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Background Report Reference

AP-42 Section Number: 12.20

Background Chapter: 4

Reference Number: 40

Title: Surce Tested: Chromic Plating Tank
Exhaust Scrubber. Date Tested:
December 11, 1986

January 1987



ENGINEERING-SCIENCE, INC.

Street Address:
75 N. FAIR OAKS
PASADENA, CA 91103

Mailing Address:
P.O. BOX 7107
PASADENA, CA 91109

ALBERT C. JAY
ELECTROPLATING

REF. 4-40

July 1, 1987

Mr. Desh Jain
South Coast Air Quality Management District
9150 Flair Drive
El Monte, California 91731

Subject: Tarby Inc.

Source test conducted on December 11, 1986

Dear Mr. Jain:

This letter provides an explanation to flow rate discrepancies between source tests conducted on the inlet and outlet of the Chrome Tank Exhaust Scrubber for Tarby Inc., 7601 Woodwind, Huntington Beach, California. It is our understanding that there is no other flow introduced to the scrubber, and inlet and outlet flows should be equal.

Stack gas flow rates were determined using EPA Reference Methods 1, 2 and 3. An S-Type pitot tube and an inclined oil manometer were used for the velocity measurements and a type-K thermocouple (chromel-alumel) with an Omega digital temperature readout were used for determining the stack temperature. Carbon dioxide (CO₂) and oxygen (O₂) were determined from analyzer readings. Moisture content of the stack gases was determined volumetrically by the liquid gain in the impingers and gravimetrically by the weight gain of the silica gel. This procedure is in accordance with EPA Method 4.

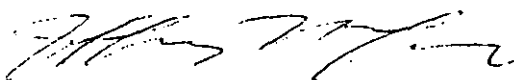
One of the requirements for this flow determination method is that stack gas flow must be stable and not excessively turbulent. A factor affecting flow stability and turbulence is sample port location. EPA Method 1 recommends sample ports be located at least eight stack diameters from any up stream flow disturbances. This criteria was met for the inlet sample port. The location of the outlet sample port was restricted to approximately $\frac{1}{2}$ a pipe diameter down stream of the exhaust blower due to short stack length. Flow conditions at this sample point may have been excessively turbulent and flow rates at the scrubber outlet may have been biased

We are fairly confident with the inlet flow rates due to the sampling procedure and sample port location. It is the recommendation of Engineering-Science that stack gas flow rates for the scrubber outlet be based on scrubber inlet flow rate results.

Attached is a sketch of the sample locations used at Tarby Inc.

If we may be of further assistance or if you have any questions please call me at 818/440-6010 or Paul Farmanian at 818/440-6148.

Truly yours



Jeffrey N Yox
Senior Engineer

Attachment

WA04201/1

EMISSIONS STACK TESTING
TARBY, INCORPORATED
HUNTINGTON BEACH, CALIFORNIA

Source Tested:

Chrome Plating Tank Exhaust Scrubber

Date Tested:

December 11, 1986

Prepared for :

TARBY, INCORPORATED
7601 Woodwind
Huntington Beach, California 92647

January 12, 1987

Prepared by

ENGINEERING-SCIENCE
75 N. Fair Oaks Avenue
P.O. Box 7107
Pasadena, California 91109

Mr. Becvar
818/440-6134

REPORT OF STACK TESTING

AT TARBY, INC.

INTRODUCTION

On December 11, 1986, personnel from Engineering-Science (ES), Pasadena, California, conducted air pollution testing at the Tarby, Inc. facility in Huntington Beach, California. The purpose of the tests was to determine the chromium emissions entering and exiting the chrome plating tank exhaust scrubber. The test method employed was CARB Method 425. The testing program was coordinated by Mr. John Alley of Tarby, Inc. Mr. Desh Jain from the SCAQMD was present to observe the testing. The ES testing team was comprised of Messrs. Paul Farmanian (team leader), Kirk Norberg, and Jeffrey Yox. Testing was conducted during the hours 0935 to 1135.

