

AP42 Section: 13.2.6

Background Chapter 4

Reference: 5

**Title: Summary of Source Test Results, Hunter Schlesser Sandblasting,
San Leanardo, CA, Bay Area Air Quality Management District,
San Francisco, CA, March 3, 1993.**

Note: This is a reference cited in *AP 42, Compilation of Air Pollutant Emission Factors, Volume I Stationary Point and Area Sources*. AP42 is located on the EPA web site at www.epa.gov/ttn/chief/ap42/

The file name refers to the reference number, the AP42 chapter and section. The file name "ref02_c01s02.pdf" would mean the reference is from AP42 chapter 1 section 2. The reference may be from a previous version of the section and no longer cited. The primary source should always be checked.

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939 Ellis Street
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(415) 771-8000

SUMMARY OF SOURCE TEST RESULTS

Report No. 93142Test Date: 02/10/93

Test Times:

Run A: 0916-1006Run B: 1023-1113Run C: 1126-1216

SOURCE INFORMATION

BAAQMD REPRESENTATIVES

Firm Name and Address HUNTER SCHLESSER SANDBLASTING 1620 Doolittle Drive San Leandro, CA 94577	Firm Representative and Title Mr. Hunter Schlessor, Owner Phone No. (510) 614-8244	Source Test Engineers C. McClure/H. Doi
Permit Conditions Number 7605: Limits visible emissions and amount of abrasive consumed.	Source: (S-2) Blasting Room Abated by (A-1) Baghouse Plant No. 7601 Operates 8 hr/day & 260 days/yr	Permit Services Division / Enforcement Division T. Bui Test Requested by: N. Lew

Operating Parameters:

Normal parts blasting operations were conducted during sampling. The Glass Bead blast room was utilized to surface finish two large motor shields and several handrails.

Applicable Regulations: Developmental Data

VN Recommended: NO

Source Test Results and Comments:

<u>METHOD:</u>	<u>TEST</u>	<u>RUN A</u>	<u>RUN B</u>	<u>RUN C</u>	<u>AVERAGE</u>	<u>LIMIT</u>
ST-17	Stack Volume Flowrate, SDCFM				1,800	
	Stack Gas Temperature, °F	60	63	64	62	
ST-23	Water Content, Volume %	1.4	1.2	1.1	1.2	
C.A.R.B. 5	Particulate, gr/SDCF	.001	.001	.001	.001	
	Particulate, lb/hr	.01	.01	.02	.01	
	Isokinetic Ratio, Act./Theo.	1.01	.99	.99		

NO COMMERCIAL USE OF THESE RESULTS IS AUTHORIZED

Air Quality Engineer II <i>C. McClure II</i> C. McClure	Date 2/24/93 Supervising Air Quality Engineer <i>K. Kunaniec</i> K. Kunaniec	Date 2/24/93 Approved by Source Test Manager <i>G. Karels</i> G. Karels
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GRAIN LOADING:

$$G(\text{gr/sdCF}) = 15.43 \frac{W_p(\text{g})}{V_o(\text{sdCF})}$$

PLANT: #7601 S-1, 2
SOURCE: H/S SAND BLASTING
DATE: 2/10/93

$$G_A = 15.43 \frac{(.0018)}{(32.438)} = 0.00086 = 0.001 \text{ gr/sdCF} \quad W_{PA} = .0018 \text{ g}$$

$$G_B = 15.43 \frac{(.0016)}{(31.445)} = 0.00078 = 0.001 \text{ gr/sdCF} \quad W_{PB} = .0016 \text{ g}$$

$$G_C = 15.43 \frac{(.0018)}{(26.804)} = 0.0010 = 0.001 \text{ gr/sdCF} \quad W_{PC} = .0018 \text{ g}$$

$$G_{\text{avg}} = 0.001 \text{ gr/sdCF}$$

$$V_{PA} = 32.438 \text{ sdCF}$$

$$V_{PB} = 31.445 \text{ sdCF}$$

$$V_{PC} = 26.804 \text{ sdCF}$$

MASS EMISSIONS: $M = \frac{G \cdot Q}{116.67}$

$$Q_o = 1820 \text{ sdCFM}$$

$$M_A = \frac{(0.00086 \times 1820)}{116.67} = 0.01 \text{ Lb/hr}$$

$$M_B = \frac{(0.00078 \times 1820)}{116.67} = 0.01 \text{ Lb/hr}$$

$$M_C = \frac{(0.0010 \times 1820)}{116.67} = 0.02 \text{ Lb/hr}$$

$$M_{\text{avg}} = 0.01 \text{ Lb/hr}$$

SOURCE TEST LAB DATA SHEET

PLANT: HUNTER'S SANDBLASTING

PAGE: 1 OF 1

SOURCE OPERATION: BAGHOUSE

INITIAL: CM

SOURCE TEST NO.:

