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## **Background Report Reference**

**AP-42 Section Number:** 12.20

**Background Chapter:** 4

**Reference Number:** 44

**Title:** Source Test Report of Ceko Filters  
Demonstration Unit Serving a Hard  
Chrome Plating Tank at Chrome  
Plating Company, 1748 Workman  
Street, Los Angeles, CA

PES

March 1989

SCREENING TEST

Source Test Report of a Ceko Filters Demonstration Unit  
Serving a Hard Chrome Plating Tank at  
Chromal Plating Company, 1748 Workman Street,  
Los Angeles, CA 90031

Conducted for the  
Metal Finishing Association of Southern California  
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3/1/89

Source Test Report of a Ceko Filters Demonstration Unit  
Serving a Hard Chrome Plating Tank at  
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Los Angeles, CA 90031

## INTRODUCTION

Pacific Environmental Services, Inc. (PES) was contracted by the Metal Finishing Association of Southern California (MFASC), to perform a screening test on the reduction efficiency of a Ceko Filters, Inc demonstration unit used to collect hexavalent chromium emissions from a hard chrome plating operation. Set up and velocity determinations were conducted on February 11, and the source testing was done on February 13, 1989.

In order to evaluate the effectiveness of the Ceko unit, it was necessary to have a hard chrome plating tank that was outfitted with an emission collection system. Chromal Plating Co. in Los Angeles, Ca, was the site chosen for the testing. Ray Bokelman, General Manager of Chromal Plating, arranged for the hookup of the demonstration unit and the tank operation during source testing.

A slip stream was taken from the main emission collection exhaust to supply the Ceko Filters, Inc Unit. The location of the extraction was approximately 6 feet before the main scrubber of Chromal Plating as shown in Figures 1 and 2. The diameter of the main duct was 24" I.D. and the slip stream was 7" I.D. narrowing down to 6" I.D.

On February 13, three locations were chosen for sampling. The first sample, C-MI-1, was taken from the main exhaust before the slip stream extraction point. This was done in order to test the Isokinetics of the slip stream system. The second sample was taken from the slip stream 6' 10" before the inlet to the demonstration unit. This sample was used to determine the quantity of emissions in the gas stream before entering the Ceko unit. The third sample was taken from the stack outlet of the Ceko unit 38" from the bottom of the stack. This sample was used to determine the emission rate and subsequently the reduction efficiency of the Ceko unit for total and hexavalent chromium emissions. Continuous velocity measurements were made with a type "S" pitot tube at the main exhaust sample location and with standard pitot tubes 54" inches after the inlet sample location, and 21" after the outlet sample location. All sampling locations and velocity measurement locations are shown in Figures 1 and 2.

Table 1: Diagram of Slip Stream System and Sample Locations

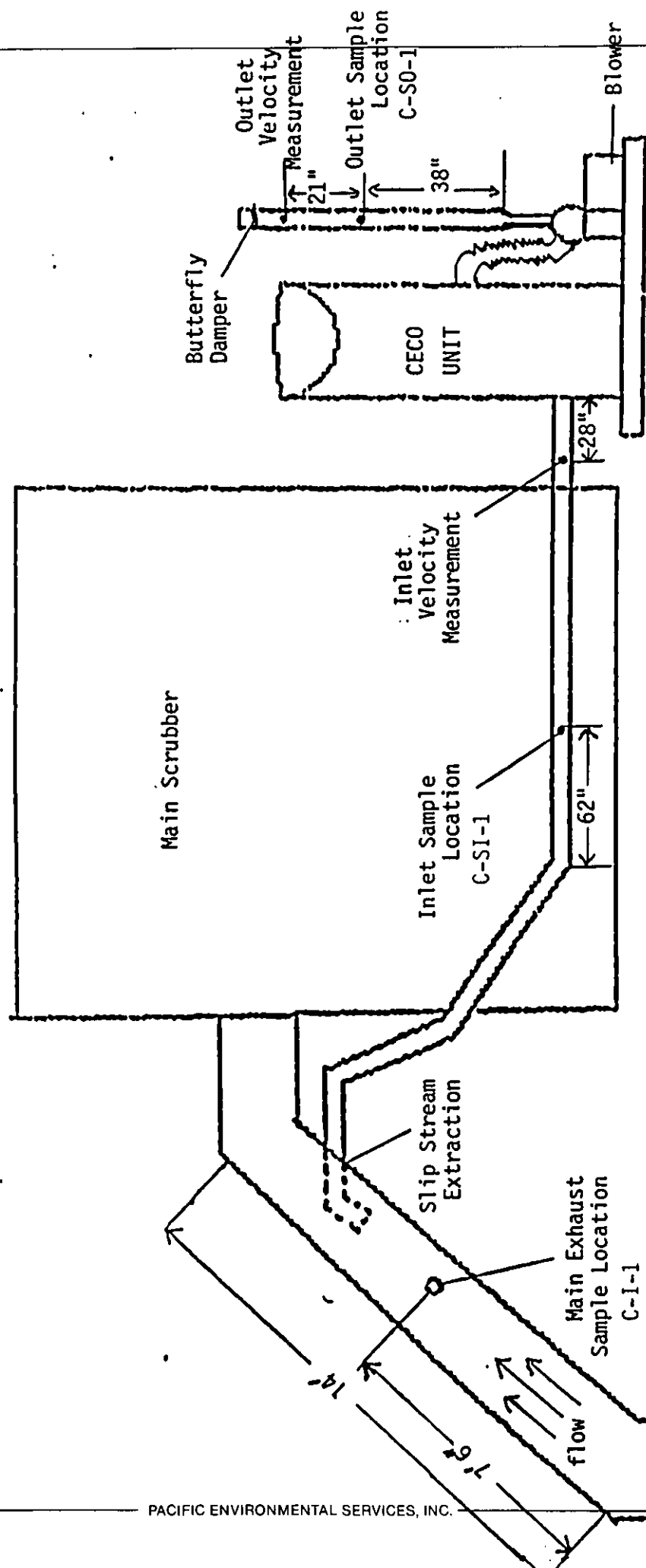
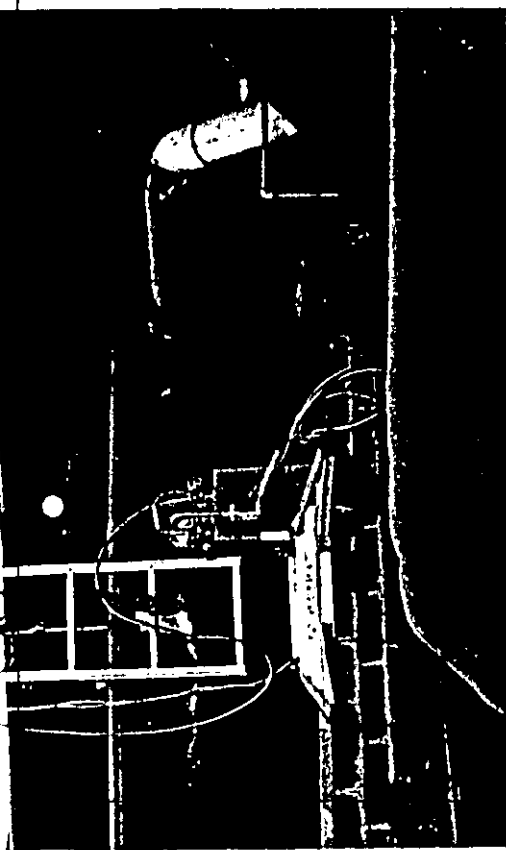
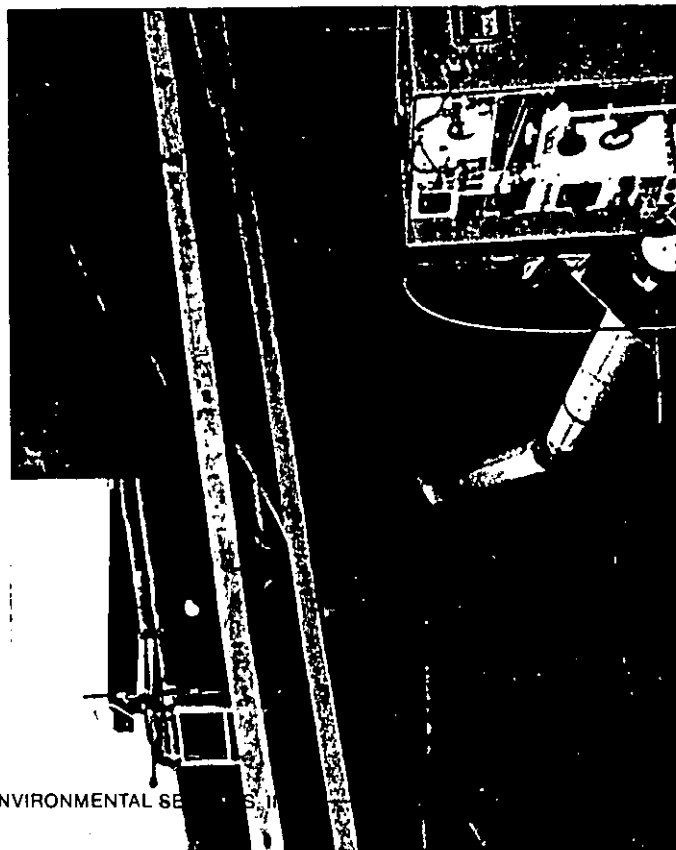