TEST METHODS

The sampling runs were conducted isokinetically. The sampling train consisted of a Teflon probe connected to four impingers in series. The first two impingers were each charged with 100 milliliters of deionized water, the third impinger was dry, and the fourth contained about 400 grams of indicating silica gel. A filter (maintained at ambient conditions) was located between the third and fourth impingers. The first, third, and fourth impingers were straight tube Greenburg-Smith impingers and the second was an orifice tip Greenburg-Smith impinger.

SCAQMD
engineer in
report
states a
glass
plate

Due to the test train configuration, samples were recovered as front half. Three separate analyses were made on the recovered test samples. One sample aliquot was dried at 105°C and analyzed gravimetrically for particulates. A second sample aliquot was prepared and analyzed for Cr⁺⁶ using visible light spectrophotometry. A third sample aliquot was analyzed by graphite furnace atomic absorption spectrophotometry to determine total chromium. The filter was weighed to determine water insoluble particulate fraction and was digested in water for sample recovery and a sample aliquot was analyzed for Cr⁺⁶ and total chromium.

TABLE 1

SUMMARY OF VOLUMETRIC FLOW DATA

The analytical procedure for determination of Cr^{+6} consisted of sample preparation and analysis. Sample aliquots were prepared by digestion with an alkaline solution of sodium hydroxide and anhydrous sodium carbonate, filtration of digested aliquots, reduction of filtrate pH to 1.0, and reaction with diphenylcarbazide to produce the characteristic red-violet color. The aliquots were analyzed using spectrophotometric comparison with standardized aliquots of known Cr^{+6} concentration, at a wavelength of 540 nm.

Total chromium analysis preparation required addition of concentrated nitric acid to sample aliquots, volatile reduction by refluxed boiling, dilution with distilled water, and filtration. Prepared sample aliquots were aspirated into an air and acetylene flame while recording amount of absorption detected at a wavelength of 357.9 nm.

Blank solutions were prepared and analyzed in the same manner for both tests to eliminate background interference.

RESULTS

The results of the testing program are summarized in Tables 1 and 2. Additional supporting data are presented in the Appendix. Additionally, a discussion of the determination of hexavalent chromium emissions is included in the Appendix.

TABLE 1
SUMMARY OF VOLUMETRIC FLOW DATA

TARBY, INC.
Huntington Beach, CA

December 11, 1986

Parameter	Scrubber Inlet	Scrubber Outlet
Velocity (FPS)	31.72	21.87
Volumetric Flow		
ACFM	8,138	5,611
DSCFM	7,797	5,490
Stack Temperature (°F)	66	57
Moisture Content (%)	1.71	1.34

TABLE 2

SUMMARY OF EMISSIONS DATA

TARBY, INC.
Huntington Beach, CA

December 11, 1986

Parameter	Scrubber Inlet	$\frac{\text{lb}}{\text{hr} \cdot \text{ft}^2}$	Scrubber Outlet	$\frac{\text{lb}}{\text{hr} \cdot \text{ft}^2}$
Particulates				
gr/DSCF	0.0063		0.0038	
lb/hr	$0.42 \frac{\text{lb}}{\text{hr}} \times \frac{1}{12 \text{ ft}^2} = 0.0084$	0.42	0.18	0.0036
Cr ⁺⁶				
ppm	0.344		0.0162	
lb/hr	0.0220	0.00044	0.0007	0.000014
Cr Total				
ppm	2.28		0.0562	
lb/hr	0.146		$0.0025 \times \frac{7797}{5490} = 0.0036$	

Total Sur. face area of tanks = 50 ft²

Total current = 3500 + 3500 = 7000 Amps

APPENDIX

ENGINEERING-SCIENCE, ARCADIA, CALIFORNIA

PLANT: TARBY, INC.
SOURCE: OUTLET
DATE: 12-11-86
RUN#: 1 PARTICULATE

FLOW DATA

STACK DIAMETER (INCHES)	28
STACK CROSS-SECTIONAL AREA (SQUARE FT)	4.28
BAROMETRIC PRESSURE (INCHES MERCURY)	29.5
OXYGEN CONTENT (%)	20.8
CARBON DIOXIDE (%)	0
MOISTURE CONTENT (%)	1.34
STACK TEMPERATURE (DEG F)	57
STACK STATIC PRESSURE (INCHES WATER)	.84
DRY STACK GAS MOLECULAR WEIGHT	28.832
VELOCITY PRESSURE (SQ RT INCHES WATER DELTA P)	.39
PITOT TUBE CORRECTION FACTOR	.84
VELOCITY (FEET PER SEC)	21.87
EXHAUST GAS FLOW RATE (ACFM)	5611
EXHAUST GAS FLOW RATE (DSCFM)	5490