TEST DATE: 2/10/93

FILTER MEDIA: GLASS FIBER, 90 MM

FILTER DATA

RUN #	FILTER #	TARE WEIGHT(g)		FINAL WEIGHT(g)		TOTAL(g)
A	3010	.3953	.3953	.3952	.3952	0.0000
B	3011	.3935	.3936	.3932	.3932	0.0000
C	3012	.3957	.3955	.3950	.3950	0.0000
DATE/TIME		12/22/92P	12/23/92A	2/16/93AM	2/17/93AM	

PROBE & NOZZLE RINSE DATA

RUN #	JAR #	TARE WEIGHT(g)		FINAL WEIGHT(g)		TOTAL(g)
A	18	58.0711	58.0710	58.0729	58.0730	.0018
B	19	55.6713	55.6712	55.6729	55.6729	.0016
C	20	54.5710	54.5709	54.5728	54.5729	.0018
DATE/TIME		1/29/93PM	2/1/93AM	2/16/93AM	2/17/93AM	

TOTAL WEIGHTS (FILTER AND PROBE & NOZZLE)

RUN #	FILTER FINAL WT(g)	P & N FINAL WT(g)	TOTAL(g)
A	0.0000	.0018	.0018
B	0.0000	.0016	.0016
C	0.0000	.0018	.0018

ISOKINETIC RATIOS

E.P.A. EQUATION

$$R_I = \frac{(T_s \text{ } ^\circ R)(V_o \text{ SCF})(K_I)}{(V_s \text{ FPS})(100 - \%H_2O)(A_n \text{ FT}^2)(t \text{ MINUTES})(P_s \text{ "Hg})}$$

$K_I = 9.414 \times 10^{-2}$
AT STANDARD
CONDITIONS OF
29.92 "Hg & 70°F

$$P_s = P_{BAR} + \left(\frac{P_{STATIC} \text{ "H}_2\text{O}}{13.6 \text{ "H}_2\text{O/"Hg}} \right) = 30.30 + \left(\frac{-4.0}{13.6} \right)$$

$$P_s = 30.006 \text{ "Hg} \quad t = \text{TIME} = 50 \text{ MINUTES}$$

$$A_n = 8.454 \times 10^{-6} (D_n \text{ mm})^2 \text{ FT}^2 \quad D_n = 3.3 \text{ mm}$$

$$A_n = 8.454 \times 10^{-6} (3.3 \text{ mm})^2 \text{ FT}^2$$

$$A_n = 9.206 \times 10^{-5} \text{ FT}^2$$

GROUP TERMS:

$$R_I = \frac{(T_s)(V_o)(9.414 \times 10^{-2})}{(V_s)(100 - \%H_2O)(9.206 \times 10^{-5})(50)(30.006)} = \frac{(T_s)(V_o)(0.6816)}{V_s(100 - \%H_2O)}$$

ROW A) $T_s = 520^\circ R$ $V_o = 32.438 \text{ SCF}$ $V_s = 114.85 \text{ FPS}$ $\%H_2O = 1.4$ $(100 - \%H_2O) = 98.6$

$$R_{IA} = \frac{(520)(32.438)(0.6816)}{(114.85)(98.6)} = \underline{\underline{1.01}}$$

ROW B) $T_s = 523^\circ R$ $V_o = 31.445 \text{ SCF}$ $V_s = 114.48 \text{ FPS}$ $\%H_2O = 1.2$ $(100 - \%H_2O) = 98.8$

$$R_{IB} = \frac{(523)(31.445)(0.6816)}{(114.48)(98.8)} = 0.991 = \underline{\underline{0.99}}$$

