIFT	**((FINAL CALIBRATION - INITIAL CALIBRATION)/INSTRUMENT RANGE)X100**			
0.0 12.5 24.0	N/A N/A N/A	0.0 0.4 #VALUE!	0.0 -0.4 #VALUE!	-0.1 0.8 #VALUE!

ZERO BIAS CHECKS		(SAMPLE SYSTEM-DIRECT)/RANGEX100		
SAMPLE ZERO	DIRECT ZERO	BIAS		DILUTION PROBE USED ALL CAL
N/A	N/A	#VALUE!	INITIAL	
N/A	N/A	#VALUE!	FINAL	
CALIBRATION BIAS CHECKS				GASES INJECTED TO PROBE TIP ONLY
CALIBRATION GAS, PPM	N/A			
SAMPLE	DIRECT	BIAS		
N/A	N/A	#VALUE!	INITIAL	
N/A	N/A	#VALUE!	FINAL	

GALLATIN STEEL COMPANY

GHENT, KENTUCKY

SUMMARY OF SULFUR DIOXIDE CALIBRATIONS
5/4/2000 - OUTER COMPARTMENTS

INSTRUMENT RANGE, PPM	30			
CALIBRATION GAS PPM	INITIAL CALIBRATION	END RUN 1	END RUN 2	END RUN 3
0.0	0.0	0.1	0.1	0.0
12.5	12.4	12.7	12.5	13.2
24.0	24.1	N/A	N/A	24.9
CALIBRATION ERROR		**((INSTRUMENT RESPONSE-CALIBRATION GAS VALUE)/INSTRUMENT RANGE)X100**		
0.0	0.0	0.3	0.2	-0.1
12.5	-0.3	0.7	0.0	2.3
24.0	0.3	#VALUE!	#VALUE!	3.0
CALIBRATION DRIFT		**((FINAL CALIBRATION - INITIAL CALIBRATION)/INSTRUMENT RANGE)X100**		
0.0	N/A	0.3	-0.1	-0.3
12.5	N/A	1.0	-0.7	2.3
24.0	N/A	#VALUE!	#VALUE!	#VALUE!

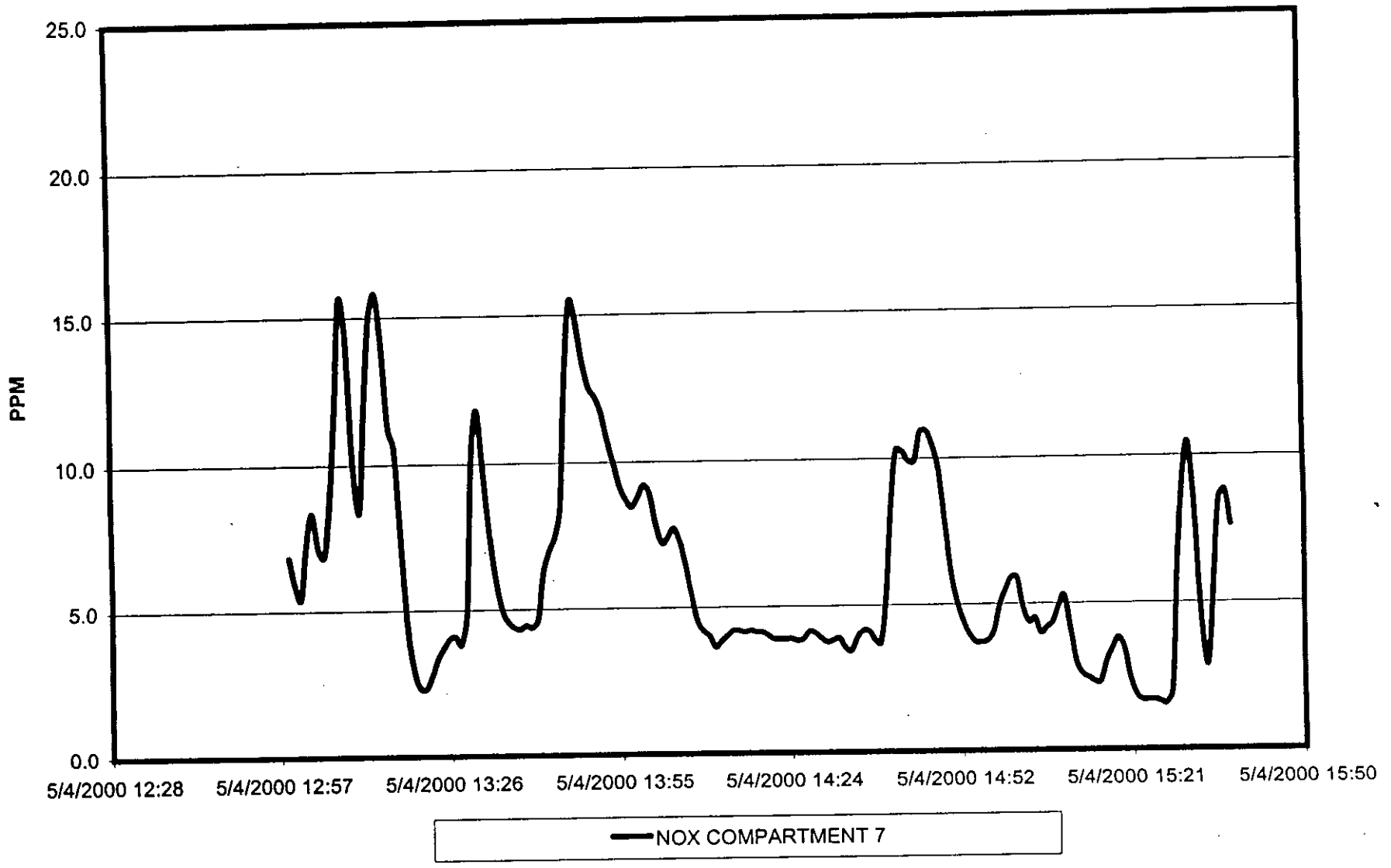
ZERO BIAS CHECKS		(SAMPLE SYSTEM-DIRECT)/RANGEX100		
SAMPLE ZERO	DIRECT ZERO	BIAS		
N/A	N/A	#VALUE!	INITIAL	DILUTION PROBE
N/A	N/A	#VALUE!	FINAL	USED ALL CAL
CALIBRATION BIAS CHECKS				GASES INJECTED
CALIBRATION GAS, PPM	N/A			TO PROBE TIP ONLY
SAMPLE	DIRECT	BIAS		
N/A	N/A	#VALUE!	INITIAL	
N/A	N/A	#VALUE!	FINAL	

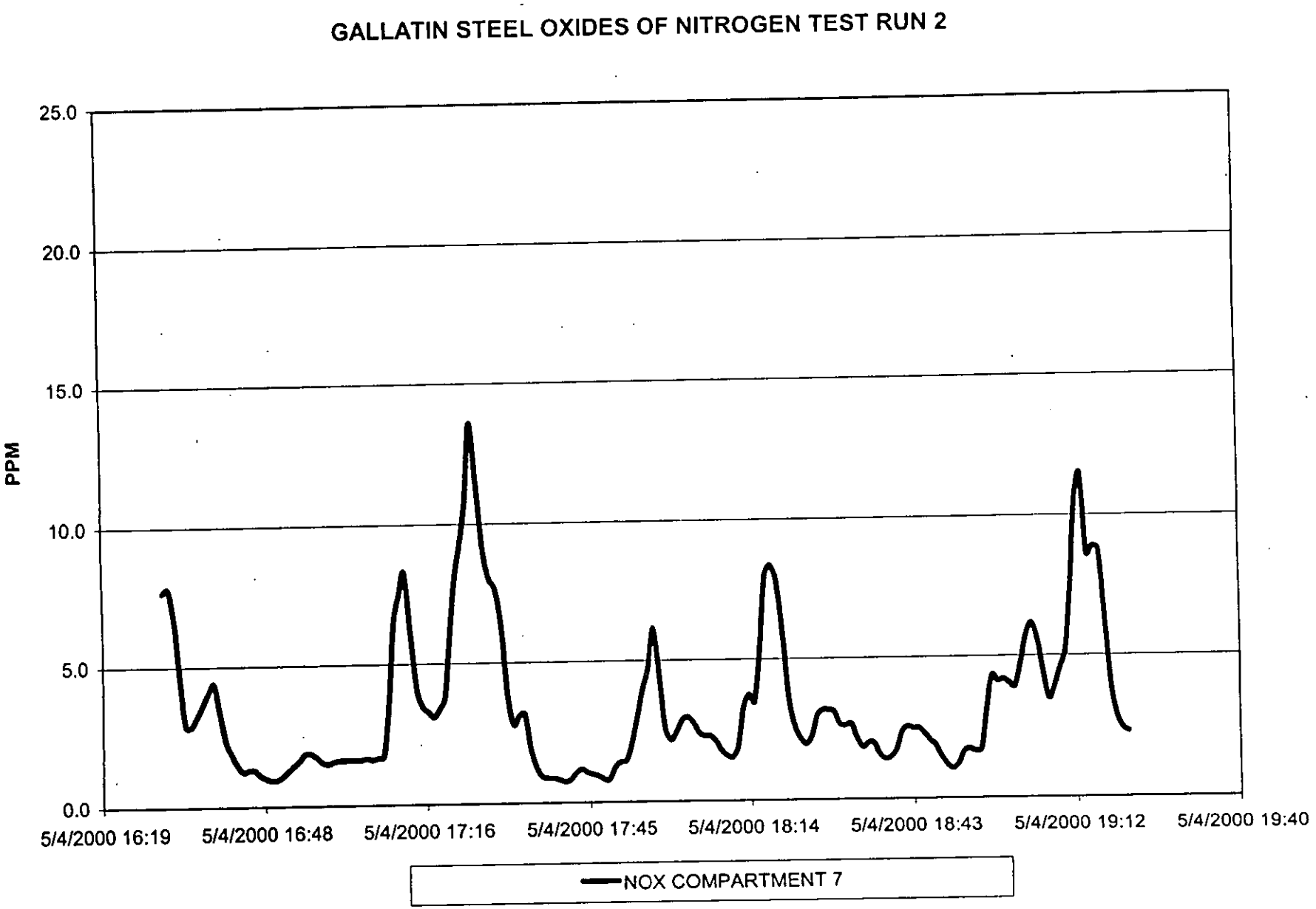
APPENDIX C

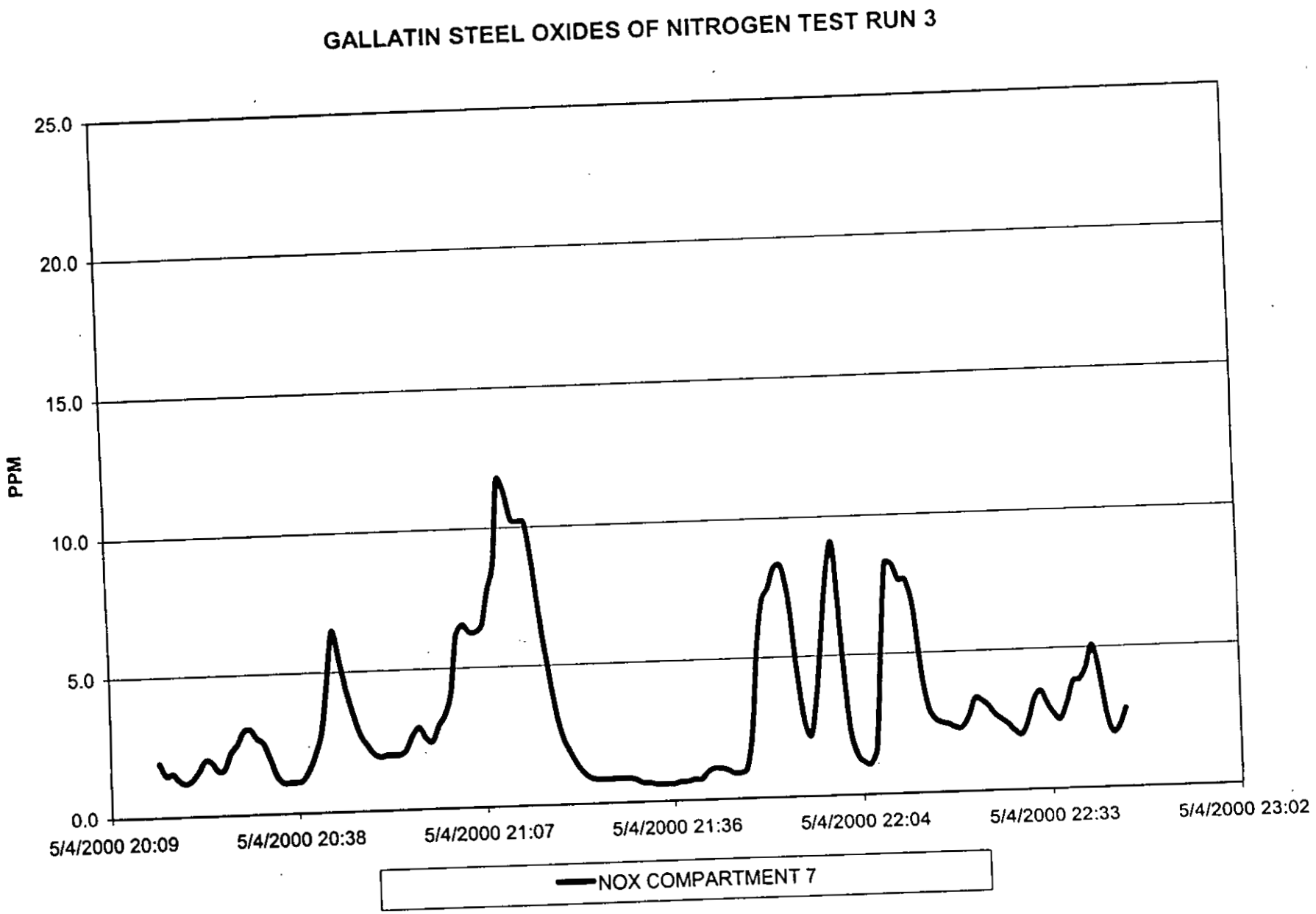
GASEOUS EMISSION DATA
SO_2 and NO_x

- DATA GRAPHS
  - NO_x - Run 1, Run 2, Run 3
  - SO_2 - Run 1, Run 2, Run 3
- DATA SUMMARY
  - 5/4/00 11:00 - 5/5/00 00:03

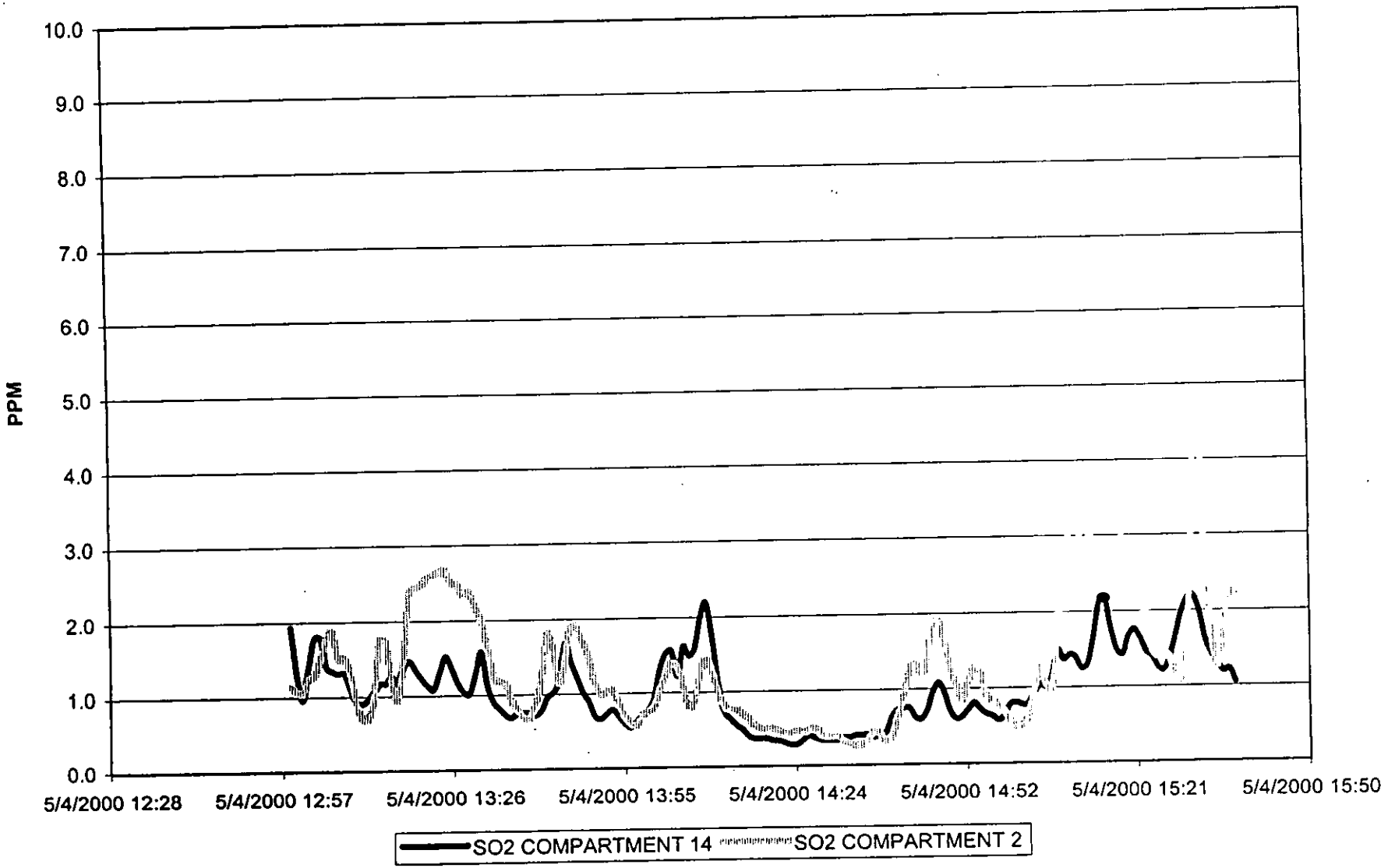
GALLATIN STEEL OXIDES OF NITROGEN TEST RUN 1



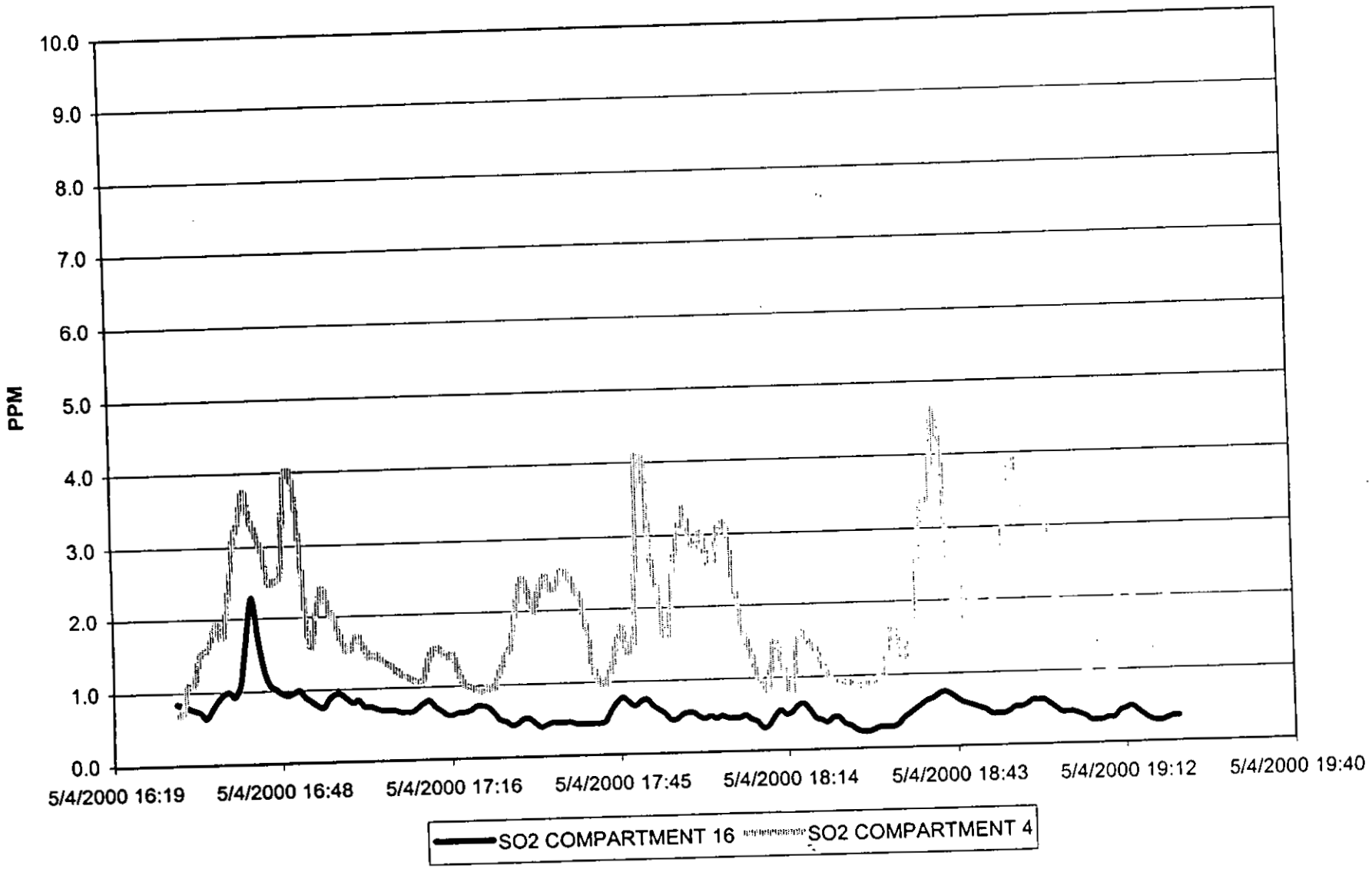

GALLATIN STEEL OXIDES OF NITROGEN TEST RUN 2
25.0
20.0
15.0
10.0
5.0
0.0
PPM
5/4/2000 16:19
5/4/2000 16:48
5/4/2000 17:16
5/4/2000 17:45
5/4/2000 18:14
5/4/2000 18:43
5/4/2000 19:12
5/4/2000 19:40
NOX COMPARTMENT 7


GALLATIN STEEL OXIDES OF NITROGEN TEST RUN 3
25.0
20.0
15.0
10.0
5.0
0.0
PPM
5/4/2000 20:09
5/4/2000 20:38
5/4/2000 21:07
5/4/2000 21:36
5/4/2000 22:04
5/4/2000 22:33
5/4/2000 23:02
NOX COMPARTMENT 7

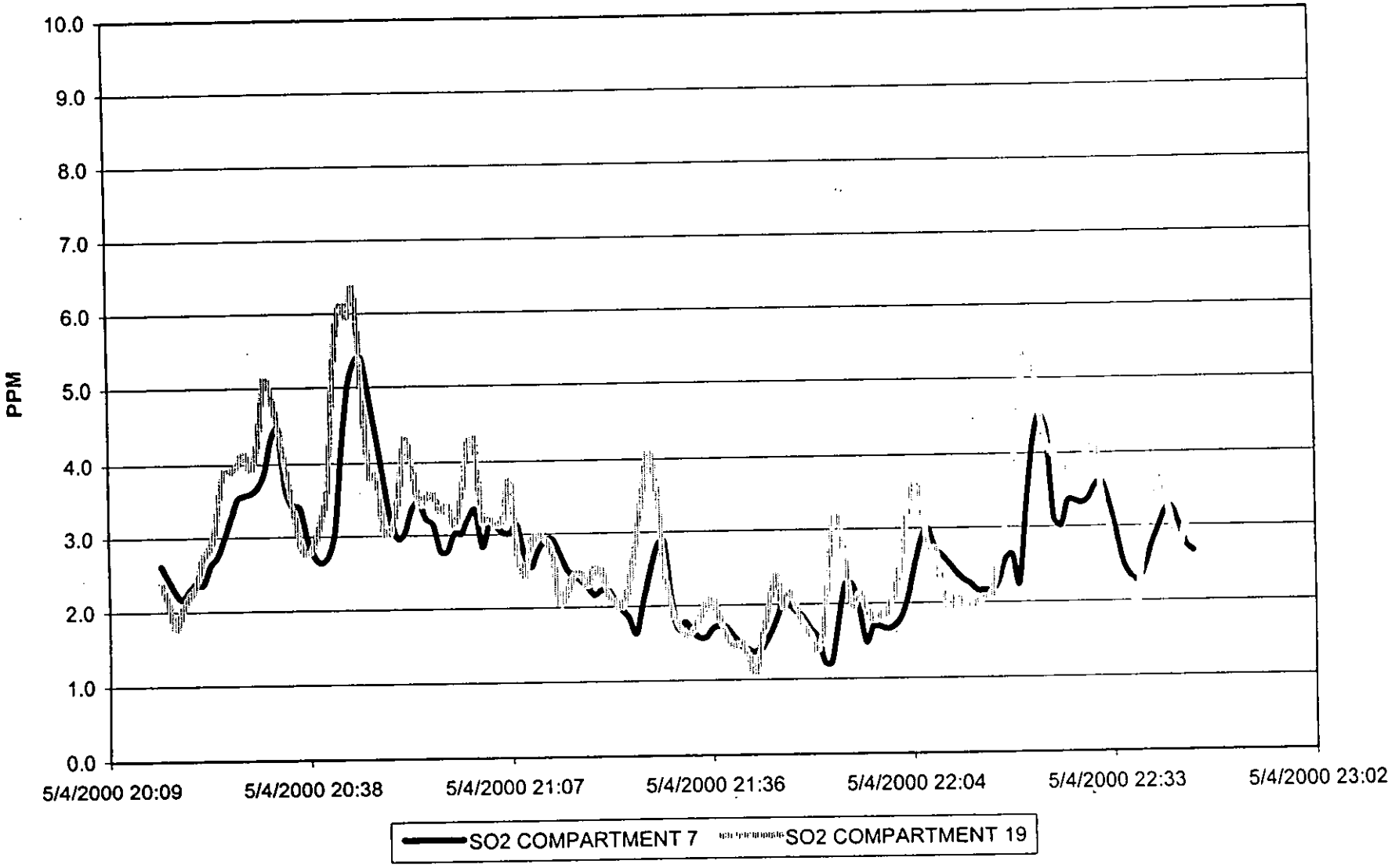
GALLATIN STEEL SULFUR DIOXIDE TEST RUN 1



GALLATIN STEEL SULFUR DIOXIDE TEST RUN 2



GALLATIN STEEL SULFUR DIOXIDE TEST RUN 3



GALLATIN STEEL SO2/NOX COMPLIANCE TEST

TIME	OBSERVED CONCENTRATION PPM			COMMENTS	CALIBRATION CORRECTIONS						CORRECTED PPM VALUES			FLOW MEASURMENTS SCFM				MASS EMISSIONS			EMISSION FACTOR		
					NOX 7		SO2 IN		SO2 OUT														
	NOX COMP 7	SO2 IN	SO2 OUT		0.0	24.9	0.0	12.5	0.0	12.5	NOX - 7	SO2 IN	SO2 OUT	COLD-1	COLD-2	HOT	TOTAL	NOX LBS/HR	SO2 IN LBS/HR	SO2 OUT LBS/HR	PRODUCTION TONS/HR	NOX LBS/TON	SO2 LBS/TON
5/4/2000 11:00	28.9	1.3	1.4	CALS	-0.1	25.1	0.2	12.3	0.1	12.6	28.7	1.1	1.3	833791	74919	225540	1134250						
5/4/2000 11:01	30.8	1.3	1.6	CALS	-0.1	25.1	0.2	12.3	0.1	12.6	30.4	1.1	1.6	833791	74919	225540	1134250						
5/4/2000 11:02	40.7	1.2	1.7	CALS	-0.1	25.1	0.2	12.3	0.1	12.6	40.4	1.1	1.6	833791	74919	225540	1134250						
5/4/2000 11:03	54.7	1.1	1.5	CALS	-0.1	25.1	0.2	12.3	0.1	12.6	54.3	1.0	1.4	833791	74919	225540	1134250						
5/4/2000 11:04	28.3	1.1	1.4	CALS	-0.1	25.1	0.2	12.3	0.1	12.6	28.1	1.0	1.3	833791	74919	225540	1134250						
5/4/2000 11:05	0.4	1.0	1.5	CALS	-0.1	25.1	0.2	12.3	0.1	12.6	0.5	0.8	1.4	833791	74919	225540	1134250						
5/4/2000 11:06	0.2	1.0	1.6	CALS	-0.1	25.1	0.2	12.3	0.1	12.6	0.2	0.8	1.5	833791	74919	225540	1134250						
5/4/2000 11:07	0.0	1.0	1.4	CALS	-0.1	25.1	0.2	12.3	0.1	12.6	0.1	0.8	1.3	833791	74919	225540	1134250						
5/4/2000 11:08	0.1	0.9	1.2	CALS	-0.1	25.1	0.2	12.3	0.1	12.6	0.2	0.8	1.1	833791	74919	225540	1134250						
5/4/2000 11:09	0.2	0.9	1.2	CALS	-0.1	25.1	0.2	12.3	0.1	12.6	0.2	0.7	1.1	833791	74919	225540	1134250						
5/4/2000 11:10	0.3	0.8	1.1	CALS	-0.1	25.1	0.2	12.3	0.1	12.6	0.3	0.7	1.0	833791	74919	225540	1134250						
5/4/2000 11:11	0.4	0.8	1.0	CALS	-0.1	25.1	0.2	12.3	0.1	12.6	0.4	0.8	0.9	833791	74919	225540	1134250						
5/4/2000 11:12	0.4	0.9	1.2	CALS	-0.1	25.1	0.2	12.3	0.1	12.6	0.4	0.8	1.1	833791	74919	225540	1134250						
5/4/2000 11:13	0.4	0.8	1.1	CALS	-0.1	25.1	0.2	12.3	0.1	12.6	0.5	0.7	1.0	833791	74919	225540	1134250						
5/4/2000 11:14	0.4	0.8	1.0	CALS	-0.1	25.1	0.2	12.3	0.1	12.6	0.5	0.7	0.9	833791	74919	225540	1134250						
5/4/2000 11:15	0.4	0.9	0.9	CALS	-0.1	25.1	0.2	12.3	0.1	12.6	0.5	0.7	0.8	833791	74919	225540	1134250						
5/4/2000 11:16	0.4	0.9	0.8	CALS	-0.1	25.1	0.2	12.3	0.1	12.6	0.5	0.7	0.7	833791	74919	225540	1134250						
5/4/2000 11:17	0.5	0.8	0.7	CALS	-0.1	25.1	0.2	12.3	0.1	12.6	0.5	0.7	0.6	833791	74919	225540	1134250						
5/4/2000 11:18	0.5	0.7	0.7	CALS	-0.1	25.1	0.2	12.3	0.1	12.6	0.5	0.6	0.6	833791	74919	225540	1134250						
5/4/2000 11:19	0.7	0.7	0.8	CALS	-0.1	25.1	0.2	12.3	0.1	12.6	0.8	0.5	0.7	833791	74919	225540	1134250						
5/4/2000 11:20	6.1	0.6	0.7	CALS	-0.1	25.1	0.2	12.3	0.1	12.6	6.1	0.5	0.6	833791	74919	225540	1134250						
5/4/2000 11:21	6.2	0.6	0.5	CALS	-0.1	25.1	0.2	12.3	0.1	12.6	6.2	0.5	0.4	833791	74919	225540	1134250						
5/4/2000 11:22	6.5	0.7	0.4	CALS	-0.1	25.1	0.2	12.3	0.1	12.6	6.5	0.5	0.3	833791	74919	225540	1134250						
5/4/2000 11:23	6.6	0.6	0.6	CALS	-0.1	25.1	0.2	12.3	0.1	12.6	6.6	0.7	0.5	833791	74919	225540	1134250						
5/4/2000 11:24	6.5	1.0	1.0	CALS	-0.1	25.1	0.2	12.3	0.1	12.6	6.5	0.9	0.9	833791	74919	225540	1134250						
5/4/2000 11:25	6.5	1.2	1.3	CALS	-0.1	25.1	0.2	12.3	0.1	12.6	6.5	1.1	1.2	833791	74919	225540	1134250						
5/4/2000 11:26	6.0	1.2	1.3	CALS	-0.1	25.1	0.2	12.3	0.1	12.6	6.0	1.1	1.2	833791	74919	225540	1134250						
5/4/2000 11:27	5.8	1.2	1.1	CALS	-0.1	25.1	0.2	12.3	0.1	12.6	5.8	1.1	1.0	833791	74919	225540	1134250						
5/4/2000 11:28	14.1	1.3	1.0	CALS	-0.1	25.1	0.2	12.3	0.1	12.6	14.0	1.1	0.9	833791	74919	225540	1134250						
5/4/2000 11:29	14.3	1.4	1.5	CALS	-0.1	25.1	0.2	12.3	0.1	12.6	14.2	1.3	1.4	833791	74919	225540	1134250						
5/4/2000 11:30	6.1	1.4	1.7	CALS	-0.1	25.1	0.2	12.3	0.1	12.6	6.1	1.3	1.7	833791	74919	225540	1134250						
5/4/2000 11:31	4.1	1.3	1.9	CALS	-0.1	25.1	0.2	12.3	0.1	12.6	4.1	1.2	1.8	833791	74919	225540	1134250						
5/4/2000 11:32	3.6	1.2	3.0	CALS	-0.1	25.1	0.2	12.3	0.1	12.6	3.6	1.1	3.0	833791	74919	225540	1134250						
5/4/2000 11:33	18.0	1.2	3.3	CALS	-0.1	25.1	0.2	12.3	0.1	12.6	17.9	1.1	3.2	833791	74919	225540	1134250						
5/4/2000 11:34	61.8	1.4	2.7	CALS	-0.1	25.1	0.2	12.3	0.1	12.6	61.1	1.3	2.6	833791	74919	225540	1134250						
5/4/2000 11:35	37.4	1.4	1.8	CALS	-0.1	25.1	0.2	12.3	0.1	12.6	37.1	1.3	1.7	833791	74919	225540	1134250						
5/4/2000 11:36	42.2	1.4	1.6	CALS	-0.1	25.1	0.2	12.3	0.1	12.6	41.9	1.3	1.5	833791	74919	225540	1134250						
5/4/2000 11:37	53.5	1.3	2.7	CALS	-0.1	25.1	0.2	12.3	0.1	12.6	53.1	1.1	2.6	833791	74919	225540	1134250						
5/4/2000 11:38	53.8	1.4	4.0	CALS	-0.1	25.1	0.2	12.3	0.1	12.6	53.4	1.3	3.9	833791	74919	225540	1134250						
5/4/2000 11:39	54.3	1.8	4.4	CALS	-0.1	25.1	0.2	12.3	0.1	12.6	53.9	1.7	4.3	833791	74919	225540	1134250						
5/4/2000 11:40	54.2	1.8	3.3	CALS	-0.1	25.1	0.2	12.3	0.1	12.6	53.8	1.7	3.2	833791	74919	225540	1134250						
5/4/2000 11:41	54.1	1.6	2.8	CALS	-0.1	25.1	0.2	12.3	0.1	12.6	53.7	1.5	2.7	833791	74919	225540	1134250						
5/4/2000 11:42	48.8	1.4	2.0	CALS	-0.1	25.1	0.2	12.3	0.1	12.6	48.5	1.3	1.9	833791	74919	225540	1134250						
5/4/2000 11:43	22.8	1.3	2.3	CALS	-0.1	25.1	0.2	12.3	0.1	12.6	22.7	1.1	2.2	833791	74919	225540	1134250						
5/4/2000 11:44	24.4	1.2	1.9	CALS	-0.1	25.1	0.2	12.3	0.1	12.6	24.3	1.1	1.8	833791	74919	225540	1134250						
5/4/2000 11:45	24.8	1.8	2.0	CALS	-0.1	25.1	0.2	12.3	0.1	12.6	24.7	1.5	1.9	833791	74919	225540	1134250						
5/4/2000 11:46	25.4	2.3	3.0	CALS	-0.1	25.1	0.2	12.3	0.1	12.6	25.2	2.2	2.9	833791	74919	225540	1134250						
5/4/2000 11:47	5.5	2.6	2.6	CALS	-0.1	25.1	0.2	12.3	0.1	12.6	5.5	2.6	2.5	833791	74919	225540	1134250						
5/4/2000 11:48	0.2	2.4	1.7	CALS	-0.1	25.1	0.2	12.3	0.1	12.6	0.2	2.4	1.6	833791	74919	225540	1134250						
5/4/2000 11:49	0.0	1.7	1.4	CALS	-0.1	25.1	0.2	12.3	0.1	12.6	0.1	1.6	1.3	833791	74919	225540	1134250						