SAMPLING DATA

DRY GAS VOLUME SAMPLED (DCF)	55.524
DRY GAS VOLUME SAMPLED (DSCF)	51.473
DRY GAS METER TEMP (DEG F)	83
DRY GAS METER GAMMA	.98
AVERAGE ORIFICE PRESSURE (INCHES H2O)	.75
TOTAL RUN TIME (MINUTES)	120
NOZZLE DIAMETER (INCHES)	.25
ISOKINETIC (%)	99.8

LABORATORY DATA

VOLUME OF MOISTURE RECOVERED (MLS)	15
PARTICULATE WEIGHT FROM NOZZLE & PROBE (MG)	12.5
PARTICULATE WEIGHT FROM FILTER (MG)	.01
PARTICULATE WEIGHT FORM IMPINGERS (MG)	0

PARTICULATE DATA

FRONT HALF PART (GR/DSCF)	3.8E-03
FRONT HALF PART (LBS/HR)	.18
BACK HALF PART (GR/DSCF)	0
BACK HALF PART (LBS/HR)	0
TOTAL PART (GR/DSCF)	3.8E-03
TOTAL PART (LBS/HR)	.19

Outlet Chome corrected to 8075 DSCFM

	<u>PPM</u>	<u>Q_s DSCFM</u>	<u>Lb/hr</u>
C _r ^{TL}	0.0162	8075	0.0011
C _r ^T	6.0562	8075	0.0037

$$(PPM)(1.58 \times 10^{-7})(MW)(Q_s) = \underline{\underline{Lb/hr}}$$

This correction is included
 due to the difference in inlet and outlet
 CFM. Since the corrected flow rate is higher,
 the emission values are conservative

Sample # 961254

Run # 1 Test Date 12-11-70

Facility TRACY COURT

[illegible]

Sample # BUNCK

Run # Test Date 12-11-86

Facility TRACY

[illegible]

TRAIN RECOVERY SHEET

Date 12-11-86
 Facility TIRBY OJUT
 Technician RR

Run # 1 OUT Method #
 Type CR 5
 Imp. Solution HW
ESH 861217

	Solution	Vol. (ml)	Volume Marked?	
Nozzle- Probe Rinse			✓	
Umbilical Rinse			✓	
		Final (ml)	Initial (ml)	Net (ml)
Impinger # <u>1-3</u>		<u>210</u>	<u>200</u>	<u>10</u>
Impinger # <u> </u>				
Impinger # <u> </u>				
Description				
Impinger Rinse				
		Final (g)	Initial (g)	
Silica Gel (Description)		<u>875.0</u>	<u>875.0</u>	<u>5.0</u>
Filter # (Description)	<u>860746</u>	Total Moisture		<u>15.0 ml</u>

Field Blanks

Disposition/Comments

TRAIN RECOVERY SHEET

Date 12-11-74

Run # 1-1N Method # _____

Facility MMM INCT

Type ✓

Technician RR

Imp. Solution HW

524 80135

Solution	Vol. (ml)	Volume Marked?	
Nozzle- Probe Rinse		✓	
Umbilical Rinse		✓	
	Final (ml)	Initial (ml)	Net (ml)
Impinger # <u>1-3</u>	<u>70</u>	<u>70</u>	<u>—</u>
Impinger # _____			
Impinger # _____			
Description			
Impinger Rinse			
Silica Gel (Description)	Final (g)	Initial (g)	
<u>USC7</u>	<u>876.10</u>	<u>851.3</u>	<u>19.7</u>
<u>1/4 USC7</u>	<u>847.4</u>	<u>832.2</u>	<u>10.2</u>
Filter # (Description)	Total Moisture		<u>29.3 ml</u>