ROW C) $T_s = 524^\circ R$ $V_o = 26.804 \text{ SCF}$ $V_s = 97.39 \text{ FPS}$ $\%H_2O = 1.1$ $(100 - \%H_2O) = 98.9$

$$R_{IC} = \frac{(524)(26.804)(0.6816)}{(97.39)(98.9)} = \underline{\underline{0.99}}$$

#760/
PLANT: A.S. STADIUM
SOURCE: S-2, 1
DATE: 2/10/93

RUN #
VO=
% H2O=

1
~~32.0126~~ > A
1.37918
1.4%

RUN #
VO=
% H2O=

2
~~31.0331~~ > B
1.20329
1.2%

RUN #
VO=
% H2O=

3
~~26.4521~~ > C
1.10341
1.1%

7601
2/10/93
S-2,1

>
 $\% H_2O_{AD} = 1.2\%$

>run htwoo
HTWOO
HOW MANY RUNS? 3

RUN # 1
WHAT IS THE WEIGHT ,GM OF CONDENSATE? 1.7
ENTER INITIAL,FINAL METER READING ! 0,31.318
ENTER METER TEMPS FOR AVERAGING
?58.5
?-10
ENTER METER VACUUMS FOR AVERAGING
?14.1
?-10
ENTER SATURATED GAS TEMPS FOR AVERAGING
?32
?-10

RUN # 2
WHAT IS THE WEIGHT ,GM OF CONDENSATE? 1.4
ENTER INITIAL,FINAL METER READING ! 0,30.793
ENTER METER TEMPS FOR AVERAGING
?65.9
?-10
ENTER METER VACUUMS FOR AVERAGING
?11.2
?-10
ENTER SATURATED GAS TEMPS FOR AVERAGING
?32.9
?-10

RUN # 3
WHAT IS THE WEIGHT ,GM OF CONDENSATE? 1.7
ENTER INITIAL,FINAL METER READING ! 0,26.532
ENTER METER TEMPS FOR AVERAGING
?71.6
?-10
ENTER METER VACUUMS FOR AVERAGING
?7.7
?-10
ENTER SATURATED GAS TEMPS FOR AVERAGING
?32
?-10

SOURCE TEST LAB DATA SHEET

IMPINGER DATA

PLANT: HUNTER'S SANDBLASTING

PAGE: 1 OF 1

SOURCE OPERATION: BAGHOUSE

INITIAL: CM

SOURCE TEST NO.:

TEST DATE: 2/10/93

IMPINGER SOLUTION: DI H2O

DATA

IMPINGER#	A TARE WEIGHT(g)	B FILLED WEIGHT(g)	C FINAL WEIGHT(g)
P-1	510.8	611.0	612.4
P-2	496.8	597.1	597.4
P-3	508.7	609.0	610.4
P-4	538.3	638.4	638.4
P-5	471.2	571.7	573.1
P-6	515.7	616.0	616.3

IMPINGER#	C-A SAMPLE WEIGHT(g)	C-B CONDENSATE WT(g)	TOTAL WEIGHT(g)
P-1	101.6	1.4	RUN A
P-2	100.6	.3	1.7
P-3	101.7	1.4	RUN B
P-4	100.1	.0	1.4
P-5	101.9	1.4	RUN C
P-6	100.6	.3	1.7

STAMP GLASS MANS
S-1 S-2 GLASS



NORMAL ~~STAMP~~ BLATTING
OPERATIONS W/FAZE COATED DRINK SAMPLING

BAY AREA AIR QUALITY MANAGEMENT DISTRICT
939 Ellis Street, San Francisco, Calif. 94109 - 771-6000

Nozzle Diameter
Pitot Tube
Gas Collector No.
Barometric Pressure
Leak Rate
TIME EACH RUN
OF POINTS
TIME EACH RUN