TIME	OBSERVED CONCENTRATION PPM			COMMENTS	CALIBRATION CORRECTIONS						CORRECTED PPM VALUES			FLOW MEASURMENTS SCFM				MASS EMISSIONS			EMISSION FACTOR		
					NOX 7		SO2 IN		SO2 OUT														
	NOX COMP 7	SO2 IN	SO2 OUT		0.0	24.9	0.0	12.3	0.0	12.5	NOX - 7	SO2 IN	SO2 OUT	COLD-1	COLD-2	HOT	TOTAL	NOX LBS/HR	SO2 IN LBS/HR	SO2 OUT LBS/HR	PRODUCTION TONS/HR	NOX LBS/TON	SO2 LBS/TON
5/4/2000 11:50	0.0	1.5	2.2	CALS	-0.1	25.1	0.2	12.3	0.1	12.6	0.1	1.4	2.1	833791	74919	225540	1134250						
5/4/2000 11:51	0.0	1.5	3.0	CALS	-0.1	25.1	0.2	12.3	0.1	12.6	0.1	1.4	3.0	833791	74919	225540	1134250						
5/4/2000 11:52	0.0	1.4	2.8	CALS	-0.1	25.1	0.2	12.3	0.1	12.6	0.1	1.3	2.7	833791	74919	225540	1134250						
5/4/2000 11:53	0.2	1.7	4.3	CALS	-0.1	25.1	0.2	12.3	0.1	12.6	0.2	1.6	4.2	833791	74919	225540	1134250						
5/4/2000 11:54	0.1	1.8	6.2	CALS	-0.1	25.1	0.2	12.3	0.1	12.6	0.2	1.7	6.1	833791	74919	225540	1134250						
5/4/2000 11:55	0.0	1.7	1.3	CALS	-0.1	25.1	0.2	12.3	0.1	12.6	0.0	1.6	1.2	833791	74919	225540	1134250						
5/4/2000 11:56	0.8	1.5	0.3	CALS	-0.1	25.1	0.2	12.3	0.1	12.6	0.8	1.4	0.2	833791	74919	225540	1134250						
5/4/2000 11:57	3.2	1.4	0.2	CALS	-0.1	25.1	0.2	12.3	0.1	12.6	3.2	1.3	0.1	833791	74919	225540	1134250						
5/4/2000 11:58	4.8	1.2	0.1	CALS	-0.1	25.1	0.2	12.3	0.1	12.6	4.8	1.1	0.0	833791	74919	225540	1134250						
5/4/2000 11:59	4.5	1.0	0.1	CALS	-0.1	25.1	0.2	12.3	0.1	12.6	4.5	0.9	0.0	833791	74919	225540	1134250						
5/4/2000 12:00	4.4	1.0	0.1	CALS	-0.1	25.1	0.2	12.3	0.1	12.6	4.5	0.9	0.0	833791	74919	225540	1134250						
5/4/2000 12:01	4.3	1.2	0.1	CALS	-0.1	25.1	0.2	12.3	0.1	12.6	4.3	1.1	0.0	833791	74919	225540	1134250						
5/4/2000 12:02	4.5	1.3	0.1	CALS	-0.1	25.1	0.2	12.3	0.1	12.6	4.5	1.2	0.0	833791	74919	225540	1134250						
5/4/2000 12:03	4.9	1.3	0.3	CALS	-0.1	25.1	0.2	12.3	0.1	12.6	4.9	1.2	0.2	833791	74919	225540	1134250						
5/4/2000 12:04	5.1	1.1	0.4	CALS	-0.1	25.1	0.2	12.3	0.1	12.6	5.1	1.0	0.3	833791	74919	225540	1134250						
5/4/2000 12:05	5.0	1.1	0.5	CALS	-0.1	25.1	0.2	12.3	0.1	12.6	5.0	1.0	0.4	833791	74919	225540	1134250						
5/4/2000 12:06	4.8	1.1	0.4	CALS	-0.1	25.1	0.2	12.3	0.1	12.6	4.8	1.0	0.3	833791	74919	225540	1134250						
5/4/2000 12:07	4.6	1.4	0.3	CALS	-0.1	25.1	0.2	12.3	0.1	12.6	4.6	1.3	0.2	833791	74919	225540	1134250						
5/4/2000 12:08	4.3	1.3	0.2	CALS	-0.1	25.1	0.2	12.3	0.1	12.6	4.3	1.1	0.1	833791	74919	225540	1134250						
5/4/2000 12:09	4.0	1.2	0.2	CALS	-0.1	25.1	0.2	12.3	0.1	12.6	4.0	1.1	0.1	833791	74919	225540	1134250						
5/4/2000 12:10	3.9	1.2	0.2	CALS	-0.1	25.1	0.2	12.3	0.1	12.6	3.9	1.1	0.1	833791	74919	225540	1134250						
5/4/2000 12:11	3.8	1.2	0.3	CALS	-0.1	25.1	0.2	12.3	0.1	12.6	3.8	1.1	0.2	833791	74919	225540	1134250						
5/4/2000 12:12	3.7	1.0	0.4	CALS	-0.1	25.1	0.2	12.3	0.1	12.6	3.7	0.9	0.3	833791	74919	225540	1134250						
5/4/2000 12:13	3.6	1.0	0.4	CALS	-0.1	25.1	0.2	12.3	0.1	12.6	3.6	0.9	0.3	833791	74919	225540	1134250						
5/4/2000 12:14	3.6	1.1	0.4	CALS	-0.1	25.1	0.2	12.3	0.1	12.6	3.6	1.0	0.3	833791	74919	225540	1134250						
5/4/2000 12:15	3.6	1.5	0.4	CALS	-0.1	25.1	0.2	12.3	0.1	12.6	3.6	1.4	0.3	833791	74919	225540	1134250						
5/4/2000 12:16	3.6	1.7	0.4	CALS	-0.1	25.1	0.2	12.3	0.1	12.6	3.6	1.6	0.3	833791	74919	225540	1134250						
5/4/2000 12:17	3.7	1.7	0.2	CALS	-0.1	25.1	0.2	12.3	0.1	12.6	3.7	1.6	0.1	833791	74919	225540	1134250						
5/4/2000 12:18	3.9	1.7	0.2	CALS	-0.1	25.1	0.2	12.3	0.1	12.6	4.0	1.6	0.1	833791	74919	225540	1134250						
5/4/2000 12:19	4.1	1.5	0.2	CALS	-0.1	25.1	0.2	12.3	0.1	12.6	4.1	1.4	0.1	833791	74919	225540	1134250						
5/4/2000 12:20	4.0	1.5	5.5	CALS	-0.1	25.1	0.2	12.3	0.1	12.6	4.0	1.4	5.4	833791	74919	225540	1134250						
5/4/2000 12:21	3.9	1.7	19.0	CALS	-0.1	25.1	0.2	12.3	0.1	12.6	4.0	1.6	19.0	833791	74919	225540	1134250						
5/4/2000 12:22	3.9	2.0	22.4	CALS	-0.1	25.1	0.2	12.3	0.1	12.6	4.0	1.9	22.4	833791	74919	225540	1134250						
5/4/2000 12:23	3.9	2.1	23.3	CALS	-0.1	25.1	0.2	12.3	0.1	12.6	3.9	2.1	23.3	833791	74919	225540	1134250						
5/4/2000 12:24	3.9	2.1	23.8	CALS	-0.1	25.1	0.2	12.3	0.1	12.6	3.9	2.0	23.8	833791	74919	225540	1134250						
5/4/2000 12:25	3.9	1.8	24.0	CALS	-0.1	25.1	0.2	12.3	0.1	12.6	4.0	1.8	23.8	833791	74919	225540	1134250						
5/4/2000 12:26	3.8	1.5	24.1	CALS	-0.1	25.1	0.2	12.3	0.1	12.6	3.8	1.4	24.1	833791	74919	225540	1134250						
5/4/2000 12:27	3.8	1.4	24.0	CALS	-0.1	25.1	0.2	12.3	0.1	12.6	3.8	1.3	24.0	833791	74919	225540	1134250						
5/4/2000 12:28	3.9	1.6	24.0	CALS	-0.1	25.1	0.2	12.3	0.1	12.6	3.9	1.5	24.0	833791	74919	225540	1134250						
5/4/2000 12:29	4.0	1.5	24.0	CALS	-0.1	25.1	0.2	12.3	0.1	12.6	4.0	1.4	24.0	833791	74919	225540	1134250						
5/4/2000 12:30	3.9	1.3	21.5	CALS	-0.1	25.1	0.2	12.3	0.1	12.6	3.9	1.1	21.5	833791	74919	225540	1134250						
5/4/2000 12:31	3.8	1.0	16.3	CALS	-0.1	25.1	0.2	12.3	0.1	12.6	3.8	0.9	16.3	833791	74919	225540	1134250						
5/4/2000 12:32	3.8	0.9	13.8	CALS	-0.1	25.1	0.2	12.3	0.1	12.6	3.8	0.7	13.8	833791	74919	225540	1134250						
5/4/2000 12:33	3.8	0.8	12.8	CALS	-0.1	25.1	0.2	12.3	0.1	12.6	3.8	0.7	12.8	833791	74919	225540	1134250						
5/4/2000 12:34	3.8	0.8	12.5	CALS	-0.1	25.1	0.2	12.3	0.1	12.6	3.8	0.7	12.4	833791	74919	225540	1134250						
5/4/2000 12:35	3.9	2.3	12.1	CALS	-0.1	25.1	0.2	12.3	0.1	12.6	3.9	2.2	12.1	833791	74919	225540	1134250						
5/4/2000 12:36	3.7	9.2	8.9	CALS	-0.1	25.1	0.2	12.3	0.1	12.6	3.7	9.3	8.8	833791	74919	225540	1134250						
5/4/2000 12:37	3.6	11.6	4.8	CALS	-0.1	25.1	0.2	12.3	0.1	12.6	3.6	11.6	4.8	833791	74919	225540	1134250						
5/4/2000 12:38	3.7	12.1	2.8	CALS	-0.1	25.1	0.2	12.3	0.1	12.6	3.7	12.3	2.7	833791	74919	225540	1134250						
5/4/2000 12:39	3.7	12.2	1.9	CALS	-0.1	25.1	0.2	12.3	0.1	12.6	3.7	12.4	1.7	833791	74919	225540	1134250						
5/4/2000 12:40	3.9	12.8	1.6	CALS	-0.1	25.1	0.2	12.3	0.1	12.6	3.9	12.9	1.6	833791	74919	225540	1134250						
5/4/2000 12:41	4.1	16.4	1.5	CALS	-0.1	25.1	0.2	12.3	0.1	12.6	4.1	16.6	1.4	833791	74919	225540	1134250						
5/4/2000 12:42	4.2	7.2	1.5	CALS	-0.1	25.1	0.2	12.3	0.1	12.6	4.2	7.3	1.4	833791	74919	225540	1134250						
5/4/2000 12:43	3.9	3.3	1.1	CALS	-0.1	25.1	0.2	12.3	0.1	12.6	4.0	3.3	1.0	833791	74919	225540	1134250						
5/4/2000 12:44	4.0	15.7	0.9	CALS	-0.1	25.1	0.2	12.3	0.1	12.6	4.0	16.1	0.8	833791	74919	225540	1134250						

TIME	OBSERVED CONCENTRATION PPM			COMMENTS	CALIBRATION CORRECTIONS						CORRECTED PPM VALUES			FLOW MEASURMENTS SCFM				MASS EMISSIONS			EMISSION FACTOR		
					NOX 7		SO2 IN		SO2 OUT														
	NOX COMP 7	SO2 IN	SO2 OUT		0.0	24.9	0.0	12.5	0.0	12.5	NOX - 7	SO2 IN	SO2 OUT	COLD-1	COLD-2	HOT	TOTAL	NOX LBS/HR	SO2 IN LBS/HR	SO2 OUT LBS/HR	PRODUCTION TONS/HR	NOX LBS/TON	SO2 LBS/TON
5/4/2000 12:45	4.1	22.3	0.8	CALS	-0.1	25.1	0.2	12.3	0.1	12.6	4.1	22.9	0.7	833791	74919	225540	1134250						
5/4/2000 12:46	4.2	23.5	0.8	CALS	-0.1	25.1	0.2	12.3	0.1	12.6	4.2	24.1	0.7	833791	74919	225540	1134250						
5/4/2000 12:47	4.9	23.8	0.8	CALS	-0.1	25.1	0.2	12.3	0.1	12.6	5.0	24.5	0.7	833791	74919	225540	1134250						
5/4/2000 12:48	8.2	24.0	0.9	CALS	-0.1	25.1	0.2	12.3	0.1	12.6	8.2	24.7	0.8	833791	74919	225540	1134250						
5/4/2000 12:49	12.0	24.1	0.9	CALS	-0.1	25.1	0.2	12.3	0.1	12.6	12.0	24.8	0.8	833791	74919	225540	1134250						
5/4/2000 12:50	13.0	24.2	1.0	CALS	-0.1	25.1	0.2	12.3	0.1	12.6	12.9	24.9	0.9	833791	74919	225540	1134250						
5/4/2000 12:51	9.5	16.3	1.1	CALS	-0.1	25.1	0.2	12.3	0.1	12.6	9.4	16.7	1.0	833791	74919	225540	1134250						
5/4/2000 12:52	6.2	4.9	1.5	RUN 1	-0.1	25.1	0.2	12.3	0.1	12.6	6.2	4.9	1.4	833791	74919	225540	1134250	50.4	33.1	16.2	182	0.28	0.20
5/4/2000 12:53	8.5	0.8	1.7	RUN 1	-0.1	25.1	0.2	12.3	0.1	12.6	8.5	0.8	1.6	833791	74919	225540	1134250	52.5	7.1	18.0	182	0.29	0.07
5/4/2000 12:54	10.6	0.3	1.5	RUN 1	-0.1	25.1	0.2	12.3	0.1	12.6	10.6	0.2	1.4	833791	74919	225540	1134250	67.4	2.3	15.4	182	0.48	0.05
5/4/2000 12:55	14.5	0.3	1.4	RUN 1	-0.1	25.1	0.2	12.3	0.1	12.6	14.4	0.1	1.3	833791	74919	225540	1134250	117.3	1.6	15.1	182	0.64	0.05
5/4/2000 12:56	12.3	0.2	1.3	RUN 1	-0.1	25.1	0.2	12.3	0.1	12.6	12.3	0.1	1.2	833791	74919	225540	1134250	99.6	0.9	14.0	182	0.55	0.04
5/4/2000 12:57	9.2	0.2	1.2	RUN 1	-0.1	25.1	0.2	12.3	0.1	12.6	9.2	0.0	1.1	833791	74919	225540	1134250	74.8	0.6	12.9	182	0.41	0.04
5/4/2000 12:58	7.6	1.6	1.2	RUN 1	-0.1	25.1	0.2	12.3	0.1	12.6	7.6	1.5	1.1	833791	74919	225540	1134250	61.6	16.7	12.9	182	0.34	0.06
5/4/2000 12:59	6.8	1.8	1.1	RUN 1	-0.1	25.1	0.2	12.3	0.1	12.6	6.8	1.8	1.0	833791	74919	225540	1134250	55.5	20.6	11.8	182	0.30	0.09
5/4/2000 13:00	5.9	1.3	1.1	RUN 1	-0.1	25.1	0.2	12.3	0.1	12.6	5.9	1.2	1.0	833791	74919	225540	1134250	47.9	13.3	11.1	182	0.26	0.07
5/4/2000 13:01	5.5	1.0	1.0	RUN 1	-0.1	25.1	0.2	12.3	0.1	12.6	5.5	0.8	1.0	833791	74919	225540	1134250	44.4	9.5	10.7	182	0.24	0.05
5/4/2000 13:02	7.3	1.4	1.2	RUN 1	-0.1	25.1	0.2	12.3	0.1	12.6	7.3	1.3	1.1	833791	74919	225540	1134250	59.6	14.6	12.9	182	0.33	0.08
5/4/2000 13:03	8.3	1.8	1.3	RUN 1	-0.1	25.1	0.2	12.3	0.1	12.6	8.3	1.7	1.2	833791	74919	225540	1134250	67.7	19.1	13.6	182	0.37	0.09
5/4/2000 13:04	7.1	1.8	1.5	RUN 1	-0.1	25.1	0.2	12.3	0.1	12.5	7.1	1.7	1.4	833791	74919	225540	1134250	58.0	19.1	15.8	182	0.32	0.10
5/4/2000 13:05	6.9	1.4	1.8	RUN 1	-0.1	25.1	0.2	12.3	0.1	12.6	6.9	1.3	1.7	833791	74919	225540	1134250	56.0	14.6	19.0	182	0.31	0.09
5/4/2000 13:06	8.7	1.3	1.9	RUN 1	-0.1	25.1	0.2	12.3	0.1	12.6	8.6	1.2	1.8	833791	74919	225540	1134250	70.2	13.9	20.1	182	0.39	0.09
5/4/2000 13:07	11.6	1.3	1.5	RUN 1	-0.1	25.1	0.2	12.3	0.1	12.6	11.6	1.2	1.4	833791	74919	225540	1134250	95.5	13.6	15.6	182	0.52	0.06
5/4/2000 13:08	15.6	1.3	1.5	RUN 1	-0.1	25.1	0.2	12.3	0.1	12.6	15.6	1.2	1.4	833791	74919	225540	1134250	126.5	13.6	16.2	182	0.69	0.06
5/4/2000 13:09	14.4	1.1	1.3	RUN 1	-0.1	25.1	0.2	12.3	0.1	12.6	14.3	1.0	1.2	833791	74919	225540	1134250	116.3	11.2	13.6	182	0.64	0.07
5/4/2000 13:10	10.0	0.8	0.8	RUN 1	-0.1	25.1	0.2	12.3	0.1	12.6	9.9	0.8	0.8	833791	74919	225540	1134250	80.8	9.1	9.3	182	0.44	0.05
5/4/2000 13:11	8.4	0.9	0.7	RUN 1	-0.1	25.1	0.2	12.3	0.1	12.6	8.4	0.8	0.6	833791	74919	225540	1134250	68.2	6.8	6.8	182	0.37	0.04
5/4/2000 13:12	11.9	1.0	0.7	RUN 1	-0.1	25.1	0.2	12.3	0.1	12.6	11.8	0.8	0.6	833791	74919	225540	1134250	96.6	9.5	6.8	182	0.53	0.04
5/4/2000 13:13	14.9	1.0	1.0	RUN 1	-0.1	25.1	0.2	12.3	0.1	12.6	14.9	0.9	0.9	833791	74919	225540	1134250	120.9	10.5	10.0	182	0.66	0.06
5/4/2000 13:14	15.8	1.2	1.7	RUN 1	-0.1	25.1	0.2	12.3	0.1	12.6	15.7	1.1	1.7	833791	74919	225540	1134250	128.0	11.9	16.7	182	0.70	0.08
5/4/2000 13:15	14.2	1.2	1.7	RUN 1	-0.1	25.1	0.2	12.3	0.1	12.6	14.2	1.1	1.6	833791	74919	225540	1134250	115.3	11.9	16.3	182	0.63	0.08
5/4/2000 13:16	11.3	1.3	1.2	RUN 1	-0.1	25.1	0.2	12.3	0.1	12.6	11.3	1.1	1.1	833791	74919	225540	1134250	91.5	12.9	12.2	182	0.50	0.07
5/4/2000 13:17	10.5	1.2	1.0	RUN 1	-0.1	25.1	0.2	12.3	0.1	12.6	10.4	1.1	0.9	833791	74919	225540	1134250	84.9	11.9	9.7	182	0.47	0.06
5/4/2000 13:18	7.2	1.4	1.6	RUN 1	-0.1	25.1	0.2	12.3	0.1	12.6	7.2	1.3	1.5	833791	74919	225540	1134250	58.5	14.6	16.5	182	0.32	0.09
5/4/2000 13:19	4.2	1.5	2.3	RUN 1	-0.1	25.1	0.2	12.3	0.1	12.6	4.2	1.4	2.3	833791	74919	225540	1134250	34.2	15.3	25.5	182	0.19	0.11
5/4/2000 13:20	2.8	1.3	2.4	RUN 1	-0.1	25.1	0.2	12.3	0.1	12.6	2.8	1.2	2.4	833791	74919	225540	1134250	23.1	13.9	26.6	182	0.13	0.11
5/4/2000 13:21	2.3	1.2	2.5	RUN 1	-0.1	25.1	0.2	12.3	0.1	12.6	2.3	1.1	2.4	833791	74919	225540	1134250	19.0	12.8	27.0	182	0.10	0.11
5/4/2000 13:22	2.3	1.1	2.6	RUN 1	-0.1	25.1	0.2	12.3	0.1	12.6	2.3	1.0	2.5	833791	74919	225540	1134250	19.0	11.5	28.0	182	0.10	0.11
5/4/2000 13:23	2.7	1.1	2.6	RUN 1	-0.1	25.1	0.2	12.3	0.1	12.6	2.8	1.0	2.5	833791	74919	225540	1134250	22.6	10.9	28.4	182	0.12	0.11
5/4/2000 13:24	3.3	1.3	2.6	RUN 1	-0.1	25.1	0.2	12.3	0.1	12.6	3.3	1.2	2.5	833791	74919	225540	1134250	27.1	13.6	26.8	182	0.15	0.12
5/4/2000 13:25	3.7	1.5	2.7	RUN 1	-0.1	25.1	0.2	12.3	0.1	12.6	3.7	1.4	2.6	833791	74919	225540	1134250	30.2	16.0	29.1	182	0.17	0.12
5/4/2000 13:26	4.0	1.4	2.5	RUN 1	-0.1	25.1	0.2	12.3	0.1	12.6	4.0	1.3	2.4	833791	74919	225540	1134250	32.7	14.3	27.3	182	0.18	0.11
5/4/2000 13:27	4.1	1.2	2.5	RUN 1	-0.1	25.1	0.2	12.3	0.1	12.6	4.1	1.1	2.4	833791	74919	225540	1134250	33.2	11.9	27.0	182	0.18	0.11
5/4/2000 13:28	3.8	1.0	2.3	RUN 1	-0.1	25.1	0.2	12.3	0.1	12.6	3.8	0.9	2.3	833791	74919	225540	1134250	31.2	10.5	25.5	182	0.17	0.10
5/4/2000 13:29	4.9	1.0	2.4	RUN 1	-0.1	25.1	0.2	12.3	0.1	12.6	5.0	0.9	2.3	833791	74919	225540	1134250	40.3	10.2	25.9	182	0.22	0.10
5/4/2000 13:30	10.0	1.3	2.2	RUN 1	-0.1	25.1	0.2	12.3	0.1	12.6	10.0	1.2	2.1	833791	74919	225540	1134250	81.4	13.3	23.7	182	0.45	0.10
5/4/2000 13:31	11.8	1.6	2.0	RUN 1	-0.1	25.1	0.2	12.3	0.1	12.6	11.8	1.5	1.9	833791	74919	225540	1134250	95.5	16.7	21.6	182	0.52	0.11
5/4/2000 13:32	9.7	1.1	1.8	RUN 1	-0.1	25.1	0.2	12.3	0.1	12.6	9.7	1.0	1.5	833791	74919	225540	1134250	78.8	11.2	17.2	182	0.43	0.08
5/4/2000 13:33	7.6	0.9	1.2	RUN 1	-0.1	25.1	0.2	12.3	0.1	12.6	7.6	0.8	1.1	833791	74919	225540	1134250	61.6	8.8	12.9	182	0.34	0.06
5/4/2000 13:34	6.0	0.8	1.2	RUN 1	-0.1	25.1	0.2	12.3	0.1	12.6	6.0	0.7	1.1	833791	74919	225540	1134250	48.4	7.8	12.2	182	0.27	0.05
5/4/2000 13:35	4.9	0.7	1.1	RUN 1	-0.1	25.1	0.2	12.3	0.1	12.6	5.0	0.6	1.0	833791	74919	225540	1134250	40.3	6.7	11.8	182	0.22	0.05
5/4/2000 13:36	4.6	0.7	0.9	RUN 1	-0.1	25.1	0.2	12.3	0.1	12.6	4.6	0.6	0.8	833791	74919	225540	1134250	37.3	6.4	9.3	182	0.20	0.04
5/4/2000 13:37	4.4	0.8	0.8	RUN 1	-0.1	25.1	0.2	12.3	0.1	12.6	4.4	0.6	0.7	833791	74919	225540	1134250	35.7	7.1	7.9	182	0.20	0.04
5/4/2000 13:38	4.3	0.8	0.7	RUN 1	-0.1	25.1	0.2	12.3	0.1	12.6	4.3	0.6	0.6	833791	74919	225540	1134250	35.2	7.1	6.8	182	0.19	0.04
5/4/2000 13:39	4.6	0.8	0.7	RUN 1	-0.1	25.1	0.2	12.3	0.1	12.6	4.5	0.6	0.6	833791	74919	225540	1134250	36.2	7.1	6.8	182	0.20	0.04

TIME	OBSERVED CONCENTRATION PPM			COMMENTS	CALIBRATION CORRECTIONS						CORRECTED PPM VALUES			FLOW MEASURMENTS SCFM				MASS EMISSIONS			EMISSION FACTOR		
					NOX 7		SO2 IN		SO2 OUT														
	NOX COMP 7	SO2 IN	SO2 OUT		0.0	24.9	0.0	12.5	0.0	12.5	NOX - 7	SO2 IN	SO2 OUT	COLD-1	COLD-2	HOT	TOTAL	NOX LBS/HR	SO2 IN LBS/HR	SO2 OUT LBS/HR	PRODUCTION TONS/HR	NOX LBS/TON	SO2 LBS/TON
5/4/2000 13:40	4.4	0.7	0.9	RUN 1	-0.1	25.1	0.2	12.3	0.1	12.6	4.4	0.6	0.8	833791	74919	225540	1134250	35.7	6.7	8.6	182	0.20	0.04
5/4/2000 13:41	4.6	0.8	1.2	RUN 1	-0.1	25.1	0.2	12.3	0.1	12.6	4.6	0.7	1.1	833791	74919	225540	1134250	37.8	7.4	12.5	182	0.21	0.05
5/4/2000 13:42	6.2	1.0	1.6	RUN 1	-0.1	25.1	0.2	12.3	0.1	12.6	6.2	0.8	1.7	833791	74919	225540	1134250	50.4	9.5	19.4	182	0.28	0.06
5/4/2000 13:43	7.0	1.0	1.6	RUN 1	-0.1	25.1	0.2	12.3	0.1	12.6	7.0	0.9	1.5	833791	74919	225540	1134250	56.5	10.2	17.2	182	0.31	0.06
5/4/2000 13:44	7.5	1.2	1.1	RUN 1	-0.1	25.1	0.2	12.3	0.1	12.6	7.5	1.1	1.0	833791	74919	225540	1134250	60.6	11.9	11.8	182	0.33	0.07
5/4/2000 13:45	8.5	1.7	1.5	RUN 1	-0.1	25.1	0.2	12.3	0.1	12.6	8.4	1.6	1.4	833791	74919	225540	1134250	68.7	17.7	15.4	182	0.38	0.09
5/4/2000 13:46	12.7	1.4	1.9	RUN 1	-0.1	25.1	0.2	12.3	0.1	12.6	12.7	1.3	1.8	833791	74919	225540	1134250	103.1	15.0	20.8	182	0.57	0.10
5/4/2000 13:47	15.4	1.2	1.9	RUN 1	-0.1	25.1	0.2	12.3	0.1	12.6	15.4	1.1	1.8	833791	74919	225540	1134250	124.9	12.6	20.1	182	0.69	0.09
5/4/2000 13:48	14.8	1.0	1.7	RUN 1	-0.1	25.1	0.2	12.3	0.1	12.6	14.7	0.9	1.6	833791	74919	225540	1134250	119.9	10.2	18.0	182	0.66	0.06
5/4/2000 13:49	13.4	0.9	1.5	RUN 1	-0.1	25.1	0.2	12.3	0.1	12.6	13.4	0.8	1.4	833791	74919	225540	1134250	108.7	8.8	15.8	182	0.60	0.07
5/4/2000 13:50	12.6	0.7	1.1	RUN 1	-0.1	25.1	0.2	12.3	0.1	12.6	12.5	0.6	1.0	833791	74919	225540	1134250	101.6	6.4	11.6	182	0.56	0.05
5/4/2000 13:51	12.2	0.7	1.0	RUN 1	-0.1	25.1	0.2	12.3	0.1	12.6	12.2	0.5	0.9	833791	74919	225540	1134250	99.1	6.1	10.0	182	0.54	0.04
5/4/2000 13:52	11.7	0.7	1.0	RUN 1	-0.1	25.1	0.2	12.3	0.1	12.6	11.7	0.6	0.9	833791	74919	225540	1134250	95.0	6.7	10.4	182	0.52	0.05
5/4/2000 13:53	10.8	0.8	1.0	RUN 1	-0.1	25.1	0.2	12.3	0.1	12.6	10.8	0.7	1.0	833791	74919	225540	1134250	87.4	7.4	10.7	182	0.48	0.05
5/4/2000 13:54	10.0	0.7	0.9	RUN 1	-0.1	25.1	0.2	12.3	0.1	12.6	10.0	0.6	0.8	833791	74919	225540	1134250	81.4	6.4	8.9	182	0.45	0.04
5/4/2000 13:55	9.2	0.6	0.7	RUN 1	-0.1	25.1	0.2	12.3	0.1	12.6	9.2	0.5	0.6	833791	74919	225540	1134250	74.8	5.4	8.8	182	0.41	0.03
5/4/2000 13:56	8.7	0.6	0.6	RUN 1	-0.1	25.1	0.2	12.3	0.1	12.6	8.7	0.4	0.5	833791	74919	225540	1134250	70.7	4.7	5.7	182	0.39	0.03
5/4/2000 13:57	8.5	0.6	0.6	RUN 1	-0.1	25.1	0.2	12.3	0.1	12.6	8.4	0.5	0.5	833791	74919	225540	1134250	68.7	5.4	5.3	182	0.38	0.03
5/4/2000 13:58	8.8	0.7	0.7	RUN 1	-0.1	25.1	0.2	12.3	0.1	12.6	8.8	0.6	0.6	833791	74919	225540	1134250	71.2	6.4	6.8	182	0.39	0.04
5/4/2000 13:59	9.2	0.8	0.8	RUN 1	-0.1	25.1	0.2	12.3	0.1	12.6	9.2	0.6	0.7	833791	74919	225540	1134250	74.8	7.1	7.5	182	0.41	0.04
5/4/2000 14:00	9.0	0.9	0.8	RUN 1	-0.1	25.1	0.2	12.3	0.1	12.6	8.9	0.8	0.7	833791	74919	225540	1134250	72.7	9.1	8.2	182	0.40	0.05
5/4/2000 14:01	7.9	1.3	1.0	RUN 1	-0.1	25.1	0.2	12.3	0.1	12.6	7.9	1.2	1.0	833791	74919	225540	1134250	64.1	13.6	10.7	182	0.35	0.07
5/4/2000 14:02	7.2	1.5	1.2	RUN 1	-0.1	25.1	0.2	12.3	0.1	12.6	7.2	1.4	1.1	833791	74919	225540	1134250	58.5	16.0	12.9	182	0.32	0.08
5/4/2000 14:03	7.4	1.5	1.4	RUN 1	-0.1	25.1	0.2	12.3	0.1	12.6	7.4	1.4	1.3	833791	74919	225540	1134250	60.1	16.3	14.7	182	0.33	0.09
5/4/2000 14:04	7.7	1.2	1.3	RUN 1	-0.1	25.1	0.2	12.3	0.1	12.6	7.7	1.1	1.2	833791	74919	225540	1134250	62.6	12.6	14.0	182	0.34	0.07
5/4/2000 14:05	7.3	1.6	1.0	RUN 1	-0.1	25.1	0.2	12.3	0.1	12.6	7.3	1.5	1.0	833791	74919	225540	1134250	59.1	17.0	10.7	182	0.32	0.08
5/4/2000 14:06	6.5	1.5	0.8	RUN 1	-0.1	25.1	0.2	12.3	0.1	12.6	6.5	1.4	0.7	833791	74919	225540	1134250	52.5	15.7	7.9	182	0.29	0.06
5/4/2000 14:07	5.4	1.6	0.9	RUN 1	-0.1	25.1	0.2	12.3	0.1	12.6	5.4	1.5	0.8	833791	74919	225540	1134250	43.8	16.7	8.9	182	0.24	0.07
5/4/2000 14:08	4.5	2.0	1.3	RUN 1	-0.1	25.1	0.2	12.3	0.1	12.6	4.5	1.8	1.2	833791	74919	225540	1134250	36.8	21.5	13.8	182	0.20	0.10
5/4/2000 14:09	4.2	2.2	1.4	RUN 1	-0.1	25.1	0.2	12.3	0.1	12.6	4.2	2.1	1.3	833791	74919	225540	1134250	34.2	23.9	15.1	182	0.19	0.11
5/4/2000 14:10	4.0	1.7	1.3	RUN 1	-0.1	25.1	0.2	12.3	0.1	12.6	4.0	1.6	1.2	833791	74919	225540	1134250	32.7	18.4	13.3	182	0.18	0.09
5/4/2000 14:11	3.8	1.0	1.0	RUN 1	-0.1	25.1	0.2	12.3	0.1	12.6	3.6	0.9	0.9	833791	74919	225540	1134250	29.7	10.5	10.0	182	0.16	0.06
5/4/2000 14:12	3.8	0.7	0.8	RUN 1	-0.1	25.1	0.2	12.3	0.1	12.6	3.8	0.6	0.7	833791	74919	225540	1134250	31.2	6.7	7.9	182	0.17	0.04
5/4/2000 14:13	4.0	0.6	0.8	RUN 1	-0.1	25.1	0.2	12.3	0.1	12.6	4.0	0.5	0.7	833791	74919	225540	1134250	32.7	5.7	7.5	182	0.18	0.04
5/4/2000 14:14	4.2	0.6	0.8	RUN 1	-0.1	25.1	0.2	12.3	0.1	12.6	4.2	0.4	0.7	833791	74919	225540	1134250	34.2	4.7	7.5	182	0.19	0.03
5/4/2000 14:15	4.2	0.5	0.7	RUN 1	-0.1	25.1	0.2	12.3	0.1	12.6	4.2	0.4	0.6	833791	74919	225540	1134250	34.2	4.0	6.8	182	0.19	0.03
5/4/2000 14:16	4.1	0.4	0.6	RUN 1	-0.1	25.1	0.2	12.3	0.1	12.6	4.1	0.3	0.5	833791	74919	225540	1134250	33.7	3.0	6.1	182	0.19	0.02
5/4/2000 14:17	4.2	0.4	0.5	RUN 1	-0.1	25.1	0.2	12.3	0.1	12.6	4.2	0.2	0.4	833791	74919	225540	1134250	34.2	2.6	5.0	182	0.19	0.02
5/4/2000 14:18	4.1	0.4	0.5	RUN 1	-0.1	25.1	0.2	12.3	0.1	12.6	4.1	0.2	0.4	833791	74919	225540	1134250	33.7	2.6	4.6	182	0.19	0.02
5/4/2000 14:19	4.1	0.4	0.5	RUN 1	-0.1	25.1	0.2	12.3	0.1	12.6	4.1	0.2	0.4	833791	74919	225540	1134250	33.7	2.6	4.6	182	0.19	0.02
5/4/2000 14:20	4.0	0.3	0.5	RUN 1	-0.1	25.1	0.2	12.3	0.1	12.6	4.0	0.2	0.4	833791	74919	225540	1134250	32.7	2.3	4.6	182	0.18	0.02
5/4/2000 14:21	3.9	0.3	0.5	RUN 1	-0.1	25.1	0.2	12.3	0.1	12.6	3.9	0.2	0.4	833791	74919	225540	1134250	31.7	2.3	4.3	182	0.17	0.02
5/4/2000 14:22	3.9	0.3	0.4	RUN 1	-0.1	25.1	0.2	12.3	0.1	12.6	3.9	0.2	0.3	833791	74919	225540	1134250	31.7	1.9	3.9	182	0.17	0.02
5/4/2000 14:23	3.9	0.3	0.4	RUN 1	-0.1	25.1	0.2	12.3	0.1	12.6	3.9	0.1	0.3	833791	74919	225540	1134250	31.7	1.6	3.9	182	0.17	0.02
5/4/2000 14:24	3.9	0.3	0.5	RUN 1	-0.1	25.1	0.2	12.3	0.1	12.6	3.9	0.1	0.4	833791	74919	225540	1134250	31.7	1.6	4.3	182	0.17	0.02
5/4/2000 14:25	3.8	0.3	0.4	RUN 1	-0.1	25.1	0.2	12.3	0.1	12.6	3.8	0.2	0.3	833791	74919	225540	1134250	31.2	2.3	3.9	182	0.17	0.02
5/4/2000 14:26	3.9	0.4	0.5	RUN 1	-0.1	25.1	0.2	12.3	0.1	12.6	3.9	0.3	0.4	833791	74919	225540	1134250	31.7	3.0	4.3	182	0.17	0.02
5/4/2000 14:27	4.1	0.4	0.5	RUN 1	-0.1	25.1	0.2	12.3	0.1	12.6	4.1	0.2	0.4	833791	74919	225540	1134250	33.7	2.6	4.6	182	0.19	0.02
5/4/2000 14:28	4.1	0.3	0.4	RUN 1	-0.1	25.1	0.2	12.3	0.1	12.6	4.1	0.2	0.3	833791	74919	225540	1134250	33.2	2.3	3.5	182	0.18	0.02
5/4/2000 14:29	3.9	0.3	0.4	RUN 1	-0.1	25.1	0.2	12.3	0.1	12.6	3.9	0.2	0.3	833791	74919	225540	1134250	31.7	2.3	3.2	182	0.17	0.02
5/4/2000 14:30	3.8	0.3	0.4	RUN 1	-0.1	25.1	0.2	12.3	0.1	12.6	3.8	0.2	0.3	833791	74919	225540	1134250	30.7	2.3	3.2	182	0.17	0.02
5/4/2000 14:31	3.8	0.3	0.4	RUN 1	-0.1	25.1	0.2	12.3	0.1	12.6	3.8	0.2	0.3	833791	74919	225540	1134250	31.2	2.3	3.2	182	0.17	0.02
5/4/2000 14:32	3.9	0.4	0.3	RUN 1	-0.1	25.1	0.2	12.3	0.1	12.6	3.9	0.2	0.2	833791	74919	225540	1134250	31.7	2.6	2.5	182	0.17	0.01
5/4/2000 14:33	3.8	0.4	0.3	RUN 1	-0.1	25.1	0.2	12.3	0.1	12.6	3.8	0.2	0.2	833791	74919	225540	1134250	29.2	2.6	2.1	182	0.16	0.01
5/4/2000 14:34	3.4	0.4	0.3	RUN 1	-0.1	25.1	0.2	12.3	0.1	12.6	3.5	0.3	0.2	833791	74919	225540	1134250	28.1	3.0	1.7	182	0.15	0.01