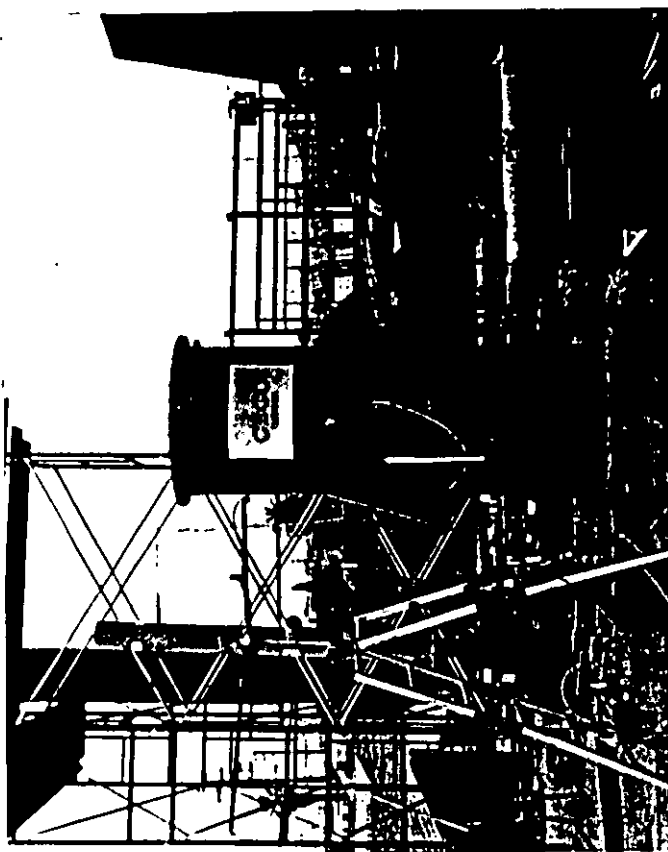
Figure 2: Sample Locations



Main Exhaust Sample Location: C-I-1



Slip Stream Sample Location: C-SI-1



Stack Outlet Sample Location: C-SO-1

## EQUIPMENT AND PROCESS DESCRIPTION

Chromal Plating Company, 1748 Workman Street, Los Angeles, CA 90031, is engaged in the business of hard chrome plating for the aircraft and a wide variety of other industries. During the test, the Ceko unit served hard chrome plating tank No. 1. The dimensions of tank No. 1 were 7' x 6' x 8'. The chrome concentration of Tank No. 1 during the test was 30% Chromic Acid. During the test the tank was covered 100% by 3/4" polyballs and the mixing air was turned off. The temperature of the tank was maintained at 120 Fahrenheit, the voltage averaged 4.5 volts, and the amperage averaged 853 amps.

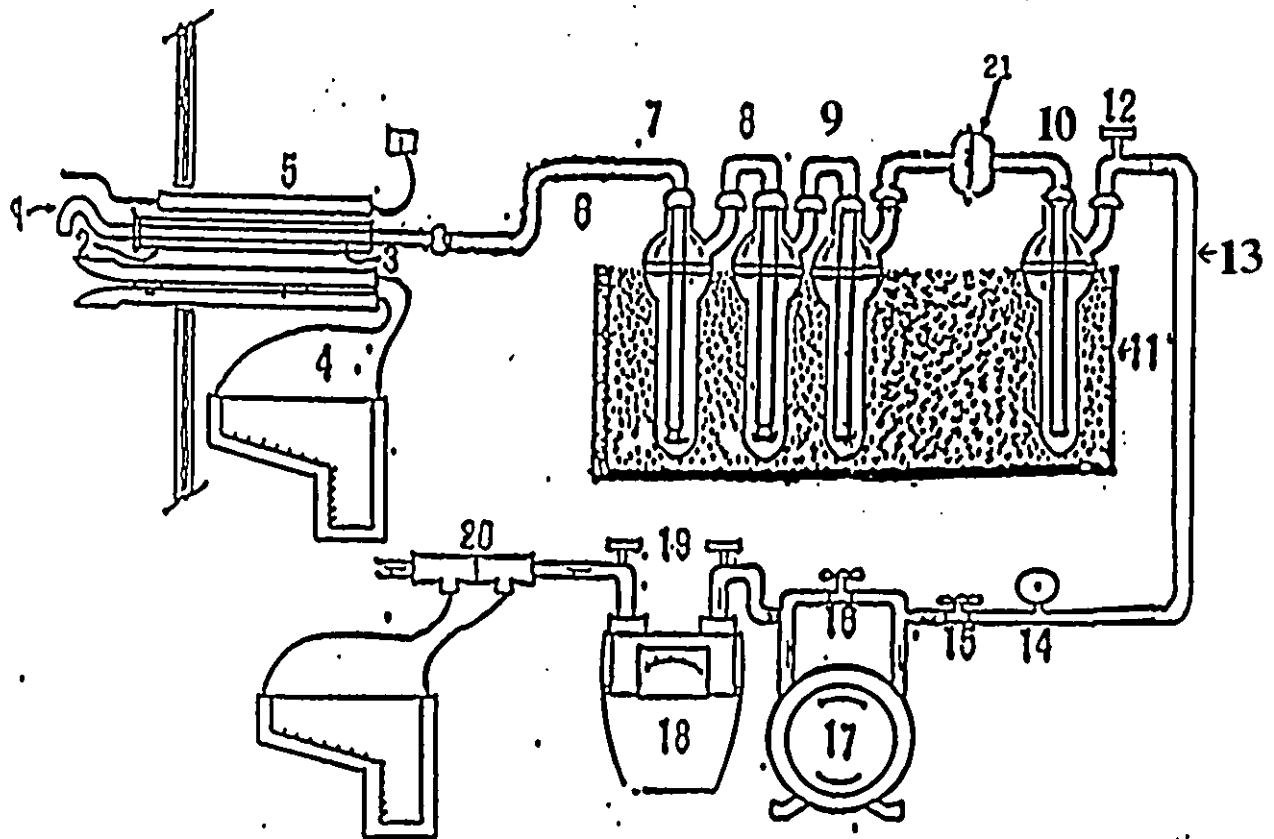
The Ceko chromic acid removal system utilized several control mechanisms. These included particle settling, inertial impaction, direct interception, particle size control, condensation, and Brownian diffusion. The Ceko unit weighed about 3000 pounds when wetted. The blower motor was 3 HP, and could handle flow rates up to 500 ACFM.