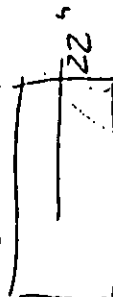
Field Blanks

Disposition/Comments

FIELD DATA

PLANT TARRY
 DATE 12-11-82
 SAMPLING LOCATION OUTLET
 SAMPLE TYPE LIQUID
 RUN NUMBER 1
 OPERATOR KAY
 AMBIENT TEMPERATURE 71
 BAROMETRIC PRESSURE 29.4
 STATIC PRESSURE (PSI) 8503.42
 FILTER NUMBER (IN) 8503.42

ES# 801217
 PROBE LENGTH AND TYPE 17.155 4FT
 NOZZLE I.D. 3/8"
 ASSUMED MOISTURE, % 0
 SAMPLE BOX NUMBER 34
 METER BOX NUMBER 34
 METER ΔP 2.17
 C FACTOR 10.98
 PROBE HEATER SETTING —
 HEATER BOX SETTING —
 REFERENCE ΔP —



SCHEMATIC OF TRAVERSE POINT LAYOUT

READ AND RECORD ALL DATA EVERY 10 MINUTES

K = 4.5

TRAVERSE POINT NUMBER	SAMPLING TIME, min	CLOCK TIME (24 hr CLOCK)	GAS METER READING (V _m), ft ³	VELOCITY HEAD (ΔP _s), in. H ₂ O	ORIFICE PRESSURE DIFFERENTIAL (ΔH), in. H ₂ O		STACK TEMPERATURE (T _s), °F	DRY GAS METER TEMPERATURE		PUMP VACUUM, in. Hg	SAMPLE BOX TEMPERATURE, °F	IMPING TEMPERATURE, °F
					DESIRED	ACTUAL		INLET (T _{m in}), °F	OUTLET (T _{m out}), °F			
1	10	9:35	7810.74	0.16	45	45	55	70	—	3"	—	—
1	10	9:45	7845	0.09	41	41	56	81	—	3"	—	—
1	30	9:55	7889	0.09	41	41	56	81	—	3"	—	—
1	30	10:05	7915	0.09	41	41	57	85	—	3"	—	—
1	40	10:15	7951	0.09	41	41	57	85	—	3"	—	—
1	50	10:25	7989.9	0.05	33	33	58	85	—	3"	—	—
1	60	10:35	8030.0	0.27	123	123	58	85	—	5"	—	—
1	70	10:45	8081	0.24	103	108	57	85	—	5"	—	—
1	80	10:55	8126	0.24	103	103	57	85	—	5"	—	—
1	90	11:05	8175	0.24	108	108	58	85	—	5"	—	—
1	100	11:15	8250	0.35	113	113	58	83	—	5"	—	—
1	110	11:25	8308	0.35	112	112	58	83	—	5"	—	—
1	120	11:35	8365.98	—	—	—	—	—	—	—	—	—
TOTAL 120 min. NA = 55.524 VA = 0.39 RH = 0.75 TS = 57 Tm = 83 VSL (H2O) = 15.0												

REMARKS:

FIELD DATA

PLANT ARBY INC.
 DATE 11 DEC 86
 SAMPLING LOCATION SCULPTURE INLET
 SAMPLE TYPE GC
 RUN NUMBER 1
 OPERATOR SP
 AMBIENT TEMPERATURE 70
 BAROMETRIC PRESSURE 29.7
 STATIC PRESSURE (PSI) 29.7
 FILTER NUMBER (4) 830347

DATE 861255
 PROBE LENGTH AND TYPE 5' G/207
 NOZZLE I.D. 2.5
 ASSURED MOISTURE % 5.0
 SAMPLE BOX NUMBER
 METER BOX NUMBER #3
 METER ΔH 193/1.02
 C FACTOR
 PROBE HEATER SETTING NONE
 HEATER BOX SETTING NONE
 REFERENCE ΔP

SCHEMATIC OF TRAVERSE POINT LAYOUT

STACK DIA = 28"