TIME	OBSERVED CONCENTRATION PPM			COMMENTS	CALIBRATION CORRECTIONS						CORRECTED PPM VALUES			FLOW MEASURMENTS SCFM				MASS EMISSIONS			EMISSION FACTOR		
					NOX 7		SO2 IN		SO2 OUT														
	NOX COMP 7	SO2 IN	SO2 OUT		0.0	24.9	0.0	12.5	0.0	12.5	NOX - 7	SO2 IN	SO2 OUT	COLD-1	COLD-2	HOT	TOTAL	NOX LBS/HR	SO2 IN LBS/HR	SO2 OUT LBS/HR	PRODUCTION TONS/HR	NOX LBS/TON	SO2 LBS/TON
5/4/2000 14:35	3.9	0.4	0.3	RUN 1	-0.1	25.1	0.2	12.3	0.1	12.6	3.9	0.3	0.2	833791	74919	225540	1134250	31.7	3.0	2.1	182	0.17	0.01
5/4/2000 14:36	4.1	0.4	0.3	RUN 1	-0.1	25.1	0.2	12.3	0.1	12.6	4.1	0.3	0.2	833791	74919	225540	1134250	33.7	3.0	2.6	182	0.19	0.02
5/4/2000 14:37	4.1	0.4	0.4	RUN 1	-0.1	25.1	0.2	12.3	0.1	12.6	4.1	0.2	0.3	833791	74919	225540	1134250	33.7	2.6	3.9	182	0.19	0.02
5/4/2000 14:38	3.8	0.4	0.4	RUN 1	-0.1	25.1	0.2	12.3	0.1	12.6	3.8	0.3	0.3	833791	74919	225540	1134250	31.2	3.0	3.5	182	0.17	0.02
5/4/2000 14:39	3.7	0.4	0.3	RUN 1	-0.1	25.1	0.2	12.3	0.1	12.6	3.7	0.3	0.2	833791	74919	225540	1134250	30.2	3.3	2.5	182	0.17	0.02
5/4/2000 14:40	5.4	0.6	0.4	RUN 1	-0.1	25.1	0.2	12.3	0.1	12.6	5.4	0.5	0.3	833791	74919	225540	1134250	43.6	5.7	3.2	182	0.24	0.02
5/4/2000 14:41	8.5	0.7	0.6	RUN 1	-0.1	25.1	0.2	12.3	0.1	12.6	8.5	0.6	0.5	833791	74919	225540	1134250	69.2	6.7	6.1	182	0.38	0.04
5/4/2000 14:42	10.3	0.8	0.9	RUN 1	-0.1	25.1	0.2	12.3	0.1	12.6	10.3	0.6	0.8	833791	74919	225540	1134250	83.4	7.1	8.9	182	0.46	0.04
5/4/2000 14:43	10.2	0.8	1.2	RUN 1	-0.1	25.1	0.2	12.3	0.1	12.6	10.2	0.6	1.1	833791	74919	225540	1134250	82.9	7.1	12.9	182	0.46	0.05
5/4/2000 14:44	9.9	0.8	1.3	RUN 1	-0.1	25.1	0.2	12.3	0.1	12.6	9.9	0.5	1.2	833791	74919	225540	1134250	80.3	5.7	14.0	182	0.44	0.05
5/4/2000 14:45	9.9	0.8	1.2	RUN 1	-0.1	25.1	0.2	12.3	0.1	12.6	9.9	0.5	1.1	833791	74919	225540	1134250	80.3	5.4	12.5	182	0.44	0.05
5/4/2000 14:46	10.8	0.7	1.3	RUN 1	-0.1	25.1	0.2	12.3	0.1	12.6	10.8	0.6	1.2	833791	74919	225540	1134250	87.9	6.7	14.0	182	0.48	0.06
5/4/2000 14:47	10.9	1.0	1.9	RUN 1	-0.1	25.1	0.2	12.3	0.1	12.6	10.9	0.8	1.8	833791	74919	225540	1134250	88.4	9.5	20.1	182	0.49	0.06
5/4/2000 14:48	10.5	1.1	1.9	RUN 1	-0.1	25.1	0.2	12.3	0.1	12.6	10.4	1.0	1.8	833791	74919	225540	1134250	84.9	10.9	20.5	182	0.47	0.09
5/4/2000 14:49	9.7	0.9	1.6	RUN 1	-0.1	25.1	0.2	12.3	0.1	12.6	9.6	0.8	1.5	833791	74919	225540	1134250	78.3	9.1	17.2	182	0.43	0.07
5/4/2000 14:50	7.8	0.7	1.3	RUN 1	-0.1	25.1	0.2	12.3	0.1	12.6	7.8	0.6	1.2	833791	74919	225540	1134250	63.1	6.4	13.3	182	0.35	0.05
5/4/2000 14:51	6.0	0.6	1.0	RUN 1	-0.1	25.1	0.2	12.3	0.1	12.6	6.0	0.5	0.9	833791	74919	225540	1134250	48.9	5.4	10.4	182	0.27	0.04
5/4/2000 14:52	5.0	0.6	0.9	RUN 1	-0.1	25.1	0.2	12.3	0.1	12.6	5.0	0.5	0.8	833791	74919	225540	1134250	40.8	5.7	8.6	182	0.22	0.04
5/4/2000 14:53	4.4	0.7	1.1	RUN 1	-0.1	25.1	0.2	12.3	0.1	12.6	4.4	0.6	1.0	833791	74919	225540	1134250	35.7	6.7	11.1	182	0.20	0.05
5/4/2000 14:54	3.9	0.8	1.3	RUN 1	-0.1	25.1	0.2	12.3	0.1	12.6	4.0	0.7	1.2	833791	74919	225540	1134250	32.2	7.8	13.3	182	0.18	0.06
5/4/2000 14:55	3.7	0.7	1.2	RUN 1	-0.1	25.1	0.2	12.3	0.1	12.6	3.7	0.6	1.1	833791	74919	225540	1134250	30.2	6.7	12.2	182	0.17	0.05
5/4/2000 14:56	3.7	0.7	0.9	RUN 1	-0.1	25.1	0.2	12.3	0.1	12.6	3.7	0.5	0.8	833791	74919	225540	1134250	30.2	6.1	8.9	182	0.17	0.04
5/4/2000 14:57	3.8	0.6	0.8	RUN 1	-0.1	25.1	0.2	12.3	0.1	12.6	3.8	0.5	0.7	833791	74919	225540	1134250	30.7	5.7	8.2	182	0.17	0.04
5/4/2000 14:58	4.1	0.6	0.8	RUN 1	-0.1	25.1	0.2	12.3	0.1	12.6	4.1	0.4	0.7	833791	74919	225540	1134250	33.2	5.0	7.9	182	0.18	0.04
5/4/2000 14:59	4.9	0.6	0.7	RUN 1	-0.1	25.1	0.2	12.3	0.1	12.6	5.0	0.5	0.6	833791	74919	225540	1134250	40.3	5.7	6.8	182	0.22	0.03
5/4/2000 15:00	5.5	0.6	0.6	RUN 1	-0.1	25.1	0.2	12.3	0.1	12.6	5.5	0.7	0.5	833791	74919	225540	1134250	44.4	7.4	5.3	182	0.24	0.04
5/4/2000 15:01	5.9	0.8	0.5	RUN 1	-0.1	25.1	0.2	12.3	0.1	12.6	5.9	0.7	0.4	833791	74919	225540	1134250	47.9	7.8	4.3	182	0.26	0.03
5/4/2000 15:02	5.9	0.8	0.5	RUN 1	-0.1	25.1	0.2	12.3	0.1	12.6	5.9	0.7	0.4	833791	74919	225540	1134250	47.9	7.4	4.6	182	0.26	0.03
5/4/2000 15:03	4.9	0.8	0.6	RUN 1	-0.1	25.1	0.2	12.3	0.1	12.6	4.9	0.7	0.5	833791	74919	225540	1134250	39.8	7.4	6.1	182	0.22	0.04
5/4/2000 15:04	4.4	0.9	1.0	RUN 1	-0.1	25.1	0.2	12.3	0.1	12.6	4.4	0.8	0.9	833791	74919	225540	1134250	35.7	9.1	9.7	182	0.20	0.05
5/4/2000 15:05	4.5	1.0	1.3	RUN 1	-0.1	25.1	0.2	12.3	0.1	12.6	4.5	0.9	1.2	833791	74919	225540	1134250	36.6	10.5	13.3	182	0.20	0.07
5/4/2000 15:06	4.0	1.0	1.0	RUN 1	-0.1	25.1	0.2	12.3	0.1	12.6	4.0	0.9	1.0	833791	74919	225540	1134250	32.7	10.2	10.7	182	0.18	0.06
5/4/2000 15:07	4.2	1.1	1.0	RUN 1	-0.1	25.1	0.2	12.3	0.1	12.6	4.2	1.0	0.9	833791	74919	225540	1134250	34.2	11.5	10.0	182	0.19	0.06
5/4/2000 15:08	4.4	1.5	1.7	RUN 1	-0.1	25.1	0.2	12.3	0.1	12.6	4.4	1.4	1.6	833791	74919	225540	1134250	35.7	15.7	18.0	182	0.20	0.09
5/4/2000 15:09	4.9	1.4	2.5	RUN 1	-0.1	25.1	0.2	12.3	0.1	12.6	4.8	1.3	2.4	833791	74919	225540	1134250	39.6	14.3	27.3	182	0.22	0.11
5/4/2000 15:10	5.3	1.4	3.0	RUN 1	-0.1	25.1	0.2	12.3	0.1	12.6	5.3	1.3	3.0	833791	74919	225540	1134250	42.8	15.0	33.4	182	0.24	0.13
5/4/2000 15:11	4.1	1.4	3.4	RUN 1	-0.1	25.1	0.2	12.3	0.1	12.6	4.1	1.3	3.3	833791	74919	225540	1134250	33.2	14.6	37.0	182	0.18	0.14
5/4/2000 15:12	2.9	1.3	2.8	RUN 1	-0.1	25.1	0.2	12.3	0.1	12.6	3.0	1.1	2.8	833791	74919	225540	1134250	24.1	12.9	31.3	182	0.13	0.12
5/4/2000 15:13	2.6	1.3	2.6	RUN 1	-0.1	25.1	0.2	12.3	0.1	12.6	2.6	1.2	2.5	833791	74919	225540	1134250	21.0	13.6	26.6	182	0.12	0.12
5/4/2000 15:14	2.4	1.8	3.2	RUN 1	-0.1	25.1	0.2	12.3	0.1	12.6	2.5	1.5	3.1	833791	74919	225540	1134250	20.0	17.4	35.6	182	0.11	0.15
5/4/2000 15:15	2.3	2.1	3.0	RUN 1	-0.1	25.1	0.2	12.3	0.1	12.6	2.3	2.0	3.8	833791	74919	225540	1134250	19.0	22.9	43.5	182	0.10	0.18
5/4/2000 15:16	2.3	2.2	3.2	RUN 1	-0.1	25.1	0.2	12.3	0.1	12.6	2.3	2.1	3.1	833791	74919	225540	1134250	19.0	23.9	34.9	182	0.10	0.16
5/4/2000 15:17	3.0	1.8	3.6	RUN 1	-0.1	25.1	0.2	12.3	0.1	12.6	3.0	1.7	3.5	833791	74919	225540	1134250	24.6	19.1	39.2	182	0.14	0.16
5/4/2000 15:18	3.4	1.5	3.9	RUN 1	-0.1	25.1	0.2	12.3	0.1	12.6	3.5	1.4	3.8	833791	74919	225540	1134250	26.1	15.7	42.8	182	0.15	0.16
5/4/2000 15:19	3.8	1.4	2.9	RUN 1	-0.1	25.1	0.2	12.3	0.1	12.6	3.8	1.3	2.8	833791	74919	225540	1134250	31.2	15.0	31.6	182	0.17	0.13
5/4/2000 15:20	3.4	1.7	2.4	RUN 1	-0.1	25.1	0.2	12.3	0.1	12.6	3.5	1.6	2.3	833791	74919	225540	1134250	28.1	17.7	26.2	182	0.15	0.12
5/4/2000 15:21	2.4	1.8	2.5	RUN 1	-0.1	25.1	0.2	12.3	0.1	12.6	2.5	1.7	2.4	833791	74919	225540	1134250	20.0	18.7	27.7	182	0.11	0.13
5/4/2000 15:22	1.9	1.8	2.6	RUN 1	-0.1	25.1	0.2	12.3	0.1	12.6	1.9	1.5	2.5	833791	74919	225540	1134250	15.5	17.4	28.8	182	0.08	0.13
5/4/2000 15:23	1.7	1.5	1.8	RUN 1	-0.1	25.1	0.2	12.3	0.1	12.6	1.7	1.4	1.7	833791	74919	225540	1134250	13.9	15.5	19.8	182	0.06	0.10
5/4/2000 15:24	1.7	1.4	1.5	RUN 1	-0.1	25.1	0.2	12.3	0.1	12.6	1.7	1.3	1.4	833791	74919	225540	1134250	13.9	14.6	15.8	182	0.08	0.08
5/4/2000 15:25	1.7	1.3	1.4	RUN 1	-0.1	25.1	0.2	12.3	0.1	12.6	1.7	1.1	1.3	833791	74919	225540	1134250	13.9	12.9	14.7	182	0.08	0.08
5/4/2000 15:26	1.6	1.2	1.4	RUN 1	-0.1	25.1	0.2	12.3	0.1	12.6	1.7	1.1	1.3	833791	74919	225540	1134250	13.4	12.6	15.1	182	0.07	0.08
5/4/2000 15:27	1.6	1.4	1.4	RUN 1	-0.1	25.1	0.2	12.3	0.1	12.6	1.6	1.3	1.3	833791	74919	225540	1134250	12.9	14.6	14.3	182	0.07	0.08
5/4/2000 15:28	2.0	1.7	1.1	RUN 1	-0.1	25.1	0.2	12.3	0.1	12.6	2.0	1.6	1.0	833791	74919	225540	1134250	16.5	18.1	11.8	182	0.09	0.06
5/4/2000 15:29	6.5	2.0	1.1	RUN 1	-0.1	25.1	0.2	12.3	0.1	12.6	6.5	1.9	1.0	833791	74919	225540	1134250	52.5	21.5	11.1	182	0.29	0.06

TIME	OBSERVED CONCENTRATION PPM			COMMENTS	CALIBRATION CORRECTIONS						CORRECTED PPM VALUES			FLOW MEASURMENTS SCFM				MASS EMISSIONS			EMISSION FACTOR		
					NOX 7		SO2 IN		SO2 OUT														
	NOX COMP 7	SO2 IN	SO2 OUT		0.0	24.9	0.0	12.5	0.0	12.5	NOX - 7	SO2 IN	SO2 OUT	COLD-1	COLD-2	HOT	TOTAL	NOX LBS/HR	SO2 IN LBS/HR	SO2 OUT LBS/HR	PRODUCTION TON/HR	NOX LBS/TON	SO2 LBS/TON
5/4/2000 15:30	9.3	2.2	1.6	RUN 1	-0.1	25.1	0.2	12.3	0.1	12.6	9.3	2.1	1.5	833791	74919	225540	1134250	75.3	23.5	17.2	182	0.41	0.11
5/4/2000 15:31	10.4	2.2	3.8	RUN 1	-0.1	25.1	0.2	12.3	0.1	12.6	10.4	2.1	3.8	833791	74919	225540	1134250	84.4	23.9	42.5	182	0.46	0.18
5/4/2000 15:32	7.9	2.0	4.5	RUN 1	-0.1	25.1	0.2	12.3	0.1	12.6	7.9	1.9	4.4	833791	74919	225540	1134250	64.1	21.5	49.7	182	0.35	0.20
5/4/2000 15:33	4.4	1.8	2.8	RUN 1	-0.1	25.1	0.2	12.3	0.1	12.6	4.4	1.5	2.8	833791	74919	225540	1134250	35.7	17.0	31.3	182	0.20	0.13
5/4/2000 15:34	2.9	1.4	1.6	RUN 1	-0.1	25.1	0.2	12.3	0.1	12.6	2.9	1.3	1.6	833791	74919	225540	1134250	23.6	15.0	17.8	182	0.13	0.09
5/4/2000 15:35	5.5	1.3	1.3	RUN 1	-0.1	25.1	0.2	12.3	0.1	12.6	5.5	1.2	1.2	833791	74919	225540	1134250	44.9	13.6	13.3	182	0.25	0.07
5/4/2000 15:36	8.5	1.2	1.7	RUN 1	-0.1	25.1	0.2	12.3	0.1	12.6	8.5	1.1	1.6	833791	74919	225540	1134250	69.2	12.2	18.3	182	0.38	0.08
5/4/2000 15:37	8.8	1.2	2.3	RUN 1	-0.1	25.1	0.2	12.3	0.1	12.6	8.8	1.1	2.2	833791	74919	225540	1134250	71.7	12.6	24.4	182	0.39	0.10
5/4/2000 15:38	7.6	1.0	2.2	CALS	-0.1	25.1	0.2	12.3	0.1	12.6	RUN 1 AVERAGE							RUN 1 AVERAGE					
5/4/2000 15:39	6.9	0.8	2.1	CALS	-0.1	25.2	0.1	12.3	0.1	12.6	6.4	0.9	1.3					52.0	10.5	14.5		0.29	0.07
5/4/2000 15:40	6.9	0.7	1.8	CALS	-0.1	25.2	0.1	12.3	0.1	12.6													
5/4/2000 15:41	7.7	0.7	1.5	CALS	-0.1	25.2	0.1	12.3	0.1	12.6	7.7	0.6	1.4	833791	74919	225540	1134250						
5/4/2000 15:42	8.3	1.0	4.1	CALS	-0.1	25.2	0.1	12.3	0.1	12.6	8.3	0.9	4.0	833791	74919	225540	1134250						
5/4/2000 15:43	8.5	1.1	1.1	CALS	-0.1	25.2	0.1	12.3	0.1	12.6	8.5	1.0	1.0	833791	74919	225540	1134250						
5/4/2000 15:44	8.0	0.8	0.3	CALS	-0.1	25.2	0.1	12.3	0.1	12.6	8.9	0.8	0.2	833791	74919	225540	1134250						
5/4/2000 15:45	9.0	0.7	0.1	CALS	-0.1	25.2	0.1	12.3	0.1	12.6	9.0	0.8	0.0	833791	74919	225540	1134250						
5/4/2000 15:46	7.3	0.7	0.1	CALS	-0.1	25.2	0.1	12.3	0.1	12.6	7.3	0.6	0.0	833791	74919	225540	1134250						
5/4/2000 15:47	5.1	0.8	1.0	CALS	-0.1	25.2	0.1	12.3	0.1	12.6	5.2	0.7	0.9	833791	74919	225540	1134250						
5/4/2000 15:48	3.6	1.1	7.9	CALS	-0.1	25.2	0.1	12.3	0.1	12.6	3.6	1.0	7.6	833791	74919	225540	1134250						
5/4/2000 15:49	2.8	0.9	11.6	CALS	-0.1	25.2	0.1	12.3	0.1	12.6	2.7	0.8	11.5	833791	74919	225540	1134250						
5/4/2000 15:50	2.1	0.7	12.4	CALS	-0.1	25.2	0.1	12.3	0.1	12.6	2.2	0.6	12.3	833791	74919	225540	1134250						
5/4/2000 15:51	2.1	0.6	12.6	CALS	-0.1	25.2	0.1	12.3	0.1	12.6	2.2	0.6	12.5	833791	74919	225540	1134250						
5/4/2000 15:52	2.1	0.6	12.7	CALS	-0.1	25.2	0.1	12.3	0.1	12.6	2.2	0.6	12.6	833791	74919	225540	1134250						
5/4/2000 15:53	1.9	0.6	12.7	CALS	-0.1	25.2	0.1	12.3	0.1	12.6	2.0	0.6	12.6	833791	74919	225540	1134250						
5/4/2000 15:54	1.6	0.6	8.8	CALS	-0.1	25.2	0.1	12.3	0.1	12.6	1.6	0.6	8.7	833791	74919	225540	1134250						
5/4/2000 15:55	1.2	0.6	2.0	CALS	-0.1	25.2	0.1	12.3	0.1	12.6	1.3	0.6	1.9	833791	74919	225540	1134250						
5/4/2000 15:56	1.1	0.6	0.6	CALS	-0.1	25.2	0.1	12.3	0.1	12.6	1.2	0.5	0.5	833791	74919	225540	1134250						
5/4/2000 15:57	1.2	0.6	0.4	CALS	-0.1	25.2	0.1	12.3	0.1	12.6	1.3	0.5	0.3	833791	74919	225540	1134250						
5/4/2000 15:58	1.4	0.6	0.3	CALS	-0.1	25.2	0.1	12.3	0.1	12.6	1.5	0.5	0.2	833791	74919	225540	1134250						
5/4/2000 15:59	1.5	0.6	0.3	CALS	-0.1	25.2	0.1	12.3	0.1	12.6	1.6	0.6	0.2	833791	74919	225540	1134250						
5/4/2000 16:00	1.3	0.7	1.1	CALS	-0.1	25.2	0.1	12.3	0.1	12.6	1.4	0.6	1.0	833791	74919	225540	1134250						
5/4/2000 16:01	1.1	0.3	1.9	CALS	-0.1	25.2	0.1	12.3	0.1	12.6	1.1	0.2	1.8	833791	74919	225540	1134250						
5/4/2000 16:02	0.9	0.1	1.5	CALS	-0.1	25.2	0.1	12.3	0.1	12.6	1.0	0.0	1.4	833791	74919	225540	1134250						
5/4/2000 16:03	0.8	0.1	1.8	CALS	-0.1	25.2	0.1	12.3	0.1	12.6	1.0	0.0	1.5	833791	74919	225540	1134250						
5/4/2000 16:04	1.1	4.5	2.1	CALS	-0.1	25.2	0.1	12.3	0.1	12.6	1.1	4.6	2.0	833791	74919	225540	1134250						
5/4/2000 16:05	1.2	10.5	2.7	CALS	-0.1	25.2	0.1	12.3	0.1	12.6	1.3	10.7	2.8	833791	74919	225540	1134250						
5/4/2000 16:06	1.4	11.8	2.6	CALS	-0.1	25.2	0.1	12.3	0.1	12.6	1.4	12.1	2.7	833791	74919	225540	1134250						
5/4/2000 16:07	1.4	12.1	2.8	CALS	-0.1	25.2	0.1	12.3	0.1	12.6	1.4	12.4	2.7	833791	74919	225540	1134250						
5/4/2000 16:08	1.3	12.3	2.8	CALS	-0.1	25.2	0.1	12.3	0.1	12.6	1.4	12.5	2.7	833791	74919	225540	1134250						
5/4/2000 16:09	1.4	11.7	2.3	CALS	-0.1	25.2	0.1	12.3	0.1	12.6	1.4	11.9	2.2	833791	74919	225540	1134250						
5/4/2000 16:10	1.1	4.8	2.3	CALS	-0.1	25.2	0.1	12.3	0.1	12.6	1.2	4.9	2.2	833791	74919	225540	1134250						
5/4/2000 16:11	12.6	1.7	2.2	CALS	-0.1	25.2	0.1	12.3	0.1	12.6	12.5	1.7	2.1	833791	74919	225540	1134250						
5/4/2000 16:12	25.1	1.1	1.9	CALS	-0.1	25.2	0.1	12.3	0.1	12.6	24.6	1.0	1.8	833791	74919	225540	1134250						
5/4/2000 16:13	25.4	0.9	1.7	CALS	-0.1	25.2	0.1	12.3	0.1	12.6	25.1	0.9	1.6	833791	74919	225540	1134250						
5/4/2000 16:14	25.4	1.0	1.6	CALS	-0.1	25.2	0.1	12.3	0.1	12.6	25.2	0.9	1.5	833791	74919	225540	1134250						
5/4/2000 16:15	24.9	1.0	1.5	CALS	-0.1	25.2	0.1	12.3	0.1	12.6	24.8	0.9	1.4	833791	74919	225540	1134250						
5/4/2000 16:16	3.8	1.1	1.5	CALS	-0.1	25.2	0.1	12.3	0.1	12.6	3.7	1.0	1.4	833791	74919	225540	1134250						
5/4/2000 16:17	-0.1	1.2	1.4	CALS	-0.1	25.2	0.1	12.3	0.1	12.6	0.0	1.2	1.3	833791	74919	225540	1134250						
5/4/2000 16:18	-0.1	1.2	1.3	CALS	-0.1	25.2	0.1	12.3	0.1	12.6	0.0	1.1	1.2	833791	74919	225540	1134250						
5/4/2000 16:19	4.5	1.1	1.2	CALS	-0.1	25.2	0.1	12.3	0.1	12.6	4.5	1.0	1.1	833791	74919	225540	1134250						
5/4/2000 16:20	3.4	1.0	1.1	CALS	-0.1	25.2	0.1	12.3	0.1	12.6	3.4	1.0	1.0	833791	74919	225540	1134250						
5/4/2000 16:21	2.4	1.0	1.1	CALS	-0.1	25.2	0.1	12.3	0.1	12.6	2.5	1.0	1.0	833791	74919	225540	1134250						
5/4/2000 16:22	2.3	1.0	1.0	CALS	-0.1	25.2	0.1	12.3	0.1	12.6	2.4	1.0	0.9	833791	74919	225540	1134250						
5/4/2000 16:23	2.1	1.0	0.8	CALS	-0.1	25.2	0.1	12.3	0.1	12.6	2.2	0.9	0.7	833791	74919	225540	1134250						
5/4/2000 16:24	2.1	0.9	0.7	CALS	-0.1	25.2	0.1	12.3	0.1	12.6	2.2	0.9	0.6	833791	74919	225540	1134250						

TIME	OBSERVED CONCENTRATION PPM			COMMENTS	CALIBRATION CORRECTIONS						CORRECTED PPM VALUES			FLOW MEASURMENTS SCFM				MASS EMISSIONS			EMISSION FACTOR		
					NOX 7		SO2 IN		SO2 OUT														
	NOX COMP 7	SO2 IN	SO2 OUT		0.0	24.9	0.0	12.5	0.0	12.5	NOX - 7	SO2 IN	SO2 OUT	COLD-1	COLD-2	HOT	TOTAL	NOX LBS/HR	SO2 IN LBS/HR	SO2 OUT LBS/HR	PRODUCTION TONS/HR	NOX LBS/TON	SO2 LBS/TON
5/4/2000 16:25	2.2	0.8	0.7	CALS	-0.1	25.2	0.1	12.3	0.1	12.6	2.3	0.8	0.6	833791	74919	225540	1134250						
5/4/2000 16:26	2.3	0.8	0.8	CALS	-0.1	25.2	0.1	12.3	0.1	12.6	2.4	0.7	0.7	833791	74919	225540	1134250						
5/4/2000 16:27	2.7	0.7	0.8	CALS	-0.1	25.2	0.1	12.3	0.1	12.6	2.7	0.6	0.7	833791	74919	225540	1134250						
5/4/2000 16:28	4.3	0.7	0.8	CALS	-0.1	25.2	0.1	12.3	0.1	12.6	4.4	0.8	0.7	833791	74919	225540	1134250						
5/4/2000 16:29	6.5	0.8	0.7	CALS	-0.1	25.2	0.1	12.3	0.1	12.6	6.5	0.7	0.6	833791	74919	225540	1134250						
5/4/2000 16:30	7.6	0.8	0.7	CALS	-0.1	25.2	0.1	12.3	0.1	12.6	7.6	0.8	0.6	833791	74919	225540	1134250						
5/4/2000 16:31	7.8	0.8	0.7	CALS	-0.1	25.2	0.1	12.3	0.1	12.6	7.8	0.7	0.6	833791	74919	225540	1134250						
5/4/2000 16:32	6.6	0.8	1.1	RUN 2	-0.1	25.2	0.1	12.3	0.1	12.6	6.6	0.7	1.0	833791	74919	225540	1134250	53.6	6.0	11.1	198	0.27	0.05
5/4/2000 16:33	4.4	0.8	1.1	RUN 2	-0.1	25.2	0.1	12.3	0.1	12.6	4.5	0.7	1.0	833791	74919	225540	1134250	36.4	7.6	11.4	198	0.18	0.05
5/4/2000 16:34	2.9	0.7	1.5	RUN 2	-0.1	25.2	0.1	12.3	0.1	12.6	2.9	0.6	1.4	833791	74919	225540	1134250	23.8	7.3	15.7	198	0.12	0.06
5/4/2000 16:35	2.9	0.8	1.6	RUN 2	-0.1	25.2	0.1	12.3	0.1	12.6	2.9	0.6	1.5	833791	74919	225540	1134250	23.8	6.3	16.4	198	0.12	0.06
5/4/2000 16:36	3.3	0.8	1.7	RUN 2	-0.1	25.2	0.1	12.3	0.1	12.6	3.3	0.7	1.6	833791	74919	225540	1134250	26.9	7.6	18.2	198	0.14	0.07
5/4/2000 16:37	3.6	0.9	1.9	RUN 2	-0.1	25.2	0.1	12.3	0.1	12.6	3.7	0.8	1.8	833791	74919	225540	1134250	29.9	9.0	20.8	198	0.15	0.08
5/4/2000 16:38	4.1	1.0	1.7	RUN 2	-0.1	25.2	0.1	12.3	0.1	12.6	4.1	0.9	1.6	833791	74919	225540	1134250	33.4	10.0	18.6	198	0.17	0.07
5/4/2000 16:39	4.4	1.0	2.3	RUN 2	-0.1	25.2	0.1	12.3	0.1	12.6	4.4	0.9	2.2	833791	74919	225540	1134250	35.9	10.4	24.7	198	0.18	0.09
5/4/2000 16:40	3.4	0.9	3.0	RUN 2	-0.1	25.2	0.1	12.3	0.1	12.6	3.5	0.9	2.9	833791	74919	225540	1134250	28.4	9.7	33.3	198	0.14	0.11
5/4/2000 16:41	2.4	1.1	3.4	RUN 2	-0.1	25.2	0.1	12.3	0.1	12.6	2.4	1.0	3.3	833791	74919	225540	1134250	19.8	11.7	36.9	198	0.10	0.12
5/4/2000 16:42	1.9	1.8	3.7	RUN 2	-0.1	25.2	0.1	12.3	0.1	12.6	1.9	1.7	3.6	833791	74919	225540	1134250	15.6	19.2	41.2	198	0.08	0.15
5/4/2000 16:43	1.5	2.3	3.4	RUN 2	-0.1	25.2	0.1	12.3	0.1	12.6	1.6	2.2	3.3	833791	74919	225540	1134250	12.8	25.4	36.9	198	0.06	0.16
5/4/2000 16:44	1.2	1.7	3.1	RUN 2	-0.1	25.2	0.1	12.3	0.1	12.6	1.3	1.7	3.0	833791	74919	225540	1134250	10.7	18.9	34.4	198	0.05	0.13
5/4/2000 16:45	1.3	1.3	2.9	RUN 2	-0.1	25.2	0.1	12.3	0.1	12.6	1.4	1.2	2.8	833791	74919	225540	1134250	11.2	13.8	31.5	198	0.06	0.11
5/4/2000 16:46	1.3	1.1	2.5	RUN 2	-0.1	25.2	0.1	12.3	0.1	12.6	1.4	1.0	2.4	833791	74919	225540	1134250	11.2	11.4	26.9	198	0.06	0.10
5/4/2000 16:47	1.1	1.0	2.5	RUN 2	-0.1	25.2	0.1	12.3	0.1	12.6	1.2	0.9	2.4	833791	74919	225540	1134250	9.7	10.7	27.2	198	0.05	0.10
5/4/2000 16:48	1.0	1.0	2.6	RUN 2	-0.1	25.2	0.1	12.3	0.1	12.6	1.1	0.9	2.5	833791	74919	225540	1134250	8.7	10.0	28.3	198	0.04	0.10
5/4/2000 16:49	0.9	0.9	4.0	RUN 2	-0.1	25.2	0.1	12.3	0.1	12.6	1.0	0.9	3.9	833791	74919	225540	1134250	8.2	9.7	44.1	198	0.04	0.14
5/4/2000 16:50	0.9	1.0	4.0	RUN 2	-0.1	25.2	0.1	12.3	0.1	12.6	1.0	0.9	3.9	833791	74919	225540	1134250	8.2	10.0	44.1	198	0.04	0.14
5/4/2000 16:51	1.1	1.0	3.3	RUN 2	-0.1	25.2	0.1	12.3	0.1	12.6	1.1	0.8	3.2	833791	74919	225540	1134250	9.2	10.4	36.5	198	0.05	0.12
5/4/2000 16:52	1.2	0.8	2.3	RUN 2	-0.1	25.2	0.1	12.3	0.1	12.6	1.3	0.8	2.2	833791	74919	225540	1134250	10.7	9.3	24.3	198	0.05	0.09
5/4/2000 16:53	1.4	0.8	1.8	RUN 2	-0.1	25.2	0.1	12.3	0.1	12.6	1.5	0.8	1.5	833791	74919	225540	1134250	12.3	8.7	16.8	198	0.06	0.06
5/4/2000 16:54	1.8	0.8	2.1	RUN 2	-0.1	25.2	0.1	12.3	0.1	12.6	1.7	0.7	2.0	833791	74919	225540	1134250	13.8	8.0	22.2	198	0.07	0.08
5/4/2000 16:55	1.9	0.8	2.4	RUN 2	-0.1	25.2	0.1	12.3	0.1	12.6	1.9	0.7	2.3	833791	74919	225540	1134250	15.8	7.6	25.8	198	0.08	0.08
5/4/2000 16:56	1.9	0.9	2.1	RUN 2	-0.1	25.2	0.1	12.3	0.1	12.6	1.9	0.8	2.0	833791	74919	225540	1134250	15.8	9.0	22.5	198	0.08	0.08
5/4/2000 16:57	1.7	0.9	2.0	RUN 2	-0.1	25.2	0.1	12.3	0.1	12.6	1.8	0.9	1.9	833791	74919	225540	1134250	14.8	9.7	21.1	198	0.07	0.08
5/4/2000 16:58	1.6	0.9	1.7	RUN 2	-0.1	25.2	0.1	12.3	0.1	12.6	1.6	0.9	1.6	833791	74919	225540	1134250	13.3	9.7	18.2	198	0.07	0.07
5/4/2000 16:59	1.5	0.9	1.5	RUN 2	-0.1	25.2	0.1	12.3	0.1	12.6	1.6	0.8	1.4	833791	74919	225540	1134250	12.8	9.0	16.1	198	0.06	0.06
5/4/2000 17:00	1.6	0.8	1.6	RUN 2	-0.1	25.2	0.1	12.3	0.1	12.6	1.6	0.7	1.5	833791	74919	225540	1134250	13.3	8.3	16.8	198	0.07	0.06
5/4/2000 17:01	1.6	0.8	1.7	RUN 2	-0.1	25.2	0.1	12.3	0.1	12.6	1.7	0.8	1.6	833791	74919	225540	1134250	13.6	8.7	18.2	198	0.07	0.07
5/4/2000 17:02	1.6	0.8	1.6	RUN 2	-0.1	25.2	0.1	12.3	0.1	12.6	1.7	0.7	1.5	833791	74919	225540	1134250	13.8	7.6	16.4	198	0.07	0.06
5/4/2000 17:03	1.8	0.8	1.4	RUN 2	-0.1	25.2	0.1	12.3	0.1	12.6	1.7	0.7	1.3	833791	74919	225540	1134250	13.8	7.6	15.0	198	0.07	0.06
5/4/2000 17:04	1.6	0.7	1.5	RUN 2	-0.1	25.2	0.1	12.3	0.1	12.6	1.7	0.6	1.4	833791	74919	225540	1134250	13.8	7.3	15.4	198	0.07	0.06
5/4/2000 17:05	1.6	0.7	1.4	RUN 2	-0.1	25.2	0.1	12.3	0.1	12.6	1.7	0.6	1.3	833791	74919	225540	1134250	13.8	6.9	14.7	198	0.07	0.05
5/4/2000 17:06	1.7	0.7	1.3	RUN 2	-0.1	25.2	0.1	12.3	0.1	12.6	1.8	0.6	1.2	833791	74919	225540	1134250	14.3	6.9	13.9	198	0.07	0.05
5/4/2000 17:07	1.6	0.7	1.3	RUN 2	-0.1	25.2	0.1	12.3	0.1	12.6	1.7	0.6	1.2	833791	74919	225540	1134250	13.8	6.9	13.2	198	0.07	0.05
5/4/2000 17:08	1.7	0.7	1.2	RUN 2	-0.1	25.2	0.1	12.3	0.1	12.6	1.8	0.6	1.1	833791	74919	225540	1134250	14.3	6.6	12.1	198	0.07	0.05
5/4/2000 17:09	1.7	0.7	1.1	RUN 2	-0.1	25.2	0.1	12.3	0.1	12.6	1.8	0.6	1.0	833791	74919	225540	1134250	14.8	6.6	11.8	198	0.07	0.05
5/4/2000 17:10	3.4	0.7	1.1	RUN 2	-0.1	25.2	0.1	12.3	0.1	12.6	3.5	0.6	1.0	833791	74919	225540	1134250	28.4	6.6	11.4	198	0.14	0.05
5/4/2000 17:11	6.5	0.7	1.1	RUN 2	-0.1	25.2	0.1	12.3	0.1	12.6	6.5	0.6	1.0	833791	74919	225540	1134250	52.6	7.3	11.1	198	0.27	0.05
5/4/2000 17:12	7.5	0.8	1.1	RUN 2	-0.1	25.2	0.1	12.3	0.1	12.6	7.5	0.7	1.0	833791	74919	225540	1134250	60.6	8.0	11.4	198	0.31	0.05
5/4/2000 17:13	8.3	0.8	1.4	RUN 2	-0.1	25.2	0.1	12.3	0.1	12.6	8.3	0.7	1.3	833791	74919	225540	1134250	67.2	8.3	14.7	198	0.34	0.06
5/4/2000 17:14	8.1	0.7	1.5	RUN 2	-0.1	25.2	0.1	12.3	0.1	12.6	8.1	0.6	1.4	833791	74919	225540	1134250	49.5	7.3	16.1	198	0.25	0.06
5/4/2000 17:15	4.1	0.7	1.5	RUN 2	-0.1	25.2	0.1	12.3	0.1	12.6	4.2	0.6	1.4	833791	74919	225540	1134250	33.9	6.6	15.7	198	0.17	0.06
5/4/2000 17:16	3.5	0.6	1.4	RUN 2	-0.1	25.2	0.1	12.3	0.1	12.6	3.6	0.5	1.3	833791	74919	225540	1134250	28.9	5.9	14.7	198	0.15	0.05
5/4/2000 17:17	3.3	0.6	1.4	RUN 2	-0.1	25.2	0.1	12.3	0.1	12.6	3.4	0.5	1.3	833791	74919	225540	1134250	27.4	5.9	15.0	198	0.14	0.05
5/4/2000 17:18	3.1	0.6	1.2	RUN 2	-0.1	25.2	0.1	12.3	0.1	12.6	3.2	0.6	1.1	833791	74919	225540	1134250	25.9	6.3	12.1	198	0.13	0.06
5/4/2000 17:19	3.4	0.6	1.0	RUN 2	-0.1	25.2	0.1	12.3	0.1	12.6	3.4	0.6	0.9	833791	74919	225540	1134250	27.9	6.3	10.3	198	0.14	0.04