## TESTING METHODOLOGY

The samples at each location were extracted with modified CARB method 425 source testing trains as described in a 1/20/89 CARB protocol (Figure 3). The source sampling trains consisted of a 0.234" - 0.310" I.D. glass nozzle, a glass probe, two impingers each with 100 ml of 0.1N sodium hydroxide, an empty impinger, an 89mm teflon coated glass fiber filter placed after the empty impinger, an impinger filled with silica gel, an umbilical cord connected to a vacuum pump, a dry gas meter, and a calibrated orifice connected to an inclined manometer.

Sampling at the three ports was conducted simultaneously for a period of 8 hours; however after 6 hours and 13 minutes the impinger with silica gel imploded so that sample was cut short immediately. Sampling was done by traversing at each location. Velocity and temperature of the emission streams were measured and recorded every 20 minutes for the main exhaust, every hour for the slip stream sample, and every 30 minutes for the outlet sample during the test. The meter temperature and the volume of the gas through the meter also were measured and recorded at the same intervals for each location. Applied voltage, bath temperature, and amperage applied to the chrome plating tank was also recorded. All information was recorded on field data sheets (Appendix).

Laboratory analyses were conducted by Thermo Analytical Laboratory in Monrovia, CA. Total chrome and hexavalent chrome concentrations were determined for the three stack samples, a



1. Glass or stainless steel sampling nozzle
2. Stainless steel probe sheath
3. Stainless steel, glass, or Teflon-lined probe
4. Type S pitot tube and manometer for  $\Delta P$  readings
5. Stack temperature sensor
6. 15 ft. teflon probe line with ball and socket connectors
7. Greenburg-Smith impinger with 100 ml. of .1 N NaOH solution
8. Greenburg-Smith impinger with 100 ml. of .1 N NaOH solution
9. Modified Greenburg-Smith impinger - dry
10. Modified Greenburg-Smith impinger filled with 200 grams of silica gel
11. Impinger case filled with ice
12. Impinger exit gas temperature sensor
13. Umbilical line to meter box
14. Vacuum gauge
15. Coarse adjustment valve
16. By-pass valve to adjust  $\Delta H$
17. Leak free vacuum pump
18. Dry gas meter
19. Dry gas meter inlet and outlet temperature sensors
20. Orifice meter with manometer for  $\Delta H$  readings
21. Filter Holder with teflon-lined glass fiber filter.

FIGURE 3  
Diagram Of Sampling Train

blank, and the plating bath solution. Analyses for total chrome used atomic absorption spectrophotometry and analyses for hexavalent chrome used diphenylcarbazine colorimetric techniques.

## RESULTS OF TESTING

After running 6 hours and 13 minutes, sampling was discontinued at the main exhaust port because of damage to the silica gel impinger. The bottom of the impinger had broken off and ice water was sucked into the pump. The inlet and outlet samples were not affected and testing continued at these two points for the full eight hours.

Flow rates in the main exhaust stream and the extraction duct were intended to provide near isokinetic velocities. From the measured flow rates the two velocities were calculated as follows.

|           |            |          |
|-----------|------------|----------|
| 24" duct  | 6678 dscfm | 34.9 fps |
| 7.2" duct | 616 dscfm  | 36.3 fps |

The main exhaust gas stream showed 0.00429 mg/scf for total chrome and 0.00346 mg/scf for hexavalent chrome. The slip stream extraction showed 0.00281 mg/scf for total chrome and 0.00217 mg/scf for hexavalent chrome.

Calculations were made from the field data sheets to determine sample volume, molecular weight, velocities, flow rates, and isokinetic testing for the gas at each sample location. Stack gas volumes were calculated from the velocity measurements taken simultaneously during sample extraction. Results are shown on the emission test calculation sheets (Appendix).

The inlet loading to the Ceko demonstration unit was 103.93 mg/hour for total chrome and 80.2 mg/hour for hexavalent chrome. The outlet emissions were 3.55 mg/hour for total chrome and 1.43 mg/hour for hexavalent chrome. In order to express the efficiency in mg/amp-hour the total gas flow needed to be used and the results divided by the amp-hours. The control efficiency for total chrome was calculated at 97.0% and for hexavalent chrome was calculated at 98.4% (Table 1).

It should be noted that the main purpose of the screening test was to determine whether the sampling system was set up properly and whether the demonstration unit was functioning at full capacity. On February 15, 1989, Mr. John Watkins, a Ceko Filters, Inc representative, removed the observation port on top of the unit



and discovered that some of the filter holders within the unit had become loose and disaligned and a water line had been cracked during shipping. Mr. Watkins repaired the unit and hosed down the effluent side of the filter and stack with tap water. The unit was restarted and operated 3 or 4 days at design conditions before the CARB tests which started on 2/22/89.

Table 1: Control Efficiency of the Deco Filter, Inc. Demonstration Unit. SCREENING TEST

| Sample Run Number | Sample Volume gal | Conc. Cr T<br>mg/l | Conc. Cr 6<br>mg/l | Cr T<br>mg | Cr 6<br>mg | Sample Meter Vol<br>dscf | Emissions Cr T<br>mg/scf | Emissions Cr 6<br>mg/scf | Flow Rate<br>dscfe | Actual Emissions |                 |
|-------------------|-------------------|--------------------|--------------------|------------|------------|--------------------------|--------------------------|--------------------------|--------------------|------------------|-----------------|
|                   |                   |                    |                    |            |            |                          |                          |                          |                    | Cr T<br>mg/hour  | Cr 6<br>mg/hour |
| C-MI-1            | 570               | 2.81               | 2.27               | 1.6017     | 1.2939     | 373.578                  | 0.00429                  | 0.00346                  | 6678               | 1717.90          | 1387.77         |
| C-SI-1            | 926               | 1.27               | 0.98               | 1.1760     | 0.9075     | 418.213                  | 0.00281                  | 0.00217                  | 616                | 103.93           | 80.2            |
| C-SO-1            | 880               | 0.0571             | 0.023              | 0.0502     | 0.0202     | 593.164                  | 0.00008                  | 0.00003                  | 698                | 3.55             | 1.43            |

| Sample Run Number | Adjusted Total     |                                    | Total Emissions              |                 | Average              |           | Emissions           |                     | Control Efficiency |           |
|-------------------|--------------------|------------------------------------|------------------------------|-----------------|----------------------|-----------|---------------------|---------------------|--------------------|-----------|
|                   | Flow Rate<br>dscfe | Total Emissions<br>Cr T<br>mg/hour | Emissions<br>Cr 6<br>mg/hour | Cr 6<br>mg/hour | Average<br>Amp-hours | Amp-hours | Cr T<br>mg/amp-hour | Cr 6<br>mg/amp-hour | Cr T<br>%          | Cr 6<br>% |
| C-MI-1            | 6678               | 1717.899                           | 1387.769                     | 853             | 2.0139               | 1.6269    | 2.0139              | 1.6269              |                    |           |
| C-SI-1            | 6678               | 1126.717                           | 869.435                      | 853             | 1.3209               | 1.0193    | 1.3209              | 1.0193              |                    |           |
| C-SO-1            | 6678               | 33.96                              | 13.68                        | 853             | 0.0398               | 0.016     | 0.0398              | 0.016               | 97.0               | 98.4      |