Source Test Data Sheet

Run No. 210/93

Box ΔH = 1.8487
Meter (Y) = 1.0096

5.625 X 5.125
-4.0"

ASSUMED H₂O

SAMPLING TRAIN: PROBE → FILTER # 3010 → IMPH # P-1 IMPH P-2 → PUMP/BOX # 80631

Traverse Point	Dist. From inches	INITIAL TRAVERSE		Traverse Point	AP H ₂ O	Vg PPS	Rate ΔH ORIFICE	METER Temp OF	Volume Ft ³ 330.71	Vac -Hg	Sat'd Gas Temp OF	T _a Duct Temp OF	REMARKS
		Duct Temp OF	ΔP H ₂ O										
A-1 7.2				A-1	4.3	115.5	1.33	55	33.85	13	32	58	
2 6.8				A-1	4.3	115.5	1.33	56	33.80	14	32	58	
3 (9.0)				A-1	4.3	115.5	1.33	56	33.85	14.5	32	58	
4 8.4				A-1	4.3	115.5	1.33	57	33.82	14.5	32	57	
A-1 4.7				A-1	4.3	115.5	1.33	58	33.85	14.5	32	60	
2 7.4				A-1	4.3	115.5	1.32	59	33.85	14.5	32	62	
3 (8.0)				A-1	4.3	116.0	1.32	60	33.85	14.5	32	62	
4 7.0				A-1	4.3	116.0	1.32	61	33.85	14.5	32	62	
T _s = 56°F				A-1	4.1	113.2	1.26	61	33.85	13.5	32	62	
ΔP for PUMP = 8.0 H ₂ O				A-1	4.1	113.2	1.26	62	33.85	13.5	32	62	
T _g = 56°F								58.5	31.02	14.1	32	60.1	
								58.2	31.00			52.0	

WATER CATCH = _____ ML

FIELD % H₂O = _____ %

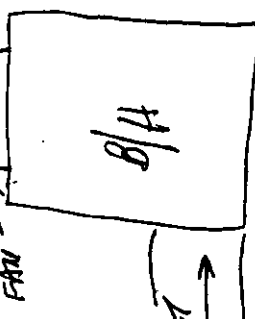
8/14

$$V_0 = \frac{530 \cdot V_m \cdot P_{bar}}{29.92 \cdot T_m} \cdot \text{SCCF}$$

$$V_0 = \frac{17.714 \cdot (21.818) \cdot (30.30)}{(518.2)} \cdot \text{SCCF}$$

$$V_0 = 32.438 \text{ SCCF}$$

MANUAL FAN



Source Test Team

CHUCK MCCLURE

Source Test Engineer II

HIROSHI DOI

Air Quality Instrument Specialist II

AMBIENT AIR



BAY AREA AIR QUALITY MANAGEMENT DISTRICT
939 Ellis Street, San Francisco, Calif. 94109 • 771-6000
Source Test Data Sheet
Run No. B
Date: 2/10/73

Nozzle Diameter 3.3
Pilot Tube LP-12
Gas Collector No. 414
Barometric Pressure 30.30
Leak Rate 0.016 at P
TIME EACH RUN 5
OF POINTS 50
TIME EACH RUN 50

Source Operation S-2
Plant #7601
Sample Type PARTICULATE
Process Cycle B/H EXHAUST
Duct Size RECT 5' X 6' 4"
Duct Pressure -4.0"
ASSUMED H₂O 1.5%

DIGI-TEMP# 4376163 BOX ΔH = 1.8487
MAG GAGE RACE# V12-11 METER(Y) = 1.0096

Sampling Train: PROBE → FILTER # 3011 → IMPH P-1 IMPH P-2 → PUMP/BOX# P0631

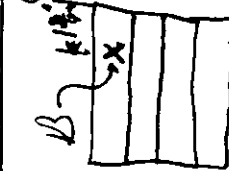
Traverse Point	Dist. From inches	INITIAL TRAVERSE		SAMPLING										REMARKS
		Duct Temp of	ΔP H ₂ O	Traverse Point	ΔP H ₂ O	Vg PPS	Time	Rate ΔH ORifice	METER Temp of	Volume Ft ³	Vac "Hg	Sat'd Gas Temp of	Tg Duct Temp of	
				0-1	4.3	116.0	5	1.32	63	36.192	12	32	62	
				1	4.3	116.0	10	1.32	63	36.192	12	33	62	
				1	4.3	116.0	15	1.32	64	36.192	11	33	62	
				1	4.2	114.7	20	1.29	65	36.192	11	33	63	
				1	4.2	114.7	25	1.29	65	36.192	11	33	63	
				1	4.2	114.7	30	1.29	66	36.192	11	33	63	
				1	4.2	114.7	35	1.29	67	36.192	11	33	63	
				1	4.2	114.7	40	1.29	68	36.192	11	33	63	
				1	4.1	113.5	45	1.26	69	36.192	11	33	64	
				1	4.1	113.5	50	1.26	69	36.192	11	33	64	
									65.9	30.50	11.2	32.9	62.9	
									50.6	31.00	9.6	32.9	62.9	