TIME	OBSERVED CONCENTRATION PPM			COMMENTS	CALIBRATION CORRECTIONS						CORRECTED PPM VALUES			FLOW MEASURMENTS SCFM				MASS EMISSIONS			EMISSION FACTOR		
					NOX 7		SO2 IN		SO2 OUT														
	NOX COMP 7	SO2 IN	SO2 OUT		0.0	24.9	0.0	12.5	0.0	12.5	NOX - 7	SO2 IN	SO2 OUT	COLD-1	COLD-2	HOT	TOTAL	NOX LBS/HR	SO2 IN LBS/HR	SO2 OUT LBS/HR	PRODUCTION TONS/HR	NOX LBS/TON	SO2 LBS/TON
5/4/2000 17:20	3.8	0.7	1.0	RUN 2	-0.1	25.2	0.1	12.3	0.1	12.6	3.9	0.6	0.9	833791	74919	225540	1134250	31.4	6.6	10.0	198	0.16	0.04
5/4/2000 17:21	6.1	0.7	1.0	RUN 2	-0.1	25.2	0.1	12.3	0.1	12.6	6.2	0.6	0.9	833791	74919	225540	1134250	50.0	7.3	9.6	198	0.25	0.04
5/4/2000 17:22	8.1	0.7	0.9	RUN 2	-0.1	25.2	0.1	12.3	0.1	12.6	8.1	0.6	0.8	833791	74919	225540	1134250	65.7	7.3	9.3	198	0.33	0.04
5/4/2000 17:23	9.3	0.7	1.0	RUN 2	-0.1	25.2	0.1	12.3	0.1	12.6	9.3	0.6	0.9	833791	74919	225540	1134250	75.7	6.9	10.0	198	0.38	0.04
5/4/2000 17:24	10.9	0.6	1.0	RUN 2	-0.1	25.2	0.1	12.3	0.1	12.6	10.9	0.5	0.9	833791	74919	225540	1134250	88.3	5.9	9.6	198	0.45	0.04
5/4/2000 17:25	13.6	0.5	1.2	RUN 2	-0.1	25.2	0.1	12.3	0.1	12.6	13.5	0.4	1.1	833791	74919	225540	1134250	109.5	4.9	12.1	198	0.55	0.04
5/4/2000 17:26	11.5	0.5	1.4	RUN 2	-0.1	25.2	0.1	12.3	0.1	12.6	11.4	0.4	1.3	833791	74919	225540	1134250	92.9	4.6	14.3	198	0.47	0.05
5/4/2000 17:27	9.0	0.4	1.6	RUN 2	-0.1	25.2	0.1	12.3	0.1	12.6	9.0	0.3	1.5	833791	74919	225540	1134250	73.2	3.9	16.4	198	0.37	0.05
5/4/2000 17:28	8.0	0.5	2.1	RUN 2	-0.1	25.2	0.1	12.3	0.1	12.6	8.0	0.4	2.0	833791	74919	225540	1134250	65.1	4.2	22.2	198	0.33	0.07
5/4/2000 17:29	7.6	0.5	2.4	RUN 2	-0.1	25.2	0.1	12.3	0.1	12.6	7.6	0.4	2.3	833791	74919	225540	1134250	62.1	4.9	26.5	198	0.31	0.08
5/4/2000 17:30	6.3	0.5	2.3	RUN 2	-0.1	25.2	0.1	12.3	0.1	12.6	6.3	0.4	2.2	833791	74919	225540	1134250	51.5	4.9	24.7	198	0.26	0.07
5/4/2000 17:31	3.9	0.5	2.0	RUN 2	-0.1	25.2	0.1	12.3	0.1	12.6	3.9	0.4	1.9	833791	74919	225540	1134250	31.9	4.2	21.5	198	0.16	0.06
5/4/2000 17:32	2.8	0.4	2.3	RUN 2	-0.1	25.2	0.1	12.3	0.1	12.6	2.9	0.3	2.2	833791	74919	225540	1134250	23.3	3.5	24.7	198	0.12	0.07
5/4/2000 17:33	3.1	0.4	2.5	RUN 2	-0.1	25.2	0.1	12.3	0.1	12.6	3.2	0.3	2.4	833791	74919	225540	1134250	25.9	3.9	26.9	198	0.13	0.08
5/4/2000 17:34	3.2	0.5	2.3	RUN 2	-0.1	25.2	0.1	12.3	0.1	12.6	3.2	0.4	2.2	833791	74919	225540	1134250	26.4	4.2	24.7	198	0.13	0.07
5/4/2000 17:35	1.9	0.5	2.4	RUN 2	-0.1	25.2	0.1	12.3	0.1	12.6	2.0	0.4	2.3	833791	74919	225540	1134250	16.3	4.2	25.8	198	0.08	0.08
5/4/2000 17:36	1.2	0.5	2.5	RUN 2	-0.1	25.2	0.1	12.3	0.1	12.6	1.3	0.4	2.4	833791	74919	225540	1134250	10.7	4.2	27.6	198	0.05	0.08
5/4/2000 17:37	0.9	0.5	2.5	RUN 2	-0.1	25.2	0.1	12.3	0.1	12.6	1.0	0.4	2.4	833791	74919	225540	1134250	8.2	4.2	26.9	198	0.04	0.08
5/4/2000 17:38	0.6	0.4	2.3	RUN 2	-0.1	25.2	0.1	12.3	0.1	12.6	0.9	0.3	2.2	833791	74919	225540	1134250	7.7	3.9	24.7	198	0.04	0.07
5/4/2000 17:39	0.6	0.4	2.1	RUN 2	-0.1	25.2	0.1	12.3	0.1	12.6	0.9	0.3	2.0	833791	74919	225540	1134250	7.7	3.9	22.9	198	0.04	0.07
5/4/2000 17:40	0.8	0.4	1.7	RUN 2	-0.1	25.2	0.1	12.3	0.1	12.6	0.9	0.3	1.8	833791	74919	225540	1134250	7.2	3.9	18.8	198	0.04	0.06
5/4/2000 17:41	0.7	0.4	1.2	RUN 2	-0.1	25.2	0.1	12.3	0.1	12.6	0.8	0.3	1.1	833791	74919	225540	1134250	6.7	3.9	12.5	198	0.03	0.04
5/4/2000 17:42	0.8	0.4	1.0	RUN 2	-0.1	25.2	0.1	12.3	0.1	12.6	0.9	0.3	0.9	833791	74919	225540	1134250	7.2	3.9	10.3	198	0.04	0.04
5/4/2000 17:43	1.1	0.5	1.0	RUN 2	-0.1	25.2	0.1	12.3	0.1	12.6	1.1	0.4	0.9	833791	74919	225540	1134250	9.2	4.2	10.0	198	0.05	0.04
5/4/2000 17:44	1.2	0.6	1.1	RUN 2	-0.1	25.2	0.1	12.3	0.1	12.6	1.3	0.5	1.0	833791	74919	225540	1134250	10.2	5.9	11.8	198	0.05	0.04
5/4/2000 17:45	1.1	0.7	1.5	RUN 2	-0.1	25.2	0.1	12.3	0.1	12.6	1.1	0.6	1.4	833791	74919	225540	1134250	9.2	7.3	15.7	198	0.05	0.06
5/4/2000 17:46	1.0	0.8	1.7	RUN 2	-0.1	25.2	0.1	12.3	0.1	12.6	1.1	0.7	1.6	833791	74919	225540	1134250	8.7	8.0	18.6	198	0.04	0.07
5/4/2000 17:47	0.9	0.7	1.4	RUN 2	-0.1	25.2	0.1	12.3	0.1	12.6	1.0	0.6	1.3	833791	74919	225540	1134250	8.2	7.3	14.7	198	0.04	0.06
5/4/2000 17:48	0.8	0.7	1.5	RUN 2	-0.1	25.2	0.1	12.3	0.1	12.6	0.9	0.6	1.4	833791	74919	225540	1134250	7.2	6.6	16.1	198	0.04	0.06
5/4/2000 17:49	0.6	0.7	4.1	RUN 2	-0.1	25.2	0.1	12.3	0.1	12.6	0.8	0.6	4.0	833791	74919	225540	1134250	7.2	7.3	44.8	198	0.04	0.13
5/4/2000 17:50	1.2	0.8	4.1	RUN 2	-0.1	25.2	0.1	12.3	0.1	12.6	1.3	0.7	4.0	833791	74919	225540	1134250	10.7	7.6	44.6	198	0.05	0.13
5/4/2000 17:51	1.4	0.7	2.7	RUN 2	-0.1	25.2	0.1	12.3	0.1	12.6	1.5	0.6	2.6	833791	74919	225540	1134250	12.3	6.6	29.7	198	0.06	0.09
5/4/2000 17:52	1.5	0.6	2.3	RUN 2	-0.1	25.2	0.1	12.3	0.1	12.6	1.6	0.5	2.2	833791	74919	225540	1134250	12.8	5.9	25.4	198	0.06	0.08
5/4/2000 17:53	2.1	0.6	1.6	RUN 2	-0.1	25.2	0.1	12.3	0.1	12.6	2.2	0.5	1.5	833791	74919	225540	1134250	17.8	5.2	17.5	198	0.09	0.06
5/4/2000 17:54	3.1	0.5	1.6	RUN 2	-0.1	25.2	0.1	12.3	0.1	12.6	3.1	0.4	1.5	833791	74919	225540	1134250	25.3	4.2	17.2	198	0.13	0.05
5/4/2000 17:55	4.0	0.5	2.6	RUN 2	-0.1	25.2	0.1	12.3	0.1	12.6	4.0	0.4	2.5	833791	74919	225540	1134250	32.9	4.2	28.6	198	0.17	0.08
5/4/2000 17:56	4.8	0.5	3.1	RUN 2	-0.1	25.2	0.1	12.3	0.1	12.6	4.8	0.4	3.0	833791	74919	225540	1134250	39.0	4.9	33.7	198	0.20	0.10
5/4/2000 17:57	6.1	0.6	3.4	RUN 2	-0.1	25.2	0.1	12.3	0.1	12.6	6.2	0.5	3.3	833791	74919	225540	1134250	50.0	5.2	36.9	198	0.25	0.11
5/4/2000 17:58	4.7	0.6	2.9	RUN 2	-0.1	25.2	0.1	12.3	0.1	12.6	4.7	0.5	2.8	833791	74919	225540	1134250	38.4	5.2	31.9	198	0.19	0.09
5/4/2000 17:59	2.8	0.5	2.9	RUN 2	-0.1	25.2	0.1	12.3	0.1	12.6	2.7	0.4	2.8	833791	74919	225540	1134250	21.8	4.6	31.2	198	0.11	0.09
5/4/2000 18:00	2.2	0.5	3.0	RUN 2	-0.1	25.2	0.1	12.3	0.1	12.6	2.3	0.4	2.9	833791	74919	225540	1134250	18.3	4.2	33.0	198	0.09	0.09
5/4/2000 18:01	2.4	0.5	2.6	RUN 2	-0.1	25.2	0.1	12.3	0.1	12.6	2.5	0.4	2.5	833791	74919	225540	1134250	20.3	4.6	28.3	198	0.10	0.08
5/4/2000 18:02	2.9	0.5	2.6	RUN 2	-0.1	25.2	0.1	12.3	0.1	12.6	2.8	0.4	2.5	833791	74919	225540	1134250	23.8	4.2	28.6	198	0.12	0.08
5/4/2000 18:03	3.0	0.5	3.1	RUN 2	-0.1	25.2	0.1	12.3	0.1	12.6	3.1	0.4	3.0	833791	74919	225540	1134250	24.8	4.6	34.0	198	0.13	0.10
5/4/2000 18:04	2.8	0.5	3.1	RUN 2	-0.1	25.2	0.1	12.3	0.1	12.6	2.9	0.4	3.0	833791	74919	225540	1134250	23.3	4.2	34.4	198	0.12	0.10
5/4/2000 18:05	2.4	0.5	2.5	RUN 2	-0.1	25.2	0.1	12.3	0.1	12.6	2.5	0.4	2.4	833791	74919	225540	1134250	20.3	4.2	27.2	198	0.10	0.08
5/4/2000 18:06	2.3	0.5	2.0	RUN 2	-0.1	25.2	0.1	12.3	0.1	12.6	2.4	0.4	1.9	833791	74919	225540	1134250	19.3	4.2	21.5	198	0.10	0.06
5/4/2000 18:07	2.3	0.5	1.6	RUN 2	-0.1	25.2	0.1	12.3	0.1	12.6	2.4	0.4	1.5	833791	74919	225540	1134250	19.3	4.6	16.8	198	0.10	0.05
5/4/2000 18:08	2.1	0.4	1.4	RUN 2	-0.1	25.2	0.1	12.3	0.1	12.6	2.2	0.3	1.3	833791	74919	225540	1134250	17.8	3.9	14.3	198	0.09	0.05
5/4/2000 18:09	1.8	0.4	1.0	RUN 2	-0.1	25.2	0.1	12.3	0.1	12.6	1.9	0.3	0.9	833791	74919	225540	1134250	15.3	3.5	10.7	198	0.08	0.04
5/4/2000 18:10	1.6	0.3	1.0	RUN 2	-0.1	25.2	0.1	12.3	0.1	12.6	1.7	0.2	0.9	833791	74919	225540	1134250	13.8	2.5	9.6	198	0.07	0.03
5/4/2000 18:11	1.6	0.3	0.9	RUN 2	-0.1	25.2	0.1	12.3	0.1	12.6	1.6	0.3	0.8	833791	74919	225540	1134250	13.3	2.9	8.6	198	0.07	0.03
5/4/2000 18:12	1.9	0.5	1.5	RUN 2	-0.1	25.2	0.1	12.3	0.1	12.6	2.0	0.4	1.4	833791	74919	225540	1134250	16.3	4.2	15.4	198	0.08	0.05
5/4/2000 18:13	3.3	0.6	1.3	RUN 2	-0.1	25.2	0.1	12.3	0.1	12.6	3.4	0.5	1.2	833791	74919	225540	1134250	27.4	5.2	13.9	198	0.14	0.05
5/4/2000 18:14	3.8	0.5	1.0	RUN 2	-0.1	25.2	0.1	12.3	0.1	12.6	3.8	0.4	0.9	833791	74919	225540	1134250	30.9	4.6	10.3	198	0.16	0.04

TIME	OBSERVED CONCENTRATION PPM			COMMENTS	CALIBRATION CORRECTIONS						CORRECTED PPM VALUES			FLOW MEASURMENTS SCFM				MASS EMISSIONS			EMISSION FACTOR		
					NOX 7		SO2 IN		SO3 OUT														
	NOX COMP 7	SO2 IN	SO2 OUT		0.0	24.9	0.0	12.5	0.0	12.5	NOX - 7	SO2 IN	SO2 OUT	COLD-1	COLD-2	HOT	TOTAL	NOX LBS/HR	SO2 IN LBS/HR	SO2 OUT LBS/HR	PRODUCTION TONS/HR	NOX LBS/TON	SO2 LBS/TON
5/4/2000 18:15	3.5	0.5	0.8	RUN 2	-0.1	25.2	0.1	12.3	0.1	12.6	3.6	0.4	0.7	833791	74919	225540	1134250	26.9	4.9	7.8	198	0.15	0.03
5/4/2000 18:16	5.4	0.6	1.4	RUN 2	-0.1	25.2	0.1	12.3	0.1	12.5	5.4	0.5	1.3	833791	74919	225540	1134250	44.0	5.9	14.7	198	0.22	0.05
5/4/2000 18:17	6.0	0.8	1.6	RUN 2	-0.1	25.2	0.1	12.3	0.1	12.6	6.0	0.6	1.5	833791	74919	225540	1134250	64.6	6.3	17.2	198	0.33	0.06
5/4/2000 18:18	6.3	0.6	1.5	RUN 2	-0.1	25.2	0.1	12.3	0.1	12.6	6.3	0.5	1.4	833791	74919	225540	1134250	67.7	5.2	15.4	198	0.34	0.05
5/4/2000 18:19	7.8	0.4	1.4	RUN 2	-0.1	25.2	0.1	12.3	0.1	12.6	7.8	0.3	1.3	833791	74919	225540	1134250	83.6	3.9	14.7	198	0.32	0.05
5/4/2000 18:20	8.0	0.4	1.2	RUN 2	-0.1	25.2	0.1	12.3	0.1	12.6	8.0	0.3	1.1	833791	74919	225540	1134250	86.5	3.5	12.5	198	0.25	0.04
5/4/2000 18:21	3.8	0.4	1.0	RUN 2	-0.1	25.2	0.1	12.3	0.1	12.6	3.7	0.3	0.9	833791	74919	225540	1134250	29.9	3.2	10.7	198	0.15	0.04
5/4/2000 18:22	2.6	0.4	1.0	RUN 2	-0.1	25.2	0.1	12.3	0.1	12.6	2.7	0.3	0.9	833791	74919	225540	1134250	21.8	3.9	9.6	198	0.11	0.03
5/4/2000 18:23	2.2	0.4	1.0	RUN 2	-0.1	25.2	0.1	12.3	0.1	12.6	2.3	0.3	0.9	833791	74919	225540	1134250	18.3	3.9	9.6	198	0.09	0.03
5/4/2000 18:24	2.0	0.3	0.9	RUN 2	-0.1	25.2	0.1	12.3	0.1	12.6	2.1	0.3	0.8	833791	74919	225540	1134250	16.8	2.9	9.3	198	0.08	0.03
5/4/2000 18:25	2.2	0.3	0.8	RUN 2	-0.1	25.2	0.1	12.3	0.1	12.6	2.3	0.2	0.8	833791	74919	225540	1134250	18.8	2.5	8.9	198	0.09	0.03
5/4/2000 18:26	3.0	0.3	0.8	RUN 2	-0.1	25.2	0.1	12.3	0.1	12.6	3.1	0.2	0.8	833791	74919	225540	1134250	24.8	1.8	8.9	198	0.13	0.03
5/4/2000 18:27	3.2	0.2	0.9	RUN 2	-0.1	25.2	0.1	12.3	0.1	12.6	3.2	0.1	0.8	833791	74919	225540	1134250	26.4	1.5	8.6	198	0.13	0.03
5/4/2000 18:28	3.2	0.2	0.9	RUN 2	-0.1	25.2	0.1	12.3	0.1	12.6	3.2	0.1	0.8	833791	74919	225540	1134250	26.4	1.5	8.9	198	0.13	0.03
5/4/2000 18:29	3.1	0.3	0.9	RUN 2	-0.1	25.2	0.1	12.3	0.1	12.6	3.2	0.2	0.8	833791	74919	225540	1134250	25.9	1.8	9.3	198	0.13	0.03
5/4/2000 18:30	2.7	0.3	1.0	RUN 2	-0.1	25.2	0.1	12.3	0.1	12.6	2.7	0.2	0.9	833791	74919	225540	1134250	22.3	2.2	10.0	198	0.11	0.03
5/4/2000 18:31	2.6	0.3	1.1	RUN 2	-0.1	25.2	0.1	12.3	0.1	12.6	2.7	0.2	1.0	833791	74919	225540	1134250	21.8	2.2	11.1	198	0.11	0.03
5/4/2000 18:32	2.7	0.3	1.8	RUN 2	-0.1	25.2	0.1	12.3	0.1	12.6	2.7	0.2	1.5	833791	74919	225540	1134250	22.3	2.2	17.2	198	0.11	0.05
5/4/2000 18:33	2.2	0.3	1.8	RUN 2	-0.1	25.2	0.1	12.3	0.1	12.6	2.3	0.2	1.5	833791	74919	225540	1134250	18.3	2.5	17.2	198	0.09	0.05
5/4/2000 18:34	1.9	0.4	1.2	RUN 2	-0.1	25.2	0.1	12.3	0.1	12.6	1.9	0.3	1.1	833791	74919	225540	1134250	15.8	3.5	12.9	198	0.08	0.04
5/4/2000 18:35	2.0	0.5	1.4	RUN 2	-0.1	25.2	0.1	12.3	0.1	12.6	2.1	0.4	1.3	833791	74919	225540	1134250	16.8	4.2	14.3	198	0.08	0.05
5/4/2000 18:36	2.0	0.5	1.7	RUN 2	-0.1	25.2	0.1	12.3	0.1	12.6	2.1	0.4	1.6	833791	74919	225540	1134250	16.8	4.9	18.6	198	0.08	0.06
5/4/2000 18:37	1.8	0.6	2.0	RUN 2	-0.1	25.2	0.1	12.3	0.1	12.6	1.7	0.5	2.0	833791	74919	225540	1134250	13.8	5.6	21.5	198	0.07	0.09
5/4/2000 18:38	1.4	0.8	3.4	RUN 2	-0.1	25.2	0.1	12.3	0.1	12.6	1.5	0.8	3.3	833791	74919	225540	1134250	12.3	6.3	37.3	198	0.06	0.11
5/4/2000 18:39	1.5	0.7	3.4	RUN 2	-0.1	25.2	0.1	12.3	0.1	12.6	1.6	0.8	3.3	833791	74919	225540	1134250	12.8	6.6	38.9	198	0.06	0.11
5/4/2000 18:40	1.7	0.7	4.6	RUN 2	-0.1	25.2	0.1	12.3	0.1	12.6	1.8	0.6	4.5	833791	74919	225540	1134250	14.8	7.3	50.9	198	0.07	0.15
5/4/2000 18:41	2.4	0.8	4.1	RUN 2	-0.1	25.2	0.1	12.3	0.1	12.6	2.4	0.7	4.0	833791	74919	225540	1134250	19.8	7.6	44.8	198	0.10	0.13
5/4/2000 18:42	2.6	0.7	2.7	RUN 2	-0.1	25.2	0.1	12.3	0.1	12.6	2.6	0.6	2.6	833791	74919	225540	1134250	21.3	7.3	29.7	198	0.11	0.09
5/4/2000 18:43	2.5	0.7	1.9	RUN 2	-0.1	25.2	0.1	12.3	0.1	12.6	2.6	0.6	1.8	833791	74919	225540	1134250	20.8	6.8	20.4	198	0.11	0.07
5/4/2000 18:44	2.5	0.6	2.3	RUN 2	-0.1	25.2	0.1	12.3	0.1	12.6	2.6	0.5	2.2	833791	74919	225540	1134250	20.8	5.9	24.3	198	0.11	0.08
5/4/2000 18:45	2.3	0.6	1.7	RUN 2	-0.1	25.2	0.1	12.3	0.1	12.6	2.4	0.5	1.8	833791	74919	225540	1134250	19.3	5.6	17.9	198	0.10	0.06
5/4/2000 18:46	2.1	0.6	2.0	RUN 2	-0.1	25.2	0.1	12.3	0.1	12.6	2.1	0.5	1.9	833791	74919	225540	1134250	17.3	5.2	21.8	198	0.09	0.07
5/4/2000 18:47	1.9	0.5	1.8	RUN 2	-0.1	25.2	0.1	12.3	0.1	12.6	1.9	0.4	1.7	833791	74919	225540	1134250	15.8	4.9	19.7	198	0.08	0.06
5/4/2000 18:48	1.5	0.5	1.8	RUN 2	-0.1	25.2	0.1	12.3	0.1	12.6	1.6	0.4	1.5	833791	74919	225540	1134250	12.8	4.8	17.5	198	0.06	0.06
5/4/2000 18:49	1.2	0.4	1.8	RUN 2	-0.1	25.2	0.1	12.3	0.1	12.6	1.3	0.3	1.5	833791	74919	225540	1134250	10.2	3.9	16.8	198	0.05	0.05
5/4/2000 18:50	1.1	0.4	2.3	RUN 2	-0.1	25.2	0.1	12.3	0.1	12.6	1.1	0.3	2.2	833791	74919	225540	1134250	9.2	3.9	24.3	198	0.05	0.07
5/4/2000 18:51	1.2	0.4	2.8	RUN 2	-0.1	25.2	0.1	12.3	0.1	12.6	1.3	0.3	2.7	833791	74919	225540	1134250	10.7	3.9	30.4	198	0.05	0.09
5/4/2000 18:52	1.7	0.5	3.2	RUN 2	-0.1	25.2	0.1	12.3	0.1	12.6	1.8	0.4	3.1	833791	74919	225540	1134250	14.3	4.2	35.1	198	0.07	0.10
5/4/2000 18:53	1.7	0.6	3.8	RUN 2	-0.1	25.2	0.1	12.3	0.1	12.6	1.8	0.4	3.7	833791	74919	225540	1134250	14.8	4.9	42.3	198	0.07	0.12
5/4/2000 18:54	1.7	0.5	3.9	RUN 2	-0.1	25.2	0.1	12.3	0.1	12.6	1.8	0.4	3.8	833791	74919	225540	1134250	14.3	4.9	42.6	198	0.07	0.12
5/4/2000 18:55	1.7	0.6	3.2	RUN 2	-0.1	25.2	0.1	12.3	0.1	12.6	1.8	0.5	3.1	833791	74919	225540	1134250	14.8	5.2	35.5	198	0.07	0.10
5/4/2000 18:56	3.2	0.6	3.3	RUN 2	-0.1	25.2	0.1	12.3	0.1	12.6	3.2	0.5	3.2	833791	74919	225540	1134250	26.4	5.9	35.8	198	0.13	0.11
5/4/2000 18:57	4.3	0.6	3.3	RUN 2	-0.1	25.2	0.1	12.3	0.1	12.6	4.4	0.5	3.2	833791	74919	225540	1134250	35.4	5.9	35.8	198	0.18	0.11
5/4/2000 18:58	4.1	0.6	3.3	RUN 2	-0.1	25.2	0.1	12.3	0.1	12.6	4.2	0.5	3.2	833791	74919	225540	1134250	33.9	5.9	36.5	198	0.17	0.11
5/4/2000 18:59	4.2	0.6	3.0	RUN 2	-0.1	25.2	0.1	12.3	0.1	12.6	4.2	0.5	2.9	833791	74919	225540	1134250	34.4	5.2	33.3	198	0.17	0.10
5/4/2000 19:00	4.1	0.5	2.2	RUN 2	-0.1	25.2	0.1	12.3	0.1	12.6	4.1	0.4	2.1	833791	74919	225540	1134250	33.4	4.6	23.6	198	0.17	0.07
5/4/2000 19:01	3.9	0.4	1.7	RUN 2	-0.1	25.2	0.1	12.3	0.1	12.6	4.0	0.3	1.6	833791	74919	225540	1134250	32.4	3.9	17.9	198	0.16	0.05
5/4/2000 19:02	4.8	0.4	1.4	RUN 2	-0.1	25.2	0.1	12.3	0.1	12.6	4.8	0.3	1.3	833791	74919	225540	1134250	39.0	3.9	14.7	198	0.20	0.05
5/4/2000 19:03	5.7	0.4	1.4	RUN 2	-0.1	25.2	0.1	12.3	0.1	12.6	5.7	0.3	1.3	833791	74919	225540	1134250	46.5	3.9	15.0	198	0.23	0.05
5/4/2000 19:04	6.1	0.4	1.4	RUN 2	-0.1	25.2	0.1	12.3	0.1	12.6	6.2	0.3	1.3	833791	74919	225540	1134250	50.0	3.5	14.3	198	0.25	0.05
5/4/2000 19:05	5.8	0.4	1.6	RUN 2	-0.1	25.2	0.1	12.3	0.1	12.6	5.6	0.3	0.9	833791	74919	225540	1134250	45.5	3.2	10.7	198	0.23	0.04
5/4/2000 19:06	4.4	0.3	1.0	RUN 2	-0.1	25.2	0.1	12.3	0.1	12.6	4.5	0.2	0.9	833791	74919	225540	1134250	38.4	2.5	10.7	198	0.18	0.03
5/4/2000 19:07	3.5	0.3	1.3	RUN 2	-0.1	25.2	0.1	12.3	0.1	12.6	3.6	0.2	1.2	833791	74919	225540	1134250	28.9	2.5	13.2	198	0.15	0.04
5/4/2000 19:08	3.9	0.3	1.5	RUN 2	-0.1	25.2	0.1	12.3	0.1	12.6	4.0	0.2	1.4	833791	74919	225540	1134250	32.4	2.5	15.7	198	0.16	0.05
5/4/2000 19:09	4.6	0.3	1.1	RUN 2	-0.1	25.2	0.1	12.3	0.1	12.6	4.6	0.3	1.0	833791	74919	225540	1134250	37.4	2.9	11.4	198	0.19	0.04