Note: The filters on all three test trains contained no more Cr 6 than the blanks, so results are not shown.  
The laboratory report is appended



## APPENDICES

# EMISSION TEST CALCULATIONS

## Definition of Symbols

- A           = cross-sectional area of stack, ft<sup>2</sup>
- A<sub>n</sub>          = Cross-sectional area of Nozzle, ft<sup>2</sup>
- W<sub>w</sub>         = Water vapor in gas stream, proportional by volume
- C<sub>p</sub>          = Pilot tube coefficient
- I            = Percent of Isokinetic Sampling
- M<sub>d</sub>          = dry molecular weight, lb/lb-mole
- M<sub>w</sub>          = Molecular weight of stack gas, lb/lb-mole
- P<sub>bar</sub>        = Barometric Pressure at the sampling site, in Hg
- P<sub>s</sub>          = Stack gas pressure, in. Hg
- Q<sub>s</sub>          = Stack volumetric flow rate, actual condition acfm
- Q<sub>(std)</sub>       = stack volumetric flow rate, actual conditions dscfm
- T<sub>m</sub>          = Average dry gas meter temperature, R = 460° + F°
- T<sub>s</sub>          = Average stack gas temperature, °R = 460° + F°
- V<sub>ic</sub>         = Total volume of liquid collected in impingers and silica gel, ml
- V<sub>m</sub>          = Volume of gas sample as measured by dry gas meter, dscf
- V<sub>m(std)</sub>       = V<sub>m</sub> corrected to standard conditions, dscf
- V<sub>w(std)</sub>       = Volume of water vapor in gas sample corrected to standard conditions, scf
- V<sub>s</sub>          = Stack gas velocity, ft/sec
- Y            = Dry gas meter calibration factor
- ΔH          = Average pressure differential across the orifice meter, in. H<sub>2</sub>O
- θ            = Total Sampling Time, min.
- 13.6         = Specific gravity of Mercury

Plant: Chromal - Ceco Unit  
 Date: 2-13-84  
 Source/Sample Number: C-MI-1

$$1. V_m(std) = 17.64 V_m Y \left[ \frac{P_{bar} + (\Delta H / 13.8)}{T_m} \right]$$

$$V_m(std) = 17.64 (368.115)(1.003) \left[ \frac{(30.64) + (3.53 / 13.8)}{(538.7)} \right]$$

$$V_m(std) = \underline{373.578} \text{ dsof}$$

2. Volume Water Vapor Collected, Standard Conditions

$V_{10} = \underline{\quad / \quad}$  condensate from impingers and Silica Gel

$V_H(std) = .04707 V_{10} = \underline{\quad / \quad}$  sof

$V_H(std) = \underline{\quad / \quad}$  sof

3. Percent Moisture, by volume

$$B_{H_2O} = \frac{V_H(std)}{V_H(std) + V_m(std)} = \frac{(\quad / \quad)}{(\quad / \quad) + (\quad / \quad)} = \underline{0.006}$$

$$B_{H_2O} = \underline{0.6 \%} \text{ obtained from sample C-SI-1}$$

4. Molecular Weight, Stack gas

Dry Molecular Weight

$$M_d = 0.440 (\% \text{ CO}_2) + 0.320 (\% \text{ O}_2) + 0.280 (\% \text{ N}_2 + \% \text{ CO})$$

$$M_d = 0.440 (\quad) + 0.320 (\quad) + 0.280 (\quad)$$

$$M_d = \underline{29.0} \text{ lb/lb-mole}$$

$$M_g = M_d + B_{H_2O} (18 - M_d) = (29.0) + (0.006) (18 - 29.0)$$

$$M_g = \underline{28.93} \text{ lb/lb-mole}$$

Plant: Chromal Coco Unit  
 Date: 2-13-89  
 Source/Sample Number: C-MI-1

5. Stack Gas Velocity Average

$$V_s(\text{avg}) = 85.49 C_D (\sqrt{\Delta P}) \text{ avg} \sqrt{\frac{T_s}{P_s M_s}}$$

$$V_s(\text{avg}) = 85.49 (0.84) (0.6294) \sqrt{\frac{(528.8)}{(30.57)(28.93)}}$$

$$V_s(\text{avg}) = \underline{34.95} \text{ - ft/sec.}$$

6. Stack Volumetric Flow Rate, Actual Conditions (Stack Temperature and Pressure)

$$Q_s = 60 V_s A = 60 (34.95) (3.14)$$

$$Q_s = \underline{6588} \text{ acfm}$$

7. Stack volumetric flow rate, standard conditions (68° F, 29.92 Hg)

$$Q(\text{std}) = 17.64 Q_s (1 - B W_s) \frac{P_s}{T_s}$$

$$Q(\text{std}) = 17.64 (6588) (1 - 0.006) \left( \frac{30.57}{528.8} \right)$$

$$Q_{\text{std}} = \underline{6678} \text{ dsocm}$$

8. Isokinetic Variation

$$\%I = K \frac{T_s V_m(\text{std})}{P_s V_s A_n \theta (1 - B W_s)}$$

$$= 0.0845 \frac{(528.8)(37350)}{(30.57)(34.95)(0.00524)(373)(1 - 0.006)}$$

$$\%I = \underline{89.9} \%$$

Plant: Chronal - Coco Unit  
 Date: 2-13-89  
 Source/Sample Number: C-ST-1

$$1. V_m(\text{std}) = 17.64 V_m \cdot Y \left[ \frac{P_{\text{bar}} + (\Delta H / 13.6)}{T_m} \right]$$

$$V_m(\text{std}) = 17.64 (406.02)(0.993) \left[ \frac{(30.64) + (2.94/13.6)}{(524.8)} \right]$$

$$V_m(\text{std}) = \underline{418.213} \text{ scf}$$

2. Volume Water Vapor Collected, Standard Conditions

$V_{10} = \underline{51.6}$  condensate from impingers and Silica Gel

$$V_H(\text{std}) = .04707 V_{10} = \underline{2.43} \text{ scf}$$

$$V_H(\text{std}) = \underline{2.43} \text{ scf}$$

3. Percent Moisture, by volume

$$B_{H_2O} = \frac{V_H(\text{std})}{V_H(\text{std}) + V_m(\text{std})} = \frac{(2.43)}{(2.43) + (418.213)} = \underline{0.006}$$

$$B_{H_2O} = \underline{0.6 \%}$$

4. Molecular Weight, Stack gas

Dry Molecular Weight

$$M_d = 0.440 (\% \text{ CO}_2) + 0.320 (\% \text{ O}_2) + 0.280 (\% \text{ N}_2 + \% \text{ CO})$$