$V_0 = \frac{530 \cdot V_m \cdot P_{bar}}{29.92 \cdot T_m} \cdot SDCF$
WATER CATCH = _____ ML
FIELD % H₂O = _____ %

$V_0 = 17.714 \cdot (30.793) \cdot (30.30)$
 $V_0 = 31.445 \cdot SDCF$

Source Test Team
CHUCK MCCLURE
Source Test Engineer II
HIROSHI DOI
Air Quality Instrument Specialist II

8-5700000000



GLASS BEAD BLASTING
SHAW-WORTH

(GLASS BEADS)

Source Operation
Plant
Sample Type
Process Cycle
Duct Size
Duct Pressure
ASSEMBLED H₂O

BAY AREA AIR QUALITY MANAGEMENT DISTRICT
939 Ellis Street, San Francisco, Calif. 94109 • 771-6000.
Source Test Data Sheet
Run No. 2/10/93
Date: 2/10/93



3.3 in. Nozzle Diameter
84 Pilot Tube
41A Gas Collector No.
30.30 Barometric Pressure
0.0048 lb Leak Rate
TIME EACH RUN
OF POINTS
TIME EACH H RUN

DIGI-TEMP# 4376163 BOX ΔH=1.8487
MAG GAGE RACK# V12-111 METER(Y)=1.0096

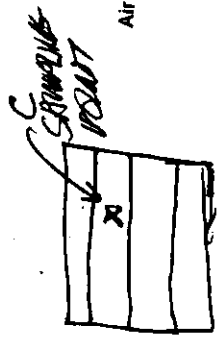
Sampling Train: PROBE → FILTER # 3012 → IMPH# 1.5 IMPH# 1.6 → PUMP/BOX# 82631

Traverse Point	Dist. From inches	INITIAL TRAVERSE		SAMPLING										REMARKS
		Duct Temp of	ΔP H ₂ O	Traverse Point	ΔP H ₂ O	V _g FPS	Time	Rate ΔH ORifice	METER Temp op	Volume Ft ³	Vac -Hg	Sat'd Gas Temp of	T _g Duct Temp of	
				C-1	3.0	97.0	5	.92	70	392.57	7.5	32	64	
				1	3.0	97.1	10	.92	70	392.57	7.5	32	64	
				1	3.0	97.1	15	.92	70	392.57	7.5	32	64	
				1	3.0	97.1	20	.92	71	403.00	7.5	32	64	
				1	3.0	97.1	25	.92	71	403.00	7.5	32	64	
				1	3.0	97.1	30	.92	72	403.00	7.5	32	64	
				1	3.1	98.7	35	.95	72	403.00	8.0	32	64	
				1	3.1	98.7	40	.95	73	413.50	8.0	32	64	
				1	3.1	98.7	45	.95	73	413.50	8.0	32	64	
				1	3.1	98.7	50	.95	74	413.50	8.0	22	64	
									71.6	36.28	7.7	32	64	
									53.3	26.53	7.7	32	64	

$V_0 = \frac{530 \cdot V_m \cdot P_{atm}}{29.92 \cdot T_m} \cdot SDCF$
WATER CATCH = _____ ML
FIELD % H₂O = _____ %

$V_0 = 17.714 (26.532) (30.30)$
(531.3)
 $V_0 = 26.804 SDCF$

Source Test Team
CHUCK MCCLURE
Source Test Engineer II
HIROSHI DOI
Air Quality Instrument Specialist II