READ AND RECORD ALL DATA EVERY 10 MINUTES

K = 4.1

TRAVERSE POINT NUMBER	SAMPLING TIME, min	CLOCK TIME (24 hr CLOCK)	GAS METER READING (V _g), in ³	VELOCITY HEAD (V _g), in. H ₂ O	ORIFICE PRESSURE DIFFERENTIAL (ΔH), in. H ₂ O		STACK TEMPERATURE (T _s), °F	DRY GAS METER TEMPERATURE		PUMP VACUUM, in. Hg	SAMPLE BOX TEMPERATURE, °F	IMPINGER TEMPERATURE, °F
					DESIRED	ACTUAL		INLET (T _{inlet}), °F	OUTLET (T _{outlet}), °F			
0	9:35		806.954	0.30	1.23	1.27	63	63		3		
10	9:45		814.2	0.32	1.31	1.35	64	66		3		
20	9:50		821.0	0.34	1.39	1.43	65	65.72		4		
30	10:00		825.0	0.34	1.39	1.43	66	71		4		
40	10:15		834.7	0.31	1.27	1.31	65.6	83		3		
50	10:25		841.0	0.31	1.27	1.31	66.8	86		3		
60	10:35		848.0	0.31	1.27	1.31	66.7	90		3		
70	10:45		854.530									
80	10:55		858.7	0.31	1.27	1.31	67.4	91		4		
90	11:05		865.9	0.31	1.27	1.31	67.1	92		3		
100	11:15		871.7	0.31	1.27	1.31	67.6	92		3		
110	11:25		878.5	0.31	1.27	1.31	69.0	93		3		
120	11:35		887.917									
TT = 120 min			V _m = 80.953	Q = 0.50	ΔH = 1.31	T _s = 66	T _m = 82				V _{60(H₂O)} = 121.3	

REMARKS:

The Determination of Hexavalent Chromium Emissions using a Diphenylcarbazide Colorimetric Method

Sample Analysis

The EPA Method 5 sampling trains were recovered in the laboratory. The probe wash and impinger solutions were combined, diluted to 500 ml and stored at room temperature. These samples were analyzed for hexavalent chromium within 24 hours after sampling following the procedure below.

The analytical procedure consisted of three steps. The initial step consisted of digesting the samples with an alkaline solution of sodium hydroxide and anhydrous sodium carbonate. The digested samples were then filtered. The second step involved reacting the digested and filtered samples with the diphenylcarbazide solution to produce the characteristic red-violet color which allowed the colorimetric determination of hexavalent chromium. The third step consisted of analyzing the reacted samples spectrophotometrically.

The samples were prepared for analysis by an initial digestion and filtration step. A 50 ml aliquot of each sample was taken and combined with approximately 40 ml of the digesting solution. This mixture was heated to near boiling with constant stirring for thirty minutes and then allowed to cool. After the solution had cooled, it was filtered through a 47-mm diameter, 3.0- μ m pore size Zeflur filter. The filtered solution was then transferred quantitatively into a 100 ml volumetric flask and diluted to the mark. A deionized water blank was prepared for analysis in the same manner.

Then the samples were reacted with a diphenylcarbazide solution. A 50 ml aliquot of the digested and filtered sample was transferred to another 100 ml volumetric flask and diluted with approximately 30 ml of deionized water. The pH of each sample was adjusted to 2 ± 0.5 with the dropwise addition of a 10% (v/v) H_2SO_4 solution.

Two ml of the diphenylcarbazide solution were added to each volumetric flask which was then diluted to the mark. This step was also carried out for seven calibration standards prepared from a standard potassium dichromate stock solution. The seven calibration standard solutions, ranging in concentration from $0.5 \mu g Cr^{+6}$ to $100 \mu g Cr^{+6}$, were used to obtain the spectrophotometric calibration factor, K_c . The samples and calibration standard solutions were allowed to stand for 15 minutes to allow full color development.

After full color development, the samples and calibration standard solutions were analyzed spectrophotometrically at the predetermined optimum wavelength.