$$M_d = 0.440 ( \quad ) + 0.320 ( \quad ) + 0.280 ( \quad )$$

$$M_d = \underline{29.0} \text{ lb/lb-mole}$$

$$M_s = M_d + B_{H_2O} (18 - M_d) = (29.0) + (0.006)(18 - 29.0)$$

$$M_s = \underline{28.93} \text{ lb/lb-mole}$$

Plant: Chromal Coco Unit  
 Date: 2-13-89  
 Source/Sample Number: C-5I-1

5. Stack Gas Velocity Average

$$V_s(\text{avg}) = 85.49 C_D (\sqrt{\Delta P}) \text{avg} \sqrt{\frac{T_s}{P_s H_s}}$$

$$V_s(\text{avg}) = 85.49 (0.99)(0.7852) \sqrt{\frac{523}{(30.46)(28.93)}}$$

$$V_s(\text{avg}) = \underline{51.2} \text{ ft/sec.}$$

6. Stack Volumetric Flow Rate, Actual Conditions (Stack Temperature and Pressure)

$$Q_s = 60 V_s A = 60 (51.2) \left( \frac{36 \pi}{57} \right)$$

$$Q_s = \underline{2443.603} \text{ acfm}$$

7. Stack volumetric flow rate, standard conditions (68° F, 29.92 Hg)

$$Q(\text{std}) = 17.64 Q_s (1-BW_s) \frac{P_s}{T_s} =$$

$$Q(\text{std}) = 17.64 (603) (1-0.006) \left( \frac{30.46}{523} \right)$$

$$Q_{\text{std}} = \underline{616} \text{ dscfm}$$

8. Isokinetic Variation

$$\%I = K \frac{T_s V_m(\text{std})}{P_s V_s A_n \theta (1-BW_s)}$$

$$= 0.0945 \frac{(523)(419.213)}{(30.46)(51.2)(0.00242)(480)(1-0.006)}$$

$$\%I = \underline{94.9} \%$$



Plant: Chromal - CECO - Unit  
 Date: 2-13-89  
 Source/Sample Number: C-50-1

$$1. V_m(\text{std}) = 17.64 V_m \cdot Y \left[ \frac{P_{\text{bar}} + (\Delta H / 13.8)}{T_m} \right]$$

$$V_m(\text{std}) = 17.64 (585.686) (.9967) \left[ \frac{(30.64) + (5.01 / 13.8)}{(578.3)} \right]$$

$$V_m(\text{std}) = \underline{593.164} \text{ dsof}$$

2. Volume Water Vapor Collected, Standard Conditions

$$V_{10} = \underline{83.6} \text{ condensate from impingers and Silica Gel}$$

$$V_H(\text{std}) = .04707 V_{10} = \underline{3.94} \text{ sof}$$

$$V_H(\text{std}) = \underline{3.94} \text{ sof}$$

3. Percent Moisture, by volume

$$B_{H_2} = \frac{V_H(\text{std})}{V_H(\text{std}) + V_m(\text{std})} = \frac{(3.94)}{(3.94) + (593.164)} = \underline{0.0066}$$

$$B_{H_2} = \underline{0.66 \%}$$

4. Molecular Weight, Stack gas

Dry Molecular Weight

$$M_d = 0.440 (\% \text{ CO}_2) + 0.320 (\% \text{ O}_2) + 0.280 (\% \text{ N}_2 + \% \text{ CO})$$

$$M_d = 0.440 ( \quad ) + 0.320 ( \quad ) + 0.280 ( \quad )$$

$$M_d = \underline{29.0} \text{ lb/lb-mole}$$

$$M_s = M_d + B_{H_2} (18 - M_d) = (29.0) + (0.0066) (18 - 29.0)$$

$$M_s = \underline{28.93} \text{ lb/lb-mole}$$

Plant: Chromal Ceco - Unit  
 Date: 2-13-89  
 Source/Sample Number: C-50-1

5. Stack Gas Velocity Average

$$V_s(\text{avg}) = 85.49 \text{ Cp } (\sqrt{\Delta P}) \text{ avg } \sqrt{\frac{T_s}{P_s H_s}}$$

$$V_s(\text{avg}) = 85.49 (0.84) (1.0527) \sqrt{\frac{(531.7)}{(30.79)(28.93)}}$$

$$V_s(\text{avg}) = \underline{58.4} \text{ - ft/sec.}$$

6. Stack Volumetric Flow Rate, Actual Conditions (Stack Temperature and Pressure)

$$Q_s = 60 V_s A = 60 (58.4) \left( \frac{30.79}{144} \right)$$

$$Q_s = \underline{688} \text{ acfm}$$

7. Stack volumetric flow rate, standard conditions (68° F, 29.92 Hg)

$$Q(\text{std}) = 17.64 Q_s (1 - B_{H_2O}) \frac{P_s}{T_s}$$

$$Q(\text{std}) = 17.64 (688) (1 - 0.0066) \left( \frac{30.79}{531.7} \right)$$

$$Q_{\text{std}} = \underline{698} \text{ dsicfm}$$

8. Isokinetic Variation

$$\%I = K \frac{T_s V_m(\text{std})}{P_s V_s A_n \theta (1 - B_{H_2O})}$$

$$= 0.0945 \frac{(531.7)(593.14)}{(30.79)(58.4)(0.000374)(480)(1 - 0.0066)}$$

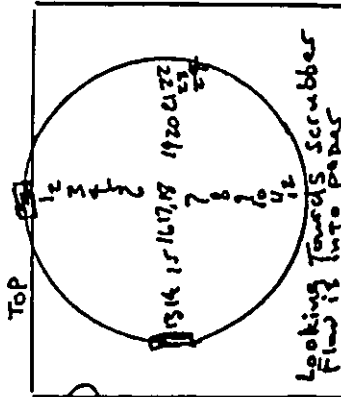
$$\%I = \underline{100.7} \%$$



# Chronal Ceko Unit

Plant 2-13-89  
 Sampling Location Main Inlet (24" dia)  
 Sample Type Chronal  
 Run Number C-MI-1  
 Operator Shawn Purcell, Paces  
 Ambient Temperature 60°F overcast  
 Barometric Pressure 30.67  
 Static Pressure (P<sub>g</sub>) -0.9" water  
 Filter Number(s) C-MI-F  
 Pretest Leak Rate = 0.004 cfm @ 12 in. Hg  
 Pretest Pitot Leak Check ✓  
 Pretest Orsat Leak Check ✓ V.A.  
 Read and Record all Data Every 20 Minutes

## FIELD DATA



Schematic of Traverse Point Layout

Probe Length and Type 3' glass  
 Pitot Tube I.D. No. Type S  
 Nozzle I.D. 0.31 0.32 0.30  
 Assumed Moisture, % 1.0  
 Temp. Readout S/N ---  
 Meter Box Number Nurech 1A  
 Meter AHe 1.92  
 C Factor 1.10  
 Meter Gamma 1.003  
 Heater Box Setting ---  
 Reference Ap 0.20  
 Post Test Leak Rate = cfm @ --- in. Hg  
 Post Test Pitot Leak Check OK  
 Post Test Orsat Leak Check N.A.