TIME	OBSERVED CONCENTRATION PPM			COMMENTS	CALIBRATION CORRECTIONS						CORRECTED PPM VALUES			FLOW MEASURMENTS SCFM				MASS EMISSIONS			EMISSION FACTOR		
					NOX 7		SO2 IN		SO2 OUT														
	NOX COMP 7	SO2 IN	SO2 OUT		0.0	24.9	0.0	12.5	0.0	12.5	NOX - 7	SO2 IN	SO2 OUT	COLD-1	COLD-2	HOT	TOTAL	NOX LBS/HR	SO2 IN LBS/HR	SO2 OUT LBS/HR	PRODUCTION TONS/HR	NOX LBS/TON	SO2 LBS/TON
5/4/2000 21:00	3.0	3.0	3.8	RUN 3	-0.1	25.3	0.1	12.3	0.1	12.9	3.0	3.0	3.4	833791	74919	225540	1134250	24.7	33.8	38.7	199	0.12	0.18
5/4/2000 21:01	3.4	3.2	4.2	RUN 3	-0.1	25.3	0.1	12.3	0.1	12.9	3.4	3.2	4.1	833791	74919	225540	1134250	27.7	36.2	46.0	199	0.14	0.21
5/4/2000 21:02	4.2	3.3	4.3	RUN 3	-0.1	25.3	0.1	12.3	0.1	12.9	4.2	3.3	4.1	833791	74919	225540	1134250	34.2	37.5	46.7	199	0.17	0.21
5/4/2000 21:03	6.1	2.8	3.2	RUN 3	-0.1	25.3	0.1	12.3	0.1	12.9	6.1	2.8	3.0	833791	74919	225540	1134250	49.7	31.8	34.5	199	0.25	0.17
5/4/2000 21:04	6.5	3.1	3.2	RUN 3	-0.1	25.3	0.1	12.3	0.1	12.9	6.5	3.1	3.1	833791	74919	225540	1134250	52.7	35.2	34.8	199	0.27	0.18
5/4/2000 21:05	6.3	3.1	3.1	RUN 3	-0.1	25.3	0.1	12.3	0.1	12.9	6.2	3.1	3.0	833791	74919	225540	1134250	50.7	34.8	33.8	199	0.25	0.17
5/4/2000 21:06	6.3	3.0	3.2	RUN 3	-0.1	25.3	0.1	12.3	0.1	12.9	6.2	3.0	3.1	833791	74919	225540	1134250	50.7	33.8	34.8	199	0.25	0.17
5/4/2000 21:07	6.5	3.0	3.7	RUN 3	-0.1	25.3	0.1	12.3	0.1	12.9	6.5	3.0	3.6	833791	74919	225540	1134250	52.7	33.8	40.8	199	0.27	0.19
5/4/2000 21:08	7.8	3.1	2.7	RUN 3	-0.1	25.3	0.1	12.3	0.1	12.9	7.7	3.1	2.6	833791	74919	225540	1134250	62.8	34.8	29.8	199	0.32	0.16
5/4/2000 21:09	8.7	2.7	2.4	RUN 3	-0.1	25.3	0.1	12.3	0.1	12.9	8.6	2.7	2.3	833791	74919	225540	1134250	70.3	30.4	26.4	199	0.35	0.14
5/4/2000 21:10	11.7	2.5	2.9	RUN 3	-0.1	25.3	0.1	12.3	0.1	12.9	11.6	2.5	2.8	833791	74919	225540	1134250	94.3	28.4	31.3	199	0.47	0.15
5/4/2000 21:11	11.3	2.6	3.0	RUN 3	-0.1	25.3	0.1	12.3	0.1	12.9	11.2	2.7	2.9	833791	74919	225540	1134250	90.6	31.1	32.4	199	0.46	0.16
5/4/2000 21:12	10.3	2.9	2.9	RUN 3	-0.1	25.3	0.1	12.3	0.1	12.9	10.2	2.9	2.8	833791	74919	225540	1134250	82.8	32.4	31.7	199	0.42	0.16
5/4/2000 21:13	10.2	2.9	2.8	RUN 3	-0.1	25.3	0.1	12.3	0.1	12.9	10.1	2.9	2.6	833791	74919	225540	1134250	82.3	32.6	29.9	199	0.41	0.16
5/4/2000 21:14	10.2	2.6	2.1	RUN 3	-0.1	25.3	0.1	12.3	0.1	12.9	10.1	2.7	2.0	833791	74919	225540	1134250	81.8	30.7	22.2	199	0.41	0.13
5/4/2000 21:15	8.5	2.5	2.2	RUN 3	-0.1	25.3	0.1	12.3	0.1	12.9	8.5	2.5	2.1	833791	74919	225540	1134250	68.6	28.0	23.6	199	0.35	0.13
5/4/2000 21:16	6.4	2.4	2.4	RUN 3	-0.1	25.3	0.1	12.3	0.1	12.9	6.4	2.4	2.3	833791	74919	225540	1134250	51.7	27.0	26.1	199	0.26	0.13
5/4/2000 21:17	4.7	2.4	2.4	RUN 3	-0.1	25.3	0.1	12.3	0.1	12.9	4.7	2.3	2.3	833791	74919	225540	1134250	38.2	26.3	26.4	199	0.19	0.13
5/4/2000 21:18	3.3	2.3	2.3	RUN 3	-0.1	25.3	0.1	12.3	0.1	12.9	3.3	2.2	2.2	833791	74919	225540	1134250	26.7	25.3	24.7	199	0.13	0.13
5/4/2000 21:19	2.4	2.2	2.5	RUN 3	-0.1	25.3	0.1	12.3	0.1	12.9	2.4	2.1	2.4	833791	74919	225540	1134250	19.7	23.9	27.1	199	0.10	0.13
5/4/2000 21:20	1.9	2.2	2.5	RUN 3	-0.1	25.3	0.1	12.3	0.1	12.9	1.9	2.2	2.4	833791	74919	225540	1134250	15.7	24.6	26.8	199	0.08	0.13
5/4/2000 21:21	1.4	2.2	2.2	RUN 3	-0.1	25.3	0.1	12.3	0.1	12.9	1.5	2.2	2.1	833791	74919	225540	1134250	12.2	24.6	23.6	199	0.06	0.12
5/4/2000 21:22	1.1	2.1	2.1	RUN 3	-0.1	25.3	0.1	12.3	0.1	12.9	1.2	2.0	2.0	833791	74919	225540	1134250	9.7	22.9	22.2	199	0.05	0.11
5/4/2000 21:23	0.9	2.0	2.0	RUN 3	-0.1	25.3	0.1	12.3	0.1	12.9	1.0	1.9	1.9	833791	74919	225540	1134250	8.2	21.5	21.5	199	0.04	0.11
5/4/2000 21:24	0.9	1.8	2.3	RUN 3	-0.1	25.3	0.1	12.3	0.1	12.9	0.9	1.8	2.2	833791	74919	225540	1134250	7.7	20.2	24.7	199	0.04	0.11
5/4/2000 21:25	0.9	1.6	2.9	RUN 3	-0.1	25.3	0.1	12.3	0.1	12.9	0.9	1.6	2.7	833791	74919	225540	1134250	7.7	17.8	31.0	199	0.04	0.12
5/4/2000 21:26	0.9	2.0	3.5	RUN 3	-0.1	25.3	0.1	12.3	0.1	12.9	0.9	2.0	3.4	833791	74919	225540	1134250	7.7	22.6	38.3	199	0.04	0.15
5/4/2000 21:27	0.9	2.5	4.1	RUN 3	-0.1	25.3	0.1	12.3	0.1	12.9	0.9	2.4	3.9	833791	74919	225540	1134250	7.7	27.3	44.3	199	0.04	0.18
5/4/2000 21:28	0.9	2.8	3.6	RUN 3	-0.1	25.3	0.1	12.3	0.1	12.9	0.9	2.8	3.5	833791	74919	225540	1134250	7.7	31.4	39.4	199	0.04	0.18
5/4/2000 21:29	0.9	2.9	2.6	RUN 3	-0.1	25.3	0.1	12.3	0.1	12.9	0.9	2.8	2.5	833791	74919	225540	1134250	7.7	32.1	27.8	199	0.04	0.15
5/4/2000 21:30	0.8	2.1	2.0	RUN 3	-0.1	25.3	0.1	12.3	0.1	12.9	0.9	2.0	1.9	833791	74919	225540	1134250	7.2	22.9	21.5	199	0.04	0.11
5/4/2000 21:31	0.7	1.7	1.7	RUN 3	-0.1	25.3	0.1	12.3	0.1	12.9	0.8	1.6	1.7	833791	74919	225540	1134250	6.2	18.5	18.7	199	0.03	0.09
5/4/2000 21:32	0.7	1.8	1.8	RUN 3	-0.1	25.3	0.1	12.3	0.1	12.9	0.8	1.7	1.5	833791	74919	225540	1134250	6.2	19.5	17.3	199	0.03	0.09
5/4/2000 21:33	0.6	1.7	1.6	RUN 3	-0.1	25.3	0.1	12.3	0.1	12.9	0.7	1.6	1.6	833791	74919	225540	1134250	5.7	18.1	17.7	199	0.03	0.09
5/4/2000 21:34	0.6	1.6	1.8	RUN 3	-0.1	25.3	0.1	12.3	0.1	12.9	0.7	1.5	1.7	833791	74919	225540	1134250	5.7	17.1	19.4	199	0.03	0.09
5/4/2000 21:35	0.6	1.6	2.0	RUN 3	-0.1	25.3	0.1	12.3	0.1	12.9	0.7	1.5	1.9	833791	74919	225540	1134250	5.7	17.1	21.5	199	0.03	0.10
5/4/2000 21:36	0.6	1.7	2.1	RUN 3	-0.1	25.3	0.1	12.3	0.1	12.9	0.7	1.6	2.0	833791	74919	225540	1134250	5.7	18.5	22.2	199	0.03	0.10
5/4/2000 21:37	0.7	1.7	1.6	RUN 3	-0.1	25.3	0.1	12.3	0.1	12.9	0.8	1.7	1.7	833791	74919	225540	1134250	6.2	18.8	19.4	199	0.03	0.10
5/4/2000 21:38	0.7	1.7	1.6	RUN 3	-0.1	25.3	0.1	12.3	0.1	12.9	0.8	1.6	1.5	833791	74919	225540	1134250	6.2	18.5	17.0	199	0.03	0.09
5/4/2000 21:39	0.7	1.6	1.5	RUN 3	-0.1	25.3	0.1	12.3	0.1	12.9	0.8	1.5	1.4	833791	74919	225540	1134250	6.7	17.1	15.6	199	0.03	0.08
5/4/2000 21:40	0.7	1.5	1.5	RUN 3	-0.1	25.3	0.1	12.3	0.1	12.9	0.8	1.4	1.4	833791	74919	225540	1134250	6.7	15.8	15.9	199	0.03	0.08
5/4/2000 21:41	1.0	1.4	1.3	RUN 3	-0.1	25.3	0.1	12.3	0.1	12.9	1.1	1.3	1.3	833791	74919	225540	1134250	8.7	15.1	14.2	199	0.04	0.07
5/4/2000 21:42	1.1	1.4	1.1	RUN 3	-0.1	25.3	0.1	12.3	0.1	12.9	1.2	1.3	1.0	833791	74919	225540	1134250	9.7	14.7	11.7	199	0.05	0.07
5/4/2000 21:43	1.1	1.4	1.6	RUN 3	-0.1	25.3	0.1	12.3	0.1	12.9	1.2	1.4	1.5	833791	74919	225540	1134250	9.7	15.4	16.6	199	0.05	0.08
5/4/2000 21:44	1.1	1.6	2.0	RUN 3	-0.1	25.3	0.1	12.3	0.1	12.9	1.1	1.5	1.9	833791	74919	225540	1134250	9.2	17.1	21.5	199	0.05	0.10
5/4/2000 21:45	0.9	1.8	2.4	RUN 3	-0.1	25.3	0.1	12.3	0.1	12.9	1.0	1.7	2.3	833791	74919	225540	1134250	8.2	19.5	25.7	199	0.04	0.11
5/4/2000 21:46	0.9	2.0	2.0	RUN 3	-0.1	25.3	0.1	12.3	0.1	12.9	1.0	2.0	1.9	833791	74919	225540	1134250	8.2	22.2	21.2	199	0.04	0.11
5/4/2000 21:47	1.1	2.0	2.2	RUN 3	-0.1	25.3	0.1	12.3	0.1	12.9	1.1	1.9	2.1	833791	74919	225540	1134250	9.2	21.9	23.3	199	0.05	0.11
5/4/2000 21:48	2.4	1.9	1.9	RUN 3	-0.1	25.3	0.1	12.3	0.1	12.9	2.5	1.8	1.8	833791	74919	225540	1134250	20.2	20.9	20.8	199	0.10	0.10
5/4/2000 21:49	5.3	1.8	1.7	RUN 3	-0.1	25.3	0.1	12.3	0.1	12.9	5.3	1.8	1.7	833791	74919	225540	1134250	43.2	19.8	18.7	199	0.22	0.10
5/4/2000 21:50	7.0	1.7	1.6	RUN 3	-0.1	25.3	0.1	12.3	0.1	12.9	7.0	1.6	1.5	833791	74919	225540	1134250	56.7	18.1	17.0	199	0.29	0.09
5/4/2000 21:51	7.5	1.5	1.4	RUN 3	-0.1	25.3	0.1	12.3	0.1	12.9	7.5	1.5	1.3	833791	74919	225540	1134250	60.8	16.8	14.9	199	0.31	0.08
5/4/2000 21:52	8.2	1.2	1.8	RUN 3	-0.1	25.3	0.1	12.3	0.1	12.9	8.2	1.2	1.7	833791	74919	225540	1134250	66.3	13.0	19.1	199	0.33	0.08
5/4/2000 21:53	8.3	1.2	2.9	RUN 3	-0.1	25.3	0.1	12.3	0.1	12.9	8.2	1.2	2.8	833791	74919	225540	1134250	66.8	13.0	31.7	199	0.34	0.11
5/4/2000 21:54	7.1	1.8	3.2	RUN 3	-0.1	25.3	0.1	12.3	0.1	12.9	7.1	1.7	3.1	833791	74919	225540	1134250	57.8	19.2	34.8	199	0.29	0.14

TIME	OBSERVED CONCENTRATION PPM			COMMENTS	CALIBRATION CORRECTIONS						CORRECTED PPM VALUES			FLOW MEASURMENTS SCFM				MASS EMISSIONS			EMISSION FACTOR		
					NOX 7		SO2 IN		SO2 OUT														
	NOX COMP 7	SO2 IN	SO2 OUT		0.0	24.9	0.0	12.5	0.0	12.5	NOX - 7	SO2 IN	SO2 OUT	COLD-1	COLD-2	HOT	TOTAL	NOX LBS/HR	SO2 IN LBS/HR	SO2 OUT LBS/HR	PRODUCTION TONS/HR	NOX LBS/TON	SO2 LBS/TON
5/4/2000 21:55	4.5	2.3	2.6	RUN 3	-0.1	25.3	0.1	12.3	0.1	12.9	4.5	2.2	2.5	833791	74919	225540	1134250	36.1	24.9	27.8	199	0.18	0.13
5/4/2000 21:56	2.7	2.3	2.0	RUN 3	-0.1	25.3	0.1	12.3	0.1	12.9	2.7	2.2	1.9	833791	74919	225540	1134250	22.2	24.9	21.2	199	0.11	0.12
5/4/2000 21:57	2.2	2.0	2.1	RUN 3	-0.1	25.3	0.1	12.3	0.1	12.9	2.2	1.9	2.0	833791	74919	225540	1134250	18.2	21.5	22.9	199	0.09	0.11
5/4/2000 21:58	3.7	1.5	1.9	RUN 3	-0.1	25.3	0.1	12.3	0.1	12.9	3.7	1.4	1.8	833791	74919	225540	1134250	30.2	16.1	20.8	199	0.15	0.09
5/4/2000 21:59	6.0	1.7	1.8	RUN 3	-0.1	25.3	0.1	12.3	0.1	12.9	6.0	1.6	1.7	833791	74919	225540	1134250	48.7	18.5	19.1	199	0.24	0.09
5/4/2000 22:00	8.1	1.7	1.8	RUN 3	-0.1	25.3	0.1	12.3	0.1	12.9	8.0	1.6	1.7	833791	74919	225540	1134250	65.3	18.5	19.8	199	0.33	0.10
5/4/2000 22:01	9.0	1.7	1.8	RUN 3	-0.1	25.3	0.1	12.3	0.1	12.9	8.9	1.6	1.8	833791	74919	225540	1134250	72.3	18.1	20.5	199	0.36	0.10
5/4/2000 22:02	5.3	1.7	2.1	RUN 3	-0.1	25.3	0.1	12.3	0.1	12.9	5.3	1.6	2.0	833791	74919	225540	1134250	42.7	18.5	22.6	199	0.21	0.10
5/4/2000 22:03	2.4	1.8	2.5	RUN 3	-0.1	25.3	0.1	12.3	0.1	12.9	2.4	1.8	2.4	833791	74919	225540	1134250	19.7	19.8	27.1	199	0.10	0.12
5/4/2000 22:04	1.4	2.1	3.2	RUN 3	-0.1	25.3	0.1	12.3	0.1	12.9	1.5	2.0	3.1	833791	74919	225540	1134250	12.2	22.9	34.8	199	0.06	0.15
5/4/2000 22:05	1.2	2.5	3.6	RUN 3	-0.1	25.3	0.1	12.3	0.1	12.9	1.3	2.4	3.5	833791	74919	225540	1134250	10.2	27.7	39.0	199	0.05	0.17
5/4/2000 22:06	1.1	2.9	3.4	RUN 3	-0.1	25.3	0.1	12.3	0.1	12.9	1.2	2.8	3.3	833791	74919	225540	1134250	9.7	32.1	36.9	199	0.05	0.17
5/4/2000 22:07	1.7	3.0	2.7	RUN 3	-0.1	25.3	0.1	12.3	0.1	12.9	1.7	3.0	2.6	833791	74919	225540	1134250	14.2	33.5	29.6	199	0.07	0.16
5/4/2000 22:08	5.3	2.7	2.7	RUN 3	-0.1	25.3	0.1	12.3	0.1	12.9	5.3	2.7	2.6	833791	74919	225540	1134250	43.2	30.4	29.6	199	0.22	0.15
5/4/2000 22:09	8.3	2.6	2.1	RUN 3	-0.1	25.3	0.1	12.3	0.1	12.9	8.2	2.6	2.0	833791	74919	225540	1134250	66.8	29.4	22.9	199	0.34	0.13
5/4/2000 22:10	8.2	2.5	1.9	RUN 3	-0.1	25.3	0.1	12.3	0.1	12.9	8.2	2.5	1.8	833791	74919	225540	1134250	66.3	28.0	20.6	199	0.33	0.12
5/4/2000 22:11	7.6	2.4	2.1	RUN 3	-0.1	25.3	0.1	12.3	0.1	12.9	7.6	2.4	2.0	833791	74919	225540	1134250	61.8	26.6	22.2	199	0.31	0.12
5/4/2000 22:12	7.6	2.3	2.0	RUN 3	-0.1	25.3	0.1	12.3	0.1	12.9	7.6	2.3	1.9	833791	74919	225540	1134250	61.8	25.6	21.2	199	0.31	0.12
5/4/2000 22:13	6.6	2.3	2.0	RUN 3	-0.1	25.3	0.1	12.3	0.1	12.9	6.6	2.2	1.9	833791	74919	225540	1134250	53.7	24.9	21.2	199	0.27	0.12
5/4/2000 22:14	4.4	2.2	2.0	RUN 3	-0.1	25.3	0.1	12.3	0.1	12.9	4.4	2.1	1.9	833791	74919	225540	1134250	35.7	23.9	21.5	199	0.18	0.11
5/4/2000 22:15	3.1	2.2	2.1	RUN 3	-0.1	25.3	0.1	12.3	0.1	12.9	3.1	2.1	2.0	833791	74919	225540	1134250	25.2	23.9	22.2	199	0.13	0.12
5/4/2000 22:16	2.6	2.2	2.1	RUN 3	-0.1	25.3	0.1	12.3	0.1	12.9	2.7	2.1	2.0	833791	74919	225540	1134250	21.7	23.9	22.9	199	0.11	0.12
5/4/2000 22:17	2.5	2.3	2.6	RUN 3	-0.1	25.3	0.1	12.3	0.1	12.9	2.5	2.2	2.5	833791	74919	225540	1134250	20.7	25.3	27.8	199	0.10	0.13
5/4/2000 22:18	2.4	2.6	3.0	RUN 3	-0.1	25.3	0.1	12.3	0.1	12.9	2.5	2.5	2.9	833791	74919	225540	1134250	20.2	28.7	33.1	199	0.10	0.16
5/4/2000 22:19	2.3	2.6	3.6	RUN 3	-0.1	25.3	0.1	12.3	0.1	12.9	2.4	2.6	3.5	833791	74919	225540	1134250	19.2	29.4	39.7	199	0.10	0.17
5/4/2000 22:20	2.3	2.3	4.6	RUN 3	-0.1	25.3	0.1	12.3	0.1	12.9	2.4	2.2	4.4	833791	74919	225540	1134250	19.2	24.9	50.3	199	0.10	0.19
5/4/2000 22:21	2.7	3.3	5.3	RUN 3	-0.1	25.3	0.1	12.3	0.1	12.9	2.7	3.5	5.1	833791	74919	225540	1134250	22.2	36.9	58.0	199	0.11	0.24
5/4/2000 22:22	3.3	4.1	5.5	RUN 3	-0.1	25.3	0.1	12.3	0.1	12.9	3.3	4.1	5.3	833791	74919	225540	1134250	27.2	46.7	59.7	199	0.14	0.27
5/4/2000 22:23	3.3	4.5	4.6	RUN 3	-0.1	25.3	0.1	12.3	0.1	12.9	3.3	4.5	4.5	833791	74919	225540	1134250	26.7	51.1	50.6	199	0.13	0.26
5/4/2000 22:24	3.1	4.3	4.1	RUN 3	-0.1	25.3	0.1	12.3	0.1	12.9	3.1	4.3	4.0	833791	74919	225540	1134250	25.2	48.8	45.0	199	0.13	0.24
5/4/2000 22:25	2.7	3.1	4.0	RUN 3	-0.1	25.3	0.1	12.3	0.1	12.9	2.8	3.1	3.9	833791	74919	225540	1134250	22.7	35.2	43.6	199	0.11	0.20
5/4/2000 22:26	2.6	3.0	3.9	RUN 3	-0.1	25.3	0.1	12.3	0.1	12.9	2.6	3.0	3.8	833791	74919	225540	1134250	21.2	33.8	42.5	199	0.11	0.19
5/4/2000 22:27	2.4	3.4	3.7	RUN 3	-0.1	25.3	0.1	12.3	0.1	12.9	2.4	3.3	3.6	833791	74919	225540	1134250	19.7	37.9	40.4	199	0.10	0.20
5/4/2000 22:28	2.1	3.4	3.8	RUN 3	-0.1	25.3	0.1	12.3	0.1	12.9	2.2	3.3	3.5	833791	74919	225540	1134250	17.7	37.9	39.0	199	0.09	0.19
5/4/2000 22:29	2.0	3.3	3.7	RUN 3	-0.1	25.3	0.1	12.3	0.1	12.9	2.1	3.3	3.6	833791	74919	225540	1134250	16.7	37.5	40.8	199	0.08	0.20
5/4/2000 22:30	2.4	3.4	4.1	RUN 3	-0.1	25.3	0.1	12.3	0.1	12.9	2.5	3.4	3.9	833791	74919	225540	1134250	20.2	38.2	44.6	199	0.10	0.21
5/4/2000 22:31	3.3	3.6	4.2	RUN 3	-0.1	25.3	0.1	12.3	0.1	12.9	3.3	3.6	4.1	833791	74919	225540	1134250	26.7	40.1	46.0	199	0.13	0.22
5/4/2000 22:32	3.5	3.6	3.4	RUN 3	-0.1	25.3	0.1	12.3	0.1	12.9	3.5	3.6	3.3	833791	74919	225540	1134250	28.7	40.6	36.9	199	0.14	0.19
5/4/2000 22:33	3.1	3.3	3.0	RUN 3	-0.1	25.3	0.1	12.3	0.1	12.9	3.1	3.3	2.9	833791	74919	225540	1134250	25.2	37.5	32.4	199	0.13	0.18
5/4/2000 22:34	2.7	2.9	2.3	RUN 3	-0.1	25.3	0.1	12.3	0.1	12.9	2.7	2.9	2.2	833791	74919	225540	1134250	22.2	32.8	25.4	199	0.11	0.15
5/4/2000 22:35	2.5	2.5	2.3	RUN 3	-0.1	25.3	0.1	12.3	0.1	12.9	2.5	2.5	2.2	833791	74919	225540	1134250	20.7	28.0	24.7	199	0.10	0.13
5/4/2000 22:36	3.1	2.3	2.2	RUN 3	-0.1	25.3	0.1	12.3	0.1	12.9	3.1	2.3	2.1	833791	74919	225540	1134250	25.2	26.0	24.0	199	0.13	0.13
5/4/2000 22:37	3.8	2.3	2.0	RUN 3	-0.1	25.3	0.1	12.3	0.1	12.9	3.8	2.2	1.9	833791	74919	225540	1134250	31.2	25.3	21.5	199	0.16	0.12
5/4/2000 22:38	3.9	2.4	2.9	RUN 3	-0.1	25.3	0.1	12.3	0.1	12.9	3.9	2.4	2.8	833791	74919	225540	1134250	31.7	27.0	31.3	199	0.16	0.15
5/4/2000 22:39	4.3	2.8	3.3	RUN 3	-0.1	25.3	0.1	12.3	0.1	12.9	4.3	2.7	3.2	833791	74919	225540	1134250	34.7	30.7	35.9	199	0.17	0.17
5/4/2000 22:40	5.1	3.0	3.9	RUN 3	-0.1	25.3	0.1	12.3	0.1	12.9	5.1	3.0	3.7	833791	74919	225540	1134250	41.2	33.5	42.2	199	0.21	0.19
5/4/2000 22:41	4.2	3.2	3.5	RUN 3	-0.1	25.3	0.1	12.3	0.1	12.9	4.2	3.2	3.4	833791	74919	225540	1134250	34.2	36.2	38.3	199	0.17	0.19
5/4/2000 22:42	2.7	3.3	3.0	RUN 3	-0.1	25.3	0.1	12.3	0.1	12.9	2.7	3.2	2.9	833791	74919	225540	1134250	22.2	36.5	32.7	199	0.11	0.17
5/4/2000 22:43	2.0	3.0	2.7	RUN 3	-0.1	25.3	0.1	12.3	0.1	12.9	2.1	3.0	2.6	833791	74919	225540	1134250	16.7	33.8	29.6	199	0.08	0.16
5/4/2000 22:44	2.2	2.6	3.0	RUN 3	-0.1	25.3	0.1	12.3	0.1	12.9	2.2	2.7	2.9	833791	74919	225540	1134250	18.2	30.7	33.1	199	0.09	0.16
5/4/2000 22:45	2.8	2.7	3.2	RUN 3	-0.1	25.3	0.1	12.3	0.1	12.9	2.9	2.6	3.0	833791	74919	225540	1134250	23.2	29.7	34.5	199	0.12	0.16
5/4/2000 22:46	4.1	2.7	3.0	RUN 3	-0.1	25.3	0.1	12.3	0.1	12.9	RUN 3 AVERAGES							RUN 3 AVERAGES					
5/4/2000 22:47	4.2	2.3	3.1	RUN 3	-0.1	25.3	0.1	12.3	0.1	12.9	3.4	2.7	2.9					27.4	30.0	32.2	199.0	0.14	0.16
5/4/2000 22:48	3.7	2.5	3.5	RUN 3	-0.1	25.3	0.1	12.3	0.1	12.9													
5/4/2000 22:49	3.4	2.7	4.0	RUN 3	-0.1	25.3	0.1	12.3	0.1	12.9				833791	74919	225540	1134250						

TIME	OBSERVED CONCENTRATION PPM			COMMENTS	CALIBRATION CORRECTIONS						CORRECTED PPM VALUES			FLOW MEASURMENTS SCFM				MASS EMISSIONS			EMISSION FACTOR		
					NOX 7		SO2 IN		SO2 OUT														
	NOX COMP 7	SO2 IN	SO2 OUT		0.0	24.9	0.0	12.5	0.0	12.5	NOX - 7	SO2 IN	SO2 OUT	COLD-1	COLD-2	HOT	TOTAL	NOX LBS/HR	SO2 IN LBS/HR	SO2 OUT LBS/HR	PRODUCTION TONS/HR	NOX LBS/TON	SO2 LBS/TON
5/4/2000 22:50	3.3	3.0	3.9		-0.1	25.3	0.1	12.3	0.1	12.9	TEST AVERAGE TIME WEIGHTED			833791	74919	225540	1134250	TEST AVERAGE TIME WEIGHTED					
5/4/2000 22:51	3.3	3.0	3.2		-0.1	25.3	0.1	12.3	0.1	12.9				833791	74919	225540	1134250						
5/4/2000 22:52	3.5	2.7	1.5		-0.1	25.3	0.1	12.3	0.1	12.9	4.4	1.3	2.0	833791	74919	225540	1134250	36.1	14.9	22.2	192.8	0.19	0.10
5/4/2000 22:53	3.4	2.1	0.4		-0.1	25.3	0.1	12.3	0.1	12.9				833791	74919	225540	1134250						
5/4/2000 22:54	3.4	2.2	0.2		-0.1	25.3	0.1	12.3	0.1	12.9				833791	74919	225540	1134250						
5/4/2000 22:55	3.3	2.1	0.2		-0.1	25.3	0.1	12.3	0.1	12.9				833791	74919	225540	1134250						
5/4/2000 22:56	3.3	2.1	0.1		-0.1	25.3	0.1	12.3	0.1	12.9	3.3	2.0	0.0	833791	74919	225540	1134250						
5/4/2000 22:57	3.5	2.1	0.1		-0.1	25.3	0.1	12.3	0.1	12.9	3.5	2.0	0.0	833791	74919	225540	1134250						
5/4/2000 22:58	3.7	2.0	0.1		-0.1	25.3	0.1	12.3	0.1	12.9	3.7	2.0	0.0	833791	74919	225540	1134250						
5/4/2000 22:59	3.8	2.1	0.0		-0.1	25.3	0.1	12.3	0.1	12.9	3.8	2.0	0.0	833791	74919	225540	1134250						
5/4/2000 23:00	3.7	2.1	0.0		-0.1	25.3	0.1	12.3	0.1	12.9	3.7	2.0	0.0	833791	74919	225540	1134250						
5/4/2000 23:01	3.9	2.0	0.0		-0.1	25.3	0.1	12.3	0.1	12.9	3.9	2.0	0.0	833791	74919	225540	1134250						
5/4/2000 23:02	4.0	2.0	4.7		-0.1	25.3	0.1	12.3	0.1	12.9	4.0	2.0	4.5	833791	74919	225540	1134250						
5/4/2000 23:03	3.9	2.0	11.3		-0.1	25.3	0.1	12.3	0.1	12.9	4.0	2.0	11.0	833791	74919	225540	1134250						
5/4/2000 23:04	3.8	2.0	12.5		-0.1	25.3	0.1	12.3	0.1	12.9	3.8	1.9	12.1	833791	74919	225540	1134250						
5/4/2000 23:05	3.7	1.9	12.9		-0.1	25.3	0.1	12.3	0.1	12.9	3.7	1.8	12.5	833791	74919	225540	1134250						
5/4/2000 23:06	3.7	1.7	13.1		-0.1	25.3	0.1	12.3	0.1	12.9	3.7	1.7	12.7	833791	74919	225540	1134250						
5/4/2000 23:07	3.7	1.5	13.1		-0.1	25.3	0.1	12.3	0.1	12.9	3.7	1.5	12.7	833791	74919	225540	1134250						
5/4/2000 23:08	3.6	1.5	13.1		-0.1	25.3	0.1	12.3	0.1	12.9	3.7	1.4	12.7	833791	74919	225540	1134250						
5/4/2000 23:09	3.6	1.5	13.3		-0.1	25.3	0.1	12.3	0.1	12.9	3.7	1.4	12.9	833791	74919	225540	1134250						
5/4/2000 23:10	3.6	1.5	13.2		-0.1	25.3	0.1	12.3	0.1	12.9	3.6	1.4	12.9	833791	74919	225540	1134250						
5/4/2000 23:11	3.6	1.5	13.3		-0.1	25.3	0.1	12.3	0.1	12.9	3.7	1.4	12.9	833791	74919	225540	1134250						
5/4/2000 23:12	3.7	1.5	10.5		-0.1	25.3	0.1	12.3	0.1	12.9	3.7	1.5	10.2	833791	74919	225540	1134250						
5/4/2000 23:13	3.4	1.5	2.5		-0.1	25.3	0.1	12.3	0.1	12.9	3.5	1.4	2.4	833791	74919	225540	1134250						
5/4/2000 23:14	3.1	1.4	0.6		-0.1	25.3	0.1	12.3	0.1	12.9	3.1	1.3	0.6	833791	74919	225540	1134250						
5/4/2000 23:15	2.9	1.3	0.3		-0.1	25.3	0.1	12.3	0.1	12.9	2.9	1.2	0.3	833791	74919	225540	1134250						
5/4/2000 23:16	2.5	1.2	0.3		-0.1	25.3	0.1	12.3	0.1	12.9	2.5	1.2	0.2	833791	74919	225540	1134250						
5/4/2000 23:17	1.7	1.2	0.3		-0.1	25.3	0.1	12.3	0.1	12.9	1.7	1.1	0.3	833791	74919	225540	1134250						
5/4/2000 23:18	1.2	1.1	5.5		-0.1	25.3	0.1	12.3	0.1	12.9	1.3	1.1	5.3	833791	74919	225540	1134250						
5/4/2000 23:19	0.9	1.0	20.8		-0.1	25.3	0.1	12.3	0.1	12.9	1.0	0.9	20.3	833791	74919	225540	1134250						
5/4/2000 23:20	0.9	0.9	24.8		-0.1	25.3	0.1	12.3	0.1	12.9	1.0	0.8	24.2	833791	74919	225540	1134250						
5/4/2000 23:21	0.9	0.8	25.3		-0.1	25.3	0.1	12.3	0.1	12.9	1.0	0.8	24.7	833791	74919	225540	1134250						
5/4/2000 23:22	1.0	0.9	25.6		-0.1	25.3	0.1	12.3	0.1	12.9	1.1	0.8	24.9	833791	74919	225540	1134250						
5/4/2000 23:23	1.0	0.8	25.2		-0.1	25.3	0.1	12.3	0.1	12.9	1.1	0.8	24.6	833791	74919	225540	1134250						
5/4/2000 23:24	1.0	0.8	25.3		-0.1	25.3	0.1	12.3	0.1	12.9	1.1	0.7	24.6	833791	74919	225540	1134250						
5/4/2000 23:25	1.0	0.8	25.3		-0.1	25.3	0.1	12.3	0.1	12.9	1.1	0.7	24.6	833791	74919	225540	1134250						
5/4/2000 23:26	0.9	0.7	18.9		-0.1	25.3	0.1	12.3	0.1	12.9	1.0	0.6	18.4	833791	74919	225540	1134250						
5/4/2000 23:27	0.9	0.7	4.5		-0.1	25.3	0.1	12.3	0.1	12.9	1.0	0.6	4.1	833791	74919	225540	1134250						
5/4/2000 23:28	0.9	0.7	1.1		-0.1	25.3	0.1	12.3	0.1	12.9	1.0	0.6	1.0	833791	74919	225540	1134250						
5/4/2000 23:29	0.9	0.6	0.6		-0.1	25.3	0.1	12.3	0.1	12.9	1.0	0.6	0.6	833791	74919	225540	1134250						
5/4/2000 23:30	0.9	2.7	0.9		-0.1	25.3	0.1	12.3	0.1	12.9	1.0	2.6	0.8	833791	74919	225540	1134250						
5/4/2000 23:31	0.9	1.0	1.4		-0.1	25.3	0.1	12.3	0.1	12.9	0.9	1.0	1.3	833791	74919	225540	1134250						
5/4/2000 23:32	0.9	0.3	1.0		-0.1	25.3	0.1	12.3	0.1	12.9	0.9	0.2	0.9	833791	74919	225540	1134250						
5/4/2000 23:33	0.9	0.1	0.8		-0.1	25.3	0.1	12.3	0.1	12.9	0.9	0.0	0.7	833791	74919	225540	1134250						
5/4/2000 23:34	0.9	0.1	0.7		-0.1	25.3	0.1	12.3	0.1	12.9	0.9	0.0	0.6	833791	74919	225540	1134250						
5/4/2000 23:35	0.9	0.1	0.6		-0.1	25.3	0.1	12.3	0.1	12.9	0.9	0.0	0.5	833791	74919	225540	1134250						
5/4/2000 23:36	0.9	0.1	0.5		-0.1	25.3	0.1	12.3	0.1	12.9	0.9	0.0	0.5	833791	74919	225540	1134250						
5/4/2000 23:37	0.9	2.8	0.5		-0.1	25.3	0.1	12.3	0.1	12.9	0.9	2.8	0.4	833791	74919	225540	1134250						
5/4/2000 23:38	0.9	17.6	0.4		-0.1	25.3	0.1	12.3	0.1	12.9	0.9	18.0	0.4	833791	74919	225540	1134250						
5/4/2000 23:39	0.9	22.7	0.4		-0.1	25.3	0.1	12.3	0.1	12.9	0.9	23.1	0.3	833791	74919	225540	1134250						
5/4/2000 23:40	0.9	23.5	0.4		-0.1	25.3	0.1	12.3	0.1	12.9	0.9	24.0	0.3	833791	74919	225540	1134250						
5/4/2000 23:41	0.9	23.8	0.5		-0.1	25.3	0.1	12.3	0.1	12.9	0.9	24.3	0.4	833791	74919	225540	1134250						
5/4/2000 23:42	0.9	23.9	0.6		-0.1	25.3	0.1	12.3	0.1	12.9	0.9	24.4	0.5	833791	74919	225540	1134250						
5/4/2000 23:43	0.9	23.7	0.8		-0.1	25.3	0.1	12.3	0.1	12.9	0.9	24.2	0.7	833791	74919	225540	1134250						
5/4/2000 23:44	0.9	16.6	1.3		-0.1	25.3	0.1	12.3	0.1	12.9	0.9	16.9	1.2	833791	74919	225540	1134250						

TIME	OBSERVED CONCENTRATION PPM			COMMENTS	CALIBRATION CORRECTIONS						CORRECTED PPM VALUES			FLOW MEASURMENTS SCFM				MASS EMISSIONS			EMISSION FACTOR		
					NOX 7		SO2 IN		SO2 OUT														
	NOX COMP 7	SO2 IN	SO2 OUT		0.0	24.9	0.0	12.5	0.0	12.5	NOX - 7	SO2 IN	SO2 OUT	COLD-1	COLD-2	HOT	TOTAL	NOX LBS/HR	SO2 IN LBS/HR	SO2 OUT LBS/HR	PRODUCTION TONS/HR	NOX LBS/TON	SO2 LBS/TON
5/4/2000 23:45	0.9	12.9	1.7		-0.1	25.3	0.1	12.3	0.1	12.9	0.9	13.1	1.8	833791	74919	225540	1134250						
5/4/2000 23:46	0.9	12.4	1.9		-0.1	25.3	0.1	12.3	0.1	12.9	0.9	12.8	1.8	833791	74919	225540	1134250						
5/4/2000 23:47	0.9	12.4	1.8		-0.1	25.3	0.1	12.3	0.1	12.9	0.9	12.8	1.7	833791	74919	225540	1134250						
5/4/2000 23:48	0.9	12.4	1.7		-0.1	25.3	0.1	12.3	0.1	12.9	1.0	12.8	1.8	833791	74919	225540	1134250						
5/4/2000 23:49	1.0	10.3	1.5		-0.1	25.3	0.1	12.3	0.1	12.9	1.1	10.4	1.4	833791	74919	225540	1134250						
5/4/2000 23:50	0.4	3.9	0.8		-0.1	25.3	0.1	12.3	0.1	12.9	0.5	3.9	0.6	833791	74919	225540	1134250						
5/4/2000 23:51	-0.1	2.4	0.1		-0.1	25.3	0.1	12.3	0.1	12.9	0.0	2.4	0.0	833791	74919	225540	1134250						
5/4/2000 23:52	-0.1	1.8	0.0		-0.1	25.3	0.1	12.3	0.1	12.9	0.0	1.8	-0.1	833791	74919	225540	1134250						
5/4/2000 23:53	2.8	0.9	-0.1		-0.1	25.3	0.1	12.3	0.1	12.9	2.7	0.8	-0.1	833791	74919	225540	1134250						
5/4/2000 23:54	18.2	1.4	-0.1		-0.1	25.3	0.1	12.3	0.1	12.9	17.9	1.4	-0.1	833791	74919	225540	1134250						
5/4/2000 23:55	25.4	3.7	-0.1		-0.1	25.3	0.1	12.3	0.1	12.9	25.0	3.7	-0.1	833791	74919	225540	1134250						
5/4/2000 23:56	25.7	3.8	-0.1		-0.1	25.3	0.1	12.3	0.1	12.9	25.3	3.8	-0.1	833791	74919	225540	1134250						
5/4/2000 23:57	25.9	3.6	-0.1		-0.1	25.3	0.1	12.3	0.1	12.9	25.5	3.6	-0.1	833791	74919	225540	1134250						
5/4/2000 23:58	26.4	3.4	0.0		-0.1	25.3	0.1	12.3	0.1	12.9	26.0	3.4	-0.1	833791	74919	225540	1134250						
5/4/2000 23:59	51.7	3.3	-0.1		-0.1	25.3	0.1	12.3	0.1	12.9	50.8	3.3	-0.1	833791	74919	225540	1134250						
5/5/2000 0:00	55.8	3.4	-0.1		-0.1	25.3	0.1	12.3	0.1	12.9	54.8	3.4	-0.1	833791	74919	225540	1134250						
5/5/2000 0:01	53.5	3.6	-0.1		-0.1	25.3	0.1	12.3	0.1	12.9	52.6	3.6	-0.1	833791	74919	225540	1134250						
5/5/2000 0:02	54.2	3.9	-0.1		-0.1	25.3	0.1	12.3	0.1	12.9	53.2	3.9	-0.1	833791	74919	225540	1134250						
5/5/2000 0:03	54.3	4.0	-0.1		-0.1	25.3	0.1	12.3	0.1	12.9	53.4	4.0	-0.1	833791	74919	225540	1134250						