EMISSION CALCULATIONS

~~The seven calibration~~

The spectrophotometric calibration factor, K_c , was calculated from the absorbance values obtained by the spectrophotometric measurement of the seven calibration standard solutions. The spectrophotometric calibration factor, K_c , was calculated using the following equation:

$$K_c = \frac{A_1 + 2A_2 + 5A_3 + 10A_4 + 15A_5 + 20A_6}{A_1^2 + A_2^2 + A_3^2 + A_4^2 + A_5^2 + A_6^2}$$

Where:

K_c = calibration factor

A_1 = absorbance of the 5 $\mu\text{g Cr}^{+6}$ standard

A_2 = " " " 10 $\mu\text{g Cr}^{+6}$ "

A_3 = " " " 25 $\mu\text{g Cr}^{+6}$ "

A_4 = " " " 50 $\mu\text{g Cr}^{+6}$ "

A_5 = " " " 75 $\mu\text{g Cr}^{+6}$ "

A_6 = " " " 100 $\mu\text{g Cr}^{+6}$ "

The total $\mu\text{g Cr}^{+6}$ in each sample, m , was calculated using the following equation:

$$m = \frac{500 K_c A F}{V_a}$$

Where 500 = volume in ml of total sample

A = absorbance of sample

F = dilution factor (if required)

V_a = volume in ml of aliquot analyzed (50)

Received: 12/15/86

TMA Inc.

REPORT

Work Order # 86-12-082

12/29/86 08:53:20

REPORT Engineering Science

TO 75 N. Fair Oaks Ave.

P.O. Box 7107

Pasadena, CA 91109

ATTEN Mr. Dennis Becvar

CLIENT ENGINEER SCI SAMPLES 9

COMPANY Engineering Science

FACILITY

WORK ID Chromium analyses

TAKEN:

TRANS

TYPE Liquids

P.O. # Verbal-D. Becvar

INVOICE under separate cover

PREPARED Thermo Analytical, Inc.

BY 150 Taylor Street

Monrovia, CA 91015

ATTEN

PHONE 818-357-3247

CONTACT GLO

CERTIFIED BY

Arnold D. Olsen

This report is for the sole and exclusive use of the client to whom it is addressed. Samples not destroyed in testing are retained a maximum of thirty (30) days unless otherwise requested.

SAMPLE IDENTIFICATION

01	861254-A
02	861254-B
03	861254-C
04	861255-A
05	861255-B
06	861255-C
07	Blank-A
08	Blank-B
09	Blank-C

TEST CODES and NAMES used on this report

CR	Chromium
CRHGAW	Chromium

Nine water samples were analyzed for chromium content by atomic absorption spectroscopy, according to TMA/ARLI methods 800-08 and 800-09. Three samples were done by flame AA and six samples (those with the +/- signs) were done by graphite furnace AA. Please see the table below for results.

Table 1

Chromium Analyses of Water Samples

Sample #	Chromium, mg/L
861254-A	0.2240 +/- 0.0100
861254-B	0.0340 +/- 0.0030
861254-C	0.0720 +/- 0.0004
861255-A	14.0
861255-B	0.56
861255-C	0.05
Blank-A	0.0130 +/- 0.0004
Blank-B	0.0070 +/- 0.0009
Blank-C	0.0460 +/- 0.0005

SOUTH COAST AIR QUALITY MANAGEMENT DISTRICT ENGINEERING DIVISION...FIELD REPORT

NAME OF APPLICANT TARBY ENGINEERING COMPANY, INC.				DATE OF INSPECTION 12/11/86	
MAILING ADDRESS 7601 Woodward Drive, Huntington Beach, California 92649				PERMIT APPL. NO. 125057 to 59	
EQUIPMENT LOCATION (ADDRESS) Same				A.P.C.B. TAG NO.	
REASON PERMIT IS REQUIRED:	NEW CONSTRUCTION ☒	CHANGE OF OWNERSHIP ☐	CHANGE OF LESSEE ☐	CHANGE OF LOCATION ☐	EQUIPMENT ALTERATION ☐
DATE CONSTRUCTION AUTHORIZED: _____ BY _____		TIME SPENT MAKING INSPECTION: FROM 9:30 a.m. TO 11:50 a.m.			
USUAL OPERATING SCHEDULE FOR THIS EQUIPMENT:					
WEATHER Clear		WIND ~ 3 mph		ESTIMATED BASIC EQUIPMENT COST: 8 A.P.C. EQUIPMENT: 8	
NAMES & TITLES OF PERSONS CONTACTED BY ENGINEER: John Alley-Tarby, Paul Farmanian & Jeffrey Fox-Engrg Science					
FOR DUST & FINE PROBLEMS ONLY:		PROCESS WEIGHT (S)	LOS. /HR.	ALLOWED LOSSES:	ESTIMATED LOSSES: 88