| Traverse Point Number | Sampling Time, / (min) / (clock) | /Clock | Gas Meter Reading (V <sub>g</sub> ) ft <sup>3</sup> | Velocity Head (AP <sub>g</sub> ) in. H <sub>2</sub> O | Orifice Pres. Differential (ΔH) in. H <sub>2</sub> O | Stack Temp. (T <sub>g</sub> ) °F | Dry Gas Meter Temp. Inlet (T <sub>m</sub> ) °F | Outlet (T <sub>m</sub> ) °F | Pump Vacuum in. Hg | Sample Box Temp. Filter Temp. °F | In-Flange Temp. °F |
|-----------------------|----------------------------------|--------|-----------------------------------------------------|-------------------------------------------------------|------------------------------------------------------|----------------------------------|------------------------------------------------|-----------------------------|--------------------|----------------------------------|--------------------|
| 1                     | 0 / 0850                         | 0850   | 0.42                                                | 0.40                                                  | 2.40                                                 | 2.4                              | 68                                             | 65                          | 6.5                | 60                               | 60                 |
| 2                     | 20 / 0910                        | 0910   | 0.42                                                | 0.36                                                  | 2.2                                                  | 2.2                              | 70                                             | 55                          | 6.0                | 59                               | 59                 |
| 3                     | 40 / 0930                        | 0930   | 0.42                                                | 0.40                                                  | 3.6                                                  | 3.6                              | 68                                             | 60                          | 7.5                | 63                               | 63                 |
| 4                     | 60 / 0950                        | 0950   | 0.42                                                | 0.42                                                  | 3.85                                                 | 3.85                             | 68                                             | 62                          | 7.0                | 55                               | 55                 |
| 5                     | 80 / 1010                        | 1010   | 0.42                                                | 0.40                                                  | 3.60                                                 | 3.6                              | 67                                             | 64                          | 7.0                | 58                               | 58                 |
| 6                     | 100 / 1030                       | 1030   | 0.42                                                | 0.36                                                  | 3.20                                                 | 3.20                             | 68                                             | 64                          | 7.0                | 55                               | 55                 |
| 7                     | 120 / 1050                       | 1050   | 0.40                                                | 0.40                                                  | 3.70                                                 | 3.70                             | 68                                             | 64                          | 7.0                | 55                               | 55                 |
| 8                     | 140 / 1110                       | 1110   | 0.40                                                | 0.40                                                  | 3.7                                                  | 3.7                              | 67                                             | 70                          | 7.5                | 55                               | 55                 |
| 9                     | 160 / 1130                       | 1130   | 0.40                                                | 0.40                                                  | 3.70                                                 | 3.7                              | 69                                             | 75                          | 7.5                | 55                               | 55                 |
| 10                    | 180 / 1150                       | 1150   | 0.40                                                | 0.40                                                  | 3.70                                                 | 3.7                              | 69                                             | 76                          | 7.5                | 55                               | 55                 |
| 11                    | 200 / 1210                       | 1210   | 0.40                                                | 0.40                                                  | 3.70                                                 | 3.7                              | 73                                             | 82                          | 7.5                | 55                               | 55                 |
| 12                    | 220 / 1230                       | 1230   | 0.40                                                | 0.40                                                  | 3.70                                                 | 3.7                              | 72                                             | 82                          | 7.5                | 55                               | 55                 |
| 13                    | 240 / 1250                       | 1250   | 0.41                                                | 0.41                                                  | 3.80                                                 | 3.8                              | 67                                             | 81                          | 7.5                | 52                               | 52                 |
| 14                    | 260 / 1310                       | 1310   | 0.40                                                | 0.40                                                  | 3.6                                                  | 3.6                              | 70                                             | 84                          | 7.5                | 50                               | 50                 |
| 15                    | 280 / 1330                       | 1330   | 0.40                                                | 0.40                                                  | 3.70                                                 | 3.7                              | 69                                             | 79                          | 7.5                | 48                               | 48                 |
| 16                    | 300 / 1350                       | 1350   | 0.39                                                | 0.39                                                  | 3.6                                                  | 3.6                              | 70                                             | 78                          | 7.0                | 47                               | 47                 |
| 17                    | 320 / 1370                       | 1370   | 0.39                                                | 0.39                                                  | 3.6                                                  | 3.6                              | 68                                             | 74                          | 7.5                | 45                               | 45                 |
| 18                    | 340 / 1390                       | 1390   | 0.40                                                | 0.40                                                  | 3.9                                                  | 3.9                              | 69                                             | 76                          | 7.5                | 44                               | 44                 |
| 19                    | 360 / 1410                       | 1410   | 0.41                                                | 0.41                                                  | 3.9                                                  | 3.9                              | 66                                             | 73                          | 8.0                | 44                               | 44                 |
| 20                    | 380 / 1430                       | 1430   | 0.41                                                | 0.41                                                  | 3.9                                                  | 3.9                              | 66                                             | 73                          | 18.0               | 44                               | 44                 |
| 21                    | 400 / 1450                       | 1450   | 0.41                                                | 0.41                                                  | 3.9                                                  | 3.9                              | 66                                             | 73                          | 18.0               | 44                               | 44                 |
| 22                    | 420 / 1470                       | 1470   | 0.41                                                | 0.41                                                  | 3.9                                                  | 3.9                              | 66                                             | 73                          | 18.0               | 44                               | 44                 |
| 23                    | 440 / 1490                       | 1490   | 0.41                                                | 0.41                                                  | 3.9                                                  | 3.9                              | 66                                             | 73                          | 18.0               | 44                               | 44                 |
| 24                    | 460 / 1510                       | 1510   | 0.41                                                | 0.41                                                  | 3.9                                                  | 3.9                              | 66                                             | 73                          | 18.0               | 44                               | 44                 |
| 25                    | 480 / 1530                       | 1530   | 0.41                                                | 0.41                                                  | 3.9                                                  | 3.9                              | 66                                             | 73                          | 18.0               | 44                               | 44                 |



## SAMPLE RECOVERY DATA

Plant: Chromal Plating Co. -> Caco Unit  
Date: 2-13-89  
Sampling Location: Main Inlet  
Sample Type: Chrom + Hexavalent Chrom  
Run Number: C-MI-1  
Sample Box Number: 1B- ~~C-MI-1~~  
Clean-up Man: Simon/Arts  
Job Number: 3625  
Comments: \_\_\_\_\_

FRONT HALF

Filter Number: C-MI-F  
Description of Filter: \_\_\_\_\_

MOISTURE

|                         | #1            | #2            | #3          |
|-------------------------|---------------|---------------|-------------|
| Impingers               |               |               |             |
| Final Volume:           | <u>106</u> ml | <u>185</u> ml | <u>1</u> ml |
| Initial Volume:         | <u>100</u> ml | <u>100</u> ml | <u>0</u> ml |
| Net Volume:             | _____ ml      | _____ ml      | _____ ml    |
| Total H <sub>2</sub> O: | _____         | _____         | _____       |

Silica Gel + Impinger

|                            | #1             | #2      | #3      |
|----------------------------|----------------|---------|---------|
| TARE Wt. + { Final Volume: | _____ g        | _____ g | _____ g |
| { Initial Volume           | <u>101.3</u> g | _____ g | _____ g |
| Net Volume                 | _____ g        | _____ g | _____ g |
| Total Moisture:            | _____          | _____   | _____   |

Description of Impinger Catch: \_\_\_\_\_

Note: Bottom of Impinger Broke. No final Silica gel weight was obtainable. *msb*

FIELD DATA

Diagram illustrating a circular arena setup. A rectangular box is positioned at the top, labeled "TOP". Inside the circle, four numbers are marked: 1 (top left), 2 (top right), 3 (bottom left), and 4 (bottom right). A vertical line runs through the center of the circle, with "78" on the left and "56" on the right. A handwritten note on the right side of the circle reads: "Looking towards each other" and "Fini is top center".