Gallatin Steel 5-4-00

comp 7 Ch 1 Nox
Ch 4 NOx b.u.
comp 14 Ch 2 inner
comp 12 Ch 3 outer

0811 injecting 12.5 ppm
0815 reading 13.7 ppm Ch 2 SO_2 comp 14
0828 injecting zero gas Ch 2 inner 0.026 volts
0830 injecting zero gas Ch 3 outer 0.026 volts
" " " Ch 4 backup Nox 0.0510 volts
0835 injecting 24.01 ppm SO_2 Ch 3 outer (comp 12)
0843 reading 0.8300 v SO_2 Ch 3 outer (comp 12)
0843 injecting 12.5 ppm SO_2 Ch 3 outer (comp 12)
0851 reading 0.450 v SO_2 Ch 3 outer (comp 12)
0852 injecting 24.01 ppm SO_2 Ch 2 inner (comp 2)
0859 reading 0.858 v SO_2 Ch 2 inner (comp 2)
0901 injecting 12.5 ppm SO_2 Ch 2 inner (comp 2)
0906 reading 0.461 v SO_2 Ch 2 inner (comp 2)

Ch 2 slope 28.8562
intercept -0.7672
Ch 3 slope 29.8558
intercept -0.8272

0910 on line

1138 inject 54.2 ppm NOx Ch 1 comp 7 — tank # 1150 psi CC 110128 — expires 8-10-2001
1141 reading 0.865 volts ✓ (54.2)
1143 inject 24.9 ppm Nox CH 1 comp 7 — tank # 1850 psi CC 109962 — expires 8-10-2001
1145 reading 0.397 volts ✓ (24.8)
1146 injecting 0.00 Nox Ch 1 comp 7
1151 reading 0.003 volts ✓ (0.0)

Gallatin Steel 5-4-00

1152 injecting 0.0 Ch 3 comp 14 SO2 inner
1152 injecting 0,0 Ch 4 comp 14 NOx backup
.032 1201 reading 0.028v Ch 3 comp 14 SO2 inner (0.1 ppm)
1201 ✓ reading 0,050 volts Ch 4 comp 14 NOx backup (0.1 ppm)
1201 injecting 54.2 NOx Ch 4 comp 14 NOx backup
1205 reading 1.002 volts Ch 4 comp 14 NOx backup
1205 injecting 24.9 ppm NOx Ch 4 comp 14 NOx backup
1209 reading 0.535 volts Ch 4 comp 14 NOx backup
1210 injecting 54.2 NOx Ch 4 comp 14 NOx backup
1215 ✓ change to read 0.920 volts Ch 4 comp 14 NOx backup (54.3 ppm)
1216 injecting 24.9 ppm NOx Ch 4 comp 14 NOx backup
1218 ✓ reading 0.445 volts NOx Ch 4 comp 14 NOx backup (24.7 ppm)
1220 injecting 24.01 ppm SO2 Ch 3 comp 2 SO2 outer
injecting 24.01 ppm SO2 Ch 4 comp 14 NOx backup
.784 1229 reading 0.785 volts SO2 Ch 3 comp 2 SO2 outer (24.1 ppm)
reading 0.053 volts zero Ch 4 NOx Backup
1230 injecting 12.5 ppm SO2 Ch 3 comp 2 outer
.419 1234 reading 0.416 volts SO2 Ch 3 comp 2 outer (12.4 ppm)
1235 injecting 12.5 ppm SO2 Ch 2 comp 14 inner, Ch 3 4 x 1 outer on line
.437 1239 reading 0.436 volts SO2 Ch 2 comp 14 inner (12.2 ppm)
1244 injecting 24.01 ppm SO2 Ch 2 comp 14 inner
✓ 1249 reading 0.845 volts SO2 Ch 2 comp 14 inner (24.2 ppm)
1250 injecting zero ppm SO2 Ch 2 comp 14 inner
✓ 1257 reading 0.028 volts SO2 Ch 2 comp 14 inner (0.2 ppm)
1258 on line

ENO Run 1 1538

5/4/00 GAL STEEL

POST RUN 1 CAL CHECKS

1540 OUT comp #2

Zero ppm	SO_2	OUT (comp 2)	0.028 v (0.1 ppm)	1546
" "	NO_x	OUT (comp 2)	0.050 v (0.1 ppm)	1545
12.5 ppm	SO_2	OUT (comp 2)	0.426 v (12.7 ppm)	1553
0 ppm	NO_x	OUT (comp 2)	0.050 v	1553
—	SO_2		~~0~~ NA	
24.9 ppm	NO_x		0.442 v (24.5 ppm)	1559

In comp # 14

Zero	SO_2	0.026 v (0.1)	1602
12.5	SO_2	0.442 v (12.3)	1608

NO_x comp 7

Zero ppm	NO_x	0.001 v (-0.1)	1618
24.9 ppm	NO_x	0.405 v (25.3)	1613

ON LINE 1620 - WAIT FOR NEXT HEAT

		SLOPE	INTCP	1v 0v
RUN 1	CH1	62.8687	-0.1429	62.7 / -0.14
	CH2	29.3875	-0.6527	28.7 / -0.653
	CH3	31.7216	-0.8253	30.90 / -0.8253
	CH4	62.2783	-3.0079	59.27 / -3.007

APROX AVG FOR RUN 1

CH1	6.3 ppm
2	1.1 ppm
3	1.4 ppm

START RUN 2 16.30 Heat1
17:24 Heat2
18:18 Heat3
END RUN 2 19:21

1924 inject 0.0 ~~Ch1 comp 7 (NOx)~~ Ch3 comp4 SO_2
Ch4 comp 4 b.u. NOx backup
1931 reading 0.063 ppm Ch3 comp4 SO_2 outer
0.106 Ch4 comp 4 NOx outer Backup
1931 injecting 12.5 ppm SO_2 Ch3 comp4 SO_2 outer
1941 reading 12.5ppm SO_2 Ch3 comp4 SO_2 outer
1941 injecting 24.9ppm NOx Ch4 comp 4 NOx outer backup
1946 reading 24.3ppm NOx Ch4 comp4 NOx outer backup
1946 injecting 24.3ppm NOx Ch1 comp7 NOx compliance NOx
1950 reading 25.0ppm NOx Ch1 comp7 NOx compliance NOx
1951 injecting 0.0ppm NOx Ch1 comp7 NOx compliance NOx
1956 reading 0.11 ppm NOx Ch1 comp7 NOx compliance
1957 injecting 0.0 ppm Ch2 comp16 SO_2 inner
2001 reading 0.11 ppm Ch2 comp16 SO_2 inner
2002 injecting 12.5ppm Ch2 comp16 SO_2 inner
2009 reading 12.2 ppm Ch2 comp16 SO_2 inner
2016 online
2017 Start RUN 3 Heat 1 ~2115 START HEAT 2

RUN 2 Results

1 NOx #7 = 3.4
2 SO_2 #16 = 0.6
3 SO_2 #4 = 1.9

1045 Plant down - End run 3

1050 inject zero gas ch3 SO_2 out comp 19
ch4 NOx out comp 19

1100 reading -0.03 ppm ch3 SO_2 out comp 19
0.106 ppm ch4 NOx out comp 19

1101 injecting 12.5 ppm SO_2 ch3 SO_2 out comp 19

1109 reading 13.2 ppm SO_2 ch3 SO_2 out comp 19

1112 injecting 24.9 ppm NOx ch4 NOx out comp 19

1116 reading 24.6 ppm NOx ch4 NOx out comp 19

1117 injecting 24.01 ppm SO_2 ch3 SO_2 out comp 19

1124 reading 25 ppm SO_2 Ch 3 SO_2 out Comp 19

1124 injecting 54.2 NOx ch4 out comp 19

1129 reading 53.8 ppm NOx ch4 out comp 19

1129 injecting ~~24.01~~ zero ppm SO_2 ch2 SO_2 in Comp 7

1136 reading 0.08 ppm SO_2 ch2 SO_2 in Comp 7

1137 injecting 24.01 ppm SO_2 ch2 SO_2 in Comp 7

1142 reading 23.9 ppm SO_2 ch2 SO_2 in Comp 7

1142 injecting 12.5 ppm SO_2 ch2 SO_2 in Comp 7

1148 reading 12.4 ppm SO_2 ch2 SO_2 in Comp 7

1149 injecting zero ppm NOx ch1 (10s) in Comp 7

1151 reading -0.14 ppm NOx ch1 (10s) in Comp 7

1152 injecting 24.9 ppm NOx ch1 (10s) in Comp 7

1156 reading 25.6 ppm NOx ch1 (10s) in Comp 7

1157 injecting 54.2 NOx ch1 (10s) in Comp 7

1202 reading 54.4 NOx ch1 (10s) in Comp 7

End of Calibrations / END OF TEST

APPENDIX D

FLOW RATES
EPA METHODS 1-4

GALLATIN STEEL SO_2 TEST
FLOW AVERAGES

Cold Duct 1		ACFM	SCFMD	SCFMW
	R1	952974.	834555.	846113.
	R2	962283.	834826.	851927.
	R3	932043.	831991.	848086.
Avg.		949100.	833791.	848709.

Cold Duct 2		ACFMD	SCFMD	SCFMW
	R1	93541.	77357.	78428.
	R2	76467.	69720.	71148.
	R3	83826.	77680.	79183.
Avg.		84611.	74919.	76253.

Hot Duct		ACFM	SCFMD	SCFMW
	R1	395103.	219690.	222732.
	R2	402313.	219601.	224099.
	R3	378720.	237330.	241921.
Avg.		392045.	225540.	229584.

Total Flow	ACFM	SCFMD	SCFMW
	1,425,756.	1,134,250.	1,154,546.

Ambient Air Services, Inc.
Environmental Consultants

106 Ambient Air Way
Starke, Florida 32091

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Volumetric Air-Flow Rates

Plant	Gallatin Steel		
Location	Ghent, Kentucky		
Stack	Cold Duct No. 1		
Run Date	5-4-00		
Run Number	1	**Volume Metered**	31.4
Start Time	0	**Meter Temp (Deg R)**	545.6
Finish Time	0	**Orsat CO2 %**	0
Barometric Pressure	30.03	**Orsat O2 %**	20.9
Stack Diameter (in.)	192	**Orsat CO %**	0
Stack Area sq. ft.	201.062	**Orsat N %**	79.1
Number of Points	12	**Condensate Volume**	9
Avg of SQRT of V.H.	1.3231	**Delta H (inches H2O)**	1.5
Meter Correction (Y)	1	**Stack Pressure**	29.80
Pitot Correction Factor	0.84	**Stack Temp (Deg R)**	592.3

==========

Moisture in stack gas, volume fraction	**0.0136598**
Dry Stack Gas, volume fraction	**0.9863402**
Molecular Weight of Stack Gas (Dry Basis)	**28.84**
Molecular Weight of Stack Gas (Stack conditions)	**28.69**
Specific gravity of Stack Gas Relative to Air	**0.990**
Excess Air (%)	
Average Stack Velocity, FPM	**4739.7**
Actual Stack Gas Flow Rate, ACFM	**952974**
Actual Stack Gas Flow Rate, (Dry) ACFMD	**939957**
Stack Gas Flow Rate (Standard conditions), SCFMD	**834555**
Stack Gas Flow Rate (Standard conditions), SCFMW	**846112.73**

Ambient Air Services, Inc.
Environmental Consultants

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Volumetric Air-Flow Rates

Plant	Gallatin Steel		
Location	Ghent, Kentucky		
Stack	Cold Duct No. 1		
Run Date	5-4-00		
Run Number	2	**Volume Metered**	31.79
Start Time	0	**Meter Temp (Deg R)**	549.0
Finish Time	0	**Orsat CO2 %**	0
Barometric Pressure	30.03	**Orsat O2 %**	20.9
Stack Diameter (in.)	192	**Orsat CO %**	0
Stack Area sq. ft.	201.062	**Orsat N %**	79.1
Number of Points	12	**Condensate Volume**	13.4
Avg of SQRT of V.H.	1.3321	**Delta H (inches H2O)**	1.5
Meter Correction (Y)	1	**Stack Pressure**	29.85
Pitot Correction Factor	0.84	**Stack Temp (Deg R)**	595

==========

Moisture in stack gas, volume fraction	**0.0200732**
Dry Stack Gas, volume fraction	**0.9799268**
Molecular Weight of Stack Gas (Dry Basis)	**28.84**
Molecular Weight of Stack Gas (Stack conditions)	**28.62**
Specific gravity of Stack Gas Relative to Air	**0.987**
Excess Air (%)	
Average Stack Velocity, FPM	**4786.0**
Actual Stack Gas Flow Rate, ACFM	**962283**
Actual Stack Gas Flow Rate, (Dry) ACFMD	**942967**
Stack Gas Flow Rate (Standard conditions), SCFMD	**834826**
Stack Gas Flow Rate (Standard conditions), SCFMW	**851926.87**

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Volumetric Air-Flow Rates

Plant	Gallatin Steel		
Location	Ghent, Kentucky		
Stack	Cold Duct No. 1		
Run Date	5-4-00		
Run Number	3	**Volume Metered**	31.196
Start Time	0	**Meter Temp (Deg R)**	546.0
Finish Time	0	**Orsat CO2 %**	0
Barometric Pressure	30.03	**Orsat O2 %**	20.9
Stack Diameter (in.)	192	**Orsat CO %**	0
Stack Area sq. ft.	201.062	**Orsat N %**	79.1
Number of Points	12	**Condensate Volume**	12.5
Avg of SQRT of V.H.	1.3087	**Delta H (inches H2O)**	1.5
Meter Correction (Y)	1	**Stack Pressure**	29.87
Pitot Correction Factor	0.84	**Stack Temp (Deg R)**	579.3

==========

Moisture in stack gas, volume fraction	**0.0189781**
Dry Stack Gas, volume fraction	**0.9810219**
Molecular Weight of Stack Gas (Dry Basis)	**28.84**
Molecular Weight of Stack Gas (Stack conditions)	**28.63**
Specific gravity of Stack Gas Relative to Air	**0.988**
Excess Air (%)	
Average Stack Velocity, FPM	**4635.6**
Actual Stack Gas Flow Rate, ACFM	**932043**
Actual Stack Gas Flow Rate, (Dry) ACFMD	**914355**
Stack Gas Flow Rate (Standard conditions), SCFMD	**831991**
Stack Gas Flow Rate (Standard conditions), SCFMW	**848086.1**

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Volumetric Air-Flow Rates

Plant	Gallatin Steel		
Location	Ghent, Kentucky		
Stack	Cold Duct No. 2		
Run Date	5-4-00		
Run Number	1	**Volume Metered**	31.4
Start Time	0	**Meter Temp (Deg R)**	545.6
Finish Time	0	**Orsat CO2 %**	0
Barometric Pressure	30.03	**Orsat O2 %**	20.9
Stack Diameter (in.)	120	**Orsat CO %**	0
Stack Area sq. ft.	78.540	**Orsat N %**	79.1
Number of Points	16	**Condensate Volume**	9
Avg of SQRT of V.H.	0.3231	**Delta H (inches H2O)**	1.5
Meter Correction (Y)	1	**Stack Pressure**	29.88
Pitot Correction Factor	0.84	**Stack Temp (Deg R)**	628.9

==========

Moisture in stack gas, volume fraction	**0.0136598**
Dry Stack Gas, volume fraction	**0.9863402**
Molecular Weight of Stack Gas (Dry Basis)	**28.84**
Molecular Weight of Stack Gas (Stack conditions)	**28.69**
Specific gravity of Stack Gas Relative to Air	**0.990**
Excess Air (%)	
Average Stack Velocity, FPM	**1191.0**
Actual Stack Gas Flow Rate, ACFM	**93541**
Actual Stack Gas Flow Rate, (Dry) ACFMD	**92263**
Stack Gas Flow Rate (Standard conditions), SCFMD	**77357**
Stack Gas Flow Rate (Standard conditions), SCFMW	**78428.315**

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Volumetric Air-Flow Rates

Plant	Gallatin Steel		
Location	Ghent, Kentucky		
Stack	Cold Duct No. 2		
Run Date	5-4-00		
Run Number	2	**Volume Metered**	31.79
Start Time	0	**Meter Temp (Deg R)**	549.0
Finish Time	0	**Orsat CO2 %**	0
Barometric Pressure	30.03	**Orsat O2 %**	20.9
Stack Diameter (in.)	120	**Orsat CO %**	0
Stack Area sq. ft.	78.540	**Orsat N %**	79.1
Number of Points	16	**Condensate Volume**	13.4
Avg of SQRT of V.H.	0.2778	**Delta H (inches H2O)**	1.5
Meter Correction (Y)	1	**Stack Pressure**	29.89
Pitot Correction Factor	0.84	**Stack Temp (Deg R)**	566.9

==========

Moisture in stack gas, volume fraction	**0.0200732**
Dry Stack Gas, volume fraction	**0.9799268**
Molecular Weight of Stack Gas (Dry Basis)	**28.84**
Molecular Weight of Stack Gas (Stack conditions)	**28.62**
Specific gravity of Stack Gas Relative to Air	**0.987**
Excess Air (%)	
Average Stack Velocity, FPM	**973.6**
Actual Stack Gas Flow Rate, ACFM	**76467**
Actual Stack Gas Flow Rate, (Dry) ACFMD	**74932**
Stack Gas Flow Rate (Standard conditions), SCFMD	**69720**
Stack Gas Flow Rate (Standard conditions), SCFMW	**71148.169**

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Volumetric Air-Flow Rates

Plant	Gallatin Steel		
Location	Ghent, Kentucky		
Stack	Cold Duct No. 2		
Run Date	5-4-00		
Run Number	3	**Volume Metered**	31.196
Start Time	0	**Meter Temp (Deg R)**	546.0
Finish Time	0	**Orsat CO2 %**	0
Barometric Pressure	30.03	**Orsat O2 %**	20.9
Stack Diameter (in.)	120	**Orsat CO %**	0
Stack Area sq. ft.	78.540	**Orsat N %**	79.1
Number of Points	16	**Condensate Volume**	12.5
Avg of SQRT of V.H.	0.3070	**Delta H (inches H2O)**	1.5
Meter Correction (Y)	1	**Stack Pressure**	29.89
Pitot Correction Factor	0.84	**Stack Temp (Deg R)**	558.4

==========

Moisture in stack gas, volume fraction	**0.0189781**
Dry Stack Gas, volume fraction	**0.9810219**
Molecular Weight of Stack Gas (Dry Basis)	**28.84**
Molecular Weight of Stack Gas (Stack conditions)	**28.63**
Specific gravity of Stack Gas Relative to Air	**0.988**
Excess Air (%)	
Average Stack Velocity, FPM	**1067.3**
Actual Stack Gas Flow Rate, ACFM	**83826**
Actual Stack Gas Flow Rate, (Dry) ACFMD	**82235**
Stack Gas Flow Rate (Standard conditions), SCFMD	**77680**
Stack Gas Flow Rate (Standard conditions), SCFMW	**79182.742**

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Volumetric Air-Flow Rates

Plant	Gallatin Steel		
Location	Ghent, Kentucky		
Stack	Hot Duct		
Run Date	5-4-00		
Run Number	1	**Volume Metered**	31.4
Start Time	0	**Meter Temp (Deg R)**	545.6
Finish Time	0	**Orsat CO2 %**	0
Barometric Pressure	30.03	**Orsat O2 %**	20.9
Stack Diameter (in.)	120	**Orsat CO %**	0
Stack Area sq. ft.	78.540	**Orsat N %**	79.1
Number of Points	16	**Condensate Volume**	9
Avg of SQRT of V.H.	1.1190	**Delta H (inches H2O)**	1.5
Meter Correction (Y)	1	**Stack Pressure**	29.68
Pitot Correction Factor	0.84	**Stack Temp (Deg R)**	929.1

==========

Moisture in stack gas, volume fraction	**0.0136598**
Dry Stack Gas, volume fraction	**0.9863402**
Molecular Weight of Stack Gas (Dry Basis)	**28.84**
Molecular Weight of Stack Gas (Stack conditions)	**28.69**
Specific gravity of Stack Gas Relative to Air	**0.990**
Excess Air (%)	
Average Stack Velocity, FPM	**5030.6**
Actual Stack Gas Flow Rate, ACFM	**395103**
Actual Stack Gas Flow Rate, (Dry) ACFMD	**389706**
Stack Gas Flow Rate (Standard conditions), SCFMD	**219690**
Stack Gas Flow Rate (Standard conditions), SCFMW	**222732.48**

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Volumetric Air-Flow Rates

Plant	Gallatin Steel		
Location	Ghent, Kentucky		
Stack	Hot Duct		
Run Date	5-4-00		
Run Number	2	**Volume Metered**	31.79
Start Time	0	**Meter Temp (Deg R)**	549.0
Finish Time	0	**Orsat CO2 %**	0
Barometric Pressure	30.03	**Orsat O2 %**	20.9
Stack Diameter (in.)	120	**Orsat CO %**	0
Stack Area sq. ft.	78.540	**Orsat N %**	79.1
Number of Points	16	**Condensate Volume**	13.4
Avg of SQRT of V.H.	1.1309	**Delta H (inches H2O)**	1.5
Meter Correction (Y)	1	**Stack Pressure**	29.63
Pitot Correction Factor	0.84	**Stack Temp (Deg R)**	938.7

==========

Moisture in stack gas, volume fraction	**0.0200732**
Dry Stack Gas, volume fraction	**0.9799268**
Molecular Weight of Stack Gas (Dry Basis)	**28.84**
Molecular Weight of Stack Gas (Stack conditions)	**28.62**
Specific gravity of Stack Gas Relative to Air	**0.987**
Excess Air (%)	
Average Stack Velocity, FPM	**5122.4**
Actual Stack Gas Flow Rate, ACFM	**402313**
Actual Stack Gas Flow Rate, (Dry) ACFMD	**394237**
Stack Gas Flow Rate (Standard conditions), SCFMD	**219601**
Stack Gas Flow Rate (Standard conditions), SCFMW	**224099.38**

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Volumetric Air-Flow Rates

Plant	Gallatin Steel		
Location	Ghent, Kentucky		
Stack	Hot Duct		
Run Date	5-4-00		
Run Number	3	**Volume Metered**	31.196
Start Time	0	**Meter Temp (Deg R)**	546.0
Finish Time	0	**Orsat CO2 %**	0
Barometric Pressure	30.03	**Orsat O2 %**	20.9
Stack Diameter (in.)	120	**Orsat CO %**	0
Stack Area sq. ft.	78.540	**Orsat N %**	79.1
Number of Points	16	**Condensate Volume**	12.5
Avg of SQRT of V.H.	1.1406	**Delta H (inches H2O)**	1.5
Meter Correction (Y)	1	**Stack Pressure**	29.57
Pitot Correction Factor	0.84	**Stack Temp (Deg R)**	816.9

==========

Moisture in stack gas, volume fraction	**0.0189781**
Dry Stack Gas, volume fraction	**0.9810219**
Molecular Weight of Stack Gas (Dry Basis)	**28.84**
Molecular Weight of Stack Gas (Stack conditions)	**28.63**
Specific gravity of Stack Gas Relative to Air	**0.988**
Excess Air (%)	
Average Stack Velocity, FPM	**4822.0**
Actual Stack Gas Flow Rate, ACFM	**378720**
Actual Stack Gas Flow Rate, (Dry) ACFMD	**371533**
Stack Gas Flow Rate (Standard conditions), SCFMD	**237330**
Stack Gas Flow Rate (Standard conditions), SCFMW	**241921.22**

APPENDIX E

- MOISTURE RUN DATA SHEETS
- FLOW TRAVERSE DATA SHEETS
- PITOT TUBES - POST TEST CALIBRATION CHECK
- THERMOCOUPLE - POST TEST CALIBRATION CHECK
- GAS METER POST TEST CALIBRATION

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TEST ID _____ PAGE 1 OF 1

Plant Gallatin Steel Source Baghouse
Plant Location Ghent Kentucky
Type of Sampling Train EPA Method 4
Type of Samples Moisture
Date 5-4-00 Run No. 1
Time Start 1326 Time End 1356
Sample Time 5.0 min/pt _____ Total Min
Bar. Pressure 30.03 "Hg Stack Pressure NA "Hg
Assumed Moisture 2.0 % FDA 0.98
Weather Overcast Temperature 70° °F
Meter Box No. 3 ΔH 1.5 Y 1.0
Orifice Cf NA Pitot Corr. Factor 0.84
Nozzle Calibration NA _____ " _____
Stack Dimensions More than one stack
Stack Area NA (Effective NA ft²)
Stack Height Approx 40 ft
Stack Diameter: Upstream NA Downstream NA
Port Size NA in Nipple Length NA
Probe Cord Length 100 feet
Remarks _____

Mat'l Processing Rate _____
Gas Meter Readings: Final 73.437 ft³
Initial 42.037 ft³
Net 31.400 ft³
Impingers Vol. Gain 4 ml
Silical Gel No. BH-1 Wt. Gain 5.0
Filter No. NA Total Condensate 9.0 ml

ORSAT

	1	2	3	4	AVG
% CO_2					
% O_2	20.9	20.9	20.9		20.9
% CO					
% N_2					79.1

F_o _____
F_o Range _____

Leak Checks: Meter Box/Pump OK
Orsat Bag NA Gas Sample System NA
Orsat Analyzer FYRITE (AMBIENT)
Pre-test 0.004 CFM 10 "Hg Post-Test 0.005 CFM 10 "Hg
Box Operator COGGINS Probe Holder PETIET
Pyrometer No. 3 Pitot Tube No. NA
Pitot Tube Leak Check: Pretest OK @ 3" @ 15sec
Post-Test(+) OK 3" H_2O 15 SEC
Post-Test(-) OK 3" H_2O 15 SEC

PORT AND TRAVERSE POINT NUMBER	DISTANCE FROM INSIDE STACK WALL (IN)	CLOCK TIME	GAS METER READING (FT^3)	STACK VELOCITY HEAD	METER ORIFICE PRESS. DIFF CALC.	METER ORIFICE PRESS. DIFF ACTUAL	STACK GAS TEMP. (°F)	SAMPLE BOX TEMP. (°F)	LAST IMPINGER TEMP. (°F)	DRY GAS METER TEMP. (°F)	VACUUM ON SAMPLE TRAIN ("Hg)
		5.0	45.9	—	—	1.5	—	—	67	78	6
		10.0	~~45.9~~ 49.8	—	—	1.5	—	—	65	81	6
		15.0	~~49.8~~ 53.1	—	—	1.5	—	—	60	84	6
		20.0	57.7	—	—	1.5	—	—	59	87	6
		25.0	62.9	—	—	1.5	—	—	58	88	6
		30.0	65.7	—	—	1.5	—	—	56	89	6
—		35.0	69.4	—	—	1.5	—	—	56	89	6
		40.0	73.437	—	—	1.5	—	—	57	89	6

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TEST ID _____ PAGE 1 OF 1

Plant Gallatin Steel Source Baghouse
Plant Location Ghent, Kentucky
Type of Sampling Train EPA Method 4
Type of Samples Moisture
Date 5-4-00 Run No. 2
Time Start 1651 Time End 1731
Sample Time 5.0 min/pt 40.0 Total Min
Bar. Pressure 30. "Hg Stack Pressure NA "Hg
Assumed Moisture 1.0 % FDA 0.99
Weather Overcast Temperature 70 °F
Meter Box No. 3 ΔH 1.5 Y 1.0
Nomograph Cf NA Pitot Corr. Factor 0.84
Nozzle Calibration NA NA
Stack Dimensions Rectangular Stack
Stack Area NA (Effective NA ft²)
Stack Height Approx 40 ft
Stack Diameter: Upstream NA Downstream NA
Port Size NA in Nipple Length NA
Probe Cord Length 100
Remarks

Mat'l Processing Rate
Gas Meter Readings: Final 105.608 ft³
Initial 73.818 ft³
Net 31.790 ft³
Impingers Vol. Gain 8 ml
Silical Gel No. BH-2 Wt. Gain 5.4
Filter No. NA Total Condensate 13.4 ml

ORSAT

	1	2	3	4	AVG
% CO_2					
% O_2	20.9	20.9	20.9		20.9
% CO					
% N_2					79.1

F_o _____
F_o Range _____

Leak Checks: Meter Box/Pump OK
Orsat Bag NA Gas Sample System NA
Orsat Analyzer FYRITE (Ambient)
Pre-test 0.007 CFM 10 "Hg Post-Test 0.000 CFM 8 "Hg
Box Operator COGGINS Probe Holder PETIET
Pyrometer No. 3 Pitot Tube No. NA
Pitot Tube Leak Check: Pretest 0.0 @ 3" @ 15 sec
Post-Test(+) OK 3" H_2O 15 sec
Post-Test(-) OK 3" H_2O 15 sec

PORT AND TRAVERSE POINT NUMBER	DISTANCE FROM INSIDE STACK WALL (IN)	CLOCK TIME	GAS METER READING (FT^3)	STACK VELOCITY HEAD	METER ORIFICE PRESS. DIFF CALC.	METER ORIFICE PRESS. DIFF ACTUAL	STACK GAS TEMP. (°F)	SAMPLE BOX TEMP. (°F)	LAST IMPINGER TEMP. (°F)	DRY GAS METER TEMP. (°F)	VACUUM ON SAMPLE TRAIN ("Hg)
		5.0	77.8	—	—	1.5	—	—	66	79	7
		10.0	81.9	—	—	1.5	—	—	64	84	7
		15.0	85.9	—	—	1.5	—	—	61	87	7
		20.0	89.6	—	—	1.5	—	—	60	89	7
		25.0	93.6	—	—	1.5	—	—	58	91	7
		30.0	97.7	—	—	1.5	—	—	58	92	7
—		35.0	101.7	—	—	1.5	—	—	56	95	7
		40.0	105.608	—	—	1.5	—	—	57	95	7

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TEST ID _____ PAGE 1 OF 1

Plant Gallatin Steel Source Bethune
Plant Location GHENT KY
Type of Sampling Train EPA M4
Type of Samples MOISTURE
Date 5/4/00 Run No. 3
Time Start 2108 Time End 2148
Sample Time 5 min/pt 40 Total Min
Bar. Pressure 30.03 "Hg Stack Pressure NA "Hg
Assumed Moisture 1 % FDA 0.99
Weather Cloudy Temperature 70 °F
Meter Box No. 3 ΔH 1.5 Y 1.0
Nomograph Cf NA Pitot Corr. Factor NA
Nozzle Calibration NA NA
Stack Dimensions More than one stack
Stack Area NA (Effective NA ft²)
Stack Height Approx 40 ft
Stack Diameter: Upstream NA Downstream NA
Port Size NA in Nipple Length NA
Probe Cord Length 100 feet
Remarks

Mat'l Processing Rate
Gas Meter Readings: Final 136.884 ft³
Initial 105.688 ft³
Net 31.196 ft³
Impingers Vol. Gain 8 ml
Silical Gel No. BH-Z3 Wt. Gain 814.5 g
Filter No. NA Total Condensate 1285 ml

ORSAT

	1	2	3	4	AVG
% CO_2					
% O_2	20.9	20.9	20.9		20.9
% CO					
% N_2					79.1

F_o _____
F_o Range _____

Leak Checks: Meter Box/Pump OK
Orsat Bag NA Gas Sample System NA
Orsat Analyzer FYRITE
Pre-test 0.002 CFM 10 "Hg Post-Test 0.002 CFM 8 "Hg
Box Operator COGGINS Probe Holder PETIET
Pyrometer No. 3 Pitot Tube No. NA
Pitot Tube Leak Check: Pretest OK @3" @15sec
Post-Test(-) OK 3" H_2O 15 SEC
Post-Test(-) OK 3" H_2O 15 SEC

PORT AND TRAVERSE POINT NUMBER	DISTANCE FROM INSIDE STACK WALL (IN)	CLOCK TIME	GAS METER READING (FT^3)	STACK VELOCITY HEAD	METER ORIFICE PRESS. DIFF CALC.	METER ORIFICE PRESS. DIFF ACTUAL	STACK GAS TEMP. (°F)	SAMPLE BOX TEMP. (°F)	LAST IMPINGER TEMP. (°F)	DRY GAS METER TEMP. (°F)	VACUUM ON SAMPLE TRAIN ("Hg)
		5.0	109.5	—	—	1.5	154	—	67	77	6
		10.0	113.4	—	—	1.5	147	—	65	81	6
		15.0	117.4	—	—	1.5	148	—	63	83	6
		20.0	121.3	—	—	1.5	149	—	60	86	6
		25.0	125.3	—	—	1.5	150	—	59	88	6
		30.0	129.1	—	—	1.5	152	—	57	90	6
—		35.0	133.0	—	—	1.5	148	—	56	91	6
		40.0	136.884	—	—	1.5	149	—	55	92	6

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PRELIMINARY VELOCITY TRAVERSE

PLANT Gallatin Steel
DATE 5-4-00
LOCATION COLD DUCT NO. 1
STACK I.D. 192.0"
BAROMETRIC PRESSURE, in.Hg 30.03
STACK GAUGE PRESSURE, in.H_2O
OPERATORS COGGINS / PETIET

TRAVERSE POINT NUMBER Static -3.1	VELOCITY HEAD (Δp_s), in.H_2O RUN1	STACK TEMPERATURE (T_s), °F
1-1	1.69	140
2	1.75	138
3	1.75	134
4	1.75	136
5	1.80	137
6	1.70	138
2-1	1.85	127
2	1.77	128
3	1.75	127
4	1.75	128
5	1.75	126
6	1.70	128
RUN3 1-1	1.68	120
2	1.61	119
Static 3	1.64	119
-2.2 4	1.75	118
5	1.82	118
6	1.82	118
2-1	1.93	119
2	1.70	119
3	1.87	120
4	1.67	120
5	1.56	121
6	1.62	121

SCHEMATIC OF TRAVERSE POINT LAYOUT

TRAVERSE POINT NUMBER Static -2.4	VELOCITY HEAD (Δp_s), in.H_2O RUN 2	STACK TEMPERATURE (T_s), °F
1-1	1.77	132
2	1.75	133
3	1.75	133
4	2.0	133
5	1.55	126
6	1.30	130
2-1	2.0	137
2	1.9	136
3	2.1	140
4	1.8	140
5	1.7	140
6	1.75	140
PTD-1		
Pitot	pos 0.0 at 3 inch	15 sec
leak ck	neg 0.0 at 3 inch	15 sec

AAS Inc. AMBIENT AIR SERVICES INCORPORATED
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PRELIMINARY VELOCITY TRAVERSE

PLANT Gallatin Steel
DATE 5-4-00
LOCATION COLD DUCT NO.2
STACK I.D. 120.0"
BAROMETRIC PRESSURE, in.Hg 30.03
STACK GAUGE PRESSURE, in.H_2O
OPERATORS COGGINS / PETIET

TRAVERSE POINT NUMBER Static -2.0	VELOCITY HEAD (Δp_s), in.H_2O RUN1	STACK TEMPERATURE (T_s), °F
1-1	0.15	156
2	0.12	160
3	0.12	161
4	0.12	163
5	0.10	160
6	0.10	165
7	0.09	164
8	0.09	160
2-1	0.09	174
2	0.10	186
3	0.09	187
4	0.12	178
5	0.10	178
6	0.10	170
7	0.10	168
8	0.09	172
RUN 3	0.10	97
1-1	0.09	98
Static 2	0.10	98
-1.8 3	0.10	98
4	0.10	98
5	0.09	99
6	0.08	99
7	0.08	99
8		

SCHEMATIC OF TRAVERSE POINT LAYOUT

TRAVERSE POINT NUMBER Static -1.9	VELOCITY HEAD (Δp_s), in.H_2O RUN 2	STACK TEMPERATURE (T_s), °F
1-1	0.11	100
2	0.09	102
3	0.09	104
4	0.08	108
5	0.07	109
6	0.07	109
7	0.07	108
8	0.07	108
2-1	0.07	107
2	0.08	109
3	0.08	108
4	0.07	107
5	0.07	108
6	0.08	108
7	0.07	107
8	0.07	108
2-1	0.09	97
2	0.09	98
3	0.09	98
4	0.10	99
5	0.10	99
6	0.10	99
7	0.10	99
8	0.10	99
PT 10-1		

leak ck pos 0.0 @3" @15sec
neg 0.0 @3" @15sec

AAS Inc. AMBIENT AIR SERVICES INCORPORATED
ENVIRONMENTAL CONSULTANTS

PRELIMINARY VELOCITY TRAVERSE

PLANT Gallatin Steel
DATE 5-4-00
LOCATION HOT DUCT
STACK I.D. 120.0"
BAROMETRIC PRESSURE, in.Hg 30.03
STACK GAUGE PRESSURE, in.H_2O -4.8
OPERATORS COGGINS PELTIET

Pitot 10-2.
leak ck 0.0 @ 3" @ 15 sec
0.0 @ 3" @ 15 sec

TRAVERSE POINT NUMBER Static -4.8	VELOCITY HEAD (Δp_s), in.H_2O RUN1	STACK TEMPERATURE (T_s), °F
1-1	1.22	437
2	1.20	442
3	1.49	476
4	1.50	478
5	1.52	483
6	1.40	478
7	1.27	463
8	1.10	456
2-1	1.20	497
2	1.30	453
3	1.15	468
4	1.05	474
5	1.20	481
6	1.25	477
7	1.15	472
8	1.10	470
1-1	1.18	329
2	1.31	330
3	1.40	328
4	1.46	341
5	1.43	365
6	1.47	353
7	1.49	352
8	1.23	353

Runs static 6.2

SCHEMATIC OF TRAVERSE POINT LAYOUT

TRAVERSE POINT NUMBER Static -5.4	VELOCITY HEAD (Δp_s), in.H_2O RUN2	STACK TEMPERATURE (T_s), °F
1-1	1.25	455
2	1.35	478
3	1.45	485
4	1.45	493
5	1.25	487
6	1.20	488
7	1.25	479
8	1.20	478
1-1	1.10	479
2	1.20	458
3	1.30	478
4	1.40	478
5	1.45	481
6	1.30	485
7	1.25	479
8	1.10	478
2-1	1.28	358
2	1.26	376
3	1.26	373
4	1.22	373
5	1.25	369
6	1.21	368
7	1.20	373
8	1.20	370

Runs

PITOT TUBE CALIBRATION MEASUREMENTS

DATE CALIBRATED 5-16-00 PITOT TUBE PT 10-1

Pitot tube assembly level? ✓ Yes _____ No

Pitot tube openings damaged? _____ Yes (explain below) _____ No ✓

α_1 - 1.0 ° (<10°), α_2 - 1.0 ° (<10°), β_1 - 0.5 ° (<5°),

β_2 - 0.5 ° (<5°)

γ - 0.5 °, θ - 0.5 °, A - 1.094 in. - (Pa + Pb)

z - A sin γ - 0.01 in.; <0.32 / <1/8 in.

w - A sin θ - 0.01 in.; <0.08 / <1/32 in.