2- MODERATE FUSHELLS
2- MODERATE FOREHANDS
SEVERAL MISC. APPARATUS

ISOKINETIC RATE SHEET

C. MCCLURE
1/93 VERSION

$$MW_{\text{DRY}} = .44 \left(\frac{\%CO_2}{100} \right) + .32 \left(\frac{\%O_2}{100} \right) + .28 \left(\frac{\%N_2 + \%CO}{100} \right) = \frac{\quad}{\text{DRY}}$$

$$MW_{\text{WET}} = \left(\frac{MW_{\text{DRY}}}{100} \right) \left(1 - \frac{\%H_2O}{100} \right) + 18 \left(\frac{\%H_2O}{100} \right) = \frac{\quad}{\text{WET}}$$

$$AVS = \frac{85.49 \left(\frac{C_{P, \text{TRAV}}}{MW_{\text{WET}}} \right)}{\left[\left(\frac{P_s}{P_a} \right) \left(\frac{T_s}{T_a} \right) \right]^{1/2}} = \frac{\quad}{\text{AVF TRAV}} \quad \text{AVF AUM}$$

$$V_s = \left[\frac{AVF}{\left(\frac{\Delta P}{T_s} \right)} \right]^{1/2} = \frac{\quad}{\text{FT/SEC}}$$

$$D_{n, \text{ACTUAL}} = 314 \left[\frac{P_a \left(\frac{T_s}{T_a} \right)}{\left(\frac{V_s}{100} \right) \left(\frac{P_s}{P_a} \right) \left(\frac{T_a}{T_s} \right)} \right]^{1/2} = \frac{\quad}{\text{ESTIMATED}}$$

NOTE: NOW RE-ENTER $C_{P, \text{ROW}}$ & $D_{n, \text{ACTUAL}}$, EVALUATE FOR AVF AUM

$$QMF = 5.072 \times 10^{-6} \left(\frac{D_{n, \text{ACTUAL}}^2 P_s}{P_a} \right) \left(\frac{100 - \%H_2O}{100} \right) \left(\frac{T_a}{T_s} \right)$$

$$QMF = \frac{\quad}{P_a} \quad \text{REMEMBER TO } \div \text{ BY } (Y)$$

$$XF = \left[\frac{2.034 \times 10^{-7} \left(\frac{D_{n, \text{ACTUAL}}^4}{P_s} \right) \Delta H_{\text{HAT}} \left(\frac{C_P}{100} \right)^2 \left(\frac{100 - \%H_2O}{100} \right)^2}{\left(\frac{MW_{\text{WET}}}{P_m} \right)} \right] = \frac{\quad}{\quad}$$

$\%H_2O (H_2O) \quad \%$

$(100 - \%H_2O) (H_2F) \quad \%$

$\%O_2 (O_2) \quad \%$

$\%CO_2 (CO_2) \quad \%$

$\Delta H_{\text{HAT}} (HAT) \quad \text{BTU/LB}$

$Y_{\text{METER}} \quad \text{LB/LB}$

$C_{P, \text{TRAV}} \quad \text{BTU/LB-}^\circ\text{F}$

$C_{P, \text{ROW}} (CP) \quad \text{BTU/LB-}^\circ\text{F}$

$\Delta P_{\text{AVG}} (DP) \quad \text{IN. H}_2\text{O}$

$D_{n, \text{ACTUAL}} (DN) \quad \text{MM}$

$P_{\text{BAROMETRIC}} \quad \text{IN. Hg}$

$P_{\text{STATIC}} \quad \text{IN. Hg}$

$$P_{\text{STACK}} = P_B + \left(\frac{P_{\text{STATIC}}}{13.6} \right) = \frac{\quad}{\text{IN. Hg}}$$

$$P_{\text{METER}} = P_B + \left(\frac{P_{\text{STATIC}}}{13.6} \right) = \frac{\quad}{\text{IN. Hg}}$$

$$T_{\text{STACK AVG}} = \frac{T_s}{(TSR)} = \frac{\quad}{^\circ\text{R}}$$

$$T_{\text{METER AVG}} = \frac{T_s}{(TMR)} = \frac{\quad}{^\circ\text{R}}$$

$$\frac{QMF}{Y} = \frac{\quad}{\quad} = \frac{\quad}{\text{STO(0)}}$$

$$AVF = \frac{\quad}{\quad} \text{STO(3)}$$

$$XF = \frac{\quad}{\quad} \text{STO(4)}$$

ISOKINETIC RATE SHEET

C. McCLORE
1/93 VERSION

$$MW_{DRY} = .44 \left(\frac{\%CO_2}{100} \right) + .32 \left(\frac{\%O_2}{100} \right) + .28 \left(\frac{\%N_2 + \%CO}{100} \right) = \frac{\quad}{\text{DRY}}$$