Probe Length and Type 1' glass  
 Pitot Tube I.D. No. 1' Standard  
 Nozzle I.D. 0.29 0.29 0.20 for #1 0.235 0.235  
 Assumed Moisture, % 1.0  
 Temp. Readout S/N ---  
 Meter Box Number Joy  
 Meter  $\Delta H_e$  1.735  
 C Factor None - this Nomograph  
 Meter Gamma 0.913  
 Heater Box Setting ---  
 Reference  $\Delta P$  0.56  
 Post Test Leak Rate = 242 cfm @ 13 in. Hg ✓  
 Post Test Pitot Leak Check ✓  
 Post Test Orsat Leak Check ✓

[illegible]

$\Delta P_r = .23$   
 (Reset manograph)  
 $\Delta P_r = .56$   
 Use plastic  
 manograph  
 $\Delta P_r = 0.56 \text{ psi}$   
 START AT 1308

SAMPLE RECOVERY DATA

Plant: Chromal Ceco Unit  
 Date: 2-13-89  
 Sampling Location: AB Slip Stream Inlet  
 Sample Type: Chrome + Hexamant Chrome  
 Run Number: C-SI-1  
 Sample Box Number: 2B - C-SI-1  
 Clean-up Man: Parks / Simon  
 Job Number: 3625  
 Comments: \_\_\_\_\_

FRONT HALF

Filter Number: C-SI-F  
 Description of Filter: \_\_\_\_\_

MOISTURE

|                         | #1            | #2            | #3          |
|-------------------------|---------------|---------------|-------------|
| Impingers               |               |               |             |
| Final Volume:           | <u>105</u> ml | <u>100</u> ml | <u>3</u> ml |
| Initial Volume:         | <u>100</u> ml | <u>100</u> ml | <u>0</u> ml |
| Net Volume:             | _____ ml      | _____ ml      | _____ ml    |
| Total H <sub>2</sub> O: | _____         | _____         | <u>8 ml</u> |

|                       | #1             | #2         | #3         |
|-----------------------|----------------|------------|------------|
| Silica Gel + Impinger |                |            |            |
| Final Volume:         | <u>168.0</u> g | <u>X</u> g | <u>X</u> g |
| Initial Volume:       | <u>124.4</u> g | <u>X</u> g | <u>X</u> g |
| Net Volume:           | <u>43.6</u> g  | <u>X</u> g | <u>X</u> g |
| Total Moisture:       | _____          | _____      | _____      |

Description of Impinger Catch: Total 51.6 ml

SAMPLE RECOVERY DATA

Plant: Chromal - Ceco Unit  
 Date: 1-13-89  
 Sampling Location: Stack Outlot  
 Sample Type: Chromo  
 Run Number: C-50-1  
 Sample Box Number: 3B-501  
 Clean-up Man: Simon/Acks  
 Job Number: 3625  
 Comments: \_\_\_\_\_

FRONT HALF

Filter Number: C-50-F  
 Description of Filter: \_\_\_\_\_

MOISTURE

|                         | #1            | #2            | #3                   |
|-------------------------|---------------|---------------|----------------------|
| Impingers               |               |               |                      |
| Final Volume:           | <u>123</u> ml | <u>100</u> ml | <u>2</u> ml          |
| Initial Volume:         | <u>100</u> ml | <u>100</u> ml | <u>0</u> ml          |
| Net Volume:             | <u>23</u> ml  | <u>0</u> ml   | <u>2</u> ml          |
| Total H <sub>2</sub> O: |               |               | <u>(Total 25 ml)</u> |

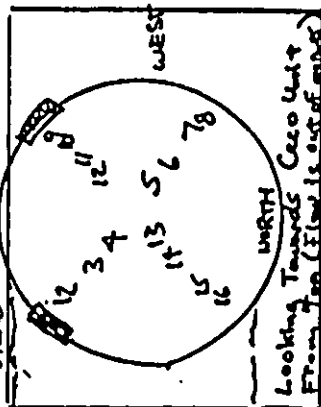
|                                 | #1             | #2 | #3                |
|---------------------------------|----------------|----|-------------------|
| Take Wt + Silica Gel + Impinger |                |    |                   |
| Final Volume:                   | <u>191.8</u> g |    |                   |
| Initial Volume                  | <u>133.2</u> g |    |                   |
| Net Volume                      | <u>58.6</u> g  |    |                   |
| Total Moisture:                 |                |    | <u>Total 83.6</u> |

Description of Impinger Catch: \_\_\_\_\_



Date Z-13-89  
Sampling Location Stack Outlet  
Sample Type Chrome  
Run Number C-50-1  
Operator Stacy, Purcell, Parks  
Ambient Temperature 60°F, overcast  
Barometric Pressure 30.64  
Static Pressure (Pg) 72.10  
Filter Number(s) C-50-F  
Pretest Leak Rate = 0.003 cfm @ 12 in. Hg  
Pretest Pitot Leak Check ✓  
Pretest Orat Leak Check N/A  
Read and Record all Data Every 30 Minutes

TYPE 42



Looking Towards Cere Unit  
From my 20 (Flow is out of my body)

## Traverse Point Layout

**Read and Record all Data Every 30 Minutes**

|                            |                      |
|----------------------------|----------------------|
| Standard (multiply by 1.3) | 1.3                  |
| Pipit Tube I.D. No.        | 279                  |
| Nozzle I.D. 279            | 279                  |
| Assumed Moisture           | 2.0                  |
| Temp. Readout S/N          | —                    |
| Meter Box Number           | NUTECH 2A            |
| Meter $\Delta H$           | 1.93                 |
| C Factor                   | 1.15                 |
| Meter Gamma                | 0.9967               |
| Heater Box Setting         | N.A.                 |
| Reference $\Delta P$       | 0.70                 |
| Post Test Leak Rate        | 22.4 cfm @ 15 in. Hg |
| Post Test Pitot Leak Check | ✓                    |
| Post Test Orsat Leak Check | N.A.                 |