P_a 0.547 in. P_b 0.547 in. D_t - 0.375

Calibration required? _____ Yes _____ No ✓

AAS Inc. AMBIENT AIR SERVICES INCORPORATED
ENVIRONMENTAL CONSULTANTS

PITOT TUBE CALIBRATION MEASUREMENTS

DATE CALIBRATED 5-16-00 PITOT TUBE PT10-2

Pitot tube assembly level? ✓ Yes _____ No

Pitot tube openings damaged? _____ Yes (explain below) ✓ No

α_1 - 1.0 ° (<10°), α_2 - 1.0 ° (<10°), β_1 - 1.0 ° (<5°),

β_2 - 0.5 ° (<5°)

γ - 1.0 °, θ - 1.0 °, A - 1.024 in. - (Pa + Pb)

z - A sin γ - 0.018 in.; <0.32 / <1/8 in.

w - A sin θ - 0.018 in.; <0.08 / <1/32 in.

P_a 0.512 in. P_b 0.512 in. D_t - 0.375"

Calibration required? _____ Yes ✓ No

PITOT TUBE CALIBRATION MEASUREMENTS

DATE CALIBRATED 5-16-00 PITOT TUBE PT12-1

Pitot tube assembly level? ✓ Yes _____ No

Pitot tube openings damaged? _____ Yes (explain below) ✓ No

α_1 - 2.0 ° (<10°), α_2 - 2.0 ° (<10°), β_1 - 1.0 ° (<5°),

β_2 - 1.0 ° (<5°)

γ - 1.0 °, θ - 1.5 °, A - 1.049 in. - (Pa + Pb)

z - A sin γ - 0.018 in.; <0.32 / <1/8 in.

w - A sin θ - 0.027 in.; <0.08 / <1/32 in.

P_a 0.524 in. P_b 0.525 in. D_t - 0.375"

Calibration required? _____ Yes ✓ No

AMBIENT AIR SERVICES, INC.
106 Ambient Air Way
Starke, Florida

THERMOCOUPLE CALIBRATION FORM

Date 5-16-00 Time 0916
Ambient Temperature 83°F Source LAB
Barometric Pressure 29.39 Source LAB
Technician's Signature Earl Coggins

Standard Thermometer Type Mercury in Glass
Manufacturer ERTCO
Serial Number 64619
Pyrometer Manufacturer Omega Model 9414
Serial Number BB3014-3 Meter Box 3

TEMPERATURE SOURCE (A)		ICE			Ambient Air			Boiling H_2O					
REFERENCE THERMOMETER	Actual Reading	32°F			83°F			212°F					
	Corrected Temperature												
CALIBRATED THERMOCOUPLE													
Serial Number	Location	Indicated Temp.	Difference (B)	Percent Diff. (C)	Indicated Temp.	Difference	Percent Diff.	Indicated Temp.	Difference	Percent Diff.	Indicated Temp.	Difference	Percent Diff.
PT12-1	Stack	32	0		83	0		213	1				
NA	Filter												
TT3	Impinger	32	0		83	0		213	1				
3in	Meter In	32	0		84	1		213	1				
3out	Meter Out	32	0		84	1		214	2				
PT10-1	Stack	32	0		84	1		213	1				
PT10-2	Stack	32	0		84	1		214	2				

Comments:

Calibration Tolerances Stack = 1.5% of value, Filter Box = ±5.4°F, Impinger = ±2°F, Meter = ±5.4°F (40CFR Pt 60, App. A Method 5, and QA Handbook Section 3.4, Method 5, page 13, Rev. 0)

(A) Type of calibration system used

(B) Reference - Indicated = Difference

(C) $\left[\frac{\text{(ref. temp. °F + 460) - (indicated temp. °F + 460)}}{\text{(reference temp. °F + 460)}} \right] \times 100$

AASI 68A

POSTTEST DRY GAS METER CALIBRATION DATA (ENGLISH UNITS)

Test numbers: all Date: 5-16-00 Meter Box number: 3

Barometric Pressure: 29.89 inches Hg. Dry Gas Meter Number: 3 Pretest Y: 0.99

Plant: Gallatin Steel Location: Ghent, KY

Orifice manomtr setting (DH), inches H20	Gas volume		Temperature				Time in minutes	Vacuum setting inches Hg	Yi
	Wet test meter (Vw), cu.ft.	Dry gas meter (Vd), cu.ft.	Wet test meter (Tw), deg F	Dry gas meter					
				Inlet (Tdi), deg F	Outlet (Tdo), deg F	Average (Td), deg F			
1.50	11.066	11.362	84.25	107.5	88.0	97.75	14.73	12.0	0.9944
1.50	12.611	12.949	85.25	109.5	89.5	99.50	16.77	12.0	0.9956
1.50	16.631	17.110	85.50	113.0	91.0	102.00	21.06	12.0	0.9977
									1.00

If there is only one thermometer on the dry gas meter, record the temperature under Td

Vw= Gas volume passing through the wet test meter, in cubic feet
Vd= Gas volume passing through the dry gas meter, in cubic feet
Tw= Temperature of the gas in the wet test meter, degrees farenheit
Tdi= Temperature of the inlet gas of the dry gas meter, degrees farenheit
Tdo= Temperature of the outlet gas of the dry gas meter, degrees farenheit
Td= Average temperature of the gas in the dry gs meter, obtained by the average of Tdi and Tdo, degrees farenheit
DH= Pressure differential across orifice, inches H2O
Yi= Ratio of accuracy of wet test meter to dry gas meter for each run.
Y= Average ratio of accuracy of wet test meter to dry gas meter for all three runs; tolerance = pretest Y plus/minus 0.05Y
Pb= Barometric pressure, inches Mercury
Time= Time of calibration run, in minutes.

APPENDIX F

- PRODUCTION DATA

- TEST NOTIFICATION LETTER

Gallatin Steel Company - Heat Data for May 4, 2000

	Run 1	Run 1	Run 1	Run 1	Run 2	Run 2	Run 2	Run 2	Run 3	Run 3	Run 3	Run 3	
				12:55 to 15:55				16:30 to 19:15				20:15 to 22:45	
Date	5/4/00	5/4/00	5/4/00		5/5/00	5/5/00	5/5/00		5/5/00	5/5/00	5/5/00		
Heat Number	A13562	C13217	A13563		A13564	C13219	A13565		A13566	C13221	A13567		
Start of Heat - Power On (time)	12:52	13:44	14:38		16:32	17:23	18:24		20:16	21:08	22:07		
1st Charge (time)	12:48	13:07	14:11		15:52	16:37	17:40		19:36	20:21	21:46		
2nd Charge (time)	0	0:00	0:00		0:00	0:00	0:00		0:00	0:00	0:00		
Power On Time (min.)	49	47	48		50	48	48		49	47	64		
Tap Time	13:59	14:45	15:37		17:29	18:22	19:17		21:09	22:07	1:24*		
Tap to Tap (minutes)	59	45	51		61	52	55		56	58	196*		
Total Scrap Weight (pounds)	391800	404000	401300		395700	397400	397900		417700	423500	409300		
Charge Carbon (pounds)	1209	1223	1217		1201	1202	1214		1207	1213	1207		
Charge Lime (pounds)	7611	7825	7617		7617	7615	7603		7611	7406	7603		
Dolo Lime (pounds)	2712	2713	2722		2722	2718	2714		2706	2700	2708		Average
Liquid Steel Tons	180.0	185.0	179.7	544.7	181.3	185.0	178.1	544.4	193.5	185.0	184.1	562.6	Melt
Run Time (minutes):				180				165				170	Tons/Hour
Tons per Hour				182				198				199	193
Delays Over 10 Minutes											*Testing	(170 min above	
											ended at	includes	
											22:45	extra	
											which was	20 minutes	
											20 min.	for	
											prior to	expected	
											expected	end of heat)	
											end of heat		
											(Heat was		
											delayed due		
											to lance		
											problem)		

Gallatin Steel Company - Fan Amps, Damper Positions and Furnace Static Pressure Readings for May 4, 2000

RUN 1:	MA 1 RUNNING AMPS	DP14A % OPEN	MA 2 RUNNING AMPS	DP14B % OPEN	MA 3 RUNNING AMPS	DP14C % OPEN	MA 4 RUNNING AMPS	DP14D % OPEN	MA 5 RUNNING AMPS	DP14E % OPEN	HG 1 RUNNING AMPS	DP13A % OPEN	HG 2 RUNNING AMPS	DP13B % OPEN	HG 3 RUNNING AMPS	DP13C % OPEN	DP 1A % OPEN	DP 2A % OPEN	DP 2 % OPEN	DP 1 % OPEN	DP 4 % OPEN	DP 4A % OPEN	DP 7A % OPEN	DP 7C % OPEN	DP 8 % OPEN	DP 7B % OPEN	DP 3 C&D % OPEN	DP 3 A&B % OPEN	DP 6 % OPEN	DP 5 % OPEN	DP 9 % OPEN	EAF C ROOF PRESSURE PT 2 inches / 100	EAF A ROOF PRESSURE PT 1 inches /100
12:55	129	10	111	100	126	100	118	100	121	100	0	2	47	100	47	100	31	1	7	40	21	0	0	63	2	0	100	100	4	23	2	-0.02	-0.08
13:10	118	10	102	100	116	100	110	100	112	100	0	2	43	100	43	100	10	1	8	40	21	0	0	63	2	0	100	100	4	12	2	0.02	-0.13
13:25	120	100	106	99	121	100	114	100	116	100	0	2	41	100	41	100	20	1	7	95	21	0	0	0	2	0	100	100	4	22	2	-0.04	-0.07
13:40	118	100	106	100	121	100	114	100	118	100	0	2	41	100	39	100	20	2	7	86	21	0	0	0	2	0	100	100	4	22	2	-0.03	-0.07
13:55	132	100	113	100	128	100	119	100	121	100	0	2	46	100	46	100	31	1	7	29	21	0	0	0	2	0	100	100	4	22	2	-0.05	-0.15
14:10	121	100	111	99	124	100	118	100	118	100	0	2	45	100	43	100	91	1	8	10	21	0	0	0	2	0	100	100	4	12	2	0.02	-0.01
14:25	121	100	106	100	121	100	114	100	116	100	0	2	45	100	43	100	91	2	7	19	21	0	0	0	2	0	100	100	4	23	2	-0.01	-0.05
14:40	123	100	111	100	124	100	114	100	118	100	0	2	46	100	46	100	31	1	8	40	95	0	0	0	2	0	100	100	4	22	2	-0.02	-0.08
14:55	120	100	106	99	121	100	113	100	116	100	0	2	43	100	42	100	10	1	7	95	21	0	0	0	2	0	100	100	4	13	2	0.01	-0.05
15:10	121	100	107	99	124	100	114	100	116	100	0	2	42	100	41	100	20	1	7	95	21	0	0	0	2	0	100	100	4	23	2	-0.03	0.02
15:25	118	100	106	100	121	100	114	100	116	100	0	2	41	100	41	100	20	1	7	95	43	0	0	0	2	0	100	100	4	23	2	-0.03	0.01
15:40	123	100	111	99	124	100	118	100	120	100	0	2	49	100	47	100	91	1	8	9	21	0	0	0	2	0	100	100	4	12	2	-0.08	-0.03
15:55	121	100	107	100	124	100	116	100	118	100	0	2	45	100	43	100	91	1	7	19	21	0	0	0	2	0	100	100	4	23	2	0.05	-0.07
RUN 2:																																	
16:30	123	100	107	100	121	100	114	100	116	100	0	2	46	100	47	100	10	1	8	20	21	0	0	0	2	0	100	100	4	13	2	-0.03	-0.13
16:45	123	100	107	100	124	100	114	100	116	100	0	2	45	100	43	100	20	1	8	95	21	0	0	0	2	0	100	100	4	23	2	-0.03	0.03
17:00	118	100	106	98	121	100	113	100	116	100	0	2	41	100	41	100	20	1	7	95	21	0	0	0	2	0	100	100	4	23	2	-0.03	0.11
17:15	120	100	106	100	121	100	114	100	116	100	0	2	41	100	41	100	20	1	8	95	20	0	0	0	2	0	100	100	4	23	2	-0.03	-0.01
17:30	117	100	107	100	124	100	116	100	118	100	0	2	45	100	45	100	91	1	7	20	21	0	0	0	2	0	100	100	4	23	2	-0.01	-0.05
17:45	121	100	107	99	122	100	114	100	116	100	0	2	45	100	44	100	91	1	7	19	29	0	0	0	2	0	100	100	4	12	2	0.01	-0.06
18:00	121	100	106	99	121	100	114	100	116	100	0	2	45	100	43	100	91	1	7	20	20	0	0	0	2	0	100	100	4	23	2	0.05	-0.06
18:15	121	100	107	100	124	100	116	100	116	100	0	2	45	100	44	100	91	1	7	19	20	0	0	0	2	0	100	100	4	22	2	-0.01	-0.06
18:30	123	100	111	100	126	100	118	100	121	100	0	2	47	100	47	100	11	1	8	49	20	0	0	0	2	0	100	100	4	12	2	-0.02	-0.09
18:45	121	100	107	99	122	100	114	100	118	100	0	2	43	100	43	100	20	2	7	95	20	0	0	0	2	0	100	100	4	22	2	-0.03	-0.08
19:00	120	100	106	100	121	100	114	100	116	100	0	2	41	100	41	100	20	1	8	95	51	0	0	0	2	0	100	100	4	22	2	-0.03	0.04
19:15	125	100	111	100	124	100	118	100	121	100	0	2	46	100	46	100	60	1	7	19	21	0	0	0	2	0	100	100	4	22	2	-0.05	-0.03
RUN 3																																	
20:15	127	100	113	100	124	100	116	100	118	100	0	2	49	100	49	100	11	2	7	20	21	0	0	0	2	0	100	100	4	13	2	-0.03	-0.14
20:30	123	100	111	100	124	100	118	100	121	100	0	2	45	100	45	100	20	2	7	95	21	0	0	0	2	0	100	100	4	22	2	-0.05	0.07
20:45	123	100	107	100	124	100	118	100	121	100	0	2	45	100	43	100	20	1	7	94	21	0	0	0	2	0	100	100	4	22	2	-0.05	-0.12
21:00	120	100	106	100	121	100	114	100	116	100	0	2	41	100	41	100	20	1	8	40	20	0	0	0	2	0	100	100	4	22	2	-0.05	-0.03
21:15	129	100	111	100	126	100	118	100	120	100	0	2	49	100	47	100	63	1	7	10	66	0	0	0	2	0	100	100	4	23	2	-0.09	-0.02
21:30	123	100	111	100	124	100	114	100	118	100	0	2	45	100	43	100	91	1	7	10	21	0	0	0	2	0	100	100	4	12	2	0.04	-0.02
21:45	121	100	107	99	122	100	114	100	118	100	0	2	45	100	43	100	91	1	7	10	59	0	0	0	2	0	100	100	4	12	2	0.03	0.00
22:00	129	100	111	100	124	100	118	100	118	100	0	2	46	100	46	100	10	1	7	44	21	0	0	0	2	0	100	100	4	13	2	0.02	-0.13
22:15	130	100	114	100	130	100	119	100	121	100	0	2	49	100	48	100	21	1	8	20	20	0	0	0	2	0	100	100	4	23	2	-0.04	-0.15
22:30	123	100	107	100	124	100	116	100	116	100	0	2	42	100	42	100	20	2	7	94	21	0	0	0	2	0	100	100	4	22	2	-0.03	0.05
22:45	125	100	111	100	124	100	118	100	121	100	0	2	45	100	43	100	22	2	7	20	20	0	0	0	2	0	100	100	4	22	2	-0.04	-0.10

Damper Legend

DP1A	C Shell water cooled damper
DP2A	C Shell slag damper
DP2	A Shell slag damper
DP1	A Shell water cooled damper
DP4	LMF roof
DP4A	LMF dilution air
DP7A	Ladle tearout
DP7C	Ladle drying
DP8	Ladle dump
DP7B	Ladle preheat
DP3D/DP3C	C Shell canopy
DP3B/DP3A	A Shell canopy
DP5	Caster canopy
DP9	Tundish deskull

MONTH _____ | # MAGNAHELIC CHECKS | YEAR _____

RUN1

PRESSURE DIFFERENTIAL IN COMPARTMENTS

COMP. NUMBER	DATE 5/4/00	DATE / /	DATE / /	DATE / /	DATE / /	DATE / /	DATE / /
TIME	12:55	13:10	13:25	13:40	13:55	14:10	14:25
1	6.5	Cleaning	7.0	6.9	7.0	6.9	7.0
2	6.4	6.5	6.5	6.9	6.5	6.5	6.5
3	6.5	6.9	6.9	6.9	6.9	6.9	6.9
4	6.6	6.9	6.9	Cleaning	7.0	6.9	7.0
5	6.9	7.0	7.0	7.2	7.0	6.9	7.0
6	7.2	7.2	7.2	7.9	7.5	Cleaning	7.5
7	7.0	7.0	7.0	7.5	7.0	6.5	7.2
8	7.0	7.2	7.0	7.5	7.0	7.0	7.2
9	6.6	7.0	6.9	7.2	6.9	7.0	7.0
10	6.5	7.2	6.9	7.5	6.9	7.0	7.0
11	6.4	6.9	6.5	7.0	6.5	6.5	6.9
12	6.9	7.0	7.0	7.2	7.0	7.0	7.0
13	7.1	7.2	7.2	7.5	7.5	7.2	7.5
14	6.9	7.0	7.0	7.2	7.0	6.9	7.0
15	6.1	6.5	6.5	6.9	6.5	6.5	6.9
16	CLEANING	7.2	7.2	7.2	7.2	7.0	7.2
17	7.5	6.2	7.2	6.5	6.2	6.2	6.5
18	7.1	7.2	Cleaning	7.5	7.0	7.2	7.2
19	6.5	6.9	7.0	6.9	6.5	6.5	6.9
20	6.5	6.5	7.0	7.0	6.9	6.9	6.9
21	7.0	7.0	7.5	7.2	Cleaning	6.9	7.0
22	7.5	7.5	8.0	7.9	7.9	7.2	7.5
23	6.3	6.2	6.5	6.2	6.5	6.0	Cleaning
24	7.5	7.5	7.5	7.5	7.5	7.2	7.2

MONTH _____	MAGNAHELIC CHECKS	YEAR _____

Run 1

PRESSURE DIFFERENTIAL IN COMPARTMENTS

COMP. NUMBER	DATE 5/4/00	DATE / /	DATE / /	DATE / /	DATE / /	DATE / /	DATE / /
TIME	14:40	14:55	15:10	15:25	15:40	15:55	16:10
1	7.0	6.9	7.0	7.0	7.0	Clean	
2	6.9	6.5	6.5	6.5	6.5	6.9	
3	7.0	6.5	6.9	7.0	6.9	7.0	
4	7.0	6.9	7.0	7.0	6.9	7.0	
5	7.0	7.0	7.0	7.0	7.0	7.2	
6	7.5	7.2	7.5	7.5	7.2	7.9	
7	7.5	7.0	7.2	7.2	7.0	7.5	
8	7.5	7.0	7.0	7.2	7.0	7.5	
9	Cleaning	7.0	7.0	7.0	6.9	7.2	
10	7.5	6.9	6.9	7.0	7.0	7.2	
11	7.0	6.5	6.5	6.9	6.5	7.0	
12	7.2	7.0	Cleaning	7.0	7.0	7.2	
13	7.9	7.2	7.5	7.5	7.5	7.5	
14	7.2	6.9	7.2	7.0	Cleaning	7.0	
15	7.0	6.2	6.9	6.9	7.0	6.9	
16	7.5	6.9	7.2	7.0	7.2	7.2	
17	6.9	7.0	7.5	7.2	7.5	7.5	
18	7.5	7.0	7.5	7.2	7.5	7.5	
19	7.0	6.2	6.9	6.9	7.0	7.0	
20	7.2	6.5	7.0	6.9	7.2	7.0	
21	7.2	6.9	7.2	7.0	7.5	7.2	
22	7.9	7.0	7.5	7.5	8.0	8.0	
23	6.5	5.9	6.2	6.2	6.5	6.5	
24	7.5	6.9	7.2	7.2	7.5	7.5	

05/04/00MAGNAHELIC CHECK SHEET EPA TEST.doc

MONTH _____	MAGNAHELIC CHECKS	YEAR _____

Run 2

PRESSURE DIFFERENTIAL IN COMPARTMENTS

COMP. NUMBER	DATE 5/4/00	DATE / /	DATE / /	DATE / /	DATE / /	DATE / /	DATE / /
TIME	16:30	16:45	17:00	17:15	17:30	17:45	18:00
1	7.0	6.9	7.0	7.0	7.0	7.1	7.0
2	6.9	6.5	6.5	6.5	6.5	cleaning	6.5
3	6.9	6.6	6.2	6.2	7.0	7.3	6.7
4	7.0	6.9	7.0	7.0	7.0	7.3	7.0
5	7.0	7.0	7.0	7.0	7.0	7.5	7.0
6	7.5	7.3	7.6	7.5	7.5	7.9	7.5
7	7.2	7.0	7.2	7.0	7.0	7.6	7.0
8	7.2	7.0	7.2	7.0	7.0	7.7	7.0
9	7.0	6.9	7.0	7.0	6.9	7.5	7.0
10	Cleaning	7.0	7.0	7.0	7.0	7.5	7.0
11	7.0	6.5	6.6	7.0	6.6	7.1	6.6
12	7.5	7.0	Cleaning	7.2	7.0	7.5	7.0
13	7.9	7.0	7.5	7.5	7.2	7.5	7.2
14	7.2	6.7	7.0	7.0	7.0	6.8	7.0
15	7.0	6.5	6.9	6.7	6.5	6.8	6.5
16	7.2	7.0	7.5	7.3	Cleaning	7.4	7.0
17	7.5	7.2	7.7	7.5	7.6	7.7	6.2
18	7.5	7.0	7.5	7.5	7.5	7.7	7.0
19	7.0	6.5	7.0	6.9	7.0	6.8	cleaning
20	7.0	6.5	7.0	7.0	7.0	7.1	7.0
21	7.2	6.9	7.2	7.0	7.5	7.4	7.2
22	8.0	7.2	7.5	7.5	8.0	8.0	7.5
23	6.5	6.0	6.2	6.3	6.5	6.5	6.5
24	7.5	7.0	7.5	7.5	7.5	7.7	7.5

MONTH MAY	MAGNAHELIC CHECKS	YEAR 2000

Run 2

PRESSURE DIFFERENTIAL IN COMPARTMENTS

COMP. NUMBER	DATE 5/4/00	DATE / /	DATE / /	DATE / /	DATE / /	DATE / /	DATE / /
TIME	18:15	18:30	18:45	19:00	19:15		
1	7.0	6.6	7.0	6.9	7.0		
2	6.5	6.4	6.6	6.6	6.7		
3	cleaning	6.6	6.8	6.9	6.8		
4	7.2	6.8	6.8	7.0	7.0		
5	7.5	6.9	7.0	7.1	7.1		
6	7.9	7.1	cleaning	7.5	7.6		
7	7.5	6.9	7.0	7.2	7.5		
8	7.5	6.9	7.1	7.2	7.5		
9	7.3	6.7	7.1	7.0	cleaning		
10	7.5	6.8	7.2	7.0	7.5		
11	7.0	6.5	6.8	6.6	7.0		
12	7.5	7.0	7.4	7.1	7.5		
13	7.5	7.1	7.3	7.3	7.6		
14	7.0	6.6	7.0	7.0	7.2		
15	6.6	6.2	6.5	6.6	6.9		
16	7.2	6.9	7.3	7.4	7.4		
17	7.8	7.2	7.5	7.6	7.7		
18	7.5	7.0	7.4	7.4	7.5		
19	6.9	6.4	6.7	6.6	6.9		
20	7.0	6.5	6.9	6.9	7.0		
21	7.2	cleaning	7.1	7.1	7.3		
22	7.9	7.6	7.6	7.4	7.9		
23	6.5	6.3	6.2	6.0	6.6		
24	7.5	7.2	7.5	7.0	7.7		

MONTH _____	MAGNAHELIC CHECKS	YEAR _____

Run 3

PRESSURE DIFFERENTIAL IN COMPARTMENTS

COMP. NUMBER	DATE 5/4/00	DATE / /	DATE / /	DATE / /	DATE / /	DATE / /	DATE / /
TIME	20:15	20:30	20:45	21:00	21:15	21:30	21:45
1	6.5	cleaning	6.5	7.0	6.8	6.8	7.0
2	6.2	6.5	6.2	6.5	6.5	7.2	6.5
3	6.5	6.6	6.5	cleaning	6.5	6.5	6.8
4	6.6	6.6	6.5	7.0	6.9	6.7	6.8
5	6.7	6.9	6.6	7.0	7.0	6.7	7.0
6	7.0	7.4	7.2	7.5	7.4	cleaning	7.4
7	7.0	7.0	7.0	7.5	7.0	7.0	7.0
8	7.0	7.0	7.0	7.5	7.0	7.0	7.0
9	6.7	6.9	6.7	7.4	6.8	7.0	7.0
10	6.7	7.0	6.7	7.4	6.8	7.0	7.0
11	6.2	6.5	6.3	7.0	6.5	6.6	6.5
12	6.8	7.0	6.7	7.2	7.0	7.2	7.0
13	7.0	7.0	7.0	7.5	7.0	7.0	7.2
14	6.5	6.5	6.5	7.0	6.8	6.8	6.8
15	6.2	6.2	6.5	6.8	6.5	6.5	6.5
16	7.0	7.0	7.0	7.2	7.0	7.0	7.0
17	cleaning	7.0	7.0	7.5	7.0	7.0	7.0
18	7.5	6.2	cleaning	7.4	7.0	7.0	7.2
19	6.5	6.2	6.5	6.6	6.5	6.5	6.6
20	7.0	6.5	6.9	7.0	6.5	6.7	7.0
21	7.1	6.5	7.0	7.2	cleaning	7.0	7.0
22	7.8	7.0	7.2	7.5	7.5	7.5	7.8
23	6.0	6.0	6.0	6.2	6.2	6.0	6.2
24	7.2	7.0	6.2	7.5	7.5	7.2	cleaning

05/04/00MAGNAHELIC CHECK SHEET EPA TEST.doc

MONTH _____	MAGNAHELIC CHECKS	YEAR _____

Run 3

PRESSURE DIFFERENTIAL IN COMPARTMENTS

COMP. NUMBER	DATE 5/4/00	DATE / /	DATE / /	END DATE / /	DATE / /	DATE / /	DATE / /
TIME	22:00	22:15	22:30	22:45	23:00		
1	7.0	6.8	6.9	7.0			
2	6.3	6.0	6.4	6.5			
3	6.6	6.5	6.5	7.0			
4	6.8	6.5	6.8	7.0			
5	6.8	6.8	7.0	7.0			
6	7.3	7.3	7.5	7.5			
7	7.2	7.0	7.0	7.0			
8	7.0	7.0	7.0	7.0			
9	cleaning	6.8	6.8	7.0			
10	7.0	6.8	7.0	7.0			
11	6.8	6.5	6.5	6.5			
12	7.3	7.0	cleaning	7.0			
13	7.2	7.0	7.0	7.0			
14	6.8	6.5	7.0	6.8			
15	6.5	6.2	6.8	6.5			
16	7.0	6.8	7.2	7.0			
17	7.0	7.0	7.5	7.2			
18	7.0	7.0	7.2	7.0			
19	6.5	6.5	6.8	6.5			
20	6.5	6.5	7.0	6.5			
21	7.0	6.9	7.0	7.0			
22	7.5	7.2	7.5	7.5			
23	6.0	6.0	6.3	6.2			
24	7.2	7.2	7.5	7.5			

GALLATIN STEEL
A Co-Steel Dofasco Partnership

COPY

March 31, 2000

Mr. Gerald Slucher
Source Sampling and Data Management
Section
Technical Services Branch
Division for Air Quality
803 Schenkel Lane
Frankfort, KY 40601-1403

RE: Gallatin Steel Company, Warsaw, KY, ID # 079-1380-0018
Permit Number F-96-009 (Revision 1)
Compliance Test Protocol for Emissions Testing

Dear Mr. Slucher:

Gallatin Steel's air testing firm, Ambient Air Services, Inc., is scheduled to be at Gallatin Steel the first week of May to conduct emissions testing on emission point E1 (01) for NOx and SO_2. In accordance with the conditions in our permit, we are not required to conduct testing for VOC, PM, CO, and lead emissions this year based on our test results for the last two years (1998 and 1999).

The protocol submitted to your attention on January 7, 1998 will be followed for the testing of NOx and SO_2 with the following listed changes.

1) For NOx, three runs each of 3 heat cycles in duration will be performed with the inlet probe being positioned in the discharge plenum of the baghouse.
2) For SO_2, in order to obtain statistically valid sampling of levels in the baghouse (since there is not homogeneity in the baghouse), we will be testing compartments in pairs (instead of testing one single compartment) over a total of four runs, each run consisting of three heats. We are requesting to test 8 of the 24 compartments during the four runs, two compartments tested during each run. The results of the sampling will provide more accurate information and will produce an average ppm level for the baghouse emissions. Please note that 40 CFR 60 supports and addresses multiple measurement sites for correctly testing particulate emissions. This same logic is also applicable to SO_2 emissions, and supports the use of an "alternate" method to produce more accurate results.

The performance testing is tentatively scheduled to begin on May 5 and we will provide you with notification of the exact test date and start time at least 10 days prior to the testing. A source testing report which presents the results of the performance tests will be submitted to the DAQ within 45 days after the completion of the fieldwork in accordance with the permit.

R.R. #1, Box 320, Ghent, KY 41045-9704 PHONE 606.567.3100 FAX 606.567.3165

If you have any questions or comments, please contact me at the address below or by telephone at 606-567-3141.

Sincerely yours,

Valerie A. Hudson

Valerie A. Hudson, P.E.
Process Manager - Environmental Systems

cc: Dan Gray, DAQ
John Allen, DAQ-Regional Office
Joe Cooksey, Ambient Air Services, Inc.

JAMES E. BICKFORD
SECRETARY

PAUL E. PATTON
GOVERNOR

COMMONWEALTH OF KENTUCKY
NATURAL RESOURCES AND ENVIRONMENTAL PROTECTION CABINET
DEPARTMENT FOR ENVIRONMENTAL PROTECTION
DIVISION FOR AIR QUALITY
803 SCHENKEL LN
FRANKFORT KY 40601-1403

May 5, 2000

Ms. Valerie Hudson
Manager, Environmental Systems
Gallatin Steel Company
US Highway 42, Route 1, Box 320
Ghent, Kentucky 41045

RE: ID# 079-1380-0018
Permit # F-96-009 (Revision 1)

Dear Ms. Hudson:

The Division acknowledges the receipt on April 5, 2000, of the test protocol for emission point E1 (01). The Division has reviewed the protocol and concurs that the appropriate test methods are being utilized.

If you have any questions regarding this matter, please contact me at (502)573-3382, Extension 324.

Sincerely,

Forrest E. Frazier, Jr., Supervisor
Metallurgy Section
Permit Review Branch

FEF/AJW

cc: William A. Clements / Regional Office
Source file / 5

APPENDIX G

PROJECT PARTICIPANTS

PROJECT PARTICIPANTS

AMBIENT AIR SERVICES, INC.

Joe Cooksey
Earl Coggins
Melvin Petit

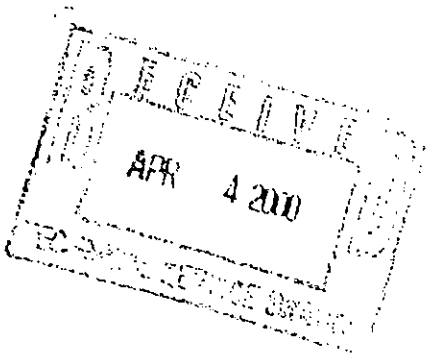
GALLATIN STEEL

Valerie Hudson
Joe Dougherty

STATE OBSERVER

Gerald Slucher

GALLATIN
STEEL
A Co-Steel Dofasco Partnership



March 31, 2000

Mr. Gerald Slucher
Source Sampling and Data Management
Section
Technical Services Branch
Division for Air Quality
803 Schenkel Lane
Frankfort, KY 40601-1403

RE: Gallatin Steel Company, Warsaw, KY, ID # 079-1380-0018
Permit Number F-96-009 (Revision 1)
Compliance Test Protocol for Emissions Testing

Dear Mr. Slucher:

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R.R. #1, Box 320, Ghent, KY 41045-9704 PHONE 606.567.3100 FAX 606.567.3165

If you have any questions or comments, please contact me at the address below or by telephone at 606-567-3141.

Sincerely yours,

Valerie A. Hudson

Valerie A. Hudson, P.E.
Process Manager - Environmental Systems

cc: Dan Gray, DAQ
John Allen, DAQ-Regional Office
Joe Cooksey, Ambient Air Services, Inc.

TIME	OBSERVED CONCENTRATION PPM			COMMENTS	CALIBRATION CORRECTIONS						CORRECTED PPM VALUES			FLOW MEASURMENTS SCFM				MASS EMISSIONS			EMISSION FACTOR		
					NOX 7		SO2 IN		SO2 OUT														
	NOX COMP 7	SO2 IN	SO2 OUT		0.0	24.9	0.0	12.5	0.0	12.5	NOX - 7	SO2 IN	SO2 OUT	COLD-1	COLD-2	HOT	TOTAL	NOX LBS/HR	SO2 IN LBS/HR	SO2 OUT LBS/HR	PRODUCTION TONS/HR	NOX LBS/TON	SO2 LBS/TON
5/4/2000 20:05	4.6	11.9	5.9	CALS	-0.1	25.3	0.1	12.3	0.1	12.9	4.6	12.1	5.7	833791	74919	225540	1134250						
5/4/2000 20:06	4.0	12.1	5.7	CALS	-0.1	25.3	0.1	12.3	0.1	12.9	4.0	12.3	5.6	833791	74919	225540	1134250						
5/4/2000 20:07	3.5	12.1	6.1	CALS	-0.1	25.3	0.1	12.3	0.1	12.9	3.5	12.3	5.9	833791	74919	225540	1134250						
5/4/2000 20:08	2.9	12.2	6.6	CALS	-0.1	25.3	0.1	12.3	0.1	12.9	2.9	12.4	6.4	833791	74919	225540	1134250						
5/4/2000 20:09	2.4	12.2	7.1	CALS	-0.1	25.3	0.1	12.3	0.1	12.9	2.4	12.4	6.9	833791	74919	225540	1134250						
5/4/2000 20:10	2.9	12.2	5.6	CALS	-0.1	25.3	0.1	12.3	0.1	12.9	2.9	12.4	5.5	833791	74919	225540	1134250						
5/4/2000 20:11	3.9	10.7	3.0	CALS	-0.1	25.3	0.1	12.3	0.1	12.9	4.0	10.8	2.8	833791	74919	225540	1134250						
5/4/2000 20:12	6.6	6.2	3.0	CALS	-0.1	25.3	0.1	12.3	0.1	12.9	6.5	6.2	2.9	833791	74919	225540	1134250						
5/4/2000 20:13	8.1	3.3	2.8	CALS	-0.1	25.3	0.1	12.3	0.1	12.9	8.0	3.3	2.7	833791	74919	225540	1134250						
5/4/2000 20:14	6.5	2.7	2.9	CALS	-0.1	25.3	0.1	12.3	0.1	12.9	6.4	2.7	2.8	833791	74919	225540	1134250						
5/4/2000 20:15	4.5	2.6	2.9	CALS	-0.1	25.3	0.1	12.3	0.1	12.9	4.5	2.5	2.7	833791	74919	225540	1134250						
5/4/2000 20:16	2.9	2.7	2.8	CALS	-0.1	25.3	0.1	12.3	0.1	12.9	2.9	2.6	2.6	833791	74919	225540	1134250						
5/4/2000 20:17	1.9	2.6	2.3	RUN 3	-0.1	25.3	0.1	12.3	0.1	12.9	2.0	2.6	2.2	833791	74919	225540	1134250	16.2	29.0	25.4	199	0.08	0.14
5/4/2000 20:18	1.5	2.4	2.1	RUN 3	-0.1	25.3	0.1	12.3	0.1	12.9	1.6	2.4	2.0	833791	74919	225540	1134250	12.7	27.0	22.6	199	0.06	0.12
5/4/2000 20:19	1.6	2.3	1.8	RUN 3	-0.1	25.3	0.1	12.3	0.1	12.9	1.6	2.2	1.7	833791	74919	225540	1134250	13.2	24.9	19.1	199	0.07	0.11
5/4/2000 20:20	1.3	2.2	2.0	RUN 3	-0.1	25.3	0.1	12.3	0.1	12.9	1.4	2.1	1.9	833791	74919	225540	1134250	11.2	23.9	21.9	199	0.06	0.12
5/4/2000 20:21	1.2	2.3	2.2	RUN 3	-0.1	25.3	0.1	12.3	0.1	12.9	1.3	2.2	2.1	833791	74919	225540	1134250	10.2	25.3	24.0	199	0.05	0.12
5/4/2000 20:22	1.3	2.4	2.3	RUN 3	-0.1	25.3	0.1	12.3	0.1	12.9	1.4	2.3	2.2	833791	74919	225540	1134250	11.2	26.3	25.4	199	0.06	0.13
5/4/2000 20:23	1.6	2.4	2.7	RUN 3	-0.1	25.3	0.1	12.3	0.1	12.9	1.7	2.3	2.6	833791	74919	225540	1134250	13.7	26.3	29.6	199	0.07	0.14
5/4/2000 20:24	2.0	2.6	2.9	RUN 3	-0.1	25.3	0.1	12.3	0.1	12.9	2.1	2.6	2.7	833791	74919	225540	1134250	16.7	29.0	31.0	199	0.08	0.15
5/4/2000 20:25	1.9	2.7	3.2	RUN 3	-0.1	25.3	0.1	12.3	0.1	12.9	2.0	2.7	3.1	833791	74919	225540	1134250	16.2	30.4	35.2	199	0.08	0.16
5/4/2000 20:26	1.6	3.0	3.9	RUN 3	-0.1	25.3	0.1	12.3	0.1	12.9	1.7	2.9	3.7	833791	74919	225540	1134250	13.7	33.1	42.2	199	0.07	0.19
5/4/2000 20:27	1.7	3.2	3.9	RUN 3	-0.1	25.3	0.1	12.3	0.1	12.9	1.7	3.2	3.8	833791	74919	225540	1134250	14.2	35.2	42.5	199	0.07	0.20
5/4/2000 20:28	2.2	3.5	4.0	RUN 3	-0.1	25.3	0.1	12.3	0.1	12.9	2.3	3.5	3.9	833791	74919	225540	1134250	18.7	39.6	43.6	199	0.09	0.21
5/4/2000 20:29	2.6	3.6	4.1	RUN 3	-0.1	25.3	0.1	12.3	0.1	12.9	2.6	3.6	4.0	833791	74919	225540	1134250	21.2	40.3	45.9	199	0.11	0.21
5/4/2000 20:30	3.0	3.6	3.9	RUN 3	-0.1	25.3	0.1	12.3	0.1	12.9	3.0	3.6	3.8	833791	74919	225540	1134250	24.7	40.6	42.9	199	0.12	0.21
5/4/2000 20:31	3.1	3.7	4.3	RUN 3	-0.1	25.3	0.1	12.3	0.1	12.9	3.1	3.7	4.1	833791	74919	225540	1134250	25.2	41.6	46.7	199	0.13	0.22
5/4/2000 20:32	2.7	3.9	5.1	RUN 3	-0.1	25.3	0.1	12.3	0.1	12.9	2.8	3.9	4.9	833791	74919	225540	1134250	22.7	44.0	55.5	199	0.11	0.25
5/4/2000 20:33	2.6	4.3	4.9	RUN 3	-0.1	25.3	0.1	12.3	0.1	12.9	2.6	4.3	4.7	833791	74919	225540	1134250	21.2	49.1	53.4	199	0.11	0.26
5/4/2000 20:34	2.0	4.5	4.4	RUN 3	-0.1	25.3	0.1	12.3	0.1	12.9	2.1	4.5	4.3	833791	74919	225540	1134250	16.7	50.5	48.5	199	0.08	0.25
5/4/2000 20:35	1.4	3.7	3.9	RUN 3	-0.1	25.3	0.1	12.3	0.1	12.9	1.4	3.6	3.8	833791	74919	225540	1134250	11.7	41.3	42.9	199	0.06	0.21
5/4/2000 20:36	1.1	3.4	3.4	RUN 3	-0.1	25.3	0.1	12.3	0.1	12.9	1.2	3.4	3.3	833791	74919	225540	1134250	9.7	38.6	36.9	199	0.05	0.19
5/4/2000 20:37	1.1	3.4	2.9	RUN 3	-0.1	25.3	0.1	12.3	0.1	12.9	1.2	3.4	2.8	833791	74919	225540	1134250	9.7	38.2	31.3	199	0.05	0.17
5/4/2000 20:38	1.1	3.0	2.8	RUN 3	-0.1	25.3	0.1	12.3	0.1	12.9	1.2	3.0	2.6	833791	74919	225540	1134250	9.7	33.5	29.9	199	0.05	0.16
5/4/2000 20:39	1.2	2.7	2.9	RUN 3	-0.1	25.3	0.1	12.3	0.1	12.9	1.3	2.7	2.8	833791	74919	225540	1134250	10.2	30.4	31.3	199	0.05	0.16
5/4/2000 20:40	1.8	2.6	3.2	RUN 3	-0.1	25.3	0.1	12.3	0.1	12.9	1.8	2.6	3.1	833791	74919	225540	1134250	13.2	29.4	34.8	199	0.07	0.16
5/4/2000 20:41	2.1	2.7	3.7	RUN 3	-0.1	25.3	0.1	12.3	0.1	12.9	2.2	2.7	3.6	833791	74919	225540	1134250	17.7	30.4	40.4	199	0.09	0.18
5/4/2000 20:42	2.9	3.1	5.4	RUN 3	-0.1	25.3	0.1	12.3	0.1	12.9	3.0	3.0	5.2	833791	74919	225540	1134250	24.2	34.5	58.7	199	0.12	0.23
5/4/2000 20:43	4.6	4.1	6.1	RUN 3	-0.1	25.3	0.1	12.3	0.1	12.9	4.6	4.1	5.9	833791	74919	225540	1134250	37.7	46.7	66.7	199	0.19	0.29
5/4/2000 20:44	6.5	5.0	6.0	RUN 3	-0.1	25.3	0.1	12.3	0.1	12.9	6.4	5.0	5.8	833791	74919	225540	1134250	52.2	56.6	65.3	199	0.26	0.31
5/4/2000 20:45	5.5	5.3	6.3	RUN 3	-0.1	25.3	0.1	12.3	0.1	12.9	5.4	5.4	6.1	833791	74919	225540	1134250	44.2	60.7	69.2	199	0.22	0.33
5/4/2000 20:46	4.3	5.4	5.0	RUN 3	-0.1	25.3	0.1	12.3	0.1	12.9	4.3	5.4	4.8	833791	74919	225540	1134250	35.2	61.3	54.5	199	0.18	0.29
5/4/2000 20:47	3.4	4.9	3.8	RUN 3	-0.1	25.3	0.1	12.3	0.1	12.9	3.5	4.9	3.7	833791	74919	225540	1134250	28.2	55.6	41.5	199	0.14	0.24
5/4/2000 20:48	2.7	4.4	3.8	RUN 3	-0.1	25.3	0.1	12.3	0.1	12.9	2.8	4.4	3.7	833791	74919	225540	1134250	22.7	49.4	41.8	199	0.11	0.23
5/4/2000 20:49	2.4	3.8	3.0	RUN 3	-0.1	25.3	0.1	12.3	0.1	12.9	2.4	3.8	2.9	833791	74919	225540	1134250	19.7	42.6	33.1	199	0.10	0.19
5/4/2000 20:50	2.1	3.2	3.0	RUN 3	-0.1	25.3	0.1	12.3	0.1	12.9	2.1	3.2	2.9	833791	74919	225540	1134250	17.2	35.2	33.1	199	0.09	0.17
5/4/2000 20:51	1.9	3.0	3.5	RUN 3	-0.1	25.3	0.1	12.3	0.1	12.9	2.0	2.9	3.3	833791	74919	225540	1134250	16.2	33.1	37.6	199	0.08	0.18
5/4/2000 20:52	2.0	3.0	4.3	RUN 3	-0.1	25.3	0.1	12.3	0.1	12.9	2.1	3.0	4.1	833791	74919	225540	1134250	16.7	34.1	46.7	199	0.08	0.20
5/4/2000 20:53	2.0	3.4	4.0	RUN 3	-0.1	25.3	0.1	12.3	0.1	12.9	2.1	3.3	3.8	833791	74919	225540	1134250	16.7	37.9	43.2	199	0.08	0.20
5/4/2000 20:54	2.0	3.5	3.4	RUN 3	-0.1	25.3	0.1	12.3	0.1	12.9	2.1	3.4	3.3	833791	74919	225540	1134250	16.7	38.9	37.3	199	0.08	0.19
5/4/2000 20:55	2.2	3.2	3.5	RUN 3	-0.1	25.3	0.1	12.3	0.1	12.9	2.2	3.2	3.4	833791	74919	225540	1134250	18.2	36.2	38.3	199	0.09	0.19
5/4/2000 20:56	2.7	3.1	3.8	RUN 3	-0.1	25.3	0.1	12.3	0.1	12.9	2.7	3.1	3.4	833791	74919	225540	1134250	22.2	35.2	38.7	199	0.11	0.19
5/4/2000 20:57	2.9	2.8	3.3	RUN 3	-0.1	25.3	0.1	12.3	0.1	12.9	3.0	2.7	3.2	833791	74919	225540	1134250	24.2	31.1	36.2	199	0.12	0.17
5/4/2000 20:58	2.6	2.8	3.4	RUN 3	-0.1	25.3	0.1	12.3	0.1	12.9	2.6	2.7	3.3	833791	74919	225540	1134250	21.2	31.1	36.9	199	0.11	0.17
5/4/2000 20:59	2.4	3.0	3.1	RUN 3	-0.1	25.3	0.1	12.3	0.1	12.9	2.5	3.0	3.0	833791	74919	225540	1134250	20.2	33.8	34.1	199	0.10	0.17

TIME	OBSERVED CONCENTRATION PPM			COMMENTS	CALIBRATION CORRECTIONS						CORRECTED PPM VALUES			FLOW MEASURMENTS SCFM				MASS EMISSIONS			EMISSION FACTOR		
					NOX 7		SO2 IN		SO2 OUT														
	NOX COMP 7	SO2 IN	SO2 OUT		0.0	24.9	0.0	12.5	0.0	12.5	NOX - 7	SO2 IN	SO2 OUT	COLD-1	COLD-2	HOT	TOTAL	NOX LBS/HR	SO2 IN LBS/HR	SO2 OUT LBS/HR	PRODUCTION TONS/HR	NOX LBS/TON	SO2 LBS/TON
5/4/2000 19:10	5.3	0.3	0.9	RUN 2	-0.1	25.2	0.1	12.3	0.1	12.6	5.3	0.3	0.8	833791	74919	225540	1134250	43.0	2.9	8.6	198	0.22	0.03
5/4/2000 19:11	7.6	0.4	2.0	RUN 2	-0.1	25.2	0.1	12.3	0.1	12.6	7.6	0.3	1.9	833791	74919	225540	1134250	61.6	3.9	21.8	198	0.31	0.06
5/4/2000 19:12	10.6	0.5	2.7	RUN 2	-0.1	25.2	0.1	12.3	0.1	12.6	10.6	0.4	2.6	833791	74919	225540	1134250	85.8	4.2	29.4	198	0.43	0.08
5/4/2000 19:13	11.5	0.5	2.5	RUN 2	-0.1	25.2	0.1	12.3	0.1	12.6	11.4	0.4	2.4	833791	74919	225540	1134250	92.9	4.6	26.9	198	0.47	0.08
5/4/2000 19:14	8.6	0.4	1.7	RUN 2	-0.1	25.2	0.1	12.3	0.1	12.6	8.6	0.3	1.6	833791	74919	225540	1134250	69.7	3.9	18.6	198	0.35	0.06
5/4/2000 19:15	8.9	0.4	1.4	RUN 2	-0.1	25.2	0.1	12.3	0.1	12.6	8.9	0.3	1.3	833791	74919	225540	1134250	72.2	3.2	14.3	198	0.36	0.04
5/4/2000 19:16	8.8	0.3	1.3	RUN 2	-0.1	25.2	0.1	12.3	0.1	12.6	8.8	0.2	1.2	833791	74919	225540	1134250	71.2	2.5	13.2	198	0.36	0.04
5/4/2000 19:17	6.3	0.3	1.3	RUN 2	-0.1	25.2	0.1	12.3	0.1	12.6	6.3	0.2	1.2	833791	74919	225540	1134250	51.0	2.2	13.6	198	0.26	0.04
5/4/2000 19:18	3.9	0.3	1.5	CALS	-0.1	25.2	0.1	12.3	0.1	12.6	RUN 2 AVERAGES			833791	74919	225540	1134250	RUN 2 AVERAGES					
5/4/2000 19:19	2.9	0.3	1.9	CALS	-0.1	25.2	0.1	12.3	0.1	12.6	3.4	0.5	1.8	833791	74919	225540	1134250	28.0	5.9	20.8	198.0	0.14	0.07
5/4/2000 19:20	2.4	0.3	2.2	CALS	-0.1	25.2	0.1	12.3	0.1	12.6				833791	74919	225540	1134250						
5/4/2000 19:21	2.3	0.3	2.3	CALS	-0.1	25.2	0.1	12.3	0.1	12.6	2.4	0.3	2.2	833791	74919	225540	1134250						
5/4/2000 19:22	2.0	0.3	1.6	CALS	-0.1	25.3	0.1	12.3	0.1	12.9	2.1	0.2	1.5	833791	74919	225540	1134250						
5/4/2000 19:23	1.8	0.4	1.9	CALS	-0.1	25.3	0.1	12.3	0.1	12.9	1.7	0.3	1.8	833791	74919	225540	1134250						
5/4/2000 19:24	1.8	0.4	2.7	CALS	-0.1	25.3	0.1	12.3	0.1	12.9	1.7	0.3	2.6	833791	74919	225540	1134250						
5/4/2000 19:25	1.8	0.5	2.1	CALS	-0.1	25.3	0.1	12.3	0.1	12.9	1.7	0.4	2.0	833791	74919	225540	1134250						
5/4/2000 19:26	1.7	0.5	0.5	CALS	-0.1	25.3	0.1	12.3	0.1	12.9	1.7	0.4	0.5	833791	74919	225540	1134250						
5/4/2000 19:27	1.7	0.5	0.2	CALS	-0.1	25.3	0.1	12.3	0.1	12.9	1.7	0.4	0.2	833791	74919	225540	1134250						
5/4/2000 19:28	1.4	0.5	0.1	CALS	-0.1	25.3	0.1	12.3	0.1	12.9	1.4	0.4	0.1	833791	74919	225540	1134250						
5/4/2000 19:29	1.0	0.5	0.1	CALS	-0.1	25.3	0.1	12.3	0.1	12.9	1.1	0.4	0.0	833791	74919	225540	1134250						
5/4/2000 19:30	0.8	0.6	0.1	CALS	-0.1	25.3	0.1	12.3	0.1	12.9	0.9	0.5	0.0	833791	74919	225540	1134250						
5/4/2000 19:31	0.7	0.6	0.1	CALS	-0.1	25.3	0.1	12.3	0.1	12.9	0.8	0.5	0.0	833791	74919	225540	1134250						
5/4/2000 19:32	0.7	0.7	0.5	CALS	-0.1	25.3	0.1	12.3	0.1	12.9	0.8	0.6	0.5	833791	74919	225540	1134250						
5/4/2000 19:33	0.7	0.7	5.1	CALS	-0.1	25.3	0.1	12.3	0.1	12.9	0.8	0.6	4.9	833791	74919	225540	1134250						
5/4/2000 19:34	0.7	0.6	9.8	CALS	-0.1	25.3	0.1	12.3	0.1	12.9	0.8	0.6	9.6	833791	74919	225540	1134250						
5/4/2000 19:35	0.6	0.6	11.9	CALS	-0.1	25.3	0.1	12.3	0.1	12.9	0.7	0.6	11.5	833791	74919	225540	1134250						
5/4/2000 19:36	0.5	0.6	12.1	CALS	-0.1	25.3	0.1	12.3	0.1	12.9	0.6	0.5	11.7	833791	74919	225540	1134250						
5/4/2000 19:37	0.5	0.5	12.2	CALS	-0.1	25.3	0.1	12.3	0.1	12.9	0.6	0.4	11.9	833791	74919	225540	1134250						
5/4/2000 19:38	0.5	0.5	12.4	CALS	-0.1	25.3	0.1	12.3	0.1	12.9	0.6	0.4	12.0	833791	74919	225540	1134250						
5/4/2000 19:39	0.6	0.5	12.5	CALS	-0.1	25.3	0.1	12.3	0.1	12.9	0.7	0.4	12.1	833791	74919	225540	1134250						
5/4/2000 19:40	0.9	0.5	12.6	CALS	-0.1	25.3	0.1	12.3	0.1	12.9	0.9	0.4	12.2	833791	74919	225540	1134250						
5/4/2000 19:41	0.8	0.5	12.4	CALS	-0.1	25.3	0.1	12.3	0.1	12.9	0.9	0.4	12.1	833791	74919	225540	1134250						
5/4/2000 19:42	0.9	0.5	8.0	CALS	-0.1	25.3	0.1	12.3	0.1	12.9	0.9	0.4	7.8	833791	74919	225540	1134250						
5/4/2000 19:43	0.8	0.5	3.5	CALS	-0.1	25.3	0.1	12.3	0.1	12.9	0.9	0.4	3.3	833791	74919	225540	1134250						
5/4/2000 19:44	0.8	0.5	1.5	CALS	-0.1	25.3	0.1	12.3	0.1	12.9	0.9	0.4	1.4	833791	74919	225540	1134250						
5/4/2000 19:45	0.8	0.4	0.7	CALS	-0.1	25.3	0.1	12.3	0.1	12.9	0.9	0.3	0.7	833791	74919	225540	1134250						
5/4/2000 19:46	0.9	0.5	0.4	CALS	-0.1	25.3	0.1	12.3	0.1	12.9	0.9	0.4	0.4	833791	74919	225540	1134250						
5/4/2000 19:47	2.4	0.5	0.8	CALS	-0.1	25.3	0.1	12.3	0.1	12.9	2.4	0.4	0.7	833791	74919	225540	1134250						
5/4/2000 19:48	22.7	0.5	1.4	CALS	-0.1	25.3	0.1	12.3	0.1	12.9	22.4	0.4	1.3	833791	74919	225540	1134250						
5/4/2000 19:49	24.9	0.4	1.5	CALS	-0.1	25.3	0.1	12.3	0.1	12.9	24.5	0.3	1.4	833791	74919	225540	1134250						
5/4/2000 19:50	25.1	0.4	1.6	CALS	-0.1	25.3	0.1	12.3	0.1	12.9	24.7	0.3	1.6	833791	74919	225540	1134250						
5/4/2000 19:51	25.0	0.4	1.6	CALS	-0.1	25.3	0.1	12.3	0.1	12.9	24.6	0.3	1.5	833791	74919	225540	1134250						
5/4/2000 19:52	22.9	0.5	1.0	CALS	-0.1	25.3	0.1	12.3	0.1	12.9	22.5	0.4	0.9	833791	74919	225540	1134250						
5/4/2000 19:53	1.8	0.5	0.5	CALS	-0.1	25.3	0.1	12.3	0.1	12.9	1.9	0.4	0.4	833791	74919	225540	1134250						
5/4/2000 19:54	-0.1	0.6	0.3	CALS	-0.1	25.3	0.1	12.3	0.1	12.9	0.0	0.5	0.2	833791	74919	225540	1134250						
5/4/2000 19:55	-0.1	0.6	0.1	CALS	-0.1	25.3	0.1	12.3	0.1	12.9	0.0	0.5	0.0	833791	74919	225540	1134250						
5/4/2000 19:56	-0.1	0.7	0.1	CALS	-0.1	25.3	0.1	12.3	0.1	12.9	0.0	0.6	0.0	833791	74919	225540	1134250						
5/4/2000 19:57	-0.1	0.9	0.2	CALS	-0.1	25.3	0.1	12.3	0.1	12.9	0.0	0.8	0.2	833791	74919	225540	1134250						
5/4/2000 19:58	0.2	1.8	0.6	CALS	-0.1	25.3	0.1	12.3	0.1	12.9	0.3	1.7	0.5	833791	74919	225540	1134250						
5/4/2000 19:59	2.1	0.4	0.8	CALS	-0.1	25.3	0.1	12.3	0.1	12.9	2.2	0.3	0.8	833791	74919	225540	1134250						
5/4/2000 20:00	2.9	0.2	0.9	CALS	-0.1	25.3	0.1	12.3	0.1	12.9	3.0	0.1	0.8	833791	74919	225540	1134250						
5/4/2000 20:01	7.1	0.1	1.0	CALS	-0.1	25.3	0.1	12.3	0.1	12.9	7.1	0.0	1.0	833791	74919	225540	1134250						
5/4/2000 20:02	9.4	1.0	2.0	CALS	-0.1	25.3	0.1	12.3	0.1	12.9	9.3	1.0	1.9	833791	74919	225540	1134250						
5/4/2000 20:03	8.7	8.4	2.9	CALS	-0.1	25.3	0.1	12.3	0.1	12.9	8.6	8.5	2.8	833791	74919	225540	1134250						
5/4/2000 20:04	6.1	11.4	5.3	CALS	-0.1	25.3	0.1	12.3	0.1	12.9	6.1	11.6	5.1	833791	74919	225540	1134250						

SECTION B – EMISSION POINTS, AFFECTED FACILITIES, APPLICABLE REGULATIONS, AND OPERATING CONDITIONS

01 (E1)

Description:

Existing melt shop, consisting of the following:

Twin-Shell DC EAF & continuous caster
Ladle and tundish bricking, deskulling, and brick tear-out
Shell bricking and brick tear-out
Two LMF's
One tundish dryer, 1.5 MMBtu/hr
One ladle dryer, 8 MMBtu/hr
Three ladle preheaters, 10 MMBtu/hr, each
Two tundish preheaters, 10 MMBtu/hr, each
Two tundish casting nozzle preheaters, 5 MMBtu/hr, each
Two stirring stations
Dump pit for handling used refractory materials
Scrap cutting from slag pot
Control Equipment: positive pressure fabric filter baghouse
Construction commenced: April, 1993

APPLICABLE REGULATIONS:

A. 401 KAR 51:017, Prevention of significant deterioration of air quality.
B. 401 KAR 60:005 40 CFR standards of performance for new sources. Section 3. (1) (dd), Standards of performance for steel plants: electric arc furnaces and argon-oxygen decarburization vessels constructed after August 17, 1983 (40 CFR Part 60, Subpart AAa).
C. 401 KAR 59:010, New process operations.

1. **Operating Limitations:**

   a. The following raw materials usage rates (including the replacement of the heel) shall not be exceeded: Scrap/substitutes: 270 tons/heat, Lime: 12 tons/heat, and Carbon/substitutes: 7 tons/heat. (Limit on PTE).

Commonwealth of Kentucky
Natural Resources and Environmental Protection Cabinet
Department for Environmental Protection
Division for Air Quality
803 Schenkel Lane
Frankfort, Kentucky 40601
(502) 573-3382

AIR QUALITY PERMIT

Permittee Name: Gallatin Steel Company
Mailing Address: RR #1, Box 320, Ghent, KY 41045

is authorized to operate a steel mill and to construct/operate a second melt shop with associated equipment and a caster and tunnel furnace.

Source Name: Gallatin Steel Company
Mailing Address: RR#1, Box 320, Ghent, KY 41045
Source Location: U.S. Highway 42 West, Warsaw, Kentucky

Permit Type: Federally-Enforceable
Review Type: PSD, Title V

Permit Number: V-99-003 (Revision 2)
Log Number: 54190, 53839, F690
Application Complete Date: November 26, 2001 (54190), May 21, 2001 (53839), June 23, 1998 (F690)
AFS Plant ID #: 21-077-00018
SIC Code: 3312

Region: CINCINNATI
County: Gallatin

Issuance Date: June 22, 2000
Revision 1 Date: August 27, 2001
Revision 2 Date: December 10, 2001
Expiration Date: June 22, 2005

John E. Hornback, Director
Division for Air Quality

TABLE OF CONTENTS

SECTION A -- PERMIT AUTHORIZATION

Pursuant to a duly submitted application the Kentucky Division for Air Quality hereby authorizes the operation of the equipment described herein in accordance with the terms and conditions of this permit. This permit has been issued under the provisions of Kentucky Revised Statutes Chapter 224 and regulations promulgated pursuant thereto and shall become the final permit unless the U.S. EPA files an objection pursuant to 401 KAR 52:100, Section 10.

The permittee shall not construct, reconstruct, or modify any affected facilities without first having submitted a complete application and receiving a permit for the planned activity from the permitting authority, except as provided in this permit or in 401 KAR 52:020, Title V Permits.

Issuance of this permit does not relieve the permittee from the responsibility of obtaining any other permits, licenses, or approvals required by this Cabinet or any other federal, state, or local agency.

Prior to commencing construction on 02(E2), the permittee is responsible for demonstrating that all BACT requirements for all emission units in the new meltshop have not changed from the BACT requirements in F-96-009(Revision 1). If any BACT requirements have changed, the permittee shall meet all new BACT requirements. Additionally, if any parameters changed that affect the modeled ambient impacts in F-96-009(Revision 1), the permittee shall be responsible for performing additional appropriate modeling analyses.

Gallatin Steel Company, and the adjacent slag processing plant, AFS # 21-077-00020, and the industrial gas plant, AFS # 21-077-00023, are considered by the Kentucky Division for Air Quality and the US EPA Region IV to be one source as defined in 401 KAR 51:017, Prevention of significant deterioration of air quality (PSD). Each is responsible and liable for their own violations unless there is a joint cause for the violations.

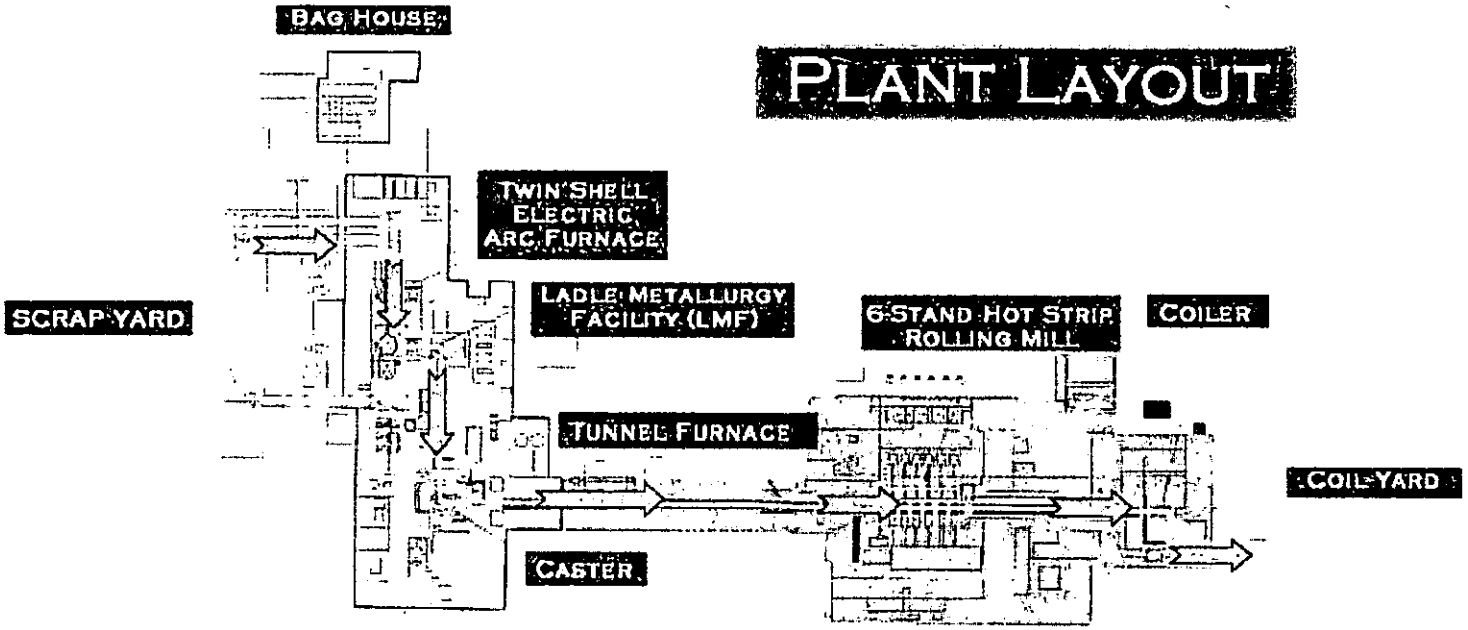
PLANT TOUR

GALLATIN STEEL

◄ HOME

C OMPANY
introduction
history
news
tour
quality certs
P RODUCTS
product info
specifications
technology
S ALES
contacts
lead times
C AREERS
careers
benefits
points of interest
C OMMUNITY
safety
events
environment
P URCHASING
about
terms
direct pay auth.

Click here for the next stop on the tour ►



PROCESS OVERVIEW

Gallatin Steel recycles scrap steel to make new hot-rolled steel coils, using a continuous Compact Strip Production or CSP process. Quality is one of our core business values, and we are ISO 9002 certified.

Reclaimed metals from sources including junked automobiles, demolished buildings and bridges, railroad wheels and old household appliances are delivered to our site via truck, rail and barge. The reclaimed metals are stored in our Scrap Yard until the metals are carried into the Melt Shop and charged in a twin-shell electric arc furnace (EAF).

The EAF melts the scrap steel by striking an electric arc that radiates energy to the scrap charge.

The molten steel is transferred to the Ladle Metallurgy Facility (LMF). At the LMF, the molten metal is refined by making alloy additions and

adjusting the ladle temperature. Once the steel meets the required chemistry and temperature, the ladle is taken to the Caster, and positioned on the rotating turret.

The caster pours the steel into a vertical water-cooled copper mold, which forms a shell the required thickness and width of the slab. The shell is then drawn down through the cooling spray chamber by rollers, solidifying as it travels. The continuous strand exits at the bottom of the machine, and is sheared into slabs of specified lengths, which then enter the tunnel furnace.

The slabs move through the Tunnel Furnace and into the Rolling Mill, where six rolling stands reduce the slabs to the final thickness at a mill exit speed of about 25 mph.

A Coiler at the end of the line captures and wraps the strip into coils suitable for shipping. The coils are banded, marked, weighed and moved to the coil yard for cooling. Coils are cool enough to ship in about 2 days.

The coils are loaded on trucks, outbound rail cars or river barges for transport to the customer.

Click here for the next stop on the tour ▶

PLANT TOUR
GALLATIN STEEL

◄ H OME
C OMPANY
i ntroduction
h istory
n ews
t our
q uality certs
P RODUCTS
p roduct i nfo
s pecifications
t echnology
S ALES
c ontacts
l ead t imes
C AREERS
c areers
b enefits
p oints of i nterest
C OMMUNITY
s afety
e vents
e nvironment
P URCHASING
a bout
t erms
d irect pay auth.

◄ previous | next ►

MELT SHOP

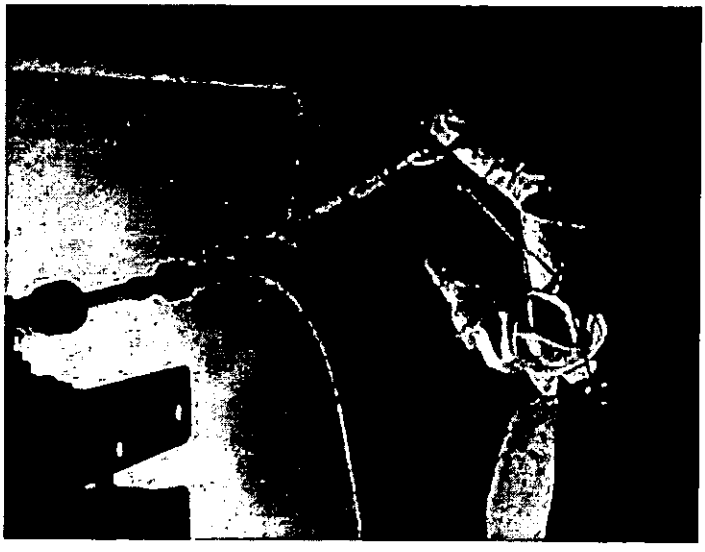
The Melt Shop melts the scrap charge to liquid steel at the required temperature and chemical analysis. It uses large amounts of electric power.

- The melting equipment consists of a twin-shell DC electric arc furnace, powered by a shared set of electrical equipment operating at up to 850 volts and 135,000 amps.
- Oxy-fuel burners placed at strategic locations around the furnace supply additional energy. A lance system is used to inject oxygen to decarbonize the steel. The lance can also inject anthracite carbon to produce a foamy slag.
- When the furnace is ready for scrap charging, an overhead crane brings a "clamshell" bucket over the furnace top and opens the bottom, charging the scrap into the furnace.
- The process of melting a charge of scrap is called a heat. The melt shop computer system identifies each production batch with a unique heat number. To begin melting, the single 30" diameter graphite electrode is lowered into the furnace, and an electric arc is struck between the top and bottom electrodes.

- The arc is like a captive lightning bolt, and radiates energy to the scrap charge from its 4000° F core, quickly boring its way down through the packed scrap. During the heat, the arc voltage is adjusted several times by the programmable controller, or PLC, which controls the furnace.

- A foamy slag is created, which protects the water cooled panels that make up the walls of the furnace and aids in heat transfer to the scrap.

- Oxygen is blown in to remove carbon and other oxidizable elements from the steel bath. It normally takes 50 to 60 minutes to melt a heat of steel and tap the furnace into a waiting ladle.



- Tapping necessitates tilting the furnace forward until liquid steel runs out of the tap hole into a ladle waiting below. The ladle sits on the platform of a transfer car, which is moved into position under the furnace.

- Some steel is always left in the furnace. The residual amount is called a heel. The heel protects the bottom electrode when scrap drops into the furnace and helps to maintain the furnace temperature.

- When the steel in the ladle reaches a target weight, the furnace moves back into its level position, and the gate is closed.

- Temperatures and samples for analysis

are taken with an automated mechanical arm. This is safer and more reliable than taking them manually. The temperature of the steel at tap is about 2960° F.

- The operators send samples of the steel to a Chemical Laboratory using a system of pneumatic tubes. The samples are analyzed on a high-tech optical emission spectrometer, and the results are sent by computer network back to the furnace operator to show the chemical composition of the steel.

- Based on the sample results, the operators can adjust the chemistry to meet specifications by making alloy additions at tap.

- After tap, the ladle of steel is lifted to the LMF car by crane.

Tapping Molten Metal from Electric Arc Furnace

◄ previous | next ►