$$MW_{WET} = \left(\frac{MW_{DRY}}{100} \right) \left(1 - \frac{\%H_2O}{100} \right) + 18 \left(\frac{\%H_2O}{100} \right) = \frac{\quad}{\text{WET}}$$

$$AVS = \frac{85.49 \left(\frac{C_{P, ROW}}{1} \right)}{\left[\left(\frac{P_s}{P_m} \right) \left(\frac{MW_{WET}}{MW_{DRY}} \right) \right]^{1/2}} = \frac{\text{AVF TRAVERSE}}{\text{AVF ROW}}$$

$$V_s = \left[\frac{AVF}{\left(\frac{\Delta P}{P_s} \right) \left(\frac{T_m}{T_s} \right)} \right]^{1/2} = \frac{\quad}{\text{FT/SEC}}$$

$$D_{m, ESTIMATED} = 314 \left[\frac{\left(\frac{P_m}{P_s} \right) \left(\frac{T_s}{T_m} \right)}{\left(\frac{V_s}{100} \right) \left(\frac{100 - \%H_2O}{100} \right) \left(\frac{P_s}{P_m} \right) \left(\frac{T_m}{T_s} \right)} \right]^{1/2} = \frac{\quad}{\text{MM}}$$

NOTE: NOW RE-ENTER $C_{P, ROW}$ & $D_{m, ACTUAL}$, EVALUATE FOR AVF, ROW

$$QMF = 5.072 \times 10^{-6} \left(\frac{D_{m, ACTUAL}^2}{P_s} \right) \left(\frac{100 - \%H_2O}{100} \right) \left(\frac{T_s}{T_m} \right) = \frac{\quad}{\quad}$$

$$QMF = \frac{\quad}{P_m} \text{ REMEMBER TO } \div \text{ BY } (Y)$$

$$XF = \left[\frac{2.034 \times 10^{-7} \left(\frac{D_{m, ACTUAL}^4}{P_s} \right) \Delta H_{H_2O} \left(\frac{C_p}{1} \right) \left(\frac{100 - \%H_2O}{100} \right)^2}{\left(\frac{P_m}{P_s} \right) \left(\frac{T_m}{T_s} \right)} \right] = \frac{\quad}{\quad}$$

$\%H_2O (H_2O) \quad \%$

$(100 - \%H_2O) (H_2F) \quad \%$

$\%O_2 (O_2) \quad \%$

$\%CO_2 (CO_2) \quad \%$

$\Delta H_{H_2O} (HAT) \quad \text{BTU/LB}$

$Y_{METER} \quad \%$

$C_{P, TRAVERSE} \quad \text{BTU/LB-°F}$

$C_{P, ROW} (C_p) \quad \text{BTU/LB-°F}$

$\Delta P_{AUG} (DP) \quad \text{IN H}_2\text{O}$

$D_{m, ACTUAL} (DN) \quad \text{MM}$

$P_{BAROMETRIC} \quad \text{IN Hg}$

$P_{STATIC} \quad \text{IN Hg}$

$$P_{STACK} = P_B + \left(\frac{P_{AUG}}{13.6} \right) = \frac{\quad}{\text{IN Hg}}$$

$$P_{METER} = P_B + \left(\frac{P_{AUG}}{13.6} \right) = \frac{\quad}{\text{IN Hg}}$$

$$T_{STACK, AVG} = \frac{T_s}{(T_s R)} = \frac{\quad}{\text{°R}}$$

$$T_{METER, AVG} = \frac{T_m}{(T_m R)} = \frac{\quad}{\text{°R}}$$

$$\frac{QMF}{Y} = \frac{\quad}{\quad} = \text{STO}(0)$$

$$AVF = \text{STO}(3)$$

$$XF = \text{STO}(4)$$

ISOKINETIC RATE SHEET

C. McCLURE
1/93 VERSION

$$MW_{\text{DRY}} = .44(\%CO_2) + .32(\%O_2) + .28(\%N_2 + \%CO) = \underline{28.844}_{\text{DRY}}$$