女

| Traverse Point Number | Sampling Time, / (24-hour (min) / clock) | /Clock | Gas Meter Reading (V) ft. | Corrected Velocity Head (ΔP <sub>g</sub> ) in. H <sub>2</sub> O | Orifice Pres.              |                | Stack Temp. (T <sub>g</sub> ) °F | Dry Gas Meter Temp.        |                             | Pump Vacuum in. Hg | Sample Box Temp. Filter Temp. °F | Im-pinger Temp. °F |
|-----------------------|------------------------------------------|--------|---------------------------|-----------------------------------------------------------------|----------------------------|----------------|----------------------------------|----------------------------|-----------------------------|--------------------|----------------------------------|--------------------|
|                       |                                          |        |                           |                                                                 | Desired                    | Actual         |                                  | Inlet (T <sub>m</sub> ) °F | Outlet (T <sub>m</sub> ) °F |                    |                                  |                    |
| 1                     | 0 / 0910                                 |        | 932.07                    | 1.00                                                            | 9.00                       | 7.0            |                                  |                            |                             | 12.5               |                                  | 56                 |
| 2                     | 30 / 0940                                |        | 967.7                     | 1.00                                                            | 9.00                       | 7.5            | 71                               | 65                         | 70                          | 12.5               |                                  | 56                 |
| 2                     | 40 / 0950                                |        | 985.0                     | STOP                                                            | TEST - SWITCHED TO SMALLER | NOTE: 1.573.67 |                                  |                            |                             | 10.0               |                                  | 57                 |
| 2                     | 40 / 0953                                |        | 985.0                     | 1.00                                                            | 4.5                        | 5.0            | 71                               | 68.73                      | 66                          | 10.0               |                                  | 57                 |
| 3                     | 40 / 1043                                |        | 007.7                     | 1.00                                                            | 4.6                        | 4.80           | 73                               | 71                         | 71                          | 10.0               |                                  | 60                 |
| 4                     | 40 / 1043                                |        | NOT TAKEN                 | 1.7                                                             | 5.5                        | 5.4            | 71                               | 82                         | 71                          | 10.0               |                                  | 60                 |
| 5                     | 40 / 1143                                |        | 081.00                    | 1.1                                                             | 5.0                        | 5.0            | 74                               | 85                         | 78                          | 7.0                |                                  | 56                 |
| 6                     | 40 / 1143                                |        | 115.8                     | 1.4                                                             | 5.2                        | 5.3            | 72                               | 84                         | 75                          | 9.0                |                                  | 55                 |
| 7                     | 40 / 1213                                |        | 156.3                     | 1.15                                                            | 5.4                        | 5.4            | 69                               | 86                         | 76                          | 9.0                |                                  | 80                 |
| 8                     | 40 / 1213                                |        | 190.0                     | 1.15                                                            | 5.4                        | 5.4            | 75                               | 87                         | 78                          | 9.5                |                                  | 53                 |
| 9                     | 40 / 1313                                |        | 226.98                    | 1.04                                                            | 5.4                        | 5.4            | 75                               | 87                         | 78                          | 9.5                |                                  | 53                 |
| 9                     | 40 / 1326                                |        | 226.98                    | 1.04                                                            | 5.4                        | 5.4            | 75                               | 87                         | 78                          | 9.5                |                                  | 53                 |
| 10                    | 270 / 1356                               |        | 262.3                     | 1.04                                                            | 4.6                        | 4.6            | 83                               | 81                         | 76                          | 9.0                |                                  | 46                 |
| 11                    | 300 / 1426                               |        | 248.2                     | 1.04                                                            | 4.6                        | 4.6            | 80                               | 84                         | 75                          | 8.0                |                                  | 47                 |
| 12                    | 330 / 1456                               |        | 353.2                     | 1.32                                                            | 4.6                        | 4.6            | 75                               | 84                         | 74                          | 9.0                |                                  | 44                 |
| 13                    | 360 / 1526                               |        | 370.4                     | 1.32                                                            | 4.6                        | 4.6            | 68                               | 83                         | 74                          | 10.0               |                                  | 41                 |
| 14                    | 390 / 1556                               |        | 411.8                     | 1.18                                                            | 5.3                        | 5.3            | 68                               | 77                         | 70                          | 10.5               |                                  | 39                 |
| 15                    | 420 / 1626                               |        | 450.0                     | 1.03                                                            | 4.85                       | 4.85           | 65                               | 77                         | 67                          | 9.8                |                                  | 39                 |
| 16                    | 450 / 1656                               |        | 481.2                     | 1.03                                                            | 4.85                       | 4.85           | 64                               | 77                         | 68                          | 9.0                |                                  | 39                 |
| 17                    | 480 / 1726                               |        | 517.73                    | 1.03                                                            | 4.85                       | 4.85           | 64                               | 77                         | 68                          | 9.0                |                                  | 39                 |

$$AP_c = 2.20$$

Reset  
Magnetograph.  
 $\Delta P_r = 0.40$

Rain →

Received: 02/14/89

IMA INC.

REPORT

Work Order # 89-02-051

REPORT Pacific Environmental Service  
TO 150 E. Foothill Blvd.  
Arcadia, CA 91006

PREPARED Thermo Analytical, Inc.  
BY 160 Taylor Street  
Monrovia, CA 91016

ATTEN Mr. Dean High

ATTEN  
PHONE 818-357-3247

CERTIFIED BY

CONTACT RSF

CLIENT PACIFIC ENVI SAMPLES 9  
COMPANY Pacific Environmental Service  
FACILITY

This report is for the sole and exclusive use of the client to whom it is addressed and represents only those samples herein described. Samples not destroyed in testing are retained a maximum of 30 days unless otherwise requested.

WORK ID #3625

TAKEN By Pacific Enviro Staff  
TRANS By Pacific Enviro Staff  
TYPE Liquids

P. O. # 3625

INVOICE under separate cover

Information reported by telephone to Scott on 2/21/89.

### SAMPLE IDENTIFICATION

01 C-FB  
02 C-SI-TB  
03 C-SO-1  
04 C-SO-F  
05 C-MI-1  
06 C-MI-F  
07 C-SI-1  
08 C-SI-F  
09 C-RB

### TEST CODES and NAMES used on this report

CRHEXS Hexavalent Chromium  
CRHGAA Chromium - Air  
CR HEX Hexavalent Chromium  
CR L Chromium - Liquids  
WC General Chemical Testing



Page 2  
Received: 02/14/89

TMA Inc.

REPORT

Work Order # 89-02-051

Results by Sample

SAMPLE ID C-FB

SAMPLE # 01 FRACTIONS: A

Date & Time Collected 02/13/89

Category

CRHEXS <0.5 CRHGAA 0.34  
ugms/Filter Total ug

SAMPLE ID C-SI-TB

SAMPLE # 02 FRACTIONS: A

Date & Time Collected 02/13/89

Category

CR\_HEX 0.026 CR\_L 0.0308 WC 223  
mg/L mg/L mls

SAMPLE ID C-SO-1

SAMPLE # 03 FRACTIONS: A

Date & Time Collected 02/13/89

Category

CR\_HEX 0.023 CR\_L 0.0571 WC 880  
mg/L mg/L mls

SAMPLE ID C-SO-F

SAMPLE # 04 FRACTIONS: A

Date & Time Collected 02/13/89

Category

CRHEXS <0.5 CRHGAA 0.32  
ugms/Filter Total ug



Received: 02/14/89

TMA Inc.

REPORT

Results by Sample

Work Order # 89-02-051

SAMPLE ID C-MI-1

SAMPLE # 05 FRACTIONS: A

Date & Time Collected 02/13/89

Category

CR\_HEX 2.27 CR\_L 2.81 WC 570  
mg/L mg/L mls

SAMPLE ID C-MI-F

SAMPLE # 06 FRACTIONS: A

Date & Time Collected 02/13/89

Category

CRHEXS <0.5 CRHGAA 0.66  
ugms/Filter Total ug

SAMPLE ID C-SI-1

SAMPLE # 07 FRACTIONS: A

Date & Time Collected 02/13/89

Category

CR\_HEX 0.98 CR\_L 1.27 WC 926  
mg/L mg/L mls

SAMPLE ID C-SI-F

SAMPLE # 08 FRACTIONS: A

Date & Time Collected 02/13/89

Category

CRHEXS <0.5 CRHGAA 1.14  
ugms/Filter Total ug



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Received: 02/14/89

TMA Inc.

REPORT

Work Order # 89-02-051

Results by Sample

SAMPLE ID C-RB

SAMPLE # 09 FRACTIONS: A

Date & Time Collected 02/13/89

Category

CR\_HEX <0.003  
mg/L

0.0027  
mg/L

WC

145  
mls



Page 5  
Received: 02/14/89

TMA Inc. REPORT

02/22/89 10:35:15

Work Order # 89-02-051

Pacific Environmental Service

Five liquids and four filters were analyzed for hexavalent and total chromium content, according to EPA method 425. The volumes of the liquids were measured. Please see the enclosed tables for the results.