OFFICIAL EQUIPMENT DESCRIPTION. CALCULATION OF PROCESS WEIGHT(S). PROCESS DESCRIPTION AND FINDINGS:
EQUIPMENT DESCRIPTION: Air Pollution Control Equipment consisting of:
1. Scrubber, Viron, Packed horizontal cross-flow type, Model No. 115-1000 5'-3" W. x 7'-4" L. x 6'-6" H. with a 2 H.P. water recirculation pump, 1 foot deep Viron-Pak Packing 8" deep, Chevron blades mist eliminator, three headers, each with 3 spray nozzles and 1/2" h.p. sump Pump.
2. Exhaust System with a 15 H.P. blower venting two hard chrome plating tanks.

BACKGROUND

The applicant was required by the District to run a Source Test to determine the efficiency of scrubber (venting two hard chrome plating tanks) for PM, hexavalent and total chromium.

The applicant contracted Engineering Science of Pasadena. The test procedure was approved (verbally) by Steve Marinoff of the District on December 9, 1986. I discussed test procedures with Steve. Steve told me that for a Particulate Matter test; the wet impingement method, as given in District's Source Test manual is approved; the only change is the use of a glass probe instead of a metal probe. For hexavalent and total chromium, CARB Method No. 425 was approved.

OBSERVATIONS

The Source Test was conducted on December 11, 1986. Wet impingement method was used for total PM. There were three impingers located in ice-baths followed by a filter and a silica gel container. A glass probe was used to collect the sample. One glass probe was installed at approximately eight diameters from the last 90° bend upstream on the scrubber.

The probe downstream of the scrubber was installed approximately two diameters downstream of the exhaust fan (which is located at the outlet of the scrubber). pH of scrubber solution was between 5.5 & 6.0
water recirculation rate = 95 g.p.m.

RECOMMENDED DISPOSITION:	☐ APPROVE FOR PERMIT.	☐ APPROVE FOR PERMIT SUBJECT TO CONDITIONS LISTED BELOW.	☒ HOLD. SEE EXPLANATION BELOW.	☐ DENY PERMIT.
--------------------------	--	---	--	---------------------------------------

Hold until evaluation is completed

REVIEWING ENGINEER:
☐ I CONCUR WITH RECOMMENDATIONS
☐ I DO NOT CONCUR WITH RECOMMENDATIONS

SIGNATURE

DJB- (44) 572-6178
Desh B. Jain, A.Q. Engineer II

South Coast Air Quality Management District Engineering Division...Field Report

NAME OF APPLICANT	APPL. NO.	INSPECTION DATE
TARBY ENGINEERING COMPANY, INC.	125057 -59	12/11/86

BASIC EQUIPMENT

Both the chrome plating tanks were operating with normal/above normal load. A 6' high chrome plating tank (A/N 125058) had five parts (from 2' to 5' long) for plating. This was the normal load according to Mr. John Alley. (This was confirmed later from Mr. Mark Dixon, the plater). The rectifier reading was 3500 A, 5.5 V.

The other chrome plating tank (A/N 125059) had one large size part - 9" diameter x 12 feet long (equivalent to at least 4 times the normal size parts). This represented more than the normal load for this tank according to Mr. Dixon. Rectifier reading: 3500 A, 6.6 V.

Mr. Dixon told me that the combined current on the two tanks very rarely exceed 7000 amps.

There was good suction at both chrome plating tanks.

Note: Total surface area of two tanks = 50 ft².

es: 3/3/87

SIGNATURE

DBT