$$MW_{\text{WET}} = \left(\frac{MW_{\text{DRY}}}{100} \right) \left(1 - \frac{\%H_2O}{100} \right) + 18 \left(\frac{\%H_2O}{100} \right) = \underline{28.682}_{\text{WET}}$$

$$AVS = \frac{85.49 \left(\frac{C_{P, \text{TRAV}}}{P_s} \right)}{\left[\left(\frac{C_{P, \text{TRAV}}}{P_s} \right) \left(\frac{MW_{\text{WET}}}{MW_{\text{DRY}}} \right) \right]^{1/2}} = \frac{2.4479}{2.448}$$

$$V_s = \left[\frac{AVF}{\left(\frac{\Delta P}{T_s} \right)} \right]^{1/2} = \underline{157.6 \text{ FT/SEC}}$$

$$D_{\text{min}} = 314 \left[\frac{\left(\frac{P_s}{V_s} \right) \left(\frac{T_s}{100} \right)}{\left(\frac{C_{P, \text{TRAV}}}{P_s} \right) \left(\frac{MW_{\text{WET}}}{MW_{\text{DRY}}} \right)} \right]^{1/2} = \underline{2.5 \text{ MM MM}}_{\text{ESTIMATED}}$$

NOTE: NOW RE-ENTER $C_{P, \text{ROW}}$ & $D_{\text{min ACTUAL}}$, EVALUATE FOR AVF_{ROW}

$$QMF = 5.072 \times 10^{-6} \left(\frac{D_{\text{min}}^2}{P_s} \right) \left(\frac{100 - \%H_2O}{T_s} \right) = \underline{2.8428}$$

$$QMF = \underline{2.8428} \quad \text{REMEMBER TO } \div \text{ BY } (Y)$$

$$XF = \left[\frac{2.034 \times 10^{-7} \left(\frac{D_{\text{min}}^4}{P_s} \right) \Delta H_{\text{HAT}} \left(\frac{C_P}{T_s} \right)}{\left(\frac{C_{P, \text{TRAV}}}{P_s} \right) \left(\frac{MW_{\text{WET}}}{MW_{\text{DRY}}} \right)} \right]^{1/2} = \underline{160.42}$$

$$\%H_2O(H_2O) \underline{1.5 \%}$$

$$(100 - \%H_2O)(H_2F) \underline{98.5}$$

$$\%O_2(O_2) \underline{20.95 \%}$$

$$\%CO_2(CO_2) \underline{0.04 \%}$$

$$\Delta H_{\text{HAT}}(HAT) \underline{1.8487}$$

$$Y_{\text{METER}} \underline{1.0096}$$

$$C_{P, \text{TRAV}} \underline{.84}$$

$$C_{P, \text{ROW}}(C_P) \underline{.84}$$

$$\Delta P_{\text{AVG}}(DP) \underline{8.0 \text{ "H}_2\text{O}}$$

$$D_{\text{min ACTUAL}}(DN) \underline{3.3 \text{ MM}}$$

$$P_{\text{BAROMETRIC}} \underline{30.30 \text{ "Hg}}$$

$$P_{\text{STATIC}} \underline{-4.0 \text{ "Hg}}$$

$$P_{\text{STACK}} = P_B + \frac{P_{\text{ATM}}(-4.0)}{13.6} = \underline{30.006 \text{ "Hg}}$$

$$P_{\text{METER}} = P_B + \frac{P_{\text{ATM}}(1.8487)}{13.6} = \underline{30.436 \text{ "Hg}}$$

$$T_{\text{STACK AVG}} = \underline{58 \text{ } ^\circ\text{F}} / (T_{\text{SR}}) \underline{518 \text{ } ^\circ\text{R}}$$

$$T_{\text{METER AVG}} = \underline{70 \text{ } ^\circ\text{F}} / (T_{\text{MR}}) \underline{530 \text{ } ^\circ\text{R}}$$

$$\frac{QMF}{Y} = \frac{(2.8428)}{(1.0096)} = \underline{2.8158}_{\text{STO}(0)}$$

$$AVF = \underline{2.448}_{\text{STO}(3)}$$

$$XF = \underline{160.42}_{\text{STO}(4)